

Appendix R
Drainage and Stormwater Management
Assessment

Appendix R.1
Drainage and Hydrology Assessment for
Mississauga Road/Old Main Street
and Bush Street

BUSH STREET & MISSISSAUGA ROAD CLASS EA

Existing Conditions Drainage Report, Draft

June 2010

10-3121



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1. INTRODUCTION

The Regional Municipality of Peel (the Region) is conducting a Schedule 'C' Municipal Class Environmental Assessment (EA) for the rehabilitation/reconstruction of Mississauga Road from Olde Base Line Road to Bush Street, through the Hamlet of Belfountain, and along Bush Street from Mississauga Road to Winston Churchill Boulevard (approximately 8.2 km). The study area is within the Credit River Watershed. The approximate limits of the study area are shown in **Figure 1**.

Mississauga Road (Peel Regional Road No. 1) is a north-south rural road under the jurisdiction of the Regional Municipality of Peel. Bush Street (Peel Regional Road 11) is a rural east-west road primarily within the Hamlet of Belfountain. Both Mississauga Road and Bush Street are two lane rural arterial roads.

Dillon Consulting Limited (Dillon) has been retained by the Region to conduct several investigations, including a Drainage and Stormwater Assessment for the study area as part of the Class EA. The Drainage and Stormwater Management Assessment includes two Phases. This Drainage Report outlines the existing conditions as part of the Phase I Assessment. The Phase II assessment will be incorporated into this document upon completion of the other investigations and to finalize the Drainage and Stormwater Management Report.

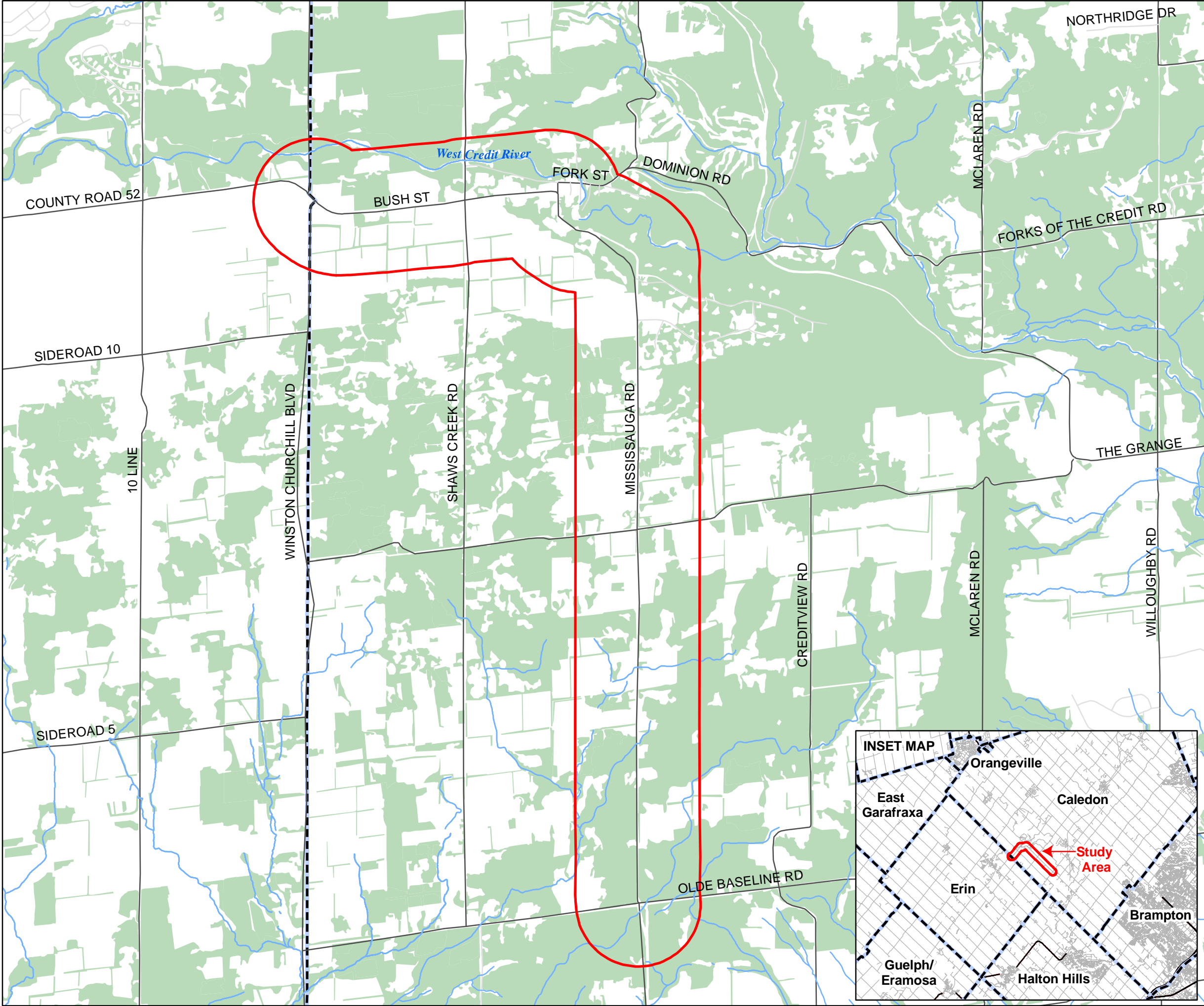
1.1 Study Objectives

The study has been divided into two Phases which include objectives as listed below.

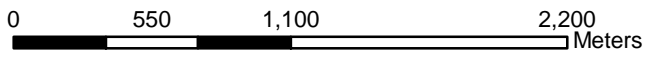
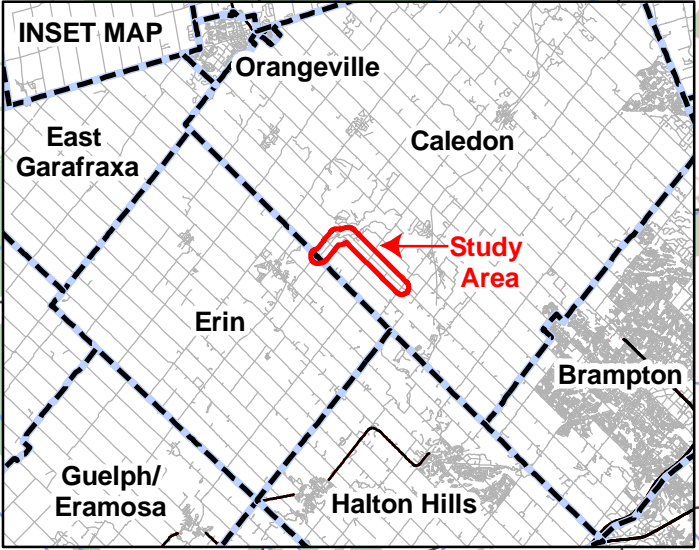
Phase I: Drainage Assessment and Hydraulic Analysis Objectives:

- Review existing drainage patterns and prepare a drainage mosaic for cross culverts and drainage system (i.e., ditches);
- Carry out hydrologic and hydraulic analysis for cross culverts for the 2, 5, 10, 25, 50 and 100 year events to determine existing levels-of-service (LOS) and any inadequacies; and
- Review the existing capacity of culverts and ditches and identify inadequacies with regard to handling stormwater drainage.

**Bush Street and Mississauga Road
Class EA
Figure 1: Study Area**



- Legend**
- Local Roads
 - Secondary Roads
 - Highway
 - Watercourse
 - Study Area
 - Woodland
 - Municipalities



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Analysis of the Regional Storm (Hurricane Hazel), including peak flow modelling and mapping of the floodplain was not completed for the catchment areas under investigation as they were predominantly under 125 ha in size and did not warrant assessment of flood hazards. As noted in Understanding Natural Hazards (MNR, 2001), the flooding hazard limit or floodplain is generally applied to watercourses that drain areas that are equal to or greater than 125 ha.

Hydraulic impacts may include increases to upstream flood levels should the existing road profile elevation be raised (e.g., existing base, crushed in place). Mitigation measures may also be recommended as an opportunity to address existing capacity deficiencies not related to the proposed works.

Phase II: Stormwater Management Plan Objectives:

- Recommend mitigation measures to address hydraulic impacts associated with preferred rehabilitation option(s).
- Develop stormwater management (SWM) design criteria for the transportation corridor that conform to requirements of Credit Valley Conservation (CVC) and the Region;
- Develop SWM options/methods that provide quality and quantity control (to include enhanced grass swales, wet ponds, artificial wetlands, dry ponds, infiltration trenches and oil/grit separators). These SWM options will mitigate impacts of the preferred rehabilitation option(s);
- Identify design methods for the SWM solutions through geotechnical, geomorphologic, stream bed and bank erosion, and meander belt analysis; and
- Evaluate alternative SWM methods and recommend preferred SWM solutions.

It is anticipated that water quality and quantity impacts resulting from road rehabilitation will be minimal due to limited change in footprint. Along the rural transportation corridor, conveyance controls such as flat bottom grass-lined or enhanced swales have been considered, and the need for pond end-of-pipe controls is limited (i.e., no widening to necessitate peak flow controls). End-of-pipe oil-grit separators may also be considered in isolated areas if curb and gutter and storm sewers are preferred.

1.2 Data Collection

Background documents, guidelines and standards were reviewed. Below is the list of information reviewed:

- 2009 Survey, Region of Peel (Auto CAD data file);
- Culvert Structure Inventory, Region of Peel;

- Regional Road Improvements In The Belfountain Area Report, Town of Caledon, Totten Sims Hubicki Associates, January 1998.;
- GIS planning data including contour mapping and 2009 airphotos;
- CVC Stormwater Management Guidelines;
- CVC Standard Parameters Document;
- CVC floodplain map for West Credit River (Map 02);
- Region of Peel, Public Works Design, Specifications & Procedures Manuals
 - Storm Sewer Design Criteria (July, 2009);
 - Regional Roads and Traffic (February, 2010);
- Soil Map of Peel County, Soil Survey Report No. 18;
- Karst of Southern Ontario and Manitoulin Island (GIS mapping), Ontario Geological Survey & Ontario Ministry of Northern Development, Mines and Forestry (MNDMF); and
- MNR Understanding Natural Hazards (2001)

In addition to the background data, a field reconnaissance was conducted on April 16, 2010 and May 4, 2010 to develop familiarity with the existing road drainage system and to ground truth the culvert and ditch information provided by the Region of Peel surveys. Observations of significant water features and evidence of substantial roadside ponding were also noted. Inventory sheets of cross culverts along Bush Street and Mississauga Road within the study area had been compiled and are presented in **Appendix A**. Cross-sectional profiles of ditches at selected locations were also undertaken.

1.3 Road Drainage Area Characteristics

Drainage deficiencies exist at various locations along Bush Street and Mississauga Road and are primarily associated with drainage which is parallel to the road (i.e., road drainage systems that includes ditches and entrance culverts). These drainage deficiencies are a result of shoulder deficiencies such as the overgrowth of vegetation that impede proper drainage, as well as ponding areas on shoulders and road due to deteriorating surfaces. There are also several locations along these roads with little or inadequate ditching for the collection of storm runoff.

As the West Credit River travels parallel to Bush Street, the surface water drainage along Bush Street and the northern portion of Mississauga Road is predominantly flowing north towards the West Credit River. A high point is located just south of entrance culvert # 27 on Mississauga Road (please refer to **Figure 12** for entrance culvert locations). Catchment areas south of this high point generally drain south-westerly within the Credit River watershed, but some local terrain also directs drainage eastward.

2. CAPACITY ASSESSMENT

A hydraulic capacity assessment of existing conditions was undertaken based on the study objectives and is summarized in the sections below. Separate approaches have been established to evaluate the cross culverts and the road drainage systems. Culverts that transverse either Bush Street or Mississauga Road within the study area are considered “cross culverts” in this assessment. The road drainage system includes entrance culverts and roadside ditches, where entrance culverts are defined as culverts, typically along driveways, that convey ditch flows. For the cross culverts and ditches, a hydrologic assessment was first completed to develop design flows, followed by a hydraulic assessment to determine the level of service (LOS) provided. Based on the inventory information compiled by the Region and applying MTO level of capacity rating, the entrance culverts were assessed.

2.1 Design Criteria

The following design criteria have been established for the cross culverts, roadside ditches and entrance culverts based on the Region of Peel Design Guidelines (Region of Peel Public Works Design, Specifications and Procedures Manuals). These criteria have been communicated to and confirmed by the Region:

Cross Culverts

- Current guidelines require culverts that cross the roadway are to be designed for a 25 year storm with a 10 minute inlet time.
- A minimum 600 mm diameter CSP, PVC or approved equivalent be used for crossings of Regional Roads.

Roadside Ditches and Entrance Culverts

- Current guidelines require that storm sewers (applies to roadside ditches, as per communication with the Region) are to be designed using the local municipality’s intensity, duration and frequency rainfall curves for a 10-year storm with 15 minute inlet time for the roadway of way only.
- For external areas draining to roadside ditches, the calculated time of concentration is determined based on a 15 minute minimum inlet time.
- A minimum 375 mm diameter CSP, PVC or approved equivalent be used for ditch crossings (entrance culverts).

2.2 Evaluation of Cross Culverts

2.2.1 Hydrologic Assessment

The approach taken in this assessment involved performing hydrologic modelling to determine the flows for a total of 14 cross culverts for a range of design flow events (i.e., 2 year to 100 year events). The Visual OTTHYMO v2.0 (VO2) hydrologic model was selected for this purpose. VO2 is a single event hydrologic model based on unit hydrograph theory and common types of unit hydrographs including Nash, William-Hann and SCS, and is well suited for various levels of hydrologic studies. In this analysis, the Nash instantaneous unit hydrograph was used, due to most of the external drainage areas to cross culverts being rural lands. Important input parameters required include the curve number of catchment area, initial abstraction value, time of concentration and the time to peak.

Drainage Area Characterization

Obtaining input parameters for the VO2 model required first establishing the drainage area tributary to each of the 14 cross culverts. **Figure 2** shows the locations of the cross culverts. A detailed GIS analysis to delineate these catchment boundaries and to characterize surface drainage patterns was undertaken using 1 m interval contour mapping. **Figure 3** presents the catchment delineation for the 13 cross culvert locations. Cross culvert # 44 is comprised of twin barrels and thus is counted as two culverts (designated as culvert # 44n and # 44s). Hence, there are a total of 14 cross culverts at 13 culvert locations shown on the map in **Figure 3**.

Some catchment areas are composed of rolling hills and depression areas where they have the potential to retain a portion of the surface runoff during storm events. In many locations, these ineffective flow areas act as reservoirs to hold water for infiltration and evaporation and many are suspected to reduce the storm runoff to the cross culverts. Such depression areas are incorporated into the VO2 model to determine whether they are deemed ineffective. Where the modelling results indicate they are ineffective drainage areas, these depression zones have been excluded in the total drainage catchment area.

Based on the Soil Map of Peel County (Soil Survey Report No. 18), the surficial soils in the study area consist mostly of Dumfries loam, Caledon loam and Farmington loam (see **Figure 4**). According to these soil classifications, catchment areas would fall into hydrologic soil groups (HSG) "AB" or "B", indicating lands of relatively good drainage and high infiltration rate. Figure 4 illustrates the soil types within the study area. The curve number (CN) is an indicator of runoff potential and is determined based on surficial soil, land-use and vegetative cover for the area of interest. An area-weighted CN and initial abstraction values (Ia) were determined for each catchment based on CVC guidelines. The time of concentration (Tc) for each catchment

was estimated based on the Upland Method and/or the Kirpich's Equation for larger rural catchment areas. The time of concentration was then used to calculate the time to peak (Tp) value, which is based on the number of 'N' cascading linear reservoirs (N = 3 assumed for this analysis). All of these parameters are incorporated into the model. Table 1 below summarizes the catchment parameters for the cross culverts drainage areas. See **Appendix B** for detailed calculations.

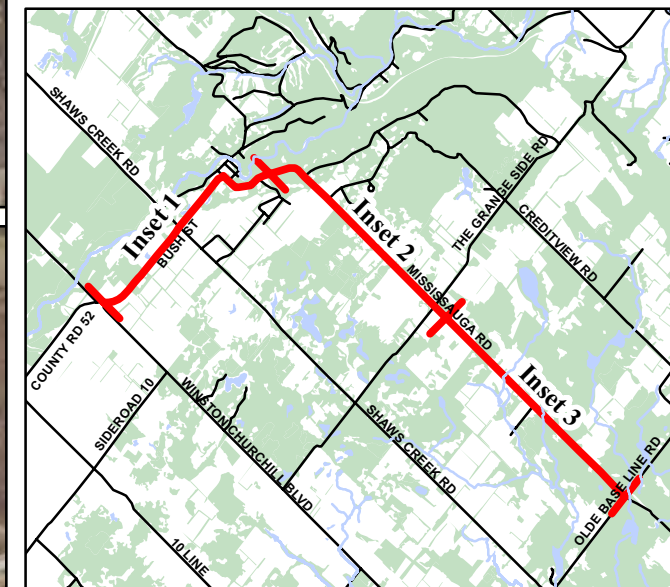
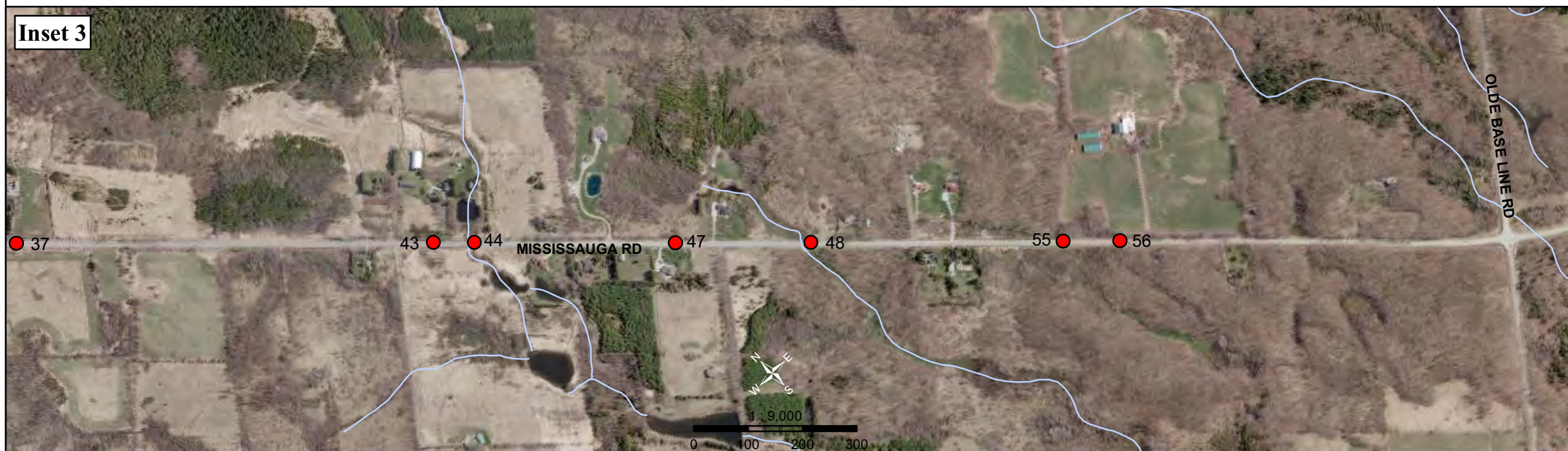
Table 1: VO2 Model Parameters for Cross Culverts

Culvert ID #	Area (ha)	Total Area (ha)	CN	Ia (mm)	Tc (hr)	Tp (hr)
2	19.15	19.15	71.3	5.8	0.37	0.24
10	8.81	8.81	68.3	6.5	2.04	1.36
14	5.57	12.27	69.8	6.1	0.08	0.07
	6.71		64.3	8.7	0.48	0.32
16	2.15	4.23	71.9	5.0	0.16	0.10
	2.08		67.6	7.7	0.13	0.09
17	35.03	35.03	65.5	7.2	1.74	1.16
24	2.77	2.77	70.7	5.4	0.17	0.11
37	11.96	21.05	66.4	5.7	0.27	0.18
	3.90		69.4	4.9	0.11	0.07
	5.19		73.3	4.0	0.17	0.11
43	1.52	48.56	62.0	8.0	0.09	0.06
	1.80		58.8	8.5	0.10	0.07
	24.19		60.0	8.6	0.55	0.37
	21.05		From culvert # 37			
44	127.28	127.28	59.9	8.3	1.18	0.79
47	0.24	0.24	77.6	3.5	0.17	0.11
48	2.66	17.52	59.8	8.6	0.11	0.07
	14.63		58.0	9.4	0.86	0.57
	0.24		From culvert # 47			
55	7.71	7.71	62.5	9.1	0.44	0.29
56	0.91	0.91	64.9	8.5	0.17	0.11

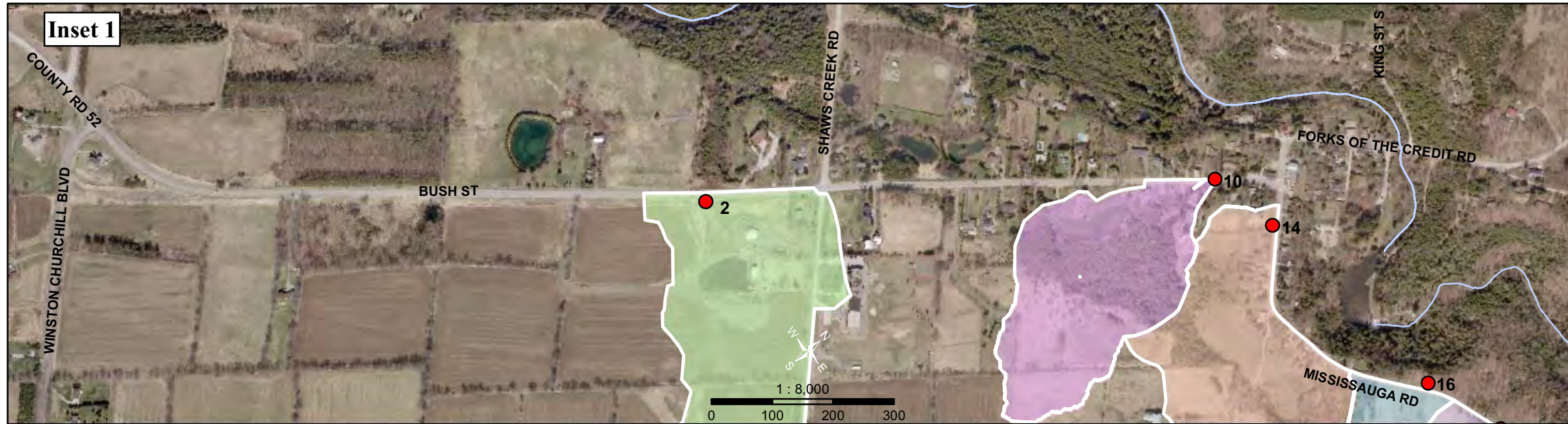
Bush Street and Mississauga Road Figure 2: Existing Cross Culvert Locations

Legend

- 16 Cross Culvert ID #
- Cross Culvert
- Watercourse



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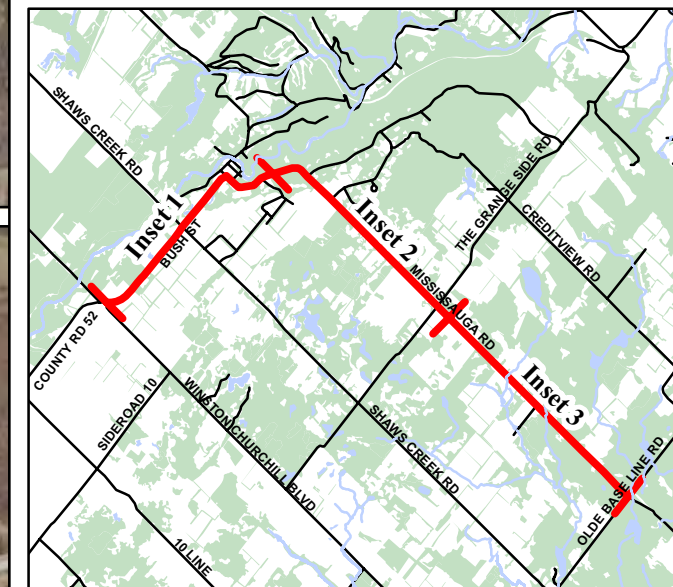
**Bush Street and Mississauga Road
Figure 3: Cross Culvert - Drainage
Areas**

Legend

- 10 Cross Culvert ID #
- Cross Culvert
- Watercourse

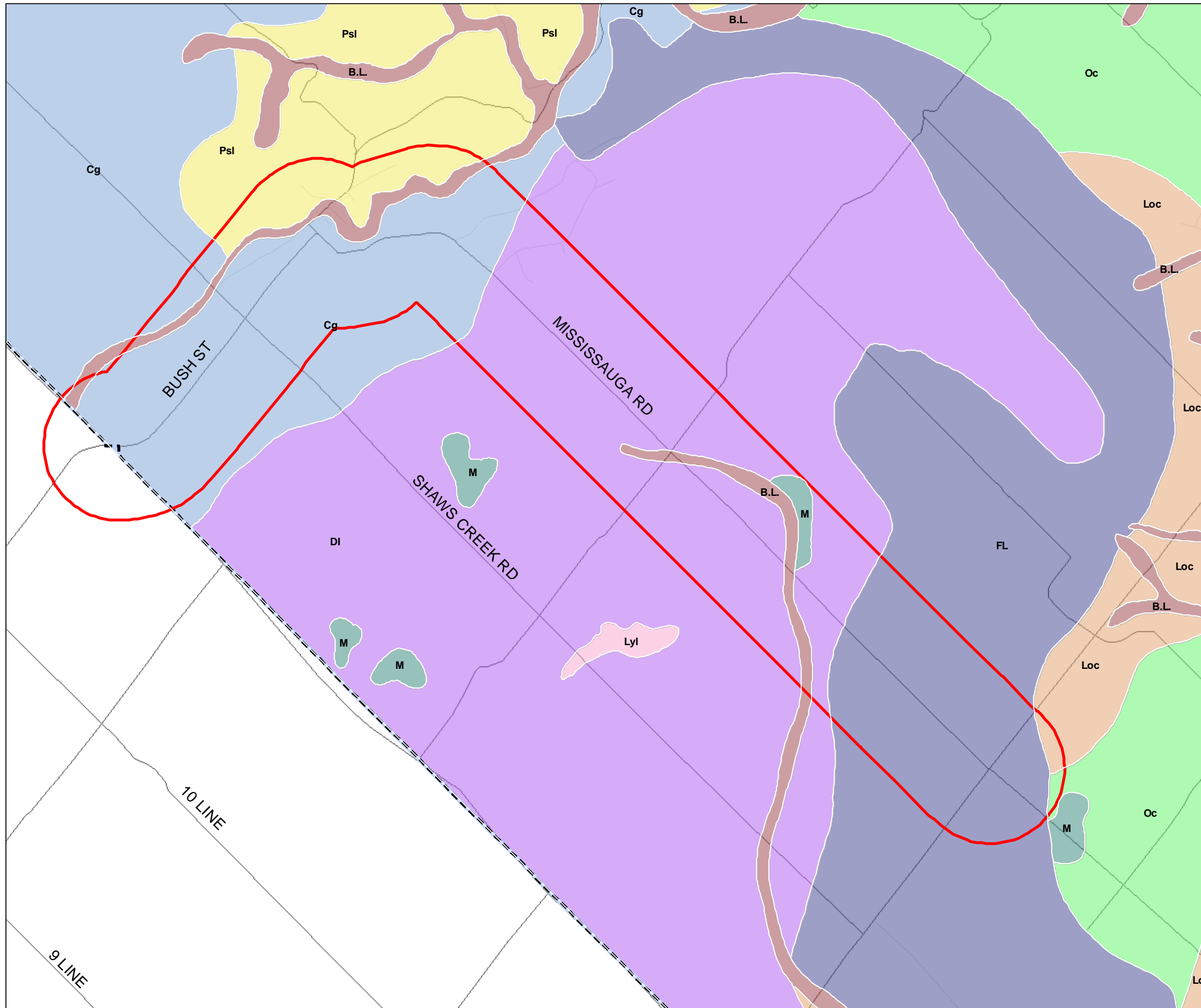
Drainage Area to Cross Culverts

- 2
- 10
- 14
- 16
- 17
- 24
- 37
- 43
- 44
- 47
- 48
- 55
- 56



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**Bush Street and Mississauga Road
Class EA
Figure 4: Soil Classification**



Legend

- Local Roads
 - Secondary Roads
 - Highway
 - Study Area
 - Municipalities
- Soil Classification**
- B.L.: Bottom Land Variable
 - Cg: Caledon Loam
 - DL: Dumfries Loam
 - FL: Farmington Loam
 - Loc: Lockport Clay
 - Lyl: Lily Loam
 - M: Muck Variable
 - Oc: Oneida Clay Loam
 - PsI: Pontypool Sandy Loam

Source: Soil Survey Report No. 18.
Soil Survey of Peel County, Ontario. 1953.



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Based on the culvert invert elevations from the survey provided by the Region of Peel, culvert # 37 appears to be directing flows across Mississauga Road in a west to east direction. According to contour mapping, however, the location of culvert # 37 has a minor dip where runoff can potentially drain from both directions to the culvert. Furthermore, field visits indicated there was ponding on both sides of the culvert and the direction of flow was not visually evident. During field inspections it was observed that the ditches draining to culvert # 37 on the east side of Mississauga Road were quite deep and an embankment along the ditches was created as a result of constructing these deep ditches. This apparent barrier may prevent flows from readily travelling from west to east and, consequently, it may be possible that flows can pool and travel in the reverse direction. Under existing conditions, catchment delineation for culvert # 37 is based on Region survey information with an easterly flow. Analysis would need to be refined at detailed design considering proposed road work and detailed field reconnaissance to confirm detailed local topography.

Importantly, it is possible that a significant portion of the study area may be lying on Karst topography, which can potentially have a substantial impact on the amount and rate of runoff generated. The Ontario Ministry of Northern Development, Mines and Forestry (MNDMF) conducted extensive study and mapping of Karst in Southern Ontario and Manitoulin Island. GIS mapping of this digital data containing reconnaissance-level field information depicting the nature and regional distributions of karstification of Paleozoic bedrock for southern Ontario was obtained from MNDMF (Brunton and Dodge, 2007). **Figure 5** illustrates the location of potential Karst in the study area. As shown on the map, a majority of the study area is either on known, inferred or is potential Karst topography.

Karst is a distinctive topography resulting from geological weathering and erosion processes. It is shaped by the dissolution of a layer or layers of soluble bedrock, usually carbonate rock such as limestone and dolomite. Due to the subterranean drainage, there may be very limited surface water because storm runoff is able to seep through cracks and openings into the ground. Many karst regions, such as those in the Niagara Escarpment, display unique surface features such as sinkholes, caverns, and dolines. The underground drainage system created as a result of bed dissolution has the potential to result in significant losses of surface runoff to the subsurface regions.

The impact of Karst topography on runoff generation is often dynamic, and can be changed by anthropogenic developments over time. Given the difficulty in quantifying runoff reductions by potential Karst formations, the VO2 model did not discount this possible reduction in runoff. In essence, it is likely that the physical flow in reality would be smaller than the predicted modelled flow, but this would need to be confirmed with a flow monitoring program and detailed

investigation. For the purpose of this study, the culvert sizing evaluation has used current modelling results and does not account for these losses.

Rainfall Data

The VO2 model was used to simulate the 2 to 100 year design events. Intensity-Duration-Frequency (IDF) data for these events was obtained from the CVC Stormwater Management Guidelines and CVC Standard Parameters documents. Based on the CVC guidelines, a 24 hour Chicago distribution was used in the model for the 2 to 100 year design storms.

Results

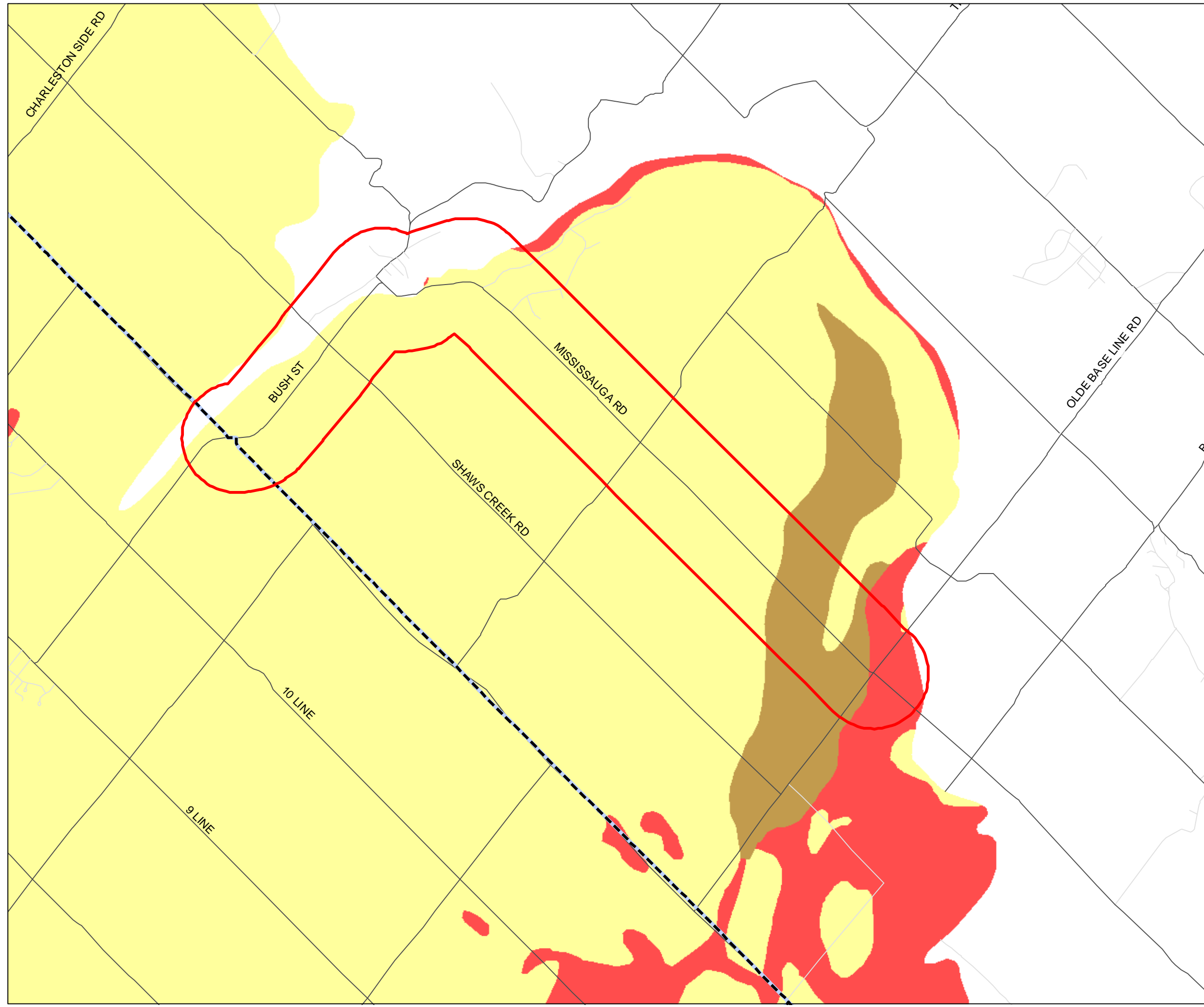
Using the model input parameters described above, the existing conditions VO2 model was run to generate peak flows. Table 2 below summarizes the modeling results for the 13 cross culvert locations. Detailed model outputs are in **Appendix C**.

Table 2: Summary of Existing Peak Flows to Draining to Each Cross Culvert

Culvert ID #	Area (ha)	VO2 Peak Flows (m ³ /s)					
		2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
2	19.15	0.65	1.10	1.44	1.90	2.30	2.65
10	8.81	0.08	0.13	0.18	0.24	0.29	0.33
14	12.27	0.24	0.43	0.60	0.83	1.02	1.20
16	4.23	0.19	0.33	0.44	0.59	0.72	0.85
17	35.03	0.31	0.54	0.72	0.96	1.18	1.38
24	2.77	0.15	0.24	0.31	0.41	0.49	0.57
37	21.05	0.31	0.50	0.65	1.42	1.88	3.29
43	48.56	0.53	0.92	1.37	2.68	3.37	4.99
44	127.28	1.19	2.12	2.87	3.91	4.86	5.70
47	0.24	0.02	0.03	0.03	0.04	0.05	0.06
48	17.52	0.16	0.28	0.39	0.53	0.66	0.87
55	7.71	0.15	0.27	0.37	0.50	0.61	0.72
56	0.91	0.03	0.06	0.08	0.11	0.13	0.16

The model results indicate relatively high peak flows for the relatively large drainage areas at some locations. There are several important factors potentially impacting the drainage characteristics of this area that suggest model flows are higher than actual flows. Runoff potential can be severely reduced due to deep losses to Karst topography. Also, with many depressed areas and rolling hills, the area of ineffective drainage may actually be higher than the conservative approach taken in the VO2 hydrologic model. As a result of these conditions, actual runoff to the cross culverts is substantially reduced relative to the modelled results.

**Bush Street and Mississauga Road
Class EA
Figure 5: Potential Karst Location**



Legend

- Local Roads
- Secondary Roads
- Highway
- Study Area
- Municipalities

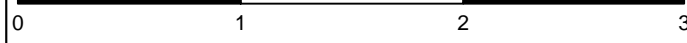
Karst Locations

- Known Location
- Inferred Location
- Potential Location

Source: Karst of Southern Ontario and Manitoulin Island. Ministry of Northern Development and Mines, 2007.



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Flooding due to poor conveyance across the road is likely limited throughout the study area due to the Karst landscape and rolling topography. Further details on this discussion are included below in the hydraulic assessment.

2.2.2 Hydraulic Assessment

The hydraulic assessment was based on a review of the culverts' physical conditions as well as hydraulic modelling using Bentley's CulvertMaster program. CulvertMaster is widely used in the design and analysis of culvert hydraulics, and solves most variables including culvert size, flow and headwater. Its can handle free surface flow, pressure and varied flow situations including backwater and drawdown curves.

A majority of the 14 cross culverts are CSPs while one is PVC pipe. Sizes range from 300 mm to 1200 mm. Table 3 summarizes the culvert characteristics.

Table 3: Cross Culvert Characteristics

Culvert ID #	Size (mm)	Type	Material	Slope (m/m)	Invert Elevation (m)		Effective X-S Area (%)
					U/S	D/S	
2	900	circular	CSP	0.017	387.32	386.73	90
10	450	circular	PVC	0.017	382.71	382.48	n/a
14	600	circular	CSP	0.028	380.43	379.94	90
16	300	circular	CSP	0.056	386.15	385.25	n/a
17	300	circular	CSP	0.035	384.68	384.33	5
24	400	circular	CSP	0.032	428.30	427.82	10
37	600	circular	CSP	0.031	418.80	418.41	60
43	900 x 500	ellipse	CSP	0.014	400.13	399.96	100
44n	1200 x 1000	ellipse	CSP	0.014	399.46	399.27	100
44s	1200 x 1000	ellipse	CSP	0.010	399.44	399.31	100
47	400	circular	CSP	0.017	398.17	397.96	60
48	400	circular	CSP	0.020	394.08	393.84	76
55	300	circular	CSP	0.026	388.76	388.43	60
56	300	circular	CSP	0.004	387.26	387.21	5

A capacity rating for each of the culverts was determined based on the existing physical conditions of the culverts as summarized in the culvert inventory compiled by the Region and the following MTO criteria shown in Table 4.

Table 4: Capacity Rating Criteria

Category	Description	Effective Cross Section
Very Good	Little to no sediment build up in pipe. Culvert ends are undamaged. Little to no debris blocking flow.	100 %
Good	Original culvert capacity diminished by 5% or less.	95 % - 99 %
Fair	Original culvert capacity diminished by less than 15%.	85 % - 94 %
Poor	Original culvert capacity diminished by less than 25%.	75 % - 84 %
Below Minimum Tolerable	Original culvert capacity diminished by more than 25%.	0 % - 74 %

Table 5 below summarized the capacity rating for each culvert and describes whether or not the current structure meets the Region's standards for minimum pipe size.

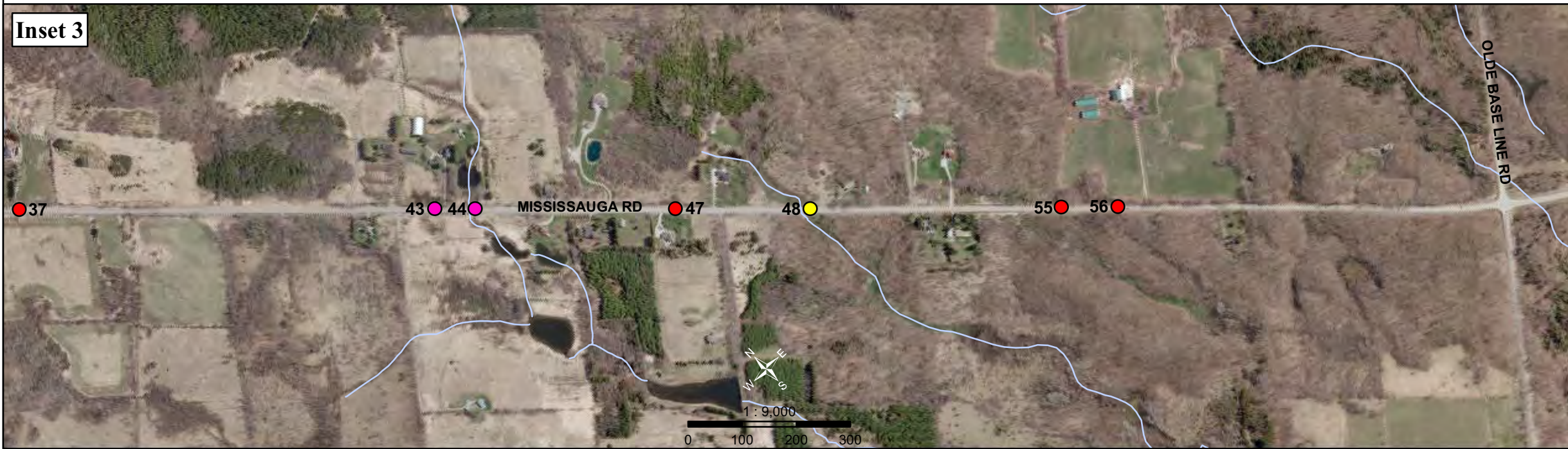
Table 5: Capacity Rating of Cross Culverts under Existing Conditions

Culvert ID #	Size (mm)	Capacity Rating (CR)	Meeting Region's current standard (min. 600mm)
2	900	Fair	Yes
10	450	Good	No
14	600	Fair	Yes
16	300	Fair	No
17	300	Below Minimum Tolerable	No
24	400	Below Minimum Tolerable	No
37	600	Below Minimum Tolerable	Yes
43	900 x 500	Very Good	Yes
44 (north)	1200 x 1000	Very Good	Yes
44 (south)	1200 x 1000	Very Good	Yes
47	400	Below Minimum Tolerable	No
48	400	Poor	No
55	300	Below Minimum Tolerable	No
56	300	Below Minimum Tolerable	No

The capacity rating along with additional information summarized in the Region's inventory sheets provides recommendations to maintain and/or upgrade specific culverts. As shown, some culvert sizes do not meet the Region's current standard; however in some cases the depth of cover over the road is not sufficient to accommodate a 600 mm culvert. However, these entrance culverts may have been consistent with standard practices at the time of construction. **Figure 6** illustrates the capacity rating and where culvert pipe sizes do not comply with the current Region standard. Detailed information is provided in **Appendix G**.

The hydraulic capacities of existing cross culverts were determined based on information provided by the Region (i.e., invert elevations and slopes) and with information recorded during the reconnaissance-level site visit (i.e., tailwater (TW) assumptions based on ponding observations at downstream side of culvert). If ponding was observed at the downstream end of the culvert, a conservative tailwater assumption would be considered whereby TW level would be set at the downstream obvert elevation in the CulvertMaster model.

The top of road elevation was determined at each cross culvert and assigned as the threshold elevation, above which flows would overtop the roadway. With these input parameters, Culvert Master was run and the hydraulic capacity with water level at the top of road elevation was estimated. Table 6 presents the maximum culvert flows before overtopping the roadway under existing conditions. Please refer to **Appendix E** for detailed input information. CulvertMaster model outputs are provided in **Appendix F**.



Bush Street and Mississauga Road Figure 6: Cross Culvert - Capacity Rating

- Legend**
- 16 Cross Culvert ID #
 - Watercourse
- Capacity Rating**
- Very Good Condition
 - Good Condition
 - Fair Condition
 - Poor Condition
 - Below Minimum Tolerable

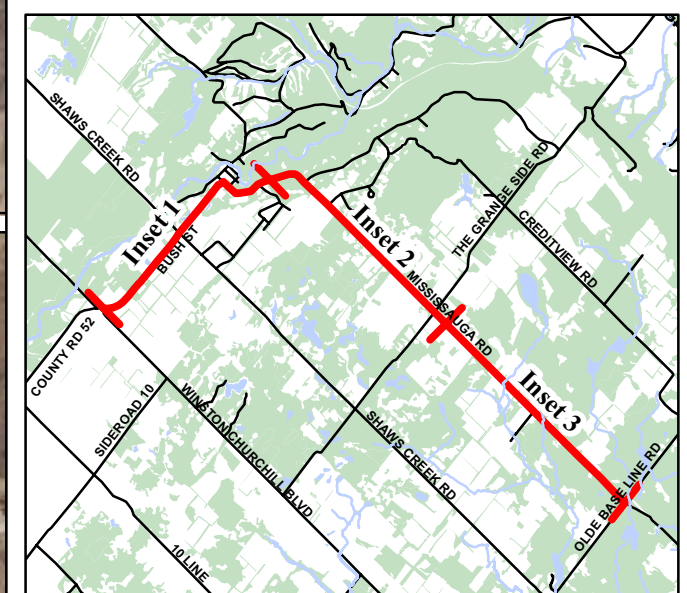


Table 6: Existing Cross Culvert Hydraulic Capacity at Top of Road Elevation

Culvert ID #	Size (mm)	Invert Elevation (m)		At Top of Road		
		U/S	D/S	Elevation (m)	Capacity (m ³ /s)	Level of Service (Return Period)
2	900	387.32	386.73	394.32	3.486	100-year
10	450	382.71	382.48	383.34	0.227	10-year
14	600	380.43	379.94	381.62	0.639	10-year
16	300	386.15	385.25	386.86	0.128	Less than 2-year
17	300	384.68	384.33	385.30	0.116	Less than 2-year
24	400	428.30	427.82	429.24	0.216	2-year
37	600	418.80	418.41	419.99	0.639	5-year
43	900 x 500	400.13	399.96	400.88	0.549	2-year
44n	1200 x 1000	399.46	399.27	400.76	1.687	10-year
44s	1200 x 1000	399.44	399.31	400.76	1.603	10-year
47	400	398.17	397.96	398.98	0.184	100-year
48	400	394.08	393.84	394.95	0.189	2-year
55	300	388.76	388.43	389.39	0.106	Less than 2-year
56	300	387.26	387.21	388.16	0.109	25-year

Comparing the hydrologic modelling results in Table 2 with the maximum culvert capacity in Table 6, an existing level of service is determined (last column of Table 6). **Figure 7** shows the existing level of service for cross culverts. As anticipated, the majority of the cross culverts do not meet the current Region's standard; that is, to provide a level of service for a 1 in 25 year storm event. This however, is expected, since many of the culverts do not even meet the minimum size requirement of 600 mm. As the culverts sizes are relatively small, flooding over the road on a frequent basis should be prevalent in this area.

If modelled flows to cross culverts are likely to be higher than reality (due to the discounting of the impact of Karst topography), the actual LOS provided by the cross culverts is presumably better than that indicated by the CulvertMaster model. The hydrologic and hydraulic model findings would indicate that flooding over the road is a frequent occurrence in this area. However, flooding issues within the study appear to be associated with drainage parallel to the road as a result of deficiencies with the drainage system (i.e. shoulder, ditches and entrance culverts). There is no known evidence of flooding due to poor drainage across the road as determined during the field visits. A local resident located near cross culvert # 43 indicated his property does experience occasional flooding due to poor conveyance of this structure. He also

noted similar problems are not evident at culvert # 44. As noted above, flooding across the road is likely limited throughout the entire study area due to the potential Karst landscape and its influence on runoff flows. Based on these reasons, it may be more realistic and appropriate to adopt the Region's 600 mm minimum pipe size rather than meet a return period LOS. Following the minimum pipe size standard would likely be sufficient at most cross culvert locations to provide a 25-year level of service.

2.3 Evaluation of Road Drainage System

A separate approach has been established to review and evaluate the road drainage system, which includes entrance culverts and roadside ditches. A hydrologic assessment was conducted for ditches using the Rational Method, while the hydraulic review was completed based on the Manning's Equation. For entrance culverts, a capacity rating analysis similar to that of the cross culverts was carried out.

2.3.1 Hydrologic Assessment of Roadside Ditches

Although there are many roadside ditches along various stretches of Bush Street and Mississauga Road, only continuous ditches of significant length and those associated with entrance culverts were included in the review. In essence, ditches of very short lengths, with no distinct flow direction (e.g. ditch slopes alternating between positive and negative grades), and ditches that do not connect to any entrance culverts were not a part of the analysis. **Figure 8** identifies these 35 ditches that were analyzed as part of this investigation.

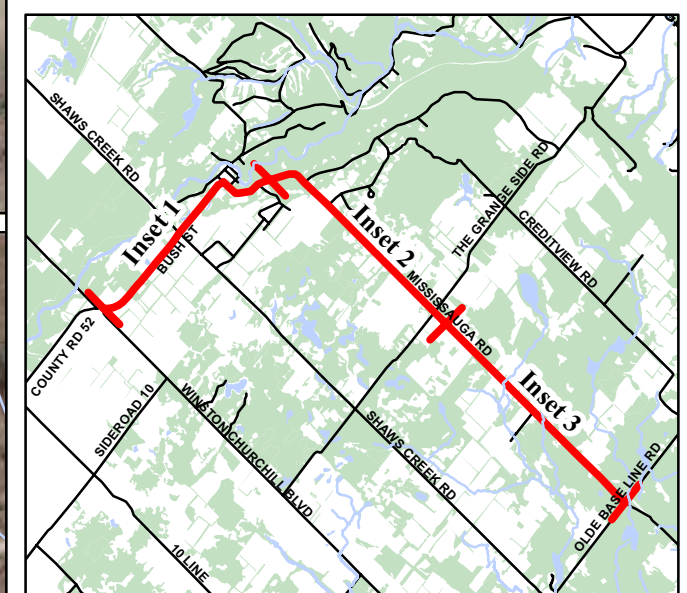
Each ditch identification number has a sub-section ID attached. A long ditch (e.g. ditch M115) may be divided into several sub-sections labelled A, B and C respectively. The points of division are landmarked by entrance culverts. For example, ditch M115 is identified with 3 distinct sections; namely, ditch M115-Section A, ditch M115-Section B and ditch M115-Section C. Each section is evaluated separately for flows. **Figure 9** illustrates how ditch sections are labelled.



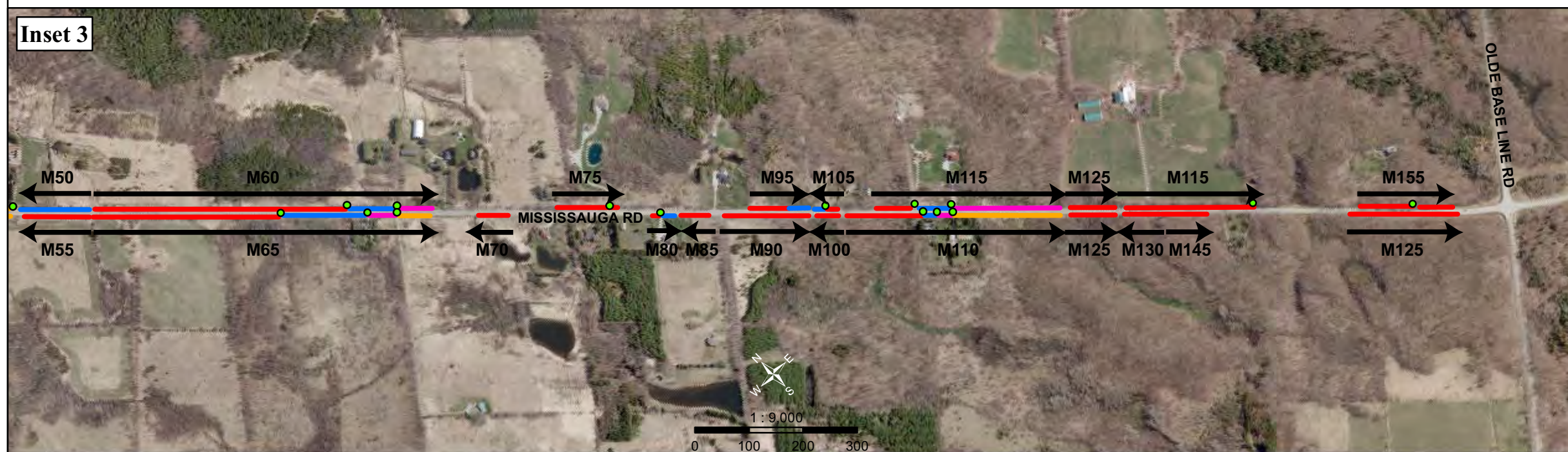
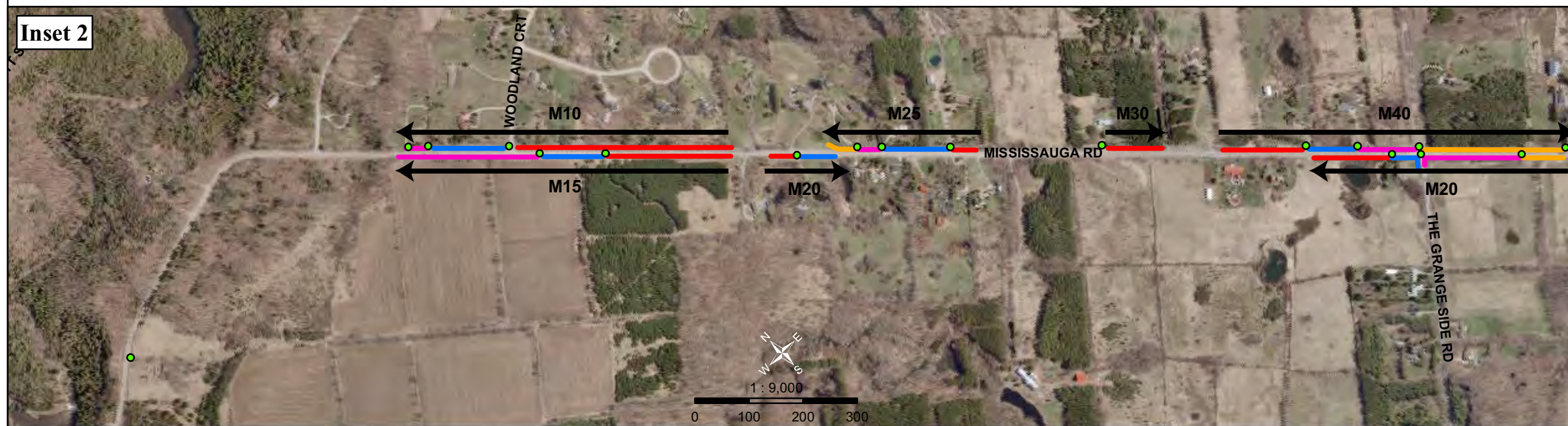
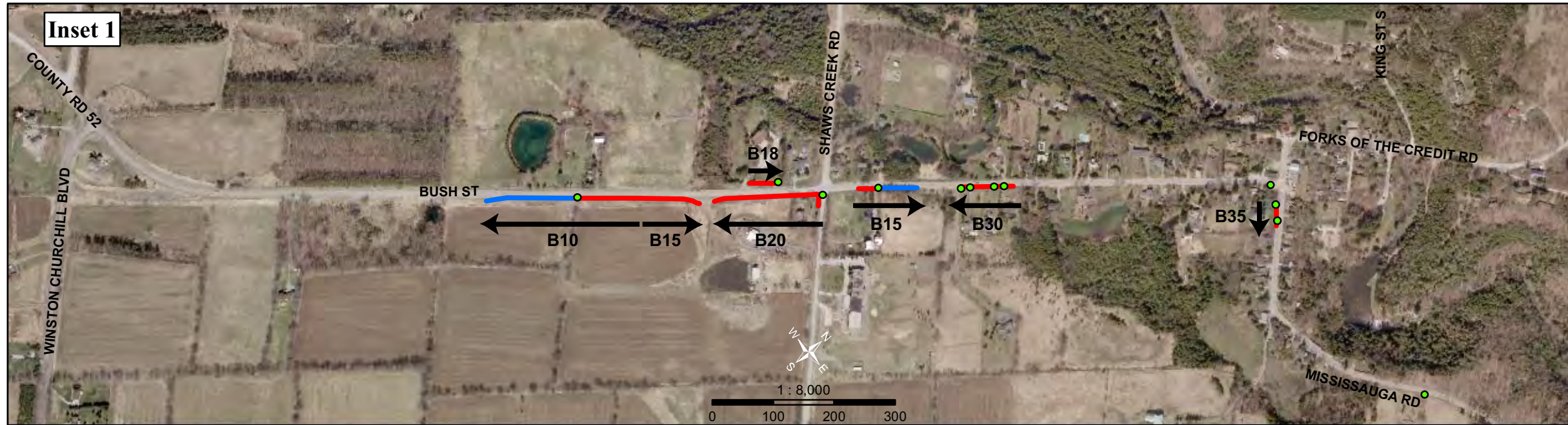
Bush Street and Mississauga Road Figure 7: Cross Culvert - Existing Level of Service

Legend

- 16 Cross Culvert ID #
 - Watercourse
- ### Existing Level of Service
- < 2 year Storm Event
 - 2 year Storm Event
 - 5 year Storm Event
 - 10 year Storm Event
 - 25 year Storm Event
 - > 100 year Storm Event



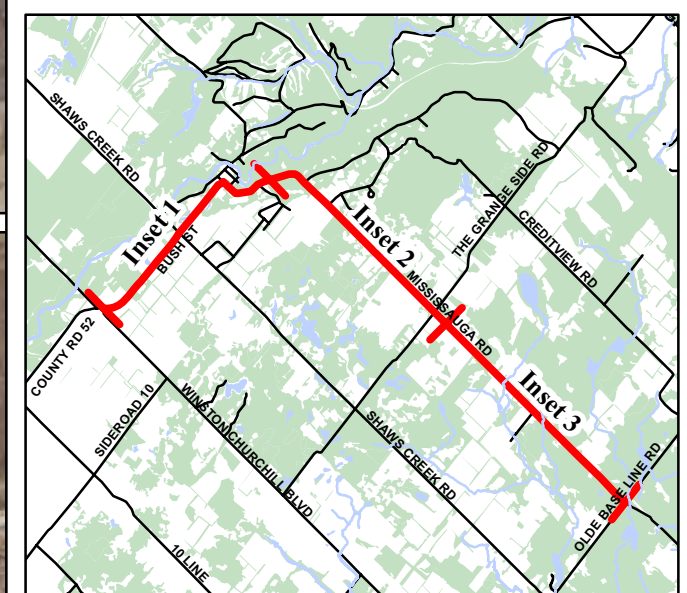
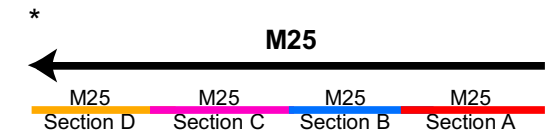
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Bush Street and Mississauga Road
Figure 8: Roadside Ditch Locations

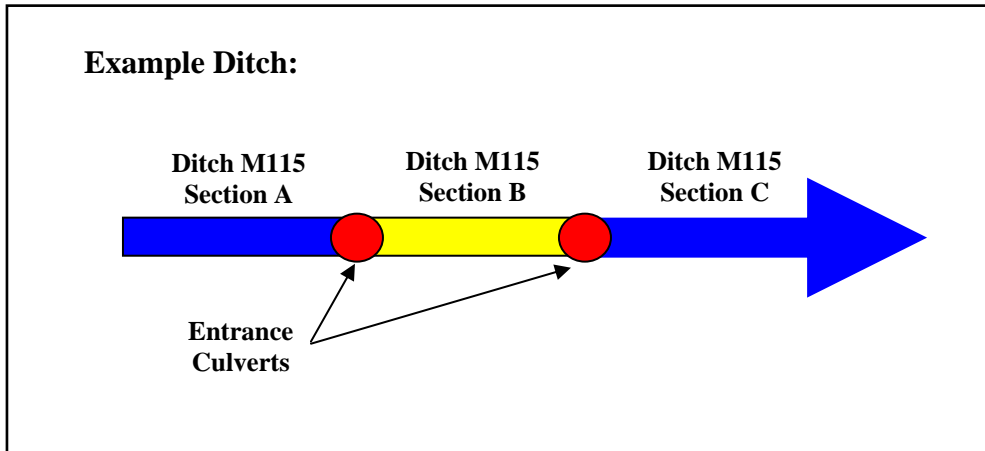
Legend

- M10 Roadside Ditch ID #
- Entrance Culvert
- Ditch Section A
- Ditch Section B
- Ditch Section C
- Ditch Section D
- Flow Direction*



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Figure 9: Ditch Identification and Section Labelling



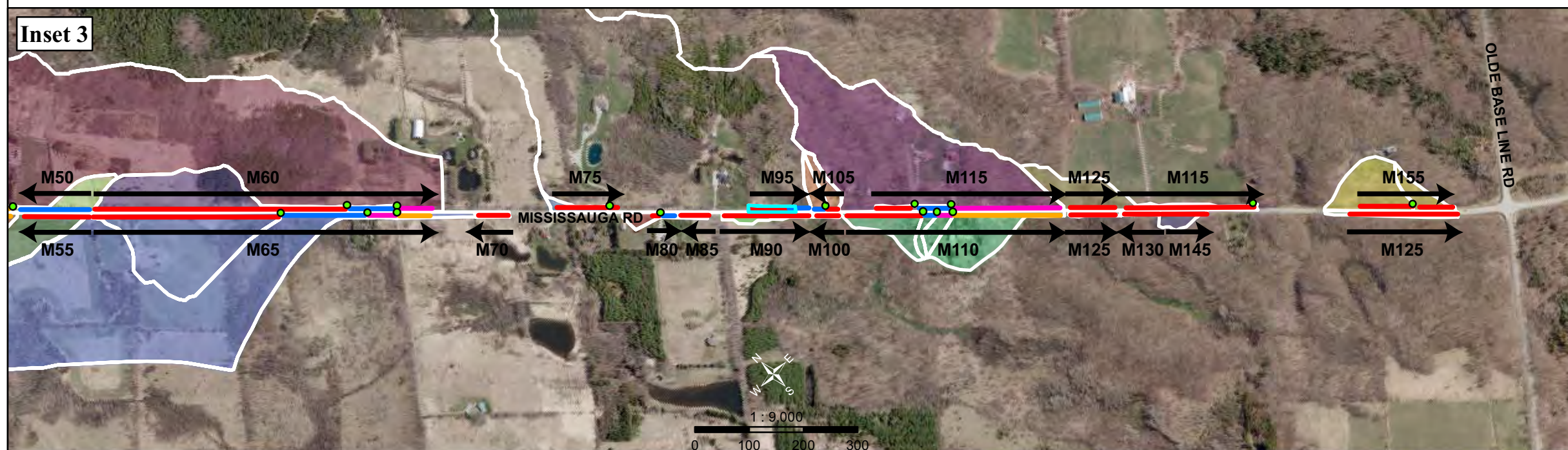
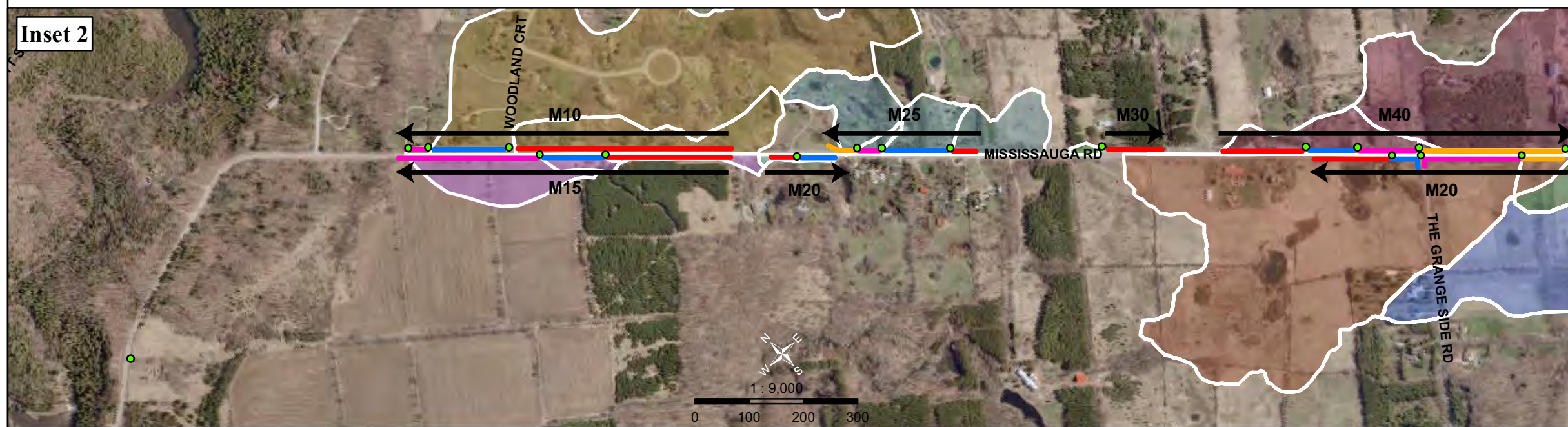
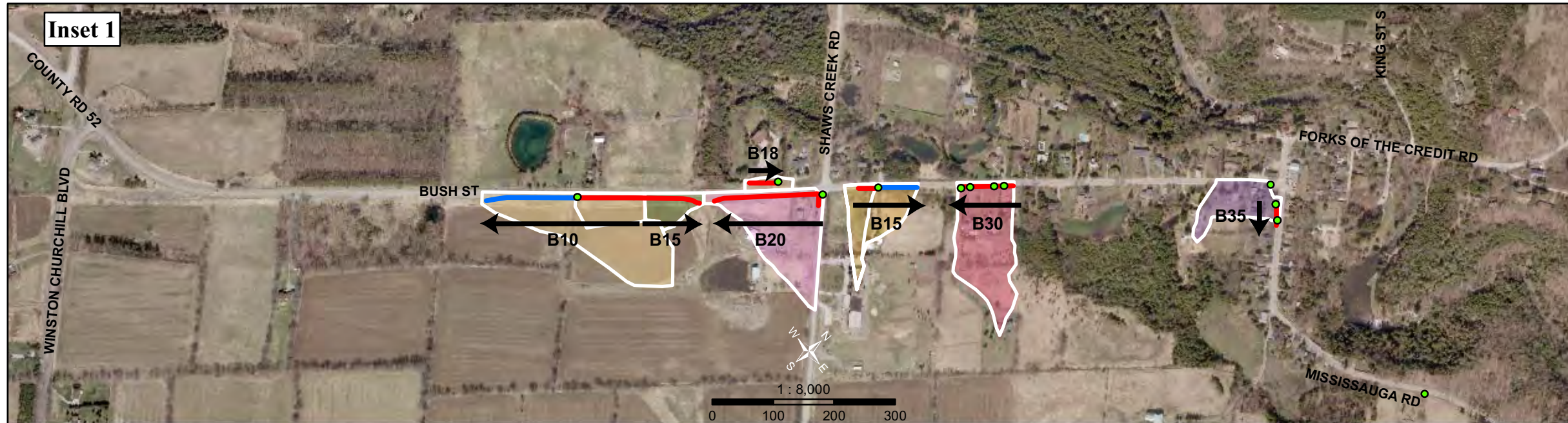
Drainage Area Characterization

The Rational Method was used to complete the hydrologic assessment of the roadside ditches. Similar to the hydrologic evaluation for cross culverts, the drainage area tributary to each of the identified ditches was first determined. A detailed GIS analysis to delineate these catchment boundaries and to characterize surface drainage patterns was conducted. **Figure 10** presents the catchment delineation for roadside ditches.

As previously mentioned in the hydrologic assessment for cross culverts, the surficial soils in the study area consist mostly of loam. The appropriate runoff coefficients C were selected from the MTO Drainage Manual (Design Chart 1.07) based on this soil texture, along with the corresponding catchment land use and topography. The corresponding time of concentration (T_c) for each catchment was subsequently estimated based on the SCS Upland Method. A minimum inlet time of 10 minutes was used following the Region of Peel storm sewer design criteria (Section 4.0, July 2009).

Rainfall Data

Based on the Region of Peel Design Guidelines, the criteria used to review the road drainage system (ditches) are to be based on the 10-year design event. The Intensity-Duration-Frequency (IDF) data for these events was obtained from the CVC Stormwater Management Guidelines and CVC Standard Parameters documents. Using the Rational Method, the peak flows to ditches were determined for the 10-year design storm.



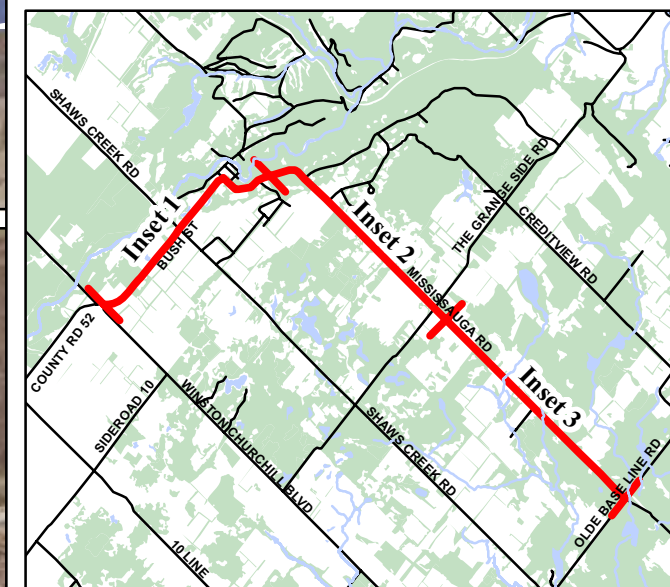
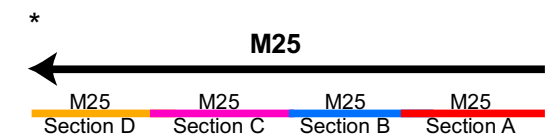
Bush Street and Mississauga Road Figure 10: Drainage Areas to Roadside Ditches

Legend

- M10** Roadside Ditch ID #
- Entrance Culvert
- Ditch Section A
- Ditch Section B
- Ditch Section C
- Ditch Section D
- Flow Direction*

Ditch Drain Areas

B10	M20	M70	M115
B15	M25	M75	M120
B18	M30	M80	M125
B20	M40	M85	M130
B25	M45	M90	M140
B30	M50	M95	M145
B35	M55	M100	M150
M10	M60	M105	M155
M15	M65	M110	



Results

Using the drainage area characteristics and the Rational Method, peak flows for each of the ditch sections were determined. Table 7 summarizes the catchment parameters for ditches as well as the results of the peak flow assessment. Please refer to **Appendix D** for detailed calculations.

Table 7: Roadside Ditches Characteristics and Peak Flows

Ditch ID	Ditch Sub-section ID	Rational Method				
		Total Drainage Area to Ditch (ha)	Area-weighted Runoff Coeff. C	T _c = t (min)	Intensity based on 10-year storm (mm/hr)	Peak Flow to Ditches Q _p = 0.00278CiA (m ³ /s)
B10	A	0.57	0.426	17.4	90.1	0.06
B10	B	2.67	0.388	19.1	85.4	0.25
B15	A	0.41	0.406	15.9	94.7	0.04
B18	A	0.16	0.607	15.8	95.0	0.03
B20	A	1.91	0.498	17.0	91.1	0.24
B25	A	0.44	0.446	15.4	96.3	0.05
B25	B	0.98	0.427	16.0	94.2	0.11
B30	A	1.84	0.415	16.2	93.7	0.20
B35	A	0.79	0.435	15.0	97.6	0.09
M10	A	2.95	0.376	18.8	86.3	0.27
M10	B	20.42	0.364	20.1	83.0	1.71
M10	C	20.47	0.365	20.7	81.6	1.69
M100	A	0.05	0.652	16.2	93.5	0.01
M105	A	0.25	0.312	15.7	95.2	0.02
M105	B	0.48	0.318	16.4	93.0	0.04
M110	A	0.62	0.337	15.5	95.9	0.06
M110	B	0.77	0.345	15.9	94.7	0.07
M110	C	0.98	0.358	16.5	92.8	0.09
M110	D	2.29	0.361	23.6	75.3	0.17
M115	A	0.06	0.608	15.8	94.8	0.01
M115	B	0.14	0.639	17.2	90.6	0.02
M115	C	7.71	0.301	25.6	71.7	0.46
M120	A	0.10	0.624	17.2	90.5	0.02
M125	A	0.91	0.307	16.3	93.4	0.07
M130	A	0.06	0.705	17.1	91.0	0.01
M140	A	0.20	0.746	19.1	85.4	0.04
M145	A	0.23	0.433	16.1	93.8	0.03
M15	A	0.38	0.607	17.3	90.2	0.06
M15	B	0.75	0.546	18.7	86.5	0.10
M15	C	2.83	0.426	23.5	75.5	0.25
M150	A	0.22	0.661	17.7	89.1	0.04
M155	A	1.07	0.317	15.9	94.7	0.09
M155	B	1.40	0.332	16.7	92.1	0.12
M20	A	0.08	0.572	15.6	95.6	0.01

Ditch ID	Ditch Sub-section ID	Rational Method				
		Total Drainage Area to Ditch (ha)	Area-weighted Runoff Coeff. C	T _c = t (min)	Intensity based on 10-year storm (mm/hr)	Peak Flow to Ditches Q _p = 0.00278CiA (m ³ /s)
M20	B	0.17	0.667	16.5	92.8	0.03
M25	A	1.53	0.380	15.6	95.6	0.15
M25	B	2.66	0.408	18.9	85.9	0.26
M25	C	2.85	0.419	19.6	84.3	0.28
M25	D	4.73	0.401	20.2	82.6	0.44
M30	A	0.09	0.538	15.0	97.6	0.01
M40	A	0.47	0.381	16.9	91.6	0.05
M40	B	0.58	0.419	17.9	88.7	0.06
M40	C	1.86	0.359	20.8	81.3	0.15
M40	D	2.16	0.399	25.4	72.0	0.17
M45	A	0.16	0.609	17.1	90.8	0.02
M45	B	0.33	0.558	17.9	88.7	0.05
M45	C	20.14	0.355	26.3	70.5	1.40
M45	D	20.61	0.357	29.5	65.6	1.34
M50	A	0.57	0.434	16.8	91.9	0.06
M55	A	1.17	0.386	15.4	96.3	0.12
M65	A	3.04	0.345	16.6	92.3	0.27
M65	B	17.38	0.325	31.7	62.6	0.98
M65	C	17.44	0.327	32.4	61.8	0.98
M65	D	17.59	0.329	36.4	57.2	0.92
M75	A	0.16	0.587	16.2	93.7	0.02
M80	A	0.14	0.443	15.0	97.6	0.02
M80	B	0.17	0.494	15.5	95.9	0.02
M85	A	0.06	0.655	16.6	92.4	0.01
M90	A	0.24	0.585	17.5	89.7	0.04
M95	A	0.09	0.597	18.2	87.8	0.01
M95	B	17.04	0.286	28.9	66.4	0.90
M60	A	2.16	0.467	23.7	75.3	0.21
M60	B	2.26	0.474	24.9	73.0	0.22
M60	C	49.30	0.391	54.8	43.2	2.31
M70	A	0.06	0.696	16.0	94.1	0.01

The catchment areas for ditches are located on potential Karst topography, as mentioned previously in the hydrologic assessment for cross culverts (please see cross culvert sections for more details). Given the difficulty in quantifying runoff reductions by potential Karst landscapes, the Rational Method did not discount this probable reduction in runoff. However, actual runoff flows to ditches may be smaller than those estimated by the current Rational Method, but would need to be confirmed with additional flow monitoring and detailed investigation. For the purpose of this study a conservative approach has been followed since the evaluation has used modelled estimates and does not account for these losses. Nevertheless, it is important that Karst be acknowledged as a potential factor affecting drainage within the study area.

2.3.2 Hydraulic Review

Roadside Ditches

The hydraulic assessment of the roadside ditches was conducted using the Manning's Equation to determine their capacities and ultimately the level of service relative to the Region's standards. Representative cross sections of the ditches were obtained during the field reconnaissance for this purpose. Based on the estimated cross-sectional, longitudinal slope information and the ditch lining material (i.e., grass, vegetation, gravel, etc.), the ditch capacities were determined.

The physical conditions and cross sectional profiles of the roadside ditches vary extensively along Bush Street and Mississauga Road. Although some ditches are indicated on the 2009 survey drawing provided by the Region, field observations sometimes revealed that those ditches were not evident. Also, the cross sectional characteristics of a single ditch may change continuously along its length. However, the "representative" ditch cross-section information was obtained in the field for the most constrained section of the ditch. For a review of the ditch capacity, this level of analysis is deemed appropriate. More detailed analysis would include a survey of the entire ditch which is beyond the scope of this work.

Table 8 presents the ditch capacities estimated by Manning's Equation. An assessment of the 10-year peak flows for the ditches and the available ditch capacities determines whether or not they meet the Level of Service based on the Region's current standard. **Figure 11** summarizes these findings.



**Bush Street and Mississauga Road
Figure 11: Roadside Ditch Level of Service**

Legend

- M10** Roadside Ditch ID #
- Entrance Culvert
- Ditches with Sufficient Capacity for 10 - Year Storm
- Ditches without Sufficient Capacity for 10 - Year Storm
- Flow Direction*

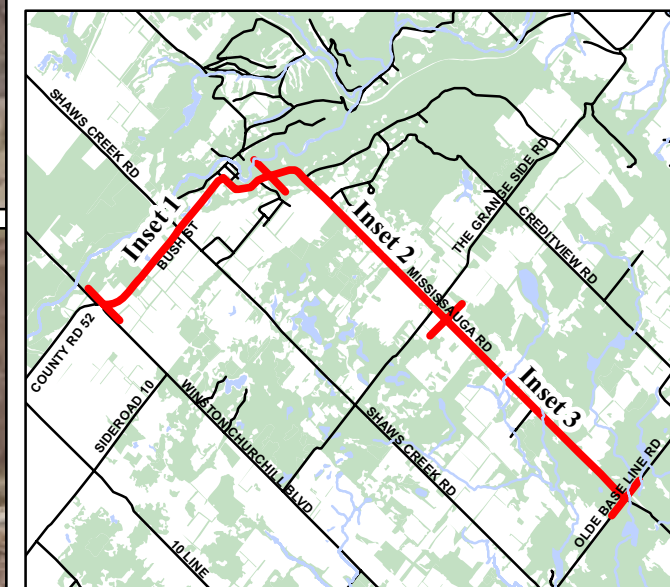
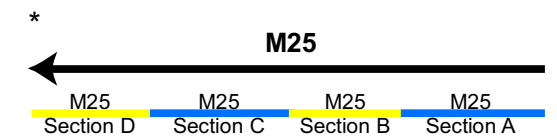


Table 8: Ditch Capacities and Level of Service

Ditch ID	Ditch Sub-section ID	Rational Method		Existing Ditch Cross Section Profile (estimated)						Level of Service (Is existing ditch capacity sufficient for the 10-year event?)
		Total Drainage Area to Ditch (ha)	Peak Flow to Ditches Q_p (m ³ /s)	Top Width (m)	Depth (m)	Side Slope (H:V)	Bottom Width (m)	Long Slope (m/m)	Maximum Ditch Capacity (m ³ /s) based on Manning's Eqn	
B10	A	0.57	0.06	1.8	0.25	2.5	0.5	0.016	0.34	Yes
B10	B	2.67	0.25	1.8	0.25	2.5	0.5	0.035	0.51	Yes
B15	A	0.41	0.04	7.0	0.49	4.1	3.0	0.090	12.1	Yes
B18	A	0.16	0.03	9.5	0.66	5.0	2.9	0.020	11.0	Yes
B20	A	1.91	0.24	3.7	0.84	2.2	0.0	0.035	5.04	Yes
B25	A	0.44	0.05	1.9	0.40	1.7	0.6	0.038	1.25	Yes
B25	B	0.98	0.11	1.9	0.40	1.7	0.6	0.084	1.85	Yes
B30	A	1.84	0.20	2.2	0.55	1.5	0.6	0.004	0.65	Yes
B35	A	0.79	0.09	0.4	0.34	0.6	0.0	0.020	0.06	No
M10	A	2.95	0.27	2.0	0.30	0.5	1.3	0.060	1.24	Yes
M10	B	20.42	1.71	3.1	1.32	1.0	0.0	0.016	4.14	Yes
M10	C	20.47	1.69	3.1	1.32	1.0	0.0	0.027	5.37	Yes
M100	A	0.05	0.01	1.5	0.40	0.0	1.5	0.011	0.84	Yes
M105	A	0.25	0.02	2.0	0.24	4.2	0.0	0.005	0.14	Yes
M105	B	0.48	0.04	2.0	0.24	4.2	0.0	0.014	0.22	Yes
M110	A	0.62	0.06	1.0	0.10	3.0	0.4	0.017	0.05	No
M110	B	0.77	0.07	1.0	0.10	3.0	0.4	0.039	0.08	Yes
M110	C	0.98	0.09	1.0	0.10	3.0	0.4	0.017	0.05	No
M110	D	2.29	0.17	1.0	0.10	3.0	0.4	0.006	0.03	No
M115	A	0.06	0.01	1.1	0.15	0.3	1.0	0.041	0.26	Yes
M115	B	0.14	0.02	1.1	0.15	0.3	1.0	0.022	0.19	Yes
M115	C	7.71	0.46	1.1	0.15	0.3	1.0	0.004	0.08	No
M120	A	0.10	0.02	No ditch evident observed in field					0	No ditch evident
M125	A	0.91	0.07	1.2	0.31	1.9	0	0.012	0.18	Yes
M130	A	0.06	0.01	No ditch evident observed in field					0	No ditch evident

Ditch ID	Ditch Sub-section ID	Rational Method		Existing Ditch Cross Section Profile (estimated)						Level of Service (Is existing ditch capacity sufficient for the 10-year event?)	
		Total Drainage Area to Ditch (ha)	Peak Flow to Ditches Q_p (m ³ /s)	Top Width (m)	Depth (m)	Side Slope (H:V)	Bottom Width (m)	Long Slope (m/m)	Maximum Ditch Capacity (m ³ /s) based on Manning's Eqn		
M140	A	0.20	0.04	1.0	0.35	0.7	0.5	0.020	0.42	Yes	
M145	A	0.23	0.03	No ditch evident observed in field						0	No ditch evident
M15	A	0.38	0.06	2.0	0.30	2.0	1.3	0.060	1.62	Yes	
M15	B	0.75	0.10	1.9	0.60	1.0	0.7	0.052	2.82	Yes	
M15	C	2.83	0.25	2.0	0.68	1.0	0.6	0.018	2.01	Yes	
M150	A	0.22	0.04	1.7	0.48	1.0	0.7	0.039	1.62	Yes	
M155	A	1.07	0.09	2.1	0.60	1.3	0.6	0.035	2.38	Yes	
M155	B	1.40	0.12	2.1	0.60	1.3	0.6	0.053	2.92	Yes	
M20	A	0.08	0.01	1.0	0.70	0.5	0	0.041	0.48	Yes	
M20	B	0.17	0.03	1.0	0.70	0.5	0	0.037	0.46	Yes	
M25	A	1.53	0.15	1.7	0.30	2.8	0	0.039	0.46	Yes	
M25	B	2.66	0.26	1.7	0.30	2.8	0	0.009	0.22	No	
M25	C	2.85	0.28	1.7	0.30	2.8	0	0.025	0.36	Yes	
M25	D	4.73	0.44	1.7	0.30	2.8	0	0.014	0.27	No	
M30	A	0.09	0.01	No ditch evident observed in field						0	No ditch evident
M40	A	0.47	0.05	1.5	0.30	0.5	1.2	0.020	0.70	Yes	
M40	B	0.58	0.06	1.5	0.30	0.5	1.2	0.058	1.17	Yes	
M40	C	1.86	0.15	1.8	0.33	2.7	0	0.010	0.28	Yes	
M40	D	2.16	0.17	3.1	0.60	1.8	0.9	0.022	2.99	Yes	
M45	A	0.16	0.02	2.5	0.75	1.0	1.0	0.034	4.49	Yes	
M45	B	0.33	0.05	4.7	1.26	1.4	1.1	0.024	14.2	Yes	
M45	C	20.14	1.40	2.1	0.65	0.8	1.0	0.020	2.43	Yes	
M45	D	20.61	1.34	2.1	0.65	0.8	1.0	0.006	1.31	No	
M50	A	0.57	0.06	1.9	0.40	1.5	0.7	0.027	1.10	Yes	
M55	A	1.17	0.12	1.2	0.33	1.2	0.4	0.023	0.43	Yes	
M65	A	3.04	0.27	2.0	0.60	1.3	0.5	0.010	1.15	Yes	
M65	B	17.38	0.98	2.0	0.60	1.3	0.5	0.003	0.61	No	

Ditch ID	Ditch Sub-section ID	Rational Method		Existing Ditch Cross Section Profile (estimated)						Level of Service (Is existing ditch capacity sufficient for the 10-year event?)
		Total Drainage Area to Ditch (ha)	Peak Flow to Ditches Q_p (m ³ /s)	Top Width (m)	Depth (m)	Side Slope (H:V)	Bottom Width (m)	Long Slope (m/m)	Maximum Ditch Capacity (m ³ /s) based on Manning's Eqn	
M65	C	17.44	0.98	2.0	0.60	1.3	0.5	0.054	2.65	Yes
M65	D	17.59	0.92	2.0	0.60	1.3	0.5	0.010	1.13	Yes
M75	A	0.16	0.02	2.2	0.20	5.5	0	0.020	0.22	Yes
M80	A	0.14	0.02	1.6	0.13	6.2	0	0.029	0.10	Yes
M80	B	0.17	0.02	1.6	0.13	6.2	0	0.029	0.10	Yes
M85	A	0.06	0.01	No ditch evident observed in field					0	No ditch evident
M90	A	0.24	0.04	2.2	0.32	3.4	0	0.024	0.52	Yes
M95	A	0.09	0.01	1.4	0.18	0.0	1.4	0.017	0.30	Yes
M95	B	17.04	0.90	1.4	0.18	0.0	1.4	0.017	0.30	No
M60	A	2.16	0.21	2.1	0.35	2.0	0.7	0.003	0.29	Yes
M60	B	2.26	0.22	2.1	0.35	2.0	0.7	0.042	1.20	Yes
M60	C	49.30	2.31	2.5	0.60	2.1	0	0.005	0.71	No
M70	A	0.06	0.01	1.5	0.60	0.6	0.8	0.025	1.12	Yes

Entrance Culverts

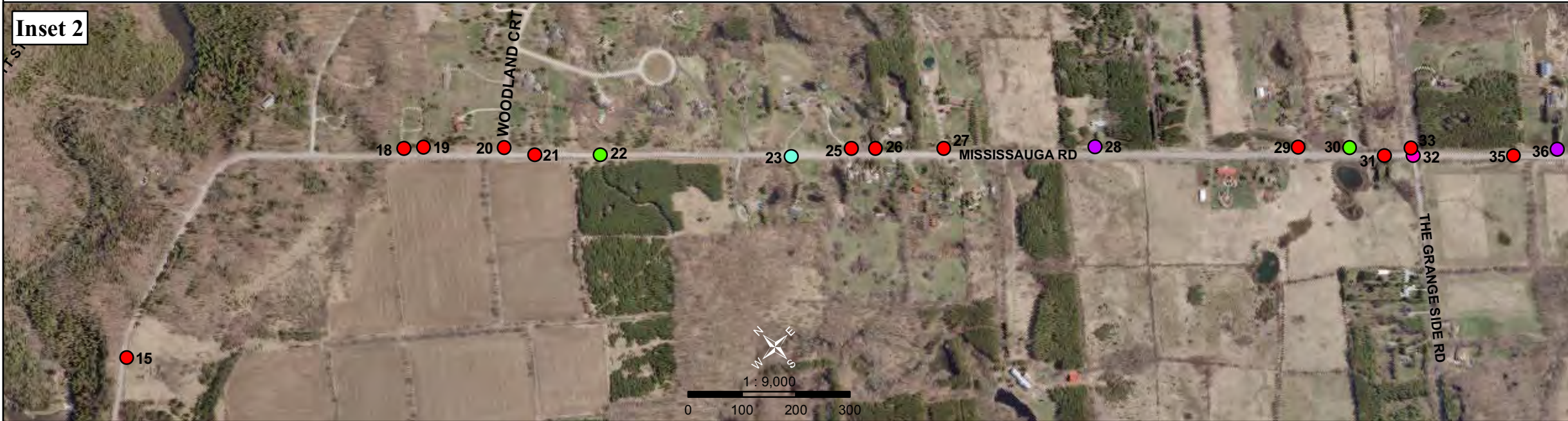
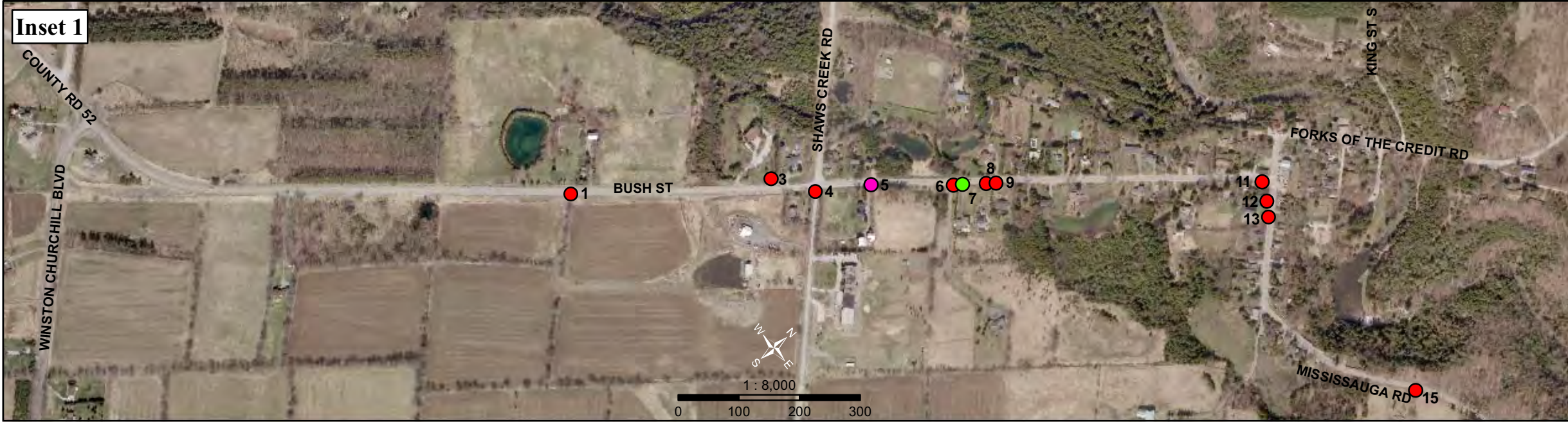
A capacity rating assignment, similar to the one conducted for cross culverts, was performed for entrance culverts as a part of this drainage system review. Table 9 presents the capacity rating of each entrance culvert and where culvert pipe sizes do not comply with current Region standards. **Figure 12** illustrates the capacity rating of entrance culverts. Please refer to **Appendix H** for detailed information.

Table 9: Capacity Rating of Entrance Culverts under Existing Conditions

Culvert ID #	Size (mm)	Meeting Region's current standard (min. 375 mm)	Effective X-Sectional Area (%)	Capacity Rating (CR)
1	300	No	0	Below Minimum Tolerable
3	350	No	60	Below Minimum Tolerable
4	350	No	15	Below Minimum Tolerable
5	300	No	100	Very Good
6	300	No	0	Below Minimum Tolerable
7	300	No	95	Good
8	300	No	30	Below Minimum Tolerable
9*	300	No	40	Below Minimum Tolerable
11	300	No	n/a	Below Minimum Tolerable**
12	300	No	25	Below Minimum Tolerable
13	300	No	50	Below Minimum Tolerable
15	300	No	10	Below Minimum Tolerable
18	400	Yes	60	Below Minimum Tolerable
19	400	Yes	40	Below Minimum Tolerable
20	500	Yes	0	Below Minimum Tolerable
21	400	Yes	0	Below Minimum Tolerable
22	400	Yes	95	Good
23	400	Yes	n/a	n/a
25	400	Yes	20	Below Minimum Tolerable
26	400	Yes	60	Below Minimum Tolerable
27	300	No	16	Below Minimum Tolerable
28	400	Yes	n/a	Fair**
29	400	Yes	60	Below Minimum Tolerable
30	600	Yes	95	Good
31	600	Yes	40	Below Minimum Tolerable
32*	600	Yes	100	Very Good
33*	400	No	0	Below Minimum Tolerable
35	500	Yes	15	Below Minimum Tolerable
36	600	Yes	90	Fair
38	400	Yes	50	Below Minimum Tolerable
39	500	Yes	60	Below Minimum Tolerable
40	600	Yes	100	Very Good
41	500	Yes	70	Below Minimum Tolerable
42	500	Yes	40	Below Minimum Tolerable

Culvert ID #	Size (mm)	Meeting Region's current standard (min. 375 mm)	Effective X-Sectional Area (%)	Capacity Rating (CR)
45	400	Yes	5	Below Minimum Tolerable
46	300	No	15	Below Minimum Tolerable
49	500	Yes	95	Good
50	400	Yes	50	Below Minimum Tolerable
51	400	Yes	90	Fair
52	400	Yes	90	Fair
53	300	No	5	Below Minimum Tolerable
54	400	Yes	75	Poor
57	200	No	0	Below Minimum Tolerable
58	200	No	n/a	Below Minimum Tolerable**
Note: * = The culvert does not cross Bush Street or Mississauga Road, but transverse smaller side roads.				
** = Region's inventory data not available for this culvert. Evaluation based on field observations.				
They are required to have a minimum size of 600 mm.				

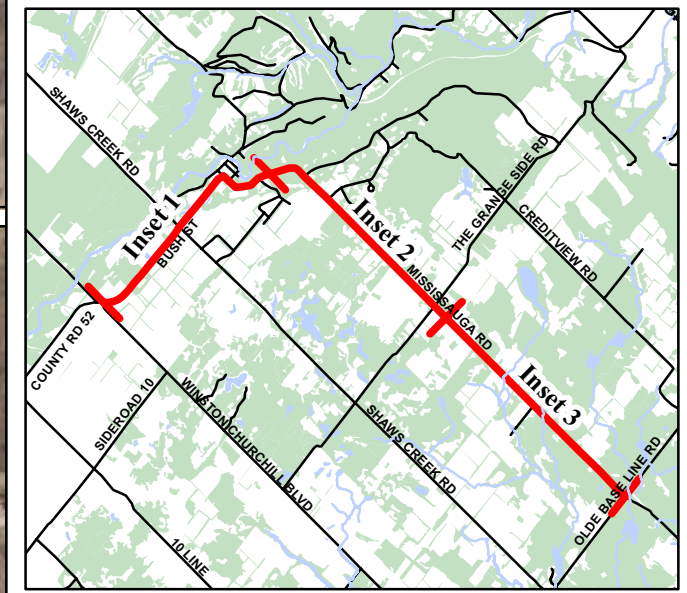
Sizes of the 44 entrance culverts range from 200 mm to 600 mm. Some culvert sizes do not meet the Region's current standards (375 mm); however in some cases the depth of cover over the driveway road is not sufficient to accommodate a 375 mm diameter structure. Also, these entrance culverts may have been consistent with standard practices at the time of construction. In general, the entrance culverts do not provide sufficient capacity as the effective area has been diminished. The capacity rating along with additional information summarized in the Region's inventory sheets provides recommendations to maintain and/or upgrade these culverts.



Bush Street and Mississauga Road
Figure 12: Entrance Culvert - Capacity Rating

Legend

- 10 Entrance Culvert ID #
- Very Good Condition
- Good Condition
- Fair Condition
- Poor Condition
- Below Minimum Tolerable
- No Available Data



3. SUMMARY

The Drainage and Stormwater Management component of the Bush Street and Mississauga Road Class Environmental Assessment consists of two Phases. Phase I: The Drainage Assessment and Hydraulic Analysis documents the existing conditions and has been completed based on a review of background data, field investigations and a capacity assessment. Two separate approaches have been carried out for a) the cross culvert capacity assessment, and b) the road drainage system.

For the cross culverts, hydrologic and hydraulic modelling was completed. A VO2 hydrologic model was set-up and run to determine peak flows for the return period events (i.e., 2 – 100 year). Model peak flows are likely higher than actual peak flows due to the potential Karst topography and influence of ineffective drainage areas. The hydraulic analysis was performed using CulvertMaster to determine the level of service (LOS) provided by each structure. The model results indicate that in general, the majority of the cross culverts fail to provide the required LOS. Furthermore, many of the cross culverts also do not meet the Region's minimum size requirement (i.e., 600 mm diameter). Since the peak flow model estimates are likely higher than actual flow, the actual LOS provided by the cross culverts is likely better than indicated by CulvertMaster. It may be more realistic and appropriate to adopt the Region's 600 mm minimum pipe size rather than meet a return period LOS. Following the pipe size standard would increase the theoretical level of service and balance the as yet undetermined extent of Karst landscape and rolling topography influencing the drainage characteristics.

For the road drainage system, which includes roadside ditches and entrance culverts, a simplified approach was taken to review the existing capacity and to identify inadequacies with regard to handling stormwater drainage. A hydrologic assessment was conducted for ditches using the Rational Method, while the hydraulic review was completed based on the Manning's Equation. For entrance culverts, a capacity rating analysis using MTO criteria was carried out based on the existing physical conditions of the culverts as summarized in the culvert inventory compiled by the Region. The catchment areas for ditches are located on potential Karst topography, as aforementioned in the hydrologic assessment for cross culverts. Conservatively, the Rational Method was applied and the peak flows calculated may be higher than actual flows. In general, the ditches evaluated provided the required LOS. However, drainage issues do exist in the study area due to shoulder deficiencies and due to lack of ditching for the collection of storm runoff. A capacity rating was assigned to each entrance culvert based on the physical condition of these structures. In general, the physical condition of the majority of the entrance culverts was such that the capacity was below tolerable. The capacity rating along with additional information summarized in the Region's inventory sheets provides recommendations to maintain and/or upgrade these culverts.

4. NEXT STEPS

The next steps include completion of the Phase II component, namely the development of a Stormwater Management Plan. First, a review of the Region's recommended road improvements will be undertaken to determine potential impacts to water resources. Alternative methods will be considered to mitigate the potential impacts. Design methods will be identified in consultation with other disciplines where appropriate (e.g., geotechnical, geomorphologic). Finally the alternative methods will be evaluated to recommend preferred stormwater management solutions.

Road improvements that could impact water resources may include additional ditches and changes in road footprint. It is anticipated that the addition of ditches will not significantly alter drainage areas and that similar flow patterns of similar magnitudes would exist under proposed conditions. Changes in the road footprint are likely to be minimal and therefore no significant water quality and quantity impacts are expected. Hydraulic impacts may include increases to upstream flood levels should the existing road profile elevation be raised (e.g., existing base, crushed in place).

Stormwater management measures will be identified to minimize potential water quality and quantity impacts. Along the rural transportation corridor, conveyance controls such as flat bottom grass-lined or enhanced swales have been considered, and the need for pond end-of-pipe controls is limited (i.e., no widening to necessitate peak flow controls). End-of-pipe oil-grit separators may also be considered in isolated areas if curb and gutter and storm sewers are preferred. To address hydraulic impacts, we will assess alternative culvert sizes. Mitigation measures may also be recommended as an opportunity to address existing capacity deficiencies not related to the proposed works.

5. REFERENCES


- Brunton, F.R., and Dodge, J.E.P. *Karst of Southern Ontario and Manitoulin Island*. Ministry of Northern Development and Mines (MNDM), 2007.
- Credit Valley Conservation (CVC), May 1996. *Stormwater Management Guidelines*.
- Credit Valley Conservation (CVC). *CVC Standard Parameters – Appendix B*.
- Ontario Ministry of Natural Resources (MNR), 2001. *Understanding Natural Hazards.Regional*.
- Ontario Ministry of Transportation (MTO), March 2010. TOR for the Inventory and Assessment of Non-Structural Culverts Located within the Huntsville Area. Appendix C, *Attachment B – Culvert Assessment Guide*.
- Regional Municipality of Peel, February 2010. *Public Works Design, Specifications and Procedures Manual – Regional Roads and Traffic*.
- Regional Municipality of Peel, July 2009. *Public Works Design, Specifications and Procedures Manual – Storm Sewer Design Criteria*.
- Soil Survey of Peel County, Ontario 1953. *Report No. 18 of the Ontario Soil Survey*. Canada Department of Agriculture, Ottawa. Ontario Agricultural College, Guelph.
- Totten Sims Hubicki Associates, 1998. *Regional Road Improvements In The Belfountain Area. Town of Caledon*.

Appendix A
Inventory Sheets


Inventory Sheets for Cross Culverts

Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2620-2626.JPG</u> Map Ref: <u>STA 1+965</u>	ID No: <u>Culvert # 10</u> Location: <u>Bush St, west of Main</u> Type: <u>culvert</u> Material: <u>PVCINC</u> Diameter (m): <u>0.45 m</u> Height (m): _____ Width (m): _____ Length (m): <u>13.3</u> U/S Invert Elev (m): <u>382.706</u> D/S Invert Elev (m): <u>382.483</u>	Slope (m/m): <u>0.01677</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): <u>0</u> Obvert to Road (m): _____ Construction Date: _____ Other Comments: <u>pond u/s</u>	Present? (Y/N): <u>Y</u> Ave. Depth (mm): <u>100 - 300</u> Velocity (m/s): _____ Flow (cms): _____ Silt (mm): _____ Tailwater/Backwater Condition: _____ _____ _____

Site Description / Comments	Site Photograph
Photo 2620 D/S side Photo 2621 D/S side Photo 2622 D/S side Photo 2623 U/S side Photo 2624 U/S side Photo 2625 U/S side Photo 2626 U/S side	Photo 2620 

Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2634-2639.JPG</u> Map Ref: <u>STA 42+955</u>	ID No: <u>Culvert # 14</u> Location: <u>Bush St, & Old Main</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.60 m</u> Height (m): _____ Width (m): _____ Length (m): <u>17.2</u> U/S Invert Elev (m): <u>380.433</u> D/S Invert Elev (m): <u>379.933</u>	Slope (m/m): <u>0.029</u> Barrel Condition: <u>good</u> Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____ Control Point U/S face of 21/22 1.87 m (12cm from 1.87m to obvert) survey at U/S face - vegetated grass /trees over bank, rocky bottom	Present? (Y/N): <u>Y</u> Ave. Depth (mm): <u>100 mm</u> Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>> 50% full D/S</u> Tailwater/Backwater Condition: _____
Site Description / Comments	Site Photograph		
Photo 2634 looking U/S Photo 2635 U/S face Photo 2636 looking U/S - showing split channel just U/S of culvert Photo 2637 looking D/S Photo 2638 looking D/S Photo 2639 culvert face of side channel side channel: v-channel small trees over bank; veg/dirt bottom Bankfull width measurements - along church parking lot 1.1m, 1.4m, 1.6m, 2.1m => ave 1.55 m (ave depth 10cm) bed: gravel substrate channel d/s slope = 5% (estimate)	Photo 2635		

Inventory of Hydraulic Structures

Project Information	Structure Information	Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2640.jpg, 2641.jpg</u> Map Ref: <u>STA 42+540</u>	ID No: <u>Culvert # 16</u> Location: <u>Bush St</u> Type: <u>circular</u> Material: <u>CSP</u> Diameter (m): <u>0.3</u> Height (m): _____ Width (m): _____ Length (m): <u>16.3</u> U/S Invert Elev (m): <u>386.152</u> D/S Invert Elev (m): <u>385.262</u>	Slope (m/m): <u>0.056</u> Barrel Condition: <u>crushed</u> Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): <u>0</u> Obvert to Road (m): _____ Construction Date: _____ Other Comments: <u>Survey for u/s invert</u> No channel d/s drains over escarpment
		Present? (Y/N): <u>N</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): _____ Tailwater/Backwater Condition: _____


Site Description / Comments	Site Photograph
Survey points inverts u/s 99.21, d/s 98.32 Photo 2640.jpg d/s face Photo 2641.jpg u/s face Confirm culvert length	Photo 2640 

Inventory of Hydraulic Structures


Project Information	Structure Information		Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2644-2645.JPG</u> Map Ref: <u>STA 42+400</u>	ID No: <u>Culvert # 17</u> Location: <u>Old Main St, west of Mississauga Rd</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.30 m</u> Height (m): _____ Width (m): _____ Length (m): <u>10.3</u> U/S Invert Elev (m): <u>384.684</u> D/S Invert Elev (m): <u>384.325</u>	Slope (m/m): <u>0.03484</u> Barrel Condition: <u>crushed</u> Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: <u>no channel</u>	Present? (Y/N): <u>N</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>full</u> Tailwater/Backwater Condition: _____ _____ _____

Site Description / Comments	Site Photograph
Photo 2645 D/S side Photo 2644 U/S side	Photo 2644 


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2663-2664.JPG</u> Map Ref: <u>STA 41+000</u>	ID No: <u>Culvert # 24</u> Location: <u>Mississauga Rd,</u> <u>south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.40 m</u> Height (m): _____ Width (m): _____ Length (m): <u>15.252</u> U/S Invert Elev (m): <u>428.304</u> D/S Invert Elev (m): <u>427.816</u>	Slope (m/m): <u>0.032</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____ no definable channel no definable ditch	Present? (Y/N): _____ Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>full on U/S end</u> Tailwater/Backwater Condition: <u>ponding</u>
Site Description / Comments	Site Photograph		
Photo 2664 Photo 2663	Photo 2664 		


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>4-May</u> Field Crew: <u>BH/IP</u> Photo No: <u>6413-6416.JPG</u> Map Ref: <u>STA 39+650</u>	ID No: <u>Culvert # 37</u> Location: <u>Mississauga Rd,</u> <u>south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.60 m</u> Height (m): _____ Width (m): _____ Length (m): <u>12.5</u> U/S Invert Elev (m): <u>418.796</u> D/S Invert Elev (m): <u>418.414</u>	Slope (m/m): <u>0.03056</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____	Present? (Y/N): <u>N (ponding both ends)</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): _____ Tailwater/Backwater Condition: _____ _____ _____
Site Description / Comments	Site Photograph		
Photo 6413 U/S side Photo 6413b U/S side Photo 6414 D/S side Photo 6415 Ditch connecting to D/S side (face south) Photo 6416 Ditch connecting to U/S side (face north)	Photo 6413b		


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2671-2675.JPG</u> Map Ref: <u>STA 38+875</u>	ID No: <u>Culvert # 43</u> Location: <u>Mississauga Rd,</u> <u>south of Old Main St.</u> Type: <u>culvert - ellipse</u> Material: <u>CSP</u> Diameter (m): <u>0.90 m</u> Height (m): <u>0.55 m</u> Width (m): <u>0.9 m</u> Length (m): <u>12.566</u> U/S Invert Elev (m): <u>400.13</u> D/S Invert Elev (m): <u>399.96</u>	Slope (m/m): <u>0.01353</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____ ponding in ditch; wide shallow	Present? (Y/N): <u>N (ponding D/S end)</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): _____ Tailwater/Backwater Condition: _____
Site Description / Comments	Site Photograph		
Photo 2671 D/S side Photo 2672 Ditch upslope Photo 2673 Ditch downslope (to MNOP) Flooding at 16065 * recommend lowering culvert; poor drainage Photo 2674 U/S face Photo 2675 U/S ditch; no ditch D/S Ditch Info: D/S Ditch - wide shallow trap TW = 1.5 m 0.5 m Rd side 0.3 m other side 1:1 s/s U/S Ditch - ponding along ditch TW = 2.5 m 0.6 m Rd side no bank fieldside	Photo 2671		


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2676-2681..JPG</u> Map Ref: <u>STA 38+800</u>	ID No: <u>Culvert # 44n & 44s</u> Location: <u>Mississauga Rd,</u> <u>south of Old Main St.</u> Type: <u>2 Cell ellipse culvert</u> Material: <u>CSP</u> Diameter (m): <u>1.20 m</u> Height (m): _____ Width (m): <u>1.0 m</u> Length (m): <u>13.815</u> U/S Invert Elev (m): <u>399.461 (N), 399.442 (S)</u> D/S Invert Elev (m): <u>399.27 (N), 399.308 (S)</u>	Slope (N) (m/m): <u>0.01383</u> Slope (S) (m/m): <u>0.00970</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____ *pond U/S embankment	Present? (Y/N): <u>Y</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>15cm gravel</u> Tailwater/Backwater Condition: <u>*TW effected by pond</u>
Site Description / Comments	Site Photograph		
Photo 2676 L U/S Photo 2677 U/S face Photo 2678 L south Photo 2679 L north Photo 2680 L D/S Photo 2681 D/S face D/S channel veg overbank 0.3 m D 2.0 m wide note: muck/gravel substrate backwater from pond no flow apparent D/S side: top gravel to obvert 0.6 m	Photo 2677		


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2682-2684.JPG</u> Map Ref: <u>STA 38+425</u>	ID No: <u>Culvert # 47</u> Location: <u>Mississauga Rd, south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.4</u> Height (m): _____ Width (m): _____ Length (m): <u>12.238</u> U/S Invert Elev (m): <u>398.172</u> D/S Invert Elev (m): <u>397.961</u>	Slope (m/m): <u>0.01724</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____	Present? (Y/N): <u>N (ponding D/S)</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>2 half full</u> Tailwater/Backwater Condition: _____ _____ _____
Site Description / Comments	Site Photograph		
Photo 2682 U/S face Photo 2683 D/S face Photo 2684 looking D/S no channel no ditch	Photo 2683 		


Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Bush St & Mississauga Project Name: <u>Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2685-2687.JPG</u> Map Ref: <u>STA 38+175</u>	ID No: <u>Culvert # 48</u> Location: <u>Mississauga Rd,</u> <u>south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.40 m</u> Height (m): _____ Width (m): _____ Length (m): <u>12.427</u> U/S Invert Elev (m): <u>394.083 S</u> D/S Invert Elev (m): <u>393.836 T</u>	Slope (m/m): <u>0.020</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____	Present? (Y/N): <u>Y</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>half full</u> Tailwater/Backwater Condition: _____ _____ _____
Site Description / Comments	Site Photograph		
Photo 2685 L D/S Photo 2686 D/S face Photo 2687 L U/S ponding D/S -> wetland D/S GW at surface along ditch ditch with water	Photo 2685		

Inventory of Hydraulic Structures

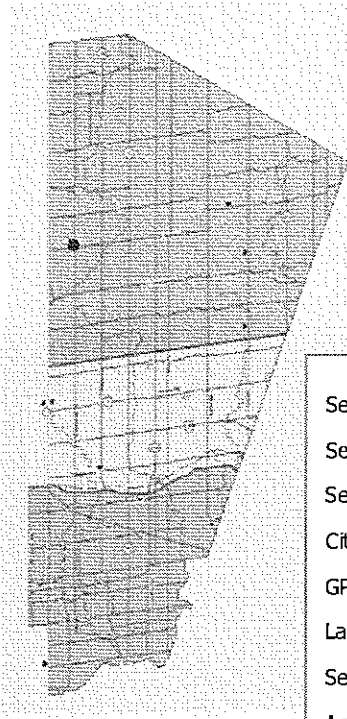
Project Information	Structure Information		Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2690.JPG</u> Map Ref: <u>STA 37+725</u>	ID No: <u>Culvert # 55</u> Location: <u>Mississauga Rd, south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.30 m</u> Height (m): _____ Width (m): _____ Length (m): <u>12.368</u> U/S Invert Elev (m): <u>388.755</u> D/S Invert Elev (m): <u>388.431</u>	Slope (m/m): <u>0.02620</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____	Present? (Y/N): <u>N (ponding at D/S side & along ditch)</u> Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): _____ Tailwater/Backwater Condition: _____
Site Description / Comments	Site Photograph		
Photo 2690 Ditch - TW 2.5 m 0.7 m D 1:1 s/s (same for both sides of road)	Photo 2690 		

Inventory of Hydraulic Structures

Project Information	Structure Information		Flow Conditions
Project Name: <u>Bush St & Mississauga Rd EA</u> Project No: <u>10-3121</u> Date: <u>16-Apr-10</u> Field Crew: <u>GT/JH/BH</u> Photo No: <u>2691-2693.JPG</u> Map Ref: <u>STA 37+625</u>	ID No: <u>Culvert # 56</u> Location: <u>Mississauga Rd, south of Old Main St.</u> Type: <u>culvert</u> Material: <u>CSP</u> Diameter (m): <u>0.30 m</u> Height (m): _____ Width (m): _____ Length (m): <u>11.496</u> U/S Invert Elev (m): <u>387.255</u> D/S Invert Elev (m): <u>387.208</u>	Slope (m/m): <u>0.004088</u> Barrel Condition: _____ Inlet Type: _____ Inlet Condition: _____ Skew Angle (deg): _____ Obvert to Road (m): _____ Construction Date: _____ Other Comments: _____	Present? (Y/N): _____ Ave. Depth (mm): _____ Velocity (m/s): _____ Flow (cms): _____ Silt (mm): <u>10 cm</u> Tailwater/Backwater Condition: _____ _____ _____
Site Description / Comments	Site Photograph		
Photo 2691 D/S face Photo 2692 look south Photo 2693 look north Photo 2694 U/S face Photo 2695 south Photo 2696 north ditch is dry	Photo 2694		

Region of Peel – Culvert Inventory Sheets

CULVERT NO. 261



Section - Road: 13690 - MISSISSAUGA ROAD
 Section Start: OLDE BASE LINE ROAD (REG. RD.# 12)
 Section End: 0.7km N.OF OLDE BASE LINE ROAD
 City/Town: CALEDON
 GPS Coord: 583682 E 4846007 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 15457
 Side of Road: East

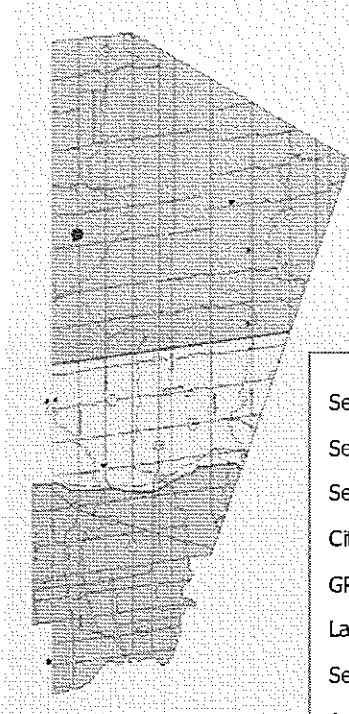
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,525
2		
3		
4	Grade and Sod w/ Ditching	\$950
5		
6		
Total Incl. Mobilization and Contingency :		\$3,219

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 5 m2
 Total Ditching Required : 6 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 5.95 m
 Centre-Line Offset North: 6.25 m
 Exposed Length South: 0 m
 Exposed Length North: 0.3 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 262



Section - Road:	13690	MISSISSAUGA ROAD
Section Start:	OLDE BASE LINE ROAD (REG. RD.# 12)	
Section End:	0.7km N.OF OLDE BASE LINE ROAD	
City/Town:	CALEDON	
GPS Coord:	583025 E	4846657 N
Last Inspected:	5/27/2005	
Service Type:	Entrance	
Address/Cross Road:	15797	
Side of Road:	East	

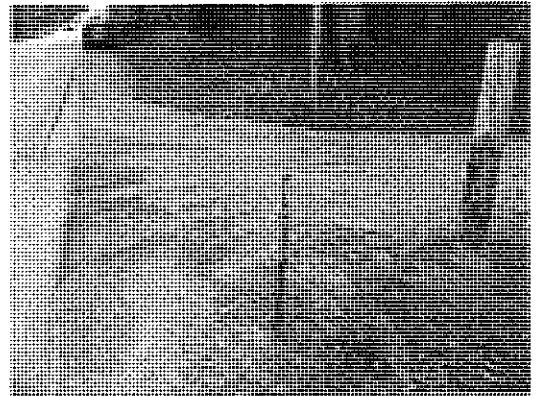
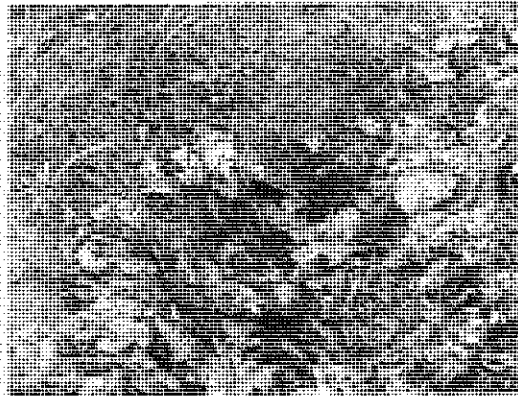
Effective Cross-Section:	50	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m2
Total Ditching Required :	15	m
Ditching on Private Prop:	0	m
Volume of HW South		m3
Volume of HW North		m3
Headwall Repair South		m3
Headwall Repair North		m3
Pre-Fab HW SA South		m2
Pre-Fab HW SA North		m2
Gabions Req. at South		m3
Gabions Req. at North		m3
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	9.2	m
Centre-Line Offset North	9.2	m
Exposed Length South	0.3	m
Exposed Length North	0.3	m
Maximum Overburden:	0.4	m
Nominal Diameter:	0.4	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/>	C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Flush/Clean & Re-Shape Ends	\$2,500
2		
3		
4	Ditching	\$2,250
5		
6		
Total Incl. Mobilization and Contingency :		\$6,063

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input checked="" type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 263



Section - Road:	13690 - MISSISSAUGA ROAD
Section Start:	OLDE BASE LINE ROAD (REG. RD.# 12)
Section End:	0.7km N.OF OLDE BASE LINE ROAD
City/Town:	CALEDON
GPS Coord:	583472 E 4846209 N
Last Inspected:	5/27/2005
Service Type:	Entrance
Address/Cross Road:	15606
Side of Road:	West

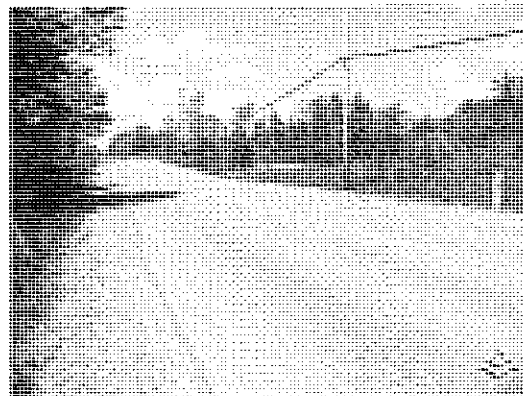
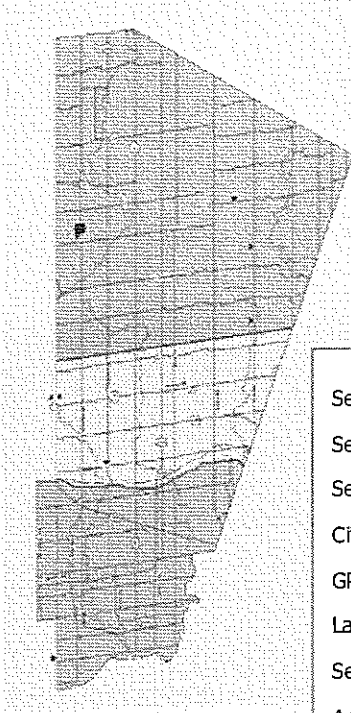
Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/> B <input type="checkbox"/> C <input checked="" type="checkbox"/>		
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Full/Partial Replacement	\$1,841
2		
3		
4	Ditching	\$4,500
5		
6		
Total Incl. Mobilization and Contingency :		\$8,051

Immediately	<input type="checkbox"/>
This Year	<input checked="" type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

Effective Cross-Section:	0 %
% Req. Replacement:	100 %
Cross Section:	
Area Req. Erosion Cntrl:	0 m ²
Total Ditching Required :	30 m
Ditching on Private Prop:	0 m
Volume of HW South	m ³
Volume of HW North	m ³
Headwall Repair South	m ³
Headwall Repair North	m ³
Pre-Fab HW SA South	m ²
Pre-Fab HW SA North	m ²
Gabions Req. at South	m ³
Gabions Req. at North	m ³
Total Barrier Length:	m
Barriers Req. Repair:	m
Barriers Replace/Install:	0 m
Number of Marker Posts:	
Markers Req. Straight:	
Markers Replace/Install:	0
Centre-Line Offset South	4.1 m
Centre-Line Offset North	4.1 m
Exposed Length South	0 m
Exposed Length North	0 m
Maximum Overburden:	0.4 m
Nominal Diameter:	0.4 m
Maximum Span:	m
Interior Height:	m

CULVERT NO. 264



Section - Road: 13690 - MISSISSAUGA ROAD
 Section Start: OLDE BASE LINE ROAD (REG. RD.# 12)
 Section End: 0.7km N. OF OLDE BASE LINE ROAD
 City/Town: CALEDON
 GPS Coord: 582902 E 4846784 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

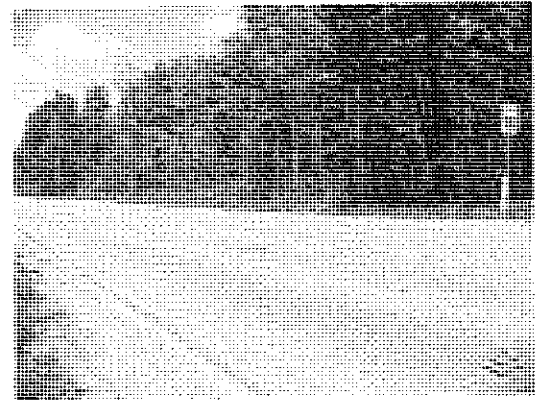
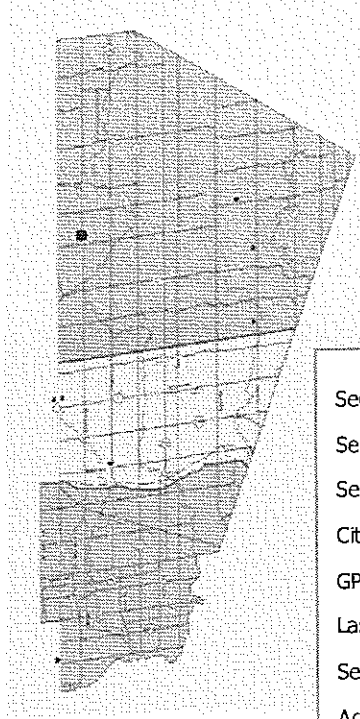
Effective Cross-Section: 76 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West: 6.1 m
 Centre-Line Offset East: 6.1 m
 Exposed Length West: 0 m
 Exposed Length East: 0 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,525
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$2,031

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 265



Section - Road: 13690 - MISSISSAUGA ROAD
 Section Start: OLDE BASE LINE ROAD (REG. RD.# 12)
 Section End: 0.7km N.OF OLDE BASE LINE ROAD
 City/Town: CALEDON
 GPS Coord: 583229 E 4846459 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

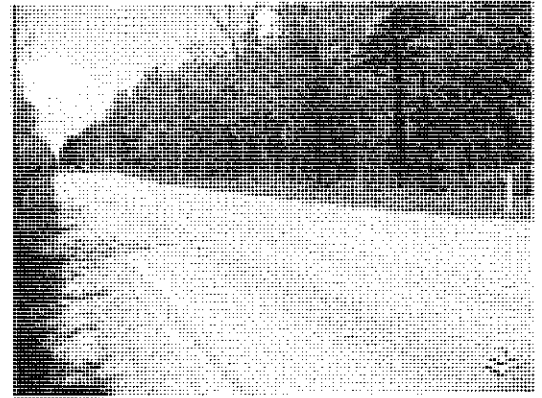
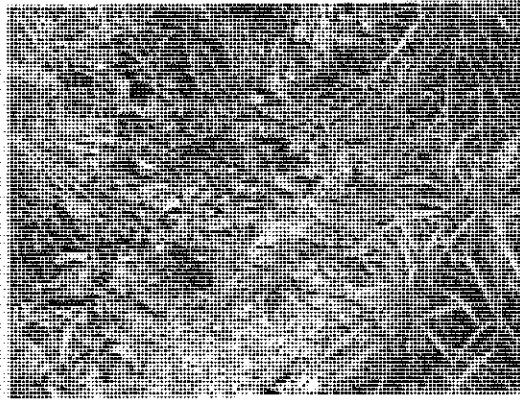
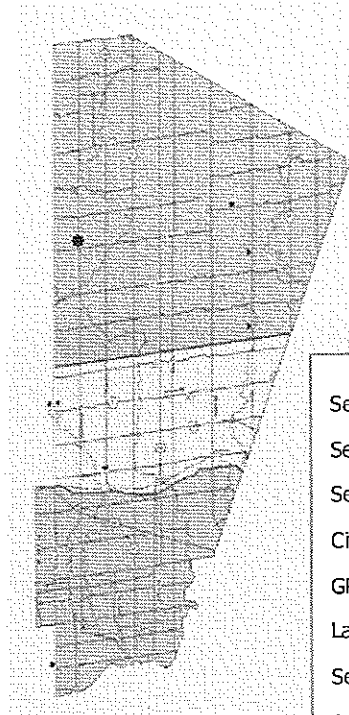
Effective Cross-Section: 60 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 4 m
 Ditching on Private Prop: 0 m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West: 5.85 m
 Centre-Line Offset East: 5.65 m
 Exposed Length West: 0.2 m
 Exposed Length East: 0 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.34 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,438
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,673

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 266



Section - Road: 13690 - MISSISSAUGA ROAD
 Section Start: OLDE BASE LINE ROAD (REG. RD.# 12)
 Section End: 0.7km N.OF OLDE BASE LINE ROAD
 City/Town: CALEDON
 GPS Coord: 583303 E 4846389 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

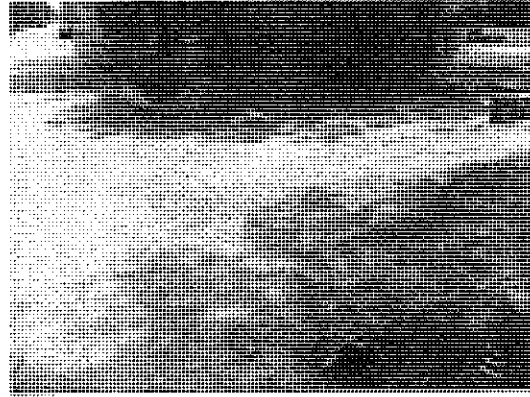
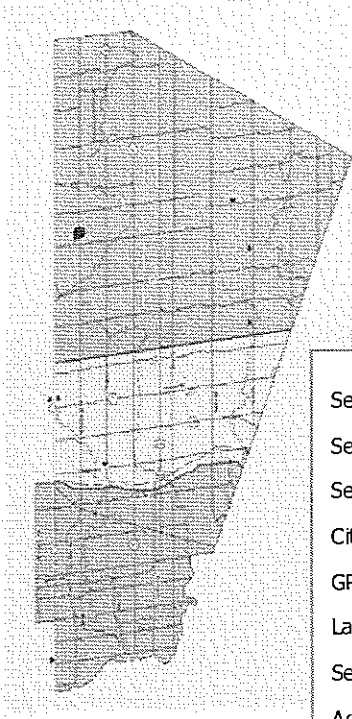
Effective Cross-Section: 5 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 1 m²
 Total Ditching Required: 2 m
 Ditching on Private Prop: 0 m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West: 5.55 m
 Centre-Line Offset East: 5.55 m
 Exposed Length West: 0 m
 Exposed Length East: 0 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,388
2		
3		
4	Ditching	\$300
5		
6		
Total Incl. Mobilization and Contingency :		\$2,235

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 267



Section - Road: 13690 - MISSISSAUGA ROAD
 Section Start: OLDE BASE LINE ROAD (REG. RD.# 12)
 Section End: 0.7km N. OF OLDE BASE LINE ROAD
 City/Town: CALEDON
 GPS Coord: 583036 E 4846690 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 15790
 Side of Road: East

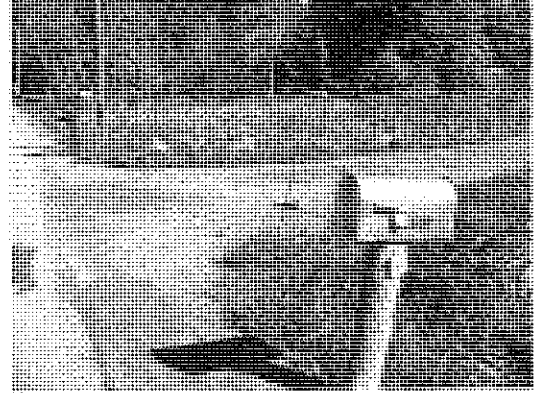
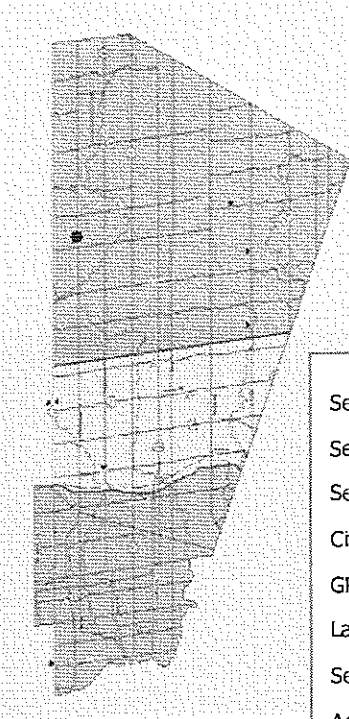
Effective Cross-Section: 90 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 4 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 3.2 m
 Centre-Line Offset North: 3.2 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.1 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$800
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$1,875

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 268



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 583089 E 4846608 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 15775
 Side of Road: East

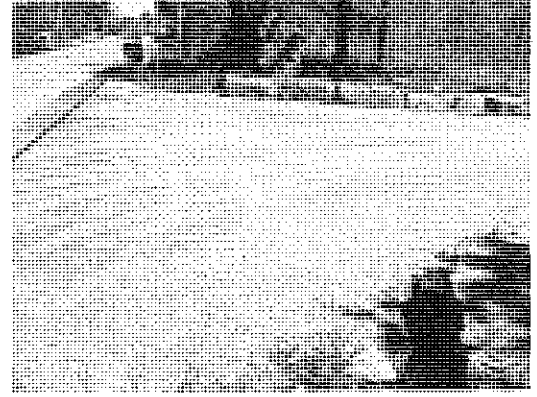
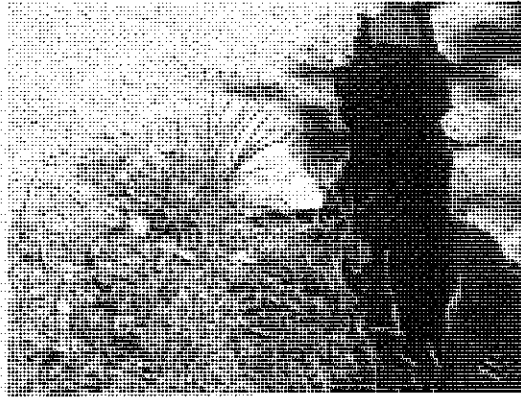
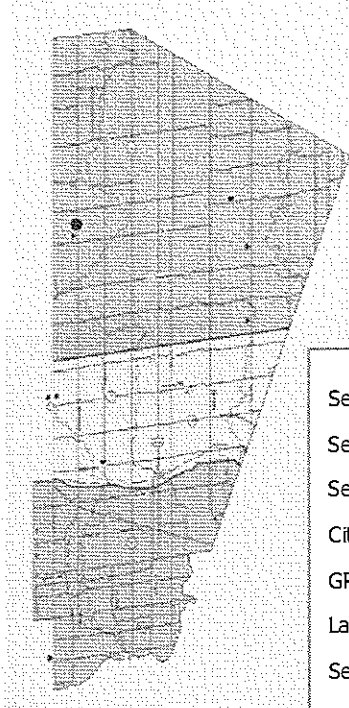
Effective Cross-Section: 5 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 9 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 3.65 m
 Centre-Line Offset North: 3.55 m
 Exposed Length South: 0.1 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$900
2		
3		
4	Ditching	\$1,350
5		
6		
Total Incl. Mobilization and Contingency :		\$2,938

Immediately
 This Year
 1 -2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 269



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S. LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582652 E 4847056 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 15977
 Side of Road: East

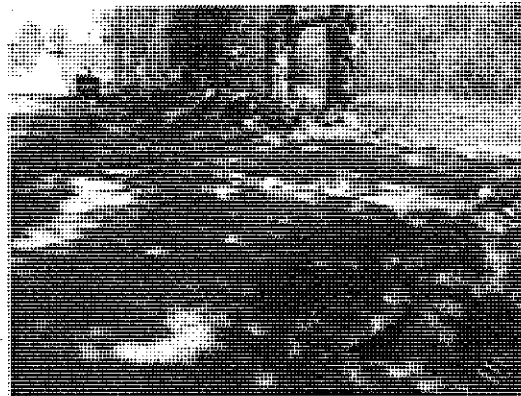
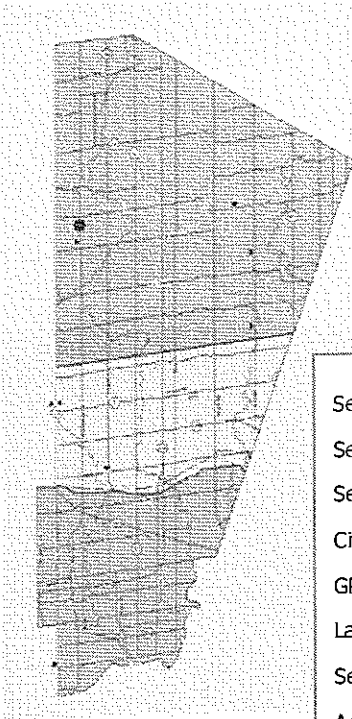
Effective Cross-Section: 5 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 20 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 5.95 m
 Centre-Line Offset North: 6.05 m
 Exposed Length South: 0.1 m
 Exposed Length North: 0.2 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span:
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,700
2		
3		
4	Ditching	\$3,000
5		
6		
Total Incl. Mobilization and Contingency :		\$6,000

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 270



Section - Road:	13760	MISSISSAUGA ROAD
Section Start:	0.7km N. OF OLDE BASE LINE ROAD	
Section End:	S. LIMITS, BELFOUNTAIN	
City/Town:	CALEDON	
GPS Coord:	582301 E	4847403 N
Last Inspected:	5/27/2005	
Service Type:	Entrance	
Address/Cross Road:	16117	
Side of Road:	East	

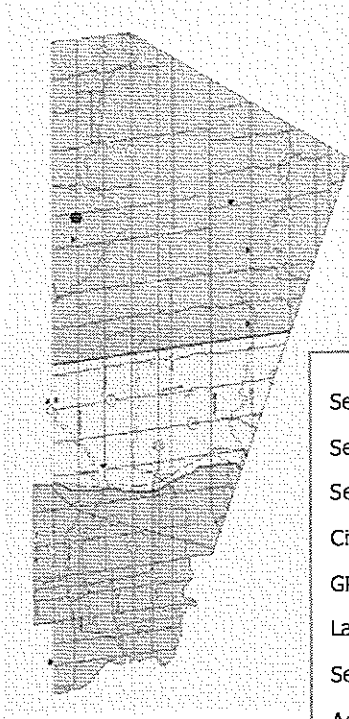
Effective Cross-Section:	60	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	4	m
Ditching on Private Prop:	0	m
Volume of HW South		m ³
Volume of HW North		m ³
Headwall Repair South		m ³
Headwall Repair North		m ³
Pre-Fab HW SA South		m ²
Pre-Fab HW SA North		m ²
Gabions Req. at South		m ³
Gabions Req. at North		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	4.7	m
Centre-Line Offset North	4.9	m
Exposed Length South	0	m
Exposed Length North	0.2	m
Maximum Overburden:	0.5	m
Nominal Diameter:	0.46	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/> C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South <input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North <input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South <input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input type="checkbox"/>

1	Flush/Clean	\$1,200
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,375

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input checked="" type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 271



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581977 E 4847725 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: East

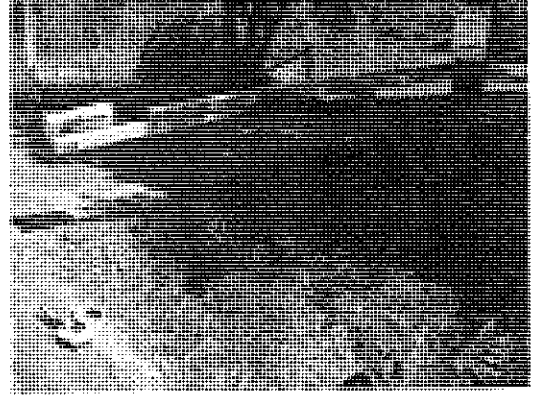
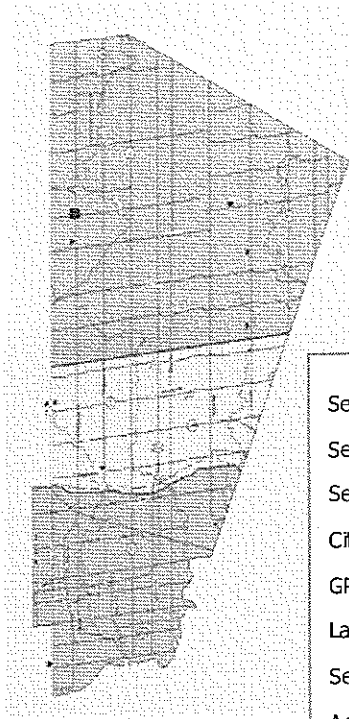
Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 20 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 2.75 m
 Centre-Line Offset North: 2.75 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.1 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$688
2		
3		
4	Ditching	\$3,000
5		
6		
Total Incl. Mobilization and Contingency :		\$4,735

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 272



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S. LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581588 E 4848111 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16437
 Side of Road: East

Effective Cross-Section: 95 %
 % Req. Replacement: 0 %
 Cross Section:

Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 4.8 m
 Centre-Line Offset North: 4.8 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 1 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

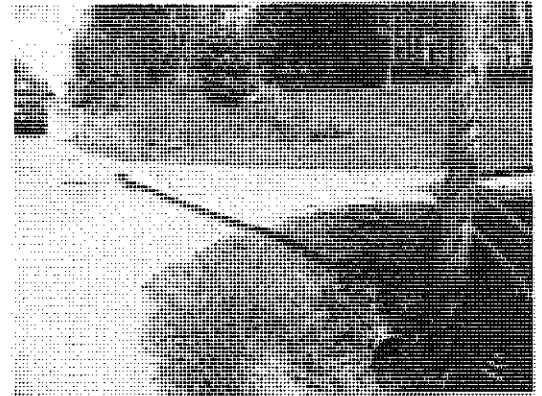
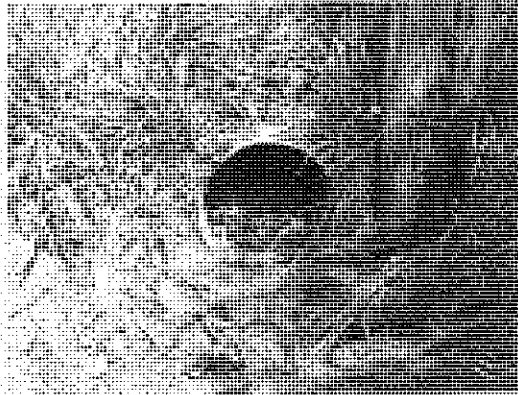
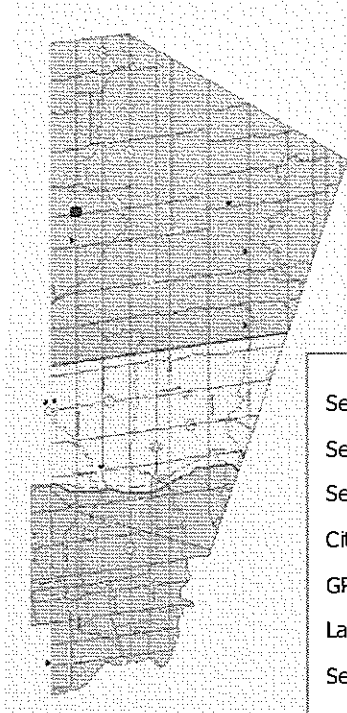
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C

No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,200
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,625

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 273



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581528 E 4848178 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16461
 Side of Road: East

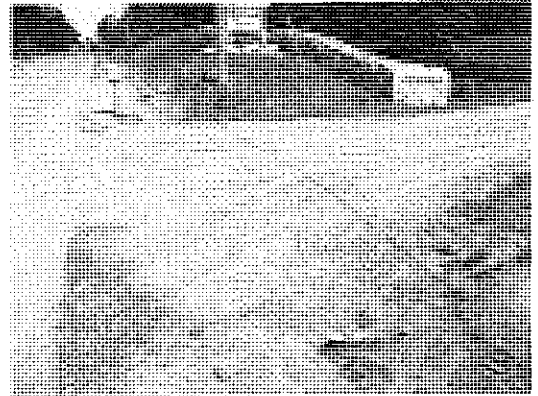
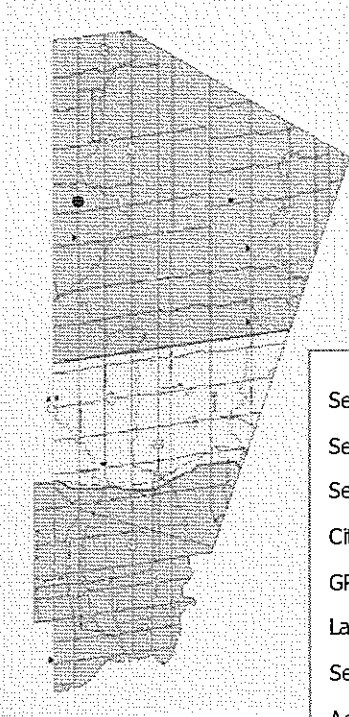
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,162
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,578

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 60 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South m3
 Volume of HW North m3
 Headwall Repair South m3
 Headwall Repair North m3
 Pre-Fab HW SA South m2
 Pre-Fab HW SA North m2
 Gabions Req. at South m3
 Gabions Req. at North m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South 4.6 m
 Centre-Line Offset North 4.7 m
 Exposed Length South 0.1 m
 Exposed Length North 0.2 m
 Maximum Overburden: 0.3 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 274



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581056 E 4848641 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16671
 Side of Road: East

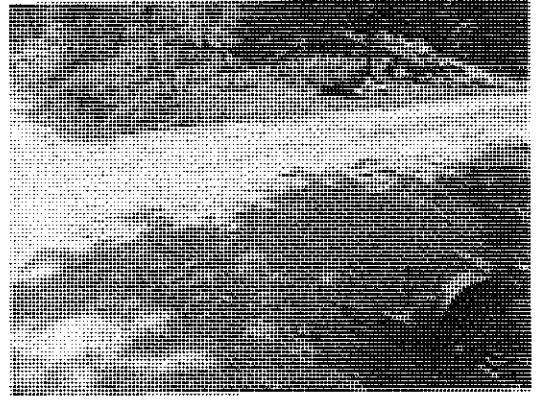
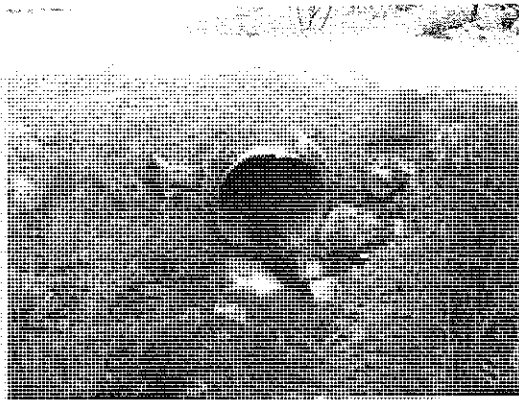
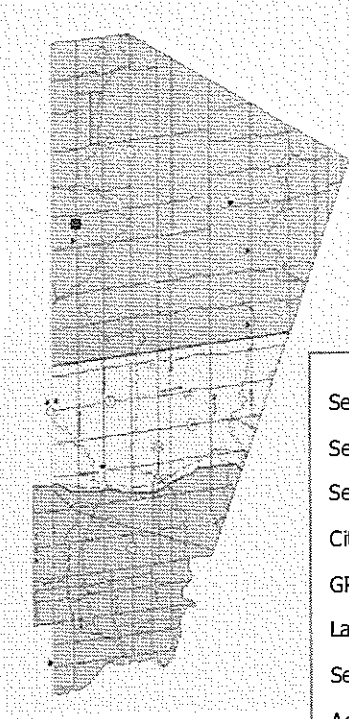
Effective Cross-Section: 16 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 4.8 m
 Centre-Line Offset North: 4.8 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.3 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,200
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,625

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 275



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582312 E 4847365 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16110
 Side of Road: West

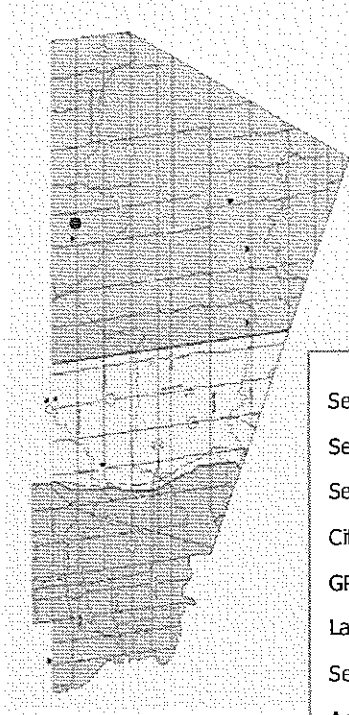
Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 2 m²
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 3.2 m
 Centre-Line Offset North: 3.1 m
 Exposed Length South: 0.2 m
 Exposed Length North: 0.1 m
 Maximum Overburden: 0.1 m
 Nominal Diameter: 0.6 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4	Grade and Sod	\$20
5		
6		
Total Incl. Mobilization and Contingency :		\$150

Immediately
 This Year
 1 -2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 276



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582355 E 4847329 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16106
 Side of Road: West

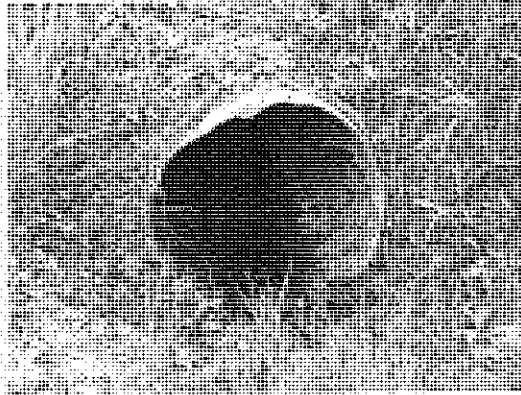
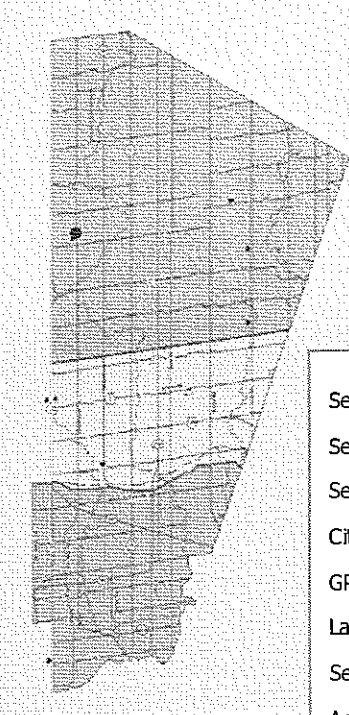
Effective Cross-Section: 40 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 4 m²
 Total Ditching Required: 6 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 3.15 m
 Centre-Line Offset North: 3.25 m
 Exposed Length South: 0 m
 Exposed Length North: 0.1 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,000
2		
3		
4	Grade and Sod w / Ditching	\$940
5		
6		
Total Incl. Mobilization and Contingency :		\$2,550

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 277



Section - Road:	13760 - MISSISSAUGA ROAD
Section Start:	0.7km N.OF OLDE BASE LINE ROAD
Section End:	S.LIMITS, BELFOUNTAIN
City/Town:	CALEDON
GPS Coord:	583066 E 4846623 N
Last Inspected:	5/27/2005
Service Type:	Entrance
Address/Cross Road:	15790-S
Side of Road:	West

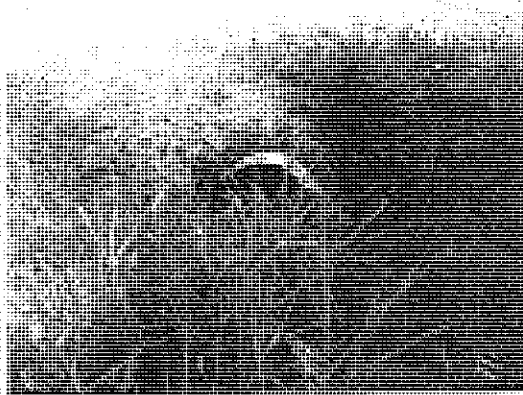
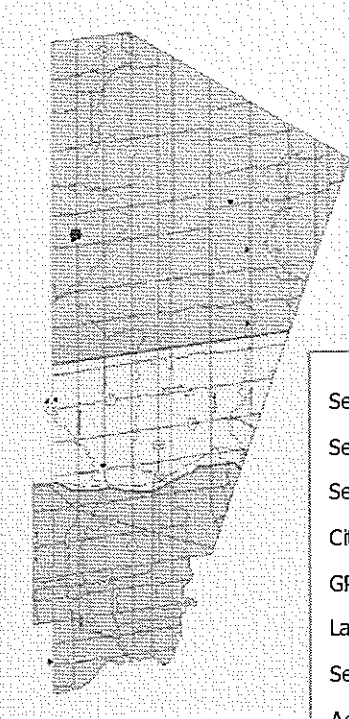
Effective Cross-Section:	90 %
% Req. Replacement:	0 %
Cross Section:	
Area Req. Erosion Cntrl:	0 m ²
Total Ditching Required :	2 m
Ditching on Private Prop:	0 m
Volume of HW South	m ³
Volume of HW North	m ³
Headwall Repair South	m ³
Headwall Repair North	m ³
Pre-Fab HW SA South	m ²
Pre-Fab HW SA North	m ²
Gabions Req. at South	m ³
Gabions Req. at North	m ³
Total Barrier Length:	m
Barriers Req. Repair:	m
Barriers Replace/Install:	0 m
Number of Marker Posts:	
Markers Req. Straight:	
Markers Replace/Install:	0
Centre-Line Offset South	3.15 m
Centre-Line Offset North	3.15 m
Exposed Length South	0.1 m
Exposed Length North	0.1 m
Maximum Overburden:	0.3 m
Nominal Diameter:	0.46 m
Maximum Span:	m
Interior Height:	m

Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/> B <input type="checkbox"/> C <input checked="" type="checkbox"/>		
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Do Nothing	\$0
2		
3		
4	Ditching	\$300
5		
6		
Total Incl. Mobilization and Contingency :		\$500

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input checked="" type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 278



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 583078 E 4846605 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 15774
 Side of Road: West

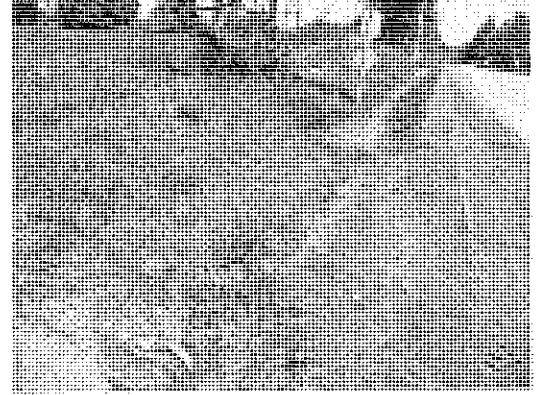
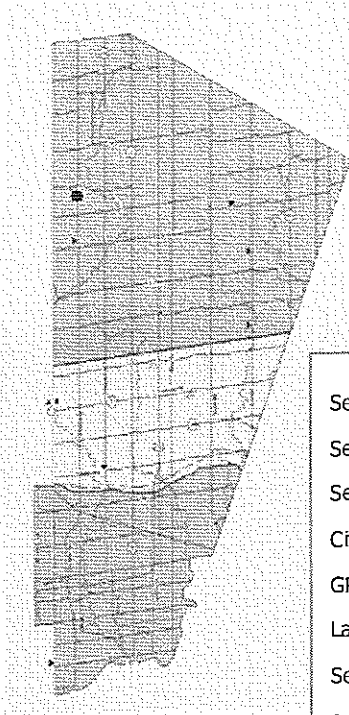
Effective Cross-Section: 75 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 3.3 m
 Centre-Line Offset North: 2.9 m
 Exposed Length South: 0.4 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.1 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$775
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,094

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 279



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S. LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 580515 E 4849173 N
 Last Inspected: 5/30/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: West

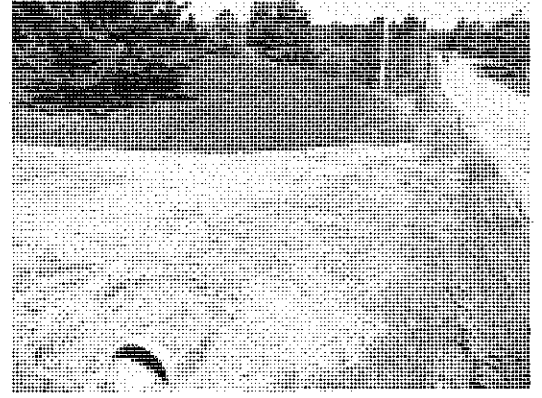
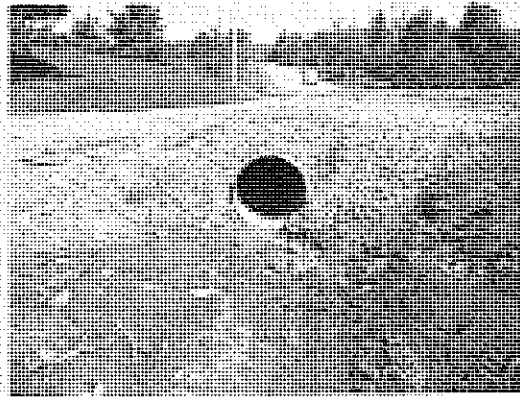
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$975
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,344

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South m3
 Volume of HW North m3
 Headwall Repair South m3
 Headwall Repair North m3
 Pre-Fab HW SA South m2
 Pre-Fab HW SA North m2
 Gabions Req. at South m3
 Gabions Req. at North m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South 3.1 m
 Centre-Line Offset North 3.1 m
 Exposed Length South 0 m
 Exposed Length North 0 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 280



Section - Road: 13760 MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 580599 E 4849086 N
 Last Inspected: 5/30/2005
 Service Type: Entrance
 Address/Cross Road: N/A
 Side of Road: West

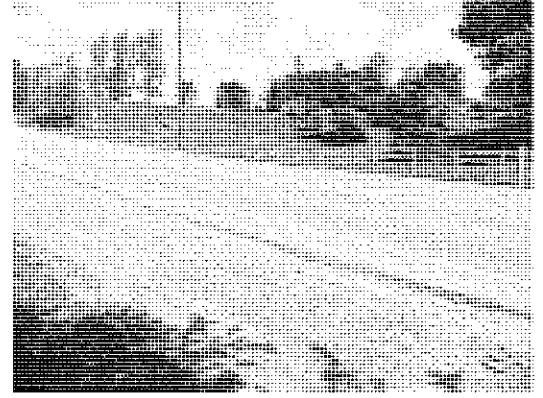
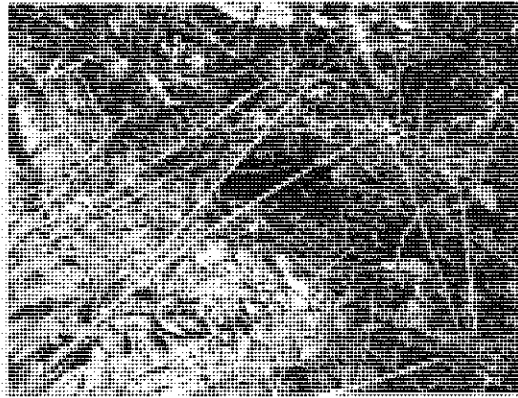
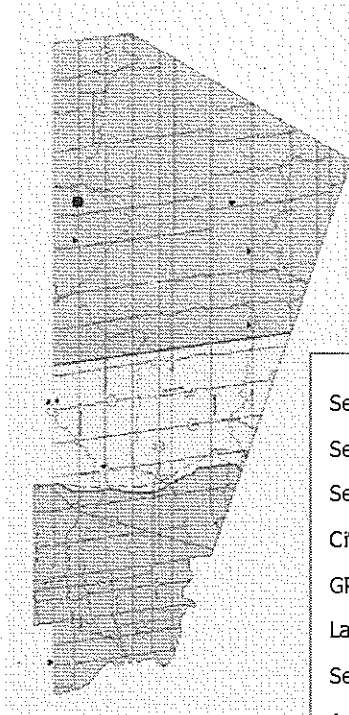
Effective Cross-Section: 95 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 5.15 m
 Centre-Line Offset North: 5.05 m
 Exposed Length South: 0.2 m
 Exposed Length North: 0.1 m
 Maximum Overburden: 0.3 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts


1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 281



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 580909 E 4848766 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

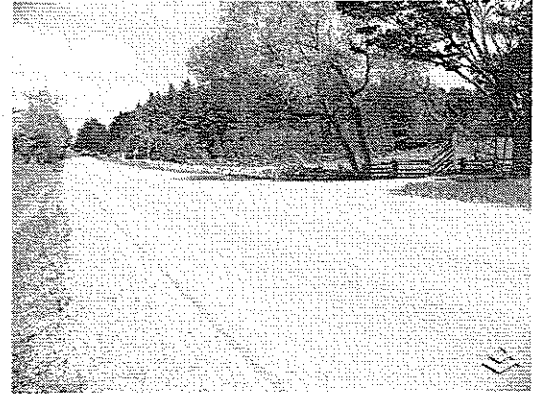
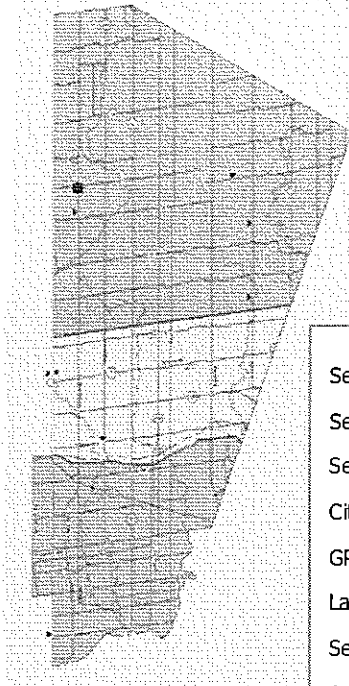
Effective Cross-Section: 10 %
 % Req. Replacement: 0 %
 Cross Section: 
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 6 m
 Ditching on Private Prop: 0 m
 Volume of HW West: m3
 Volume of HW East: m3
 Headwall Repair West: m3
 Headwall Repair East: m3
 Pre-Fab HW SA West: m2
 Pre-Fab HW SA East: m2
 Gabions Req. at West: m3
 Gabions Req. at East: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West: 7.55 m
 Centre-Line Offset East: 7.55 m
 Exposed Length West: 0 m
 Exposed Length East: 0 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,888
2		
3		
4	Ditching	\$900
5		
6		
Total Incl. Mobilization and Contingency :		\$3,610

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 282



Section - Road:	13760	MISSISSAUGA ROAD
Section Start:	0.7km N.OF OLDE BASE LINE ROAD	
Section End:	S.LIMITS, BELFOUNTAIN	
City/Town:	CALEDON	
GPS Coord:	581861 E	4847819 N
Last Inspected:	5/31/2005	
Service Type:	Cross	
Address/Cross Road:	N/A	
Side of Road:	N/A	

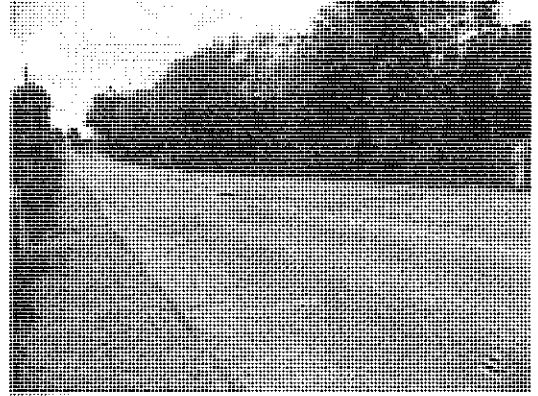
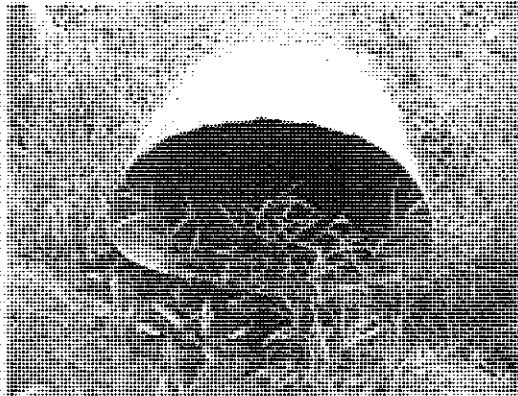
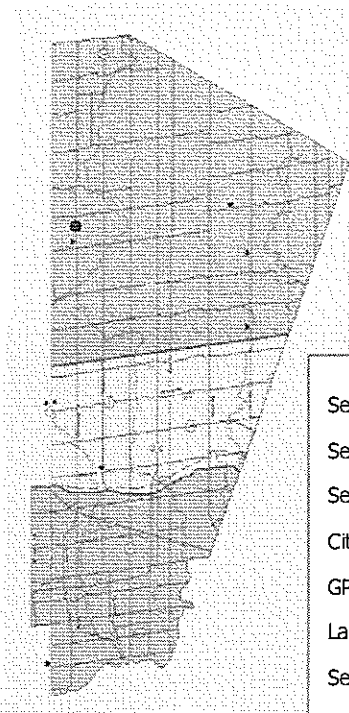
Effective Cross-Section:	60	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	2	m ²
Total Ditching Required :	2	m
Ditching on Private Prop:	0	m
Volume of HW West		m ³
Volume of HW East		m ³
Headwall Repair West		m ³
Headwall Repair East		m ³
Pre-Fab HW SA West		m ²
Pre-Fab HW SA East		m ²
Gabions Req. at West		m ³
Gabions Req. at East		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:	2	
Markers Req. Straight:	0	
Markers Replace/Install:	0	
Centre-Line Offset West	6.4	m
Centre-Line Offset East	6.4	m
Exposed Length West	0	m
Exposed Length East	0	m
Maximum Overburden:	0.6	m
Nominal Diameter:	0.4	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input checked="" type="checkbox"/>
	C <input type="checkbox"/>	
No Headwall Present at West	<input checked="" type="checkbox"/>	Pre-Fab Headwall at West <input type="checkbox"/>
No Headwall Present at East	<input checked="" type="checkbox"/>	Pre-Fab Headwall at East <input type="checkbox"/>
Concrete Headwall at West	<input type="checkbox"/>	Gabion Headwall at West <input type="checkbox"/>
Concrete Headwall at East	<input type="checkbox"/>	Gabion Headwall at East <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input checked="" type="checkbox"/>

1	Flush/Clean & Re-Shape Ends	\$1,800
2		
3		
4	Grade and Sod w/ Ditching	\$320
5		
6		
Total Incl. Mobilization and Contingency :		\$2,775

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input checked="" type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 283



Section - Road:	13760 -	MISSISSAUGA ROAD
Section Start:	0.7km N. OF OLDE BASE LINE ROAD	
Section End:	S.LIMITS, BELFOUNTAIN	
City/Town:	CALEDON	
GPS Coord:	582404 E	4847277 N
Last Inspected:	5/31/2005	
Service Type:	Cross	
Address/Cross Road:	N/A	
Side of Road:	N/A	

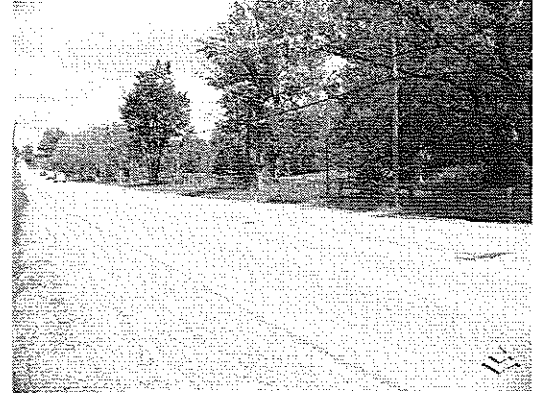
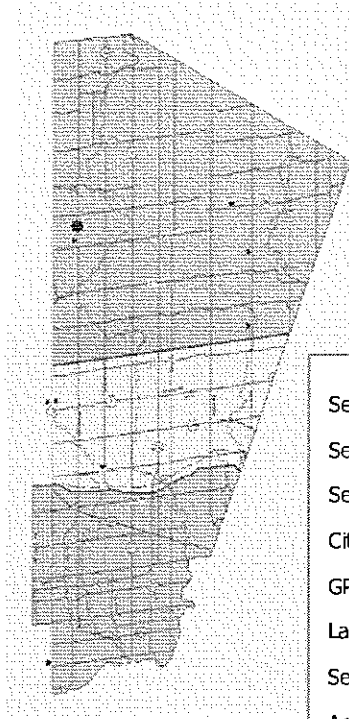
Effective Cross-Section:	100	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	4	m
Ditching on Private Prop:	0	m
Volume of HW West		m ³
Volume of HW East		m ³
Headwall Repair West		m ³
Headwall Repair East		m ³
Pre-Fab HW SA West		m ²
Pre-Fab HW SA East		m ²
Gabions Req. at West		m ³
Gabions Req. at East		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:	2	
Markers Req. Straight:	0	
Markers Replace/Install:	0	
Centre-Line Offset West	6.1	m
Centre-Line Offset East	5.9	m
Exposed Length West	0.4	m
Exposed Length East	0.2	m
Maximum Overburden:	0.1	m
Nominal Diameter:		m
Maximum Span:	0.85	m
Interior Height:	0.56	m

Shape/Type:	Flat Bottom	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input checked="" type="checkbox"/>
	C <input type="checkbox"/>	
No Headwall Present at West	<input checked="" type="checkbox"/>	Pre-Fab Headwall at West <input type="checkbox"/>
No Headwall Present at East	<input checked="" type="checkbox"/>	Pre-Fab Headwall at East <input type="checkbox"/>
Concrete Headwall at West	<input type="checkbox"/>	Gabion Headwall at West <input type="checkbox"/>
Concrete Headwall at East	<input type="checkbox"/>	Gabion Headwall at East <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input checked="" type="checkbox"/>

1	Do Nothing	\$0
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$875

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input checked="" type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 284



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582455 E 4847221 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

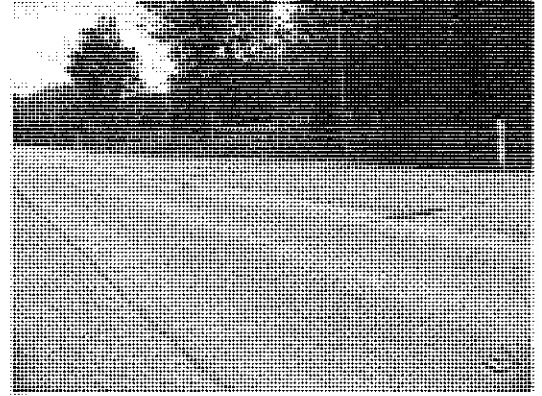
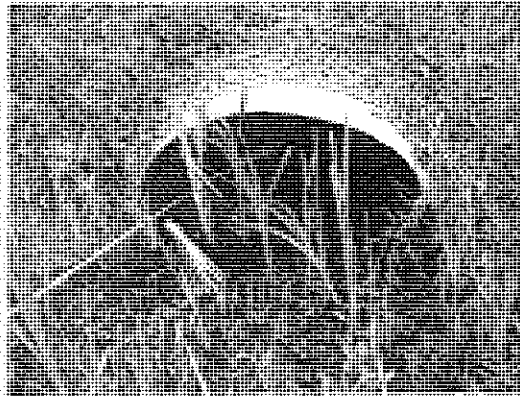
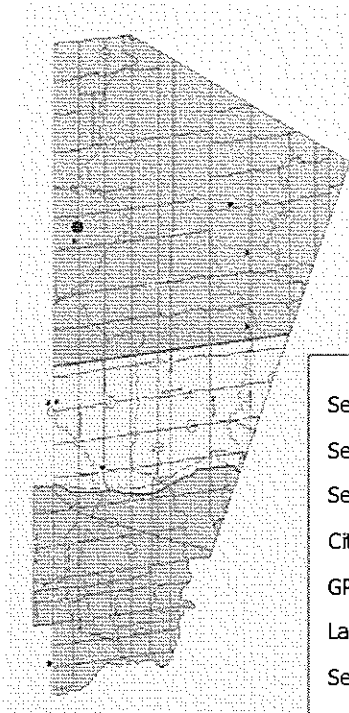
Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West: 6.8 m
 Centre-Line Offset East: 6.9 m
 Exposed Length West: 0.3 m
 Exposed Length East: 0.4 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: m
 Maximum Span: 1 m
 Interior Height: 0.7 m

Shape/Type: Flat Bottom
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 285



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N. OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582452 E 4847225 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

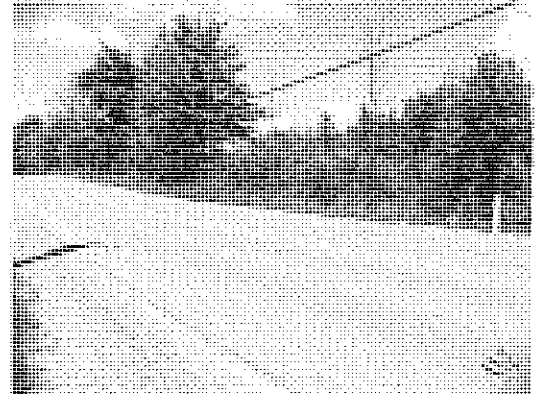
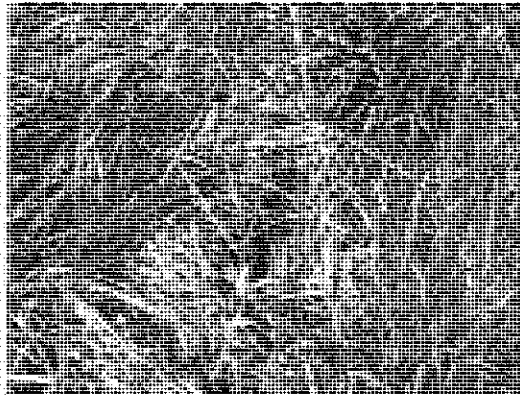
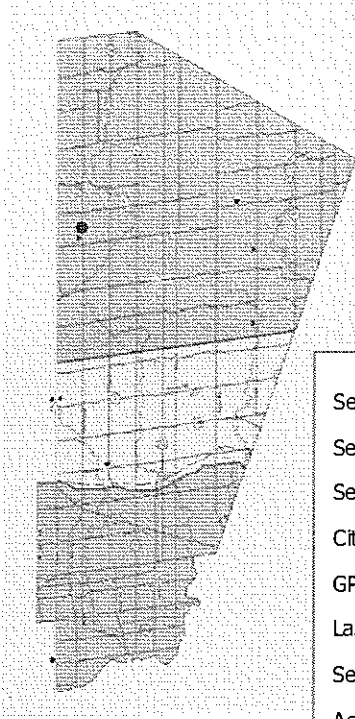
Shape/Type: Flat Bottom
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW West m³
 Volume of HW East m³
 Headwall Repair West m³
 Headwall Repair East m³
 Pre-Fab HW SA West m²
 Pre-Fab HW SA East m²
 Gabions Req. at West m³
 Gabions Req. at East m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 2
 Markers Req. Straight: 0
 Markers Replace/Install: 0
 Centre-Line Offset West 6.95 m
 Centre-Line Offset East 6.75 m
 Exposed Length West 0.3 m
 Exposed Length East 0.1 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: m
 Maximum Span: 1 m
 Interior Height: 0.7 m

CULVERT NO. 286



Section - Road:	13760	-	MISSISSAUGA ROAD
Section Start:	0.7km N.OF OLDE BASE LINE ROAD		
Section End:	S.LIMITS, BELFOUNTAIN		
City/Town:	CALEDON		
GPS Coord:	582726	E	4846964 N
Last Inspected:	5/31/2005		
Service Type:	Cross		
Address/Cross Road:	N/A		
Side of Road:	N/A		

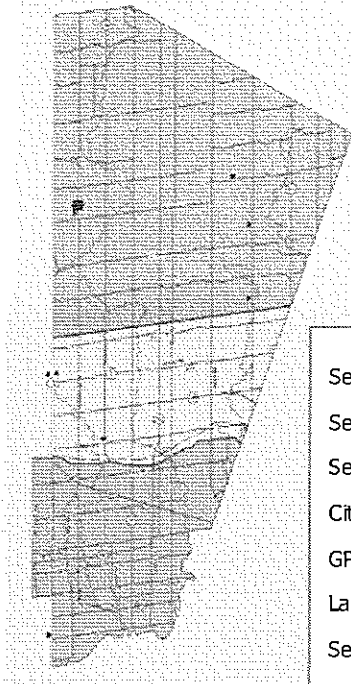
Effective Cross-Section:	60	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	4	m
Ditching on Private Prop:	0	m
Volume of HW West		m ³
Volume of HW East		m ³
Headwall Repair West		m ³
Headwall Repair East		m ³
Pre-Fab HW SA West		m ²
Pre-Fab HW SA East		m ²
Gabions Req. at West		m ³
Gabions Req. at East		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:	2	
Markers Req. Straight:	0	
Markers Replace/Install:	0	
Centre-Line Offset West	3.1	m
Centre-Line Offset East	9.1	m
Exposed Length West	0	m
Exposed Length East	6	m
Maximum Overburden:	0.7	m
Nominal Diameter:	0.4	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input checked="" type="checkbox"/>
	C <input type="checkbox"/>	
No Headwall Present at West	<input checked="" type="checkbox"/>	Pre-Fab Headwall at West <input type="checkbox"/>
No Headwall Present at East	<input checked="" type="checkbox"/>	Pre-Fab Headwall at East <input type="checkbox"/>
Concrete Headwall at West	<input type="checkbox"/>	Gabion Headwall at West <input type="checkbox"/>
Concrete Headwall at East	<input type="checkbox"/>	Gabion Headwall at East <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input checked="" type="checkbox"/>

1	Flush/Clean	\$1,525
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,781

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input checked="" type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 287



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582920 E 4846775 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: East

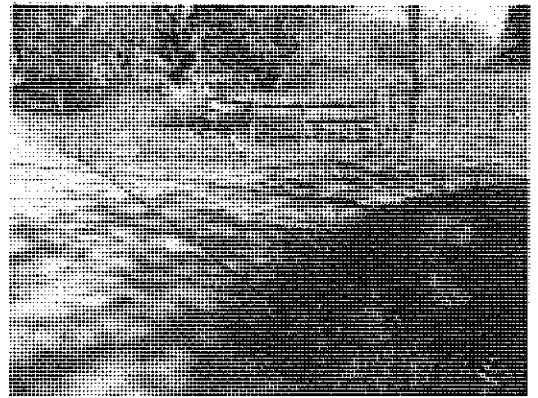
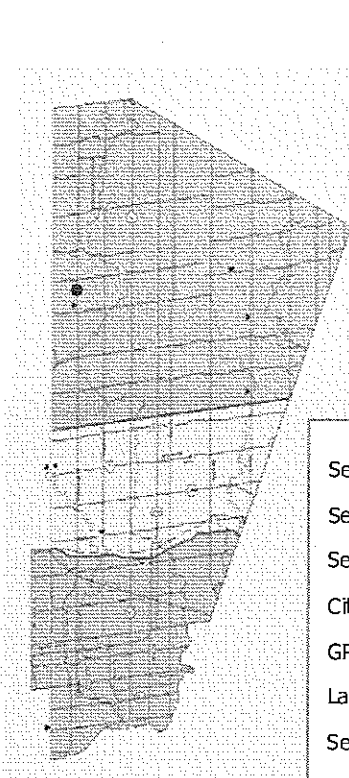
Effective Cross-Section: 95 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 3 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 3.2 m
 Centre-Line Offset North: 3 m
 Exposed Length South: 0.5 m
 Exposed Length North: 0.3 m
 Maximum Overburden: 0 m
 Nominal Diameter: 0.6 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$975
2		
3		
4	Ditching	\$450
5		
6		
Total Incl. Mobilization and Contingency :		\$1,906

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 288



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 582363 E 4847324 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: East

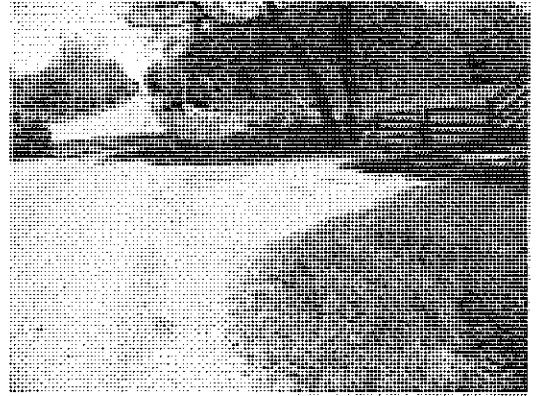
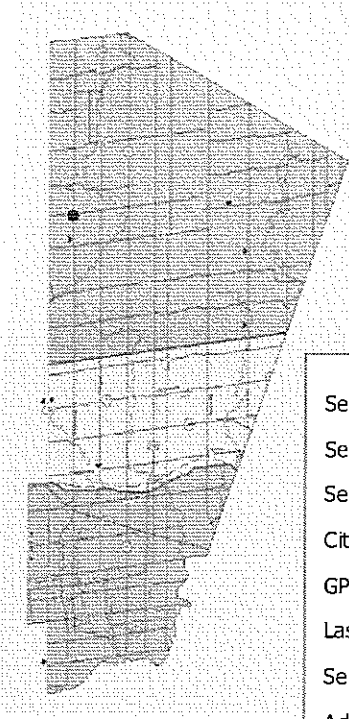
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,100
2		
3		
4	Ditching	\$450
5		
6		
Total Incl. Mobilization and Contingency :		\$2,063

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 70 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 3 m
 Ditching on Private Prop: 0 m
 Volume of HW South m³
 Volume of HW North m³
 Headwall Repair South m³
 Headwall Repair North m³
 Pre-Fab HW SA South m²
 Pre-Fab HW SA North m²
 Gabions Req. at South m³
 Gabions Req. at North m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South 4.25 m
 Centre-Line Offset North 4.55 m
 Exposed Length South 0.1 m
 Exposed Length North 0.4 m
 Maximum Overburden: 0.6 m
 Nominal Diameter: 0.5 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 289



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581862 E 4847829 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 16311
 Side of Road: East

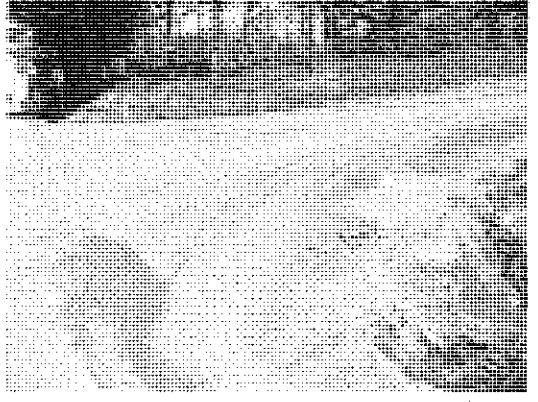
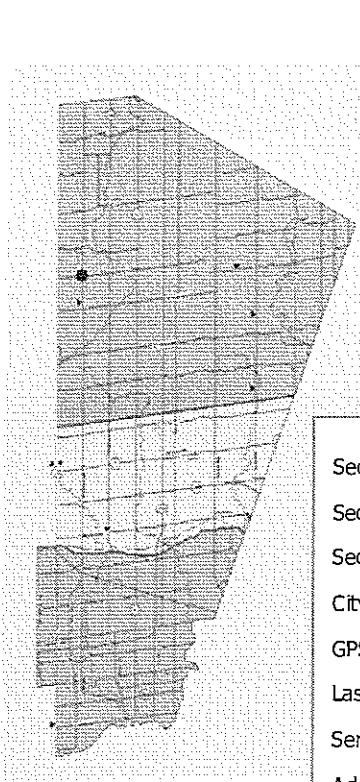
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,500
2		
3		
4	Ditching	\$900
5		
6		
Total Incl. Mobilization and Contingency :		\$3,125

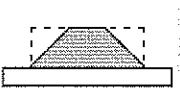
Immediately
 This Year
 1 -2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 90 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 6 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 5.2 m
 Centre-Line Offset North: 5.2 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.8 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 290



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581663 E 4848034 N
 Last Inspected: 5/27/2005
 Service Type: Intersection
 Address/Cross Road: Mississauga Rd + The Gra
 Side of Road: East

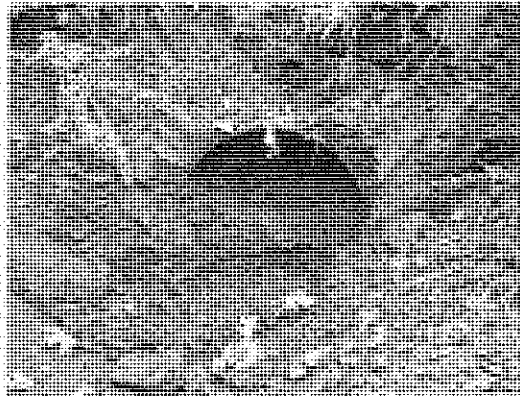
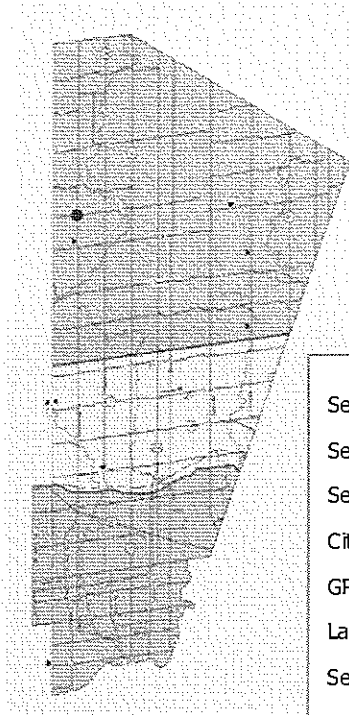
Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section: 
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South m³
 Volume of HW North m³
 Headwall Repair South m³
 Headwall Repair North m³
 Pre-Fab HW SA South m²
 Pre-Fab HW SA North m²
 Gabions Req. at South m³
 Gabions Req. at North m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 1
 Markers Req. Straight: 0
 Markers Replace/Install: 1
 Centre-Line Offset South 10.2 m
 Centre-Line Offset North 10.2 m
 Exposed Length South 0 m
 Exposed Length North 0 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$2,550
2		
3		
4		
5		
6	Replace/Install Marker Posts	\$10
Total Incl. Mobilization and Contingency :		\$3,325

Immediately
 This Year
 1 -2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 291



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581675 E 4848001 N
 Last Inspected: 5/27/2005
 Service Type: Intersection
 Address/Cross Road: Mississauga Rd + The Gra
 Side of Road: West

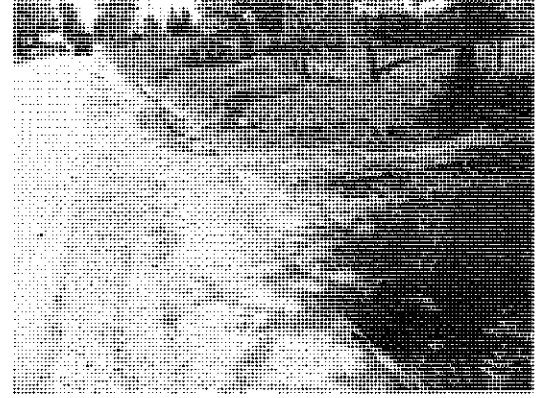
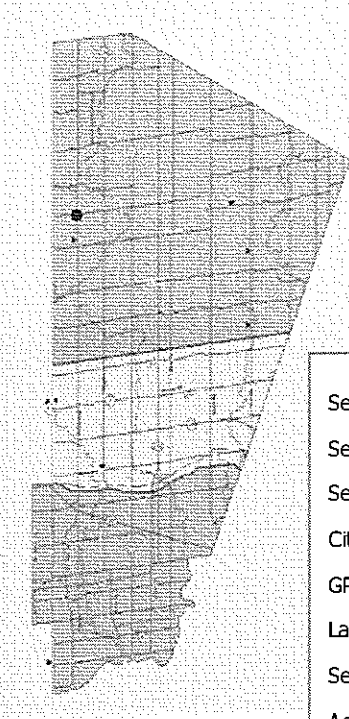
Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South m3
 Volume of HW North m3
 Headwall Repair South m3
 Headwall Repair North m3
 Pre-Fab HW SA South m2
 Pre-Fab HW SA North m2
 Gabions Req. at South m3
 Gabions Req. at North m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 1
 Markers Req. Straight: 1
 Markers Replace/Install: 1
 Centre-Line Offset South 10.2 m
 Centre-Line Offset North 10.2 m
 Exposed Length South 0 m
 Exposed Length North 0 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$2,550
2		
3		
4		
5		
6	Straighten & Replace/Install Marker Posts	\$20
Total Incl. Mobilization and Contingency :		\$3,338

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 292



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581792 E 4847887 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: West

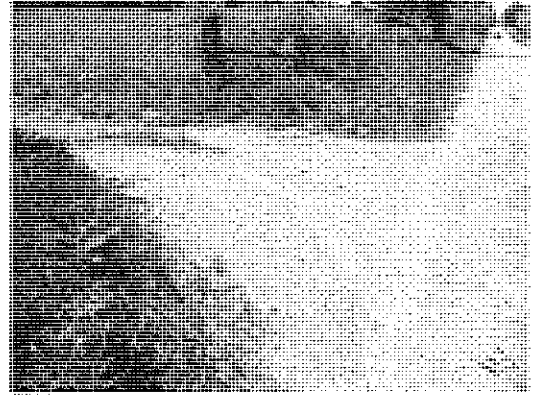
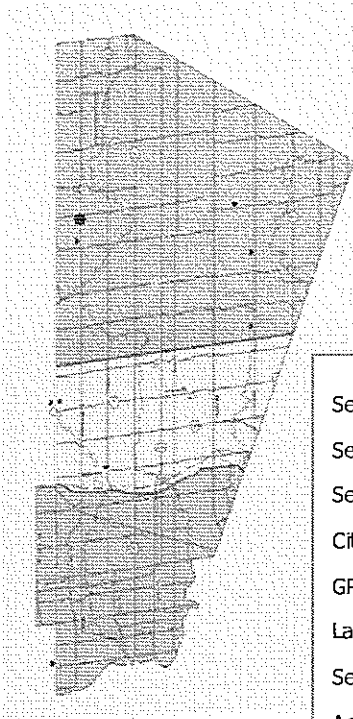
Effective Cross-Section: 15 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 2.5 m
 Centre-Line Offset North: 2.5 m
 Exposed Length South: 0.1 m
 Exposed Length North: 0.1 m
 Maximum Overburden: 0.3 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$625
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$906

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 293



Section - Road:	13760 -	MISSISSAUGA ROAD
Section Start:	0.7km N.OF OLDE BASE LINE ROAD	
Section End:	S.LIMITS, BELFOUNTAIN	
City/Town:	CALEDON	
GPS Coord:	581958 E	4847722 N
Last Inspected:	5/27/2005	
Service Type:	Field Entrance	
Address/Cross Road:	N/A	
Side of Road:	West	

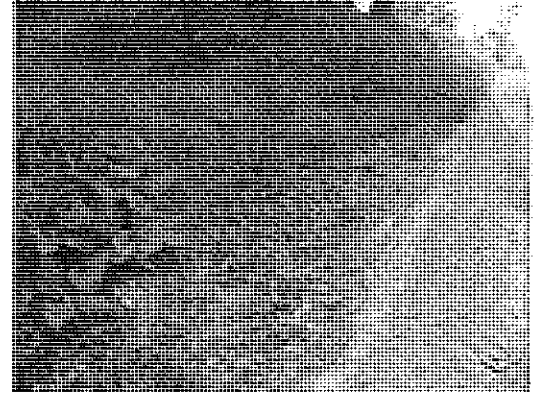
Effective Cross-Section:	5	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	8	m
Ditching on Private Prop:	0	m
Volume of HW South		m ³
Volume of HW North		m ³
Headwall Repair South		m ³
Headwall Repair North		m ³
Pre-Fab HW SA South		m ²
Pre-Fab HW SA North		m ²
Gabions Req. at South		m ³
Gabions Req. at North		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	3.1	m
Centre-Line Offset North	3.1	m
Exposed Length South	0	m
Exposed Length North	0	m
Maximum Overburden:	0.2	m
Nominal Diameter:	0.3	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/>	C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Flush/Clean & Re-Shape Ends	\$975
2		
3		
4	Ditching	\$1,200
5		
6		
Total Incl. Mobilization and Contingency :		\$2,844

Immediately	<input type="checkbox"/>
This Year	<input checked="" type="checkbox"/>
1 -2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 294



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581952 E 4847423 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: West

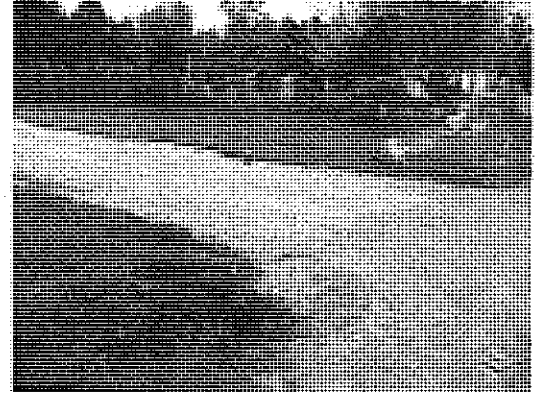
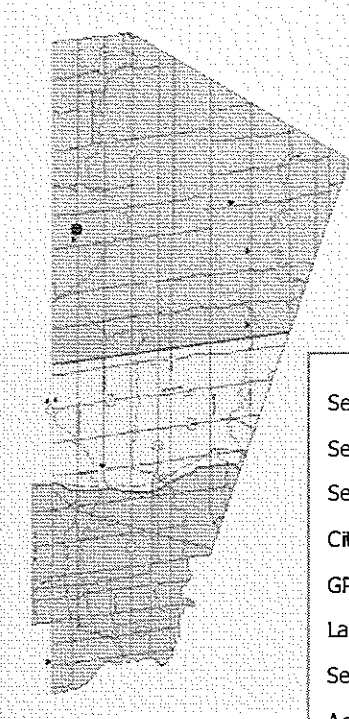
Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 2 m2
 Total Ditching Required : 9 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 4.5 m
 Centre-Line Offset North: 4.5 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.1 m
 Nominal Diameter: 0.3 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$1,125
2		
3		
4	Ditching	\$1,350
5		
6		
Total Incl. Mobilization and Contingency :		\$3,219

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 295



Section - Road:	13760	MISSISSAUGA ROAD	
Section Start:	0.7km N.OF OLDE BASE LINE ROAD		
Section End:	S.LIMITS, BELFOUNTAIN		
City/Town:	CALEDON		
GPS Coord:	582696	E	4846952 N
Last Inspected:	5/27/2005		
Service Type:	Entrance		
Address/Cross Road:	15938		
Side of Road:	West		

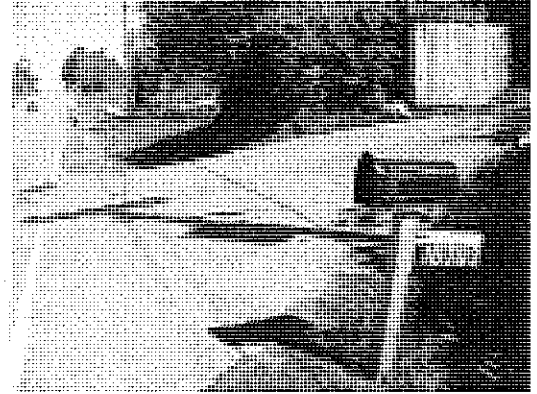
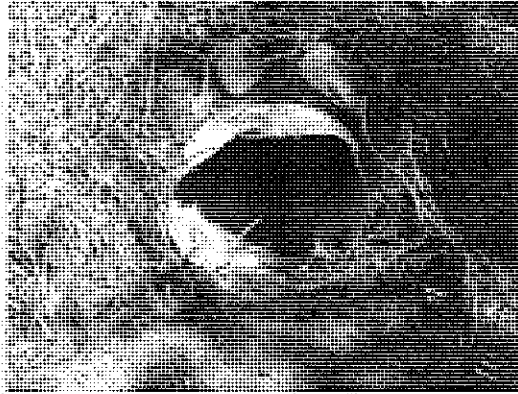
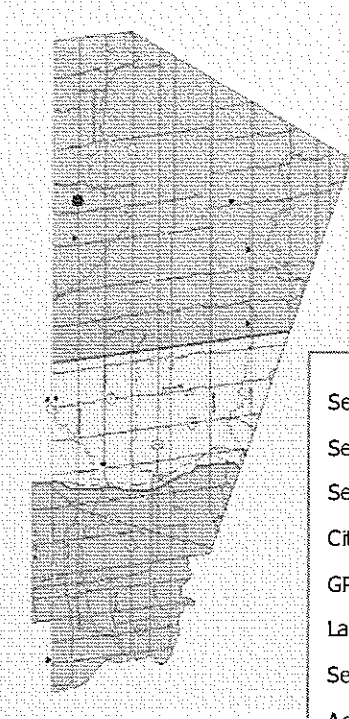
Effective Cross-Section:	15	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	3	m
Ditching on Private Prop:	0	m
Volume of HW South		m ³
Volume of HW North		m ³
Headwall Repair South		m ³
Headwall Repair North		m ³
Pre-Fab HW SA South		m ²
Pre-Fab HW SA North		m ²
Gabions Req. at South		m ³
Gabions Req. at North		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	3.1	m
Centre-Line Offset North	3.1	m
Exposed Length South	0.1	m
Exposed Length North	0.1	m
Maximum Overburden:	0.1	m
Nominal Diameter:	0.3	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/>	C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Flush/Clean	\$775
2		
3		
4	Ditching	\$450
5		
6		
Total Incl. Mobilization and Contingency :		\$1,656

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input checked="" type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 296



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 580970 E 4848723 N
 Last Inspected: 5/30/2005
 Service Type: Entrance
 Address/Cross Road: 16703
 Side of Road: East

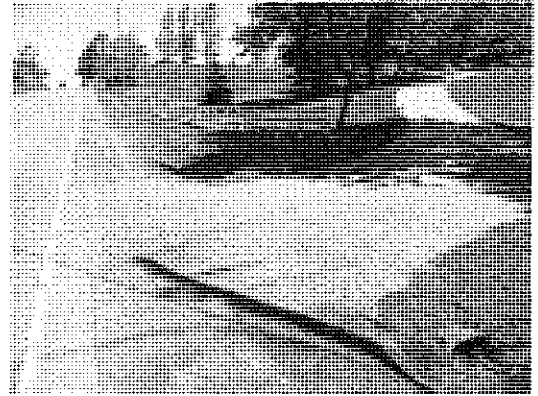
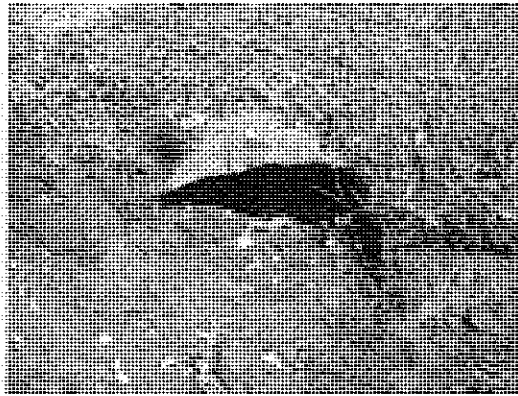
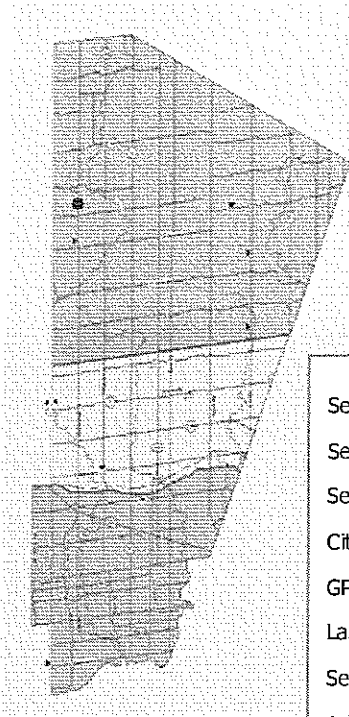
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,400
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,875

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 60 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW South m³
 Volume of HW North m³
 Headwall Repair South m³
 Headwall Repair North m³
 Pre-Fab HW SA South m²
 Pre-Fab HW SA North m²
 Gabions Req. at South m³
 Gabions Req. at North m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South 4.8 m
 Centre-Line Offset North 4.8 m
 Exposed Length South 0.1 m
 Exposed Length North 0.1 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 297



Section - Road:	13760	MISSISSAUGA ROAD
Section Start:	0.7km N. OF OLDE BASE LINE ROAD	
Section End:	S.LIMITS, BELFOUNTAIN	
City/Town:	CALEDON	
GPS Coord:	580933 E	4848749 N
Last Inspected:	5/30/2005	
Service Type:	Entrance	
Address/Cross Road:	16735	
Side of Road:	East	

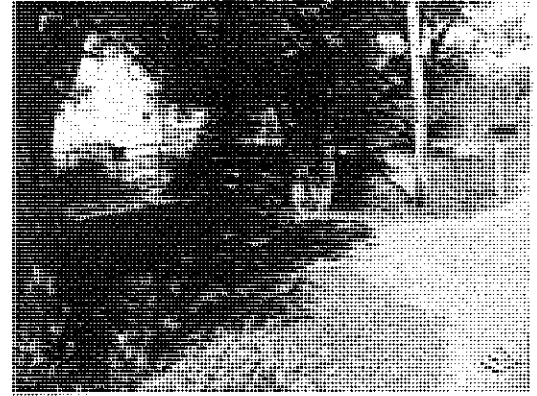
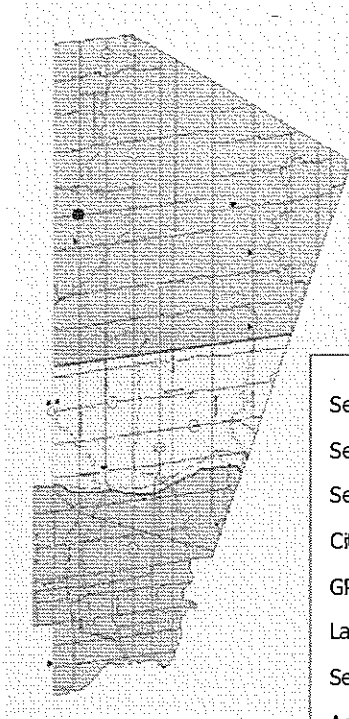
Shape/Type:	Round		
Material:	Corrugated Steel		
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/>	C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South	<input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North	<input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South	<input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Flush/Clean & Re-Shape Ends	\$1,112
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,515

Immediately	<input type="checkbox"/>
This Year	<input checked="" type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

Effective Cross-Section:	20	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	0	m
Ditching on Private Prop:		m
Volume of HW South		m ³
Volume of HW North		m ³
Headwall Repair South		m ³
Headwall Repair North		m ³
Pre-Fab HW SA South		m ²
Pre-Fab HW SA North		m ²
Gabions Req. at South		m ³
Gabions Req. at North		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	3.8	m
Centre-Line Offset North	3.5	m
Exposed Length South	0.2	m
Exposed Length North	0.5	m
Maximum Overburden:	0.4	m
Nominal Diameter:	0.46	m
Maximum Span:		m
Interior Height:		m

CULVERT NO. 298



Section - Road: 13760 - MISSISSAUGA ROAD
 Section Start: 0.7km N.OF OLDE BASE LINE ROAD
 Section End: S.LIMITS, BELFOUNTAIN
 City/Town: CALEDON
 GPS Coord: 581622 E 4848059 N
 Last Inspected: 5/30/2005
 Service Type: Entrance
 Address/Cross Road: 16416
 Side of Road: West

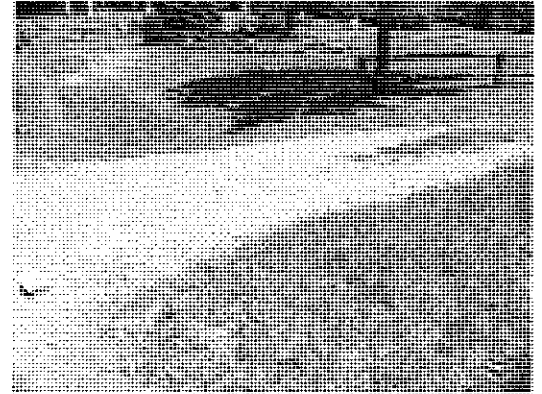
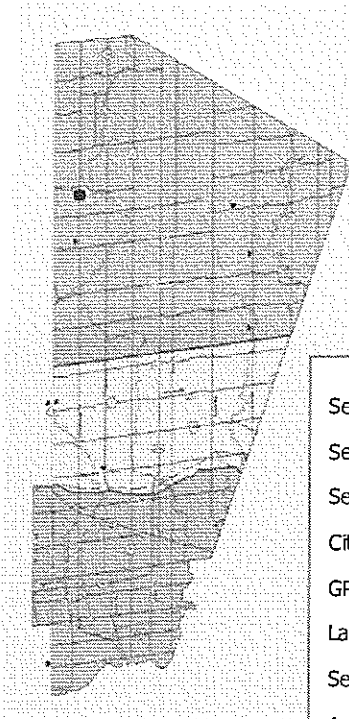
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$888
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$1,985

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 40 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 4 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 3.55 m
 Centre-Line Offset North: 3.55 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.8 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 299



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 580374 E 4849321 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: East

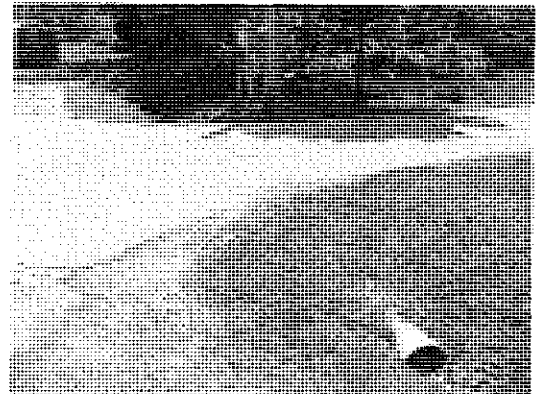
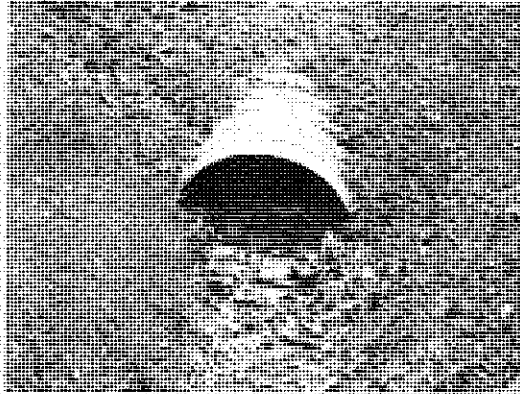
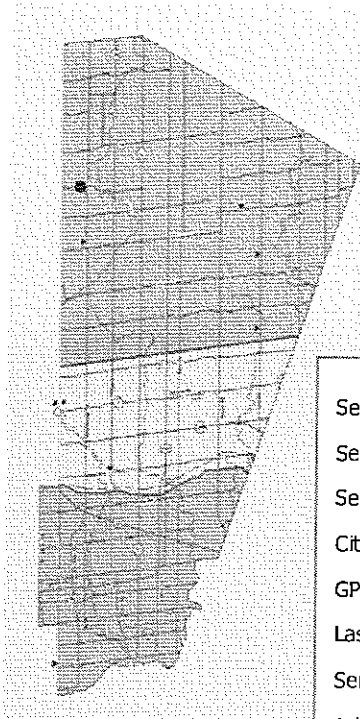
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,000
2		
3		
4	Ditching	\$900
5		
6		
Total Incl. Mobilization and Contingency :		\$2,500

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 40 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 6 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 3.2 m
 Centre-Line Offset North: 3.2 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 300



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 579342 E 4849435 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: N/A
 Side of Road: West

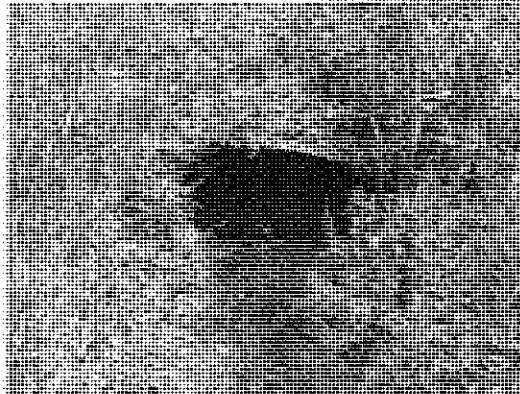
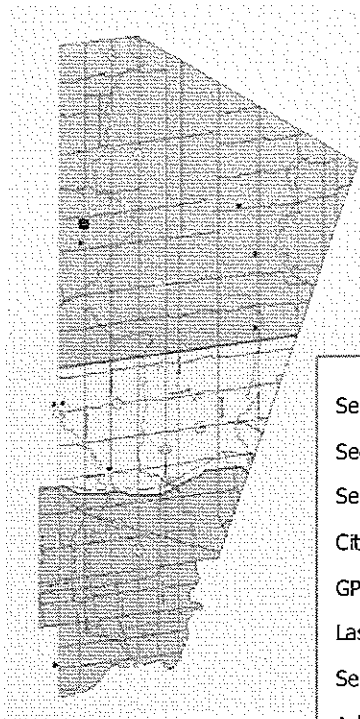
Effective Cross-Section: 50 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 8 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 4.55 m
 Centre-Line Offset North: 4.85 m
 Exposed Length South: 0.1 m
 Exposed Length North: 0.4 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.4 m
 Maximum Span:
 Interior Height:

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts


1	Flush/Clean	\$1,175
2		
3		
4	Ditching	\$1,200
5		
6		
Total Incl. Mobilization and Contingency :		\$3,094

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 301



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 582200 E 4847484 N
 Last Inspected: 5/27/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: West

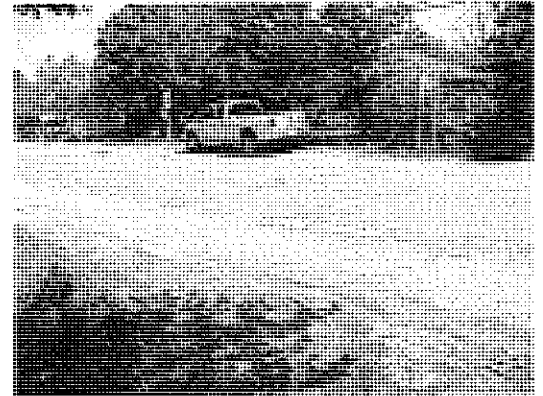
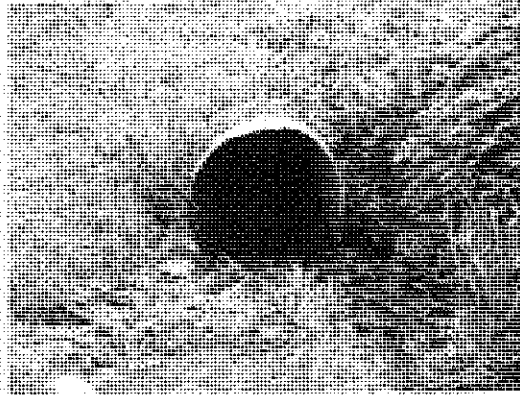
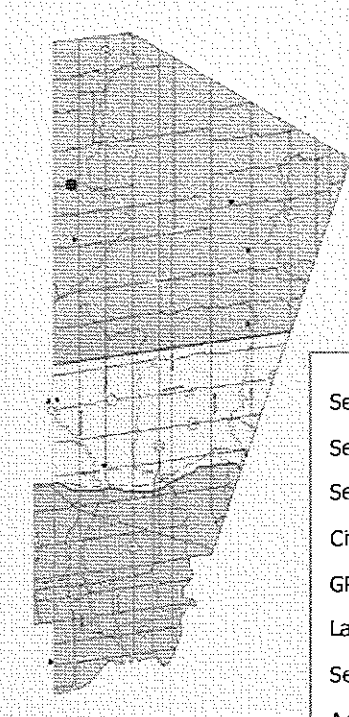
Effective Cross-Section: 50 %
 % Req. Replacement: 0 %
 Cross Section: 
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 20 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 3.25 m
 Centre-Line Offset North: 3.25 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: m
 Maximum Span: 1 m
 Interior Height: 0.6 m

Shape/Type: Oval
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,012
2		
3		
4	Ditching	\$3,000
5		
6		
Total Incl. Mobilization and Contingency :		\$5,140

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 302



Section - Road:	14240	MISSISSAUGA ROAD
Section Start:	S.LIMITS, BELFOUNTAIN	
Section End:	REG. RD. # 11	
City/Town:	CALEDON	
GPS Coord:	579349 E	4849423 N
Last Inspected:	5/31/2005	
Service Type:	Cross	
Address/Cross Road:	N/A	
Side of Road:	N/A	

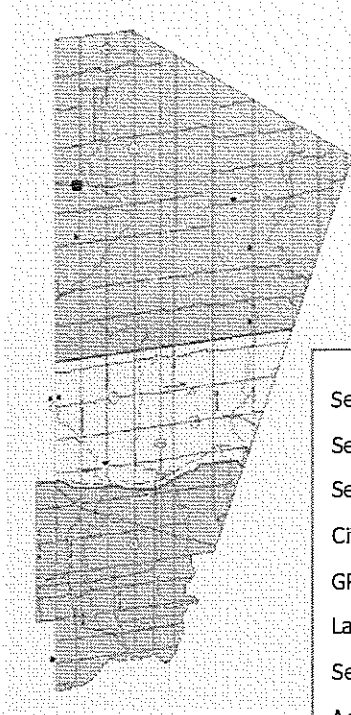
Effective Cross-Section:	90	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	0	m
Ditching on Private Prop:		m
Volume of HW West		m ³
Volume of HW East		m ³
Headwall Repair West		m ³
Headwall Repair East		m ³
Pre-Fab HW SA West		m ²
Pre-Fab HW SA East		m ²
Gabions Req. at West		m ³
Gabions Req. at East		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	2	
Centre-Line Offset West	8.55	m
Centre-Line Offset East	8.85	m
Exposed Length West	0.1	m
Exposed Length East	0.4	m
Maximum Overburden:	0.4	m
Nominal Diameter:	0.6	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input checked="" type="checkbox"/>
	C <input type="checkbox"/>	
No Headwall Present at West	<input checked="" type="checkbox"/>	Pre-Fab Headwall at West <input type="checkbox"/>
No Headwall Present at East	<input checked="" type="checkbox"/>	Pre-Fab Headwall at East <input type="checkbox"/>
Concrete Headwall at West	<input type="checkbox"/>	Gabion Headwall at West <input type="checkbox"/>
Concrete Headwall at East	<input type="checkbox"/>	Gabion Headwall at East <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input type="checkbox"/>

1	Flush/Clean	\$2,175
2		
3		
4		
5		
6	Do Nothing	\$0
Total Incl. Mobilization and Contingency :		\$2,844

Immediately	<input type="checkbox"/>
This Year	<input type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input checked="" type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 303



Section - Road: 14240 MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 579848 E 4849496 N
 Last Inspected: 5/31/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

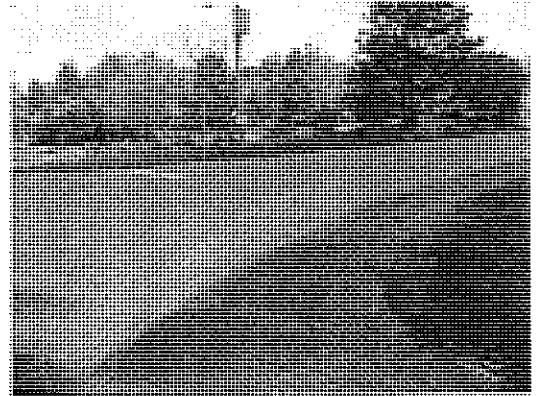
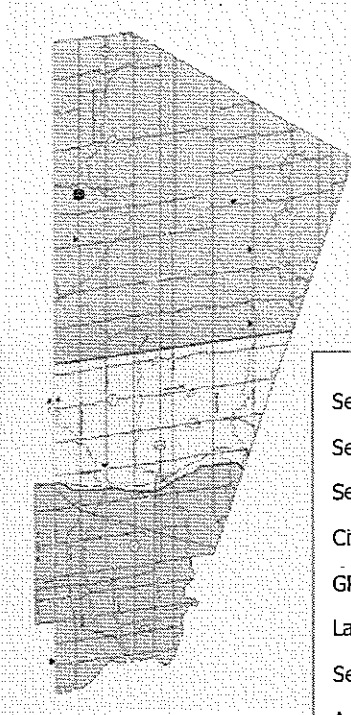
Effective Cross-Section: 5 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 3 m2
 Total Ditching Required: 9 m
 Ditching on Private Prop: 0 m
 Volume of HW West: m3
 Volume of HW East: m3
 Headwall Repair West: m3
 Headwall Repair East: m3
 Pre-Fab HW SA West: m2
 Pre-Fab HW SA East: m2
 Gabions Req. at West: m3
 Gabions Req. at East: m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 1
 Markers Req. Straight: 0
 Markers Replace/Install: 1
 Centre-Line Offset West: 5.3 m
 Centre-Line Offset East: 5.1 m
 Exposed Length West: 0.2 m
 Exposed Length East: 0 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,500
2		
3		
4	Grade and Sod w / Ditching	\$1,380
5		
6	Do Nothing	\$0
Total Incl. Mobilization and Contingency :		\$3,725

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 304



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 580493 E 4849207 N
 Last Inspected: 5/27/2005
 Service Type: Intersection
 Address/Cross Road: Mississauga Rd + Woodla
 Side of Road: East

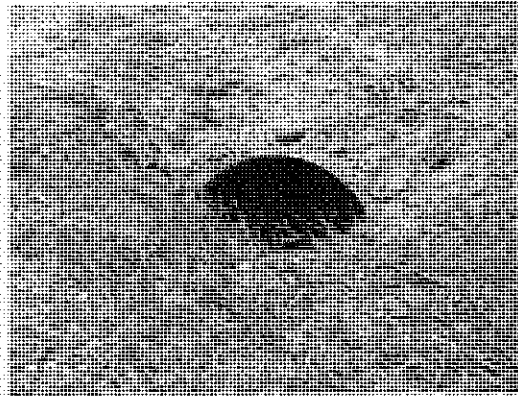
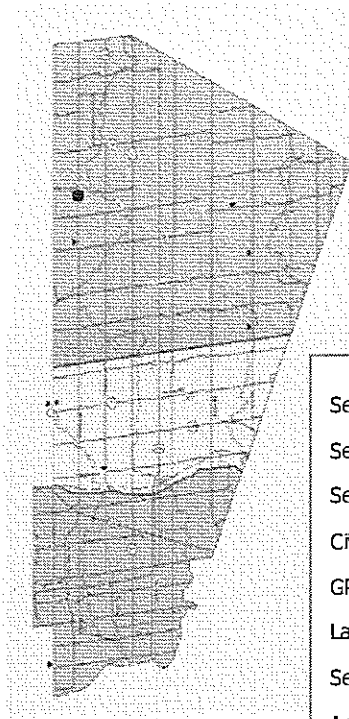
Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 2 m²
 Total Ditching Required : 8 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m³
 Volume of HW North: m³
 Headwall Repair South: m³
 Headwall Repair North: m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 10.95 m
 Centre-Line Offset North: 11.25 m
 Exposed Length South: 0 m
 Exposed Length North: 0.3 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$2,775
2		
3		
4	Grade and Sod w / Ditching	\$1,220
5		
6		
Total Incl. Mobilization and Contingency :		\$5,119

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 305



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 580347 E 4849350 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 17025
 Side of Road: East

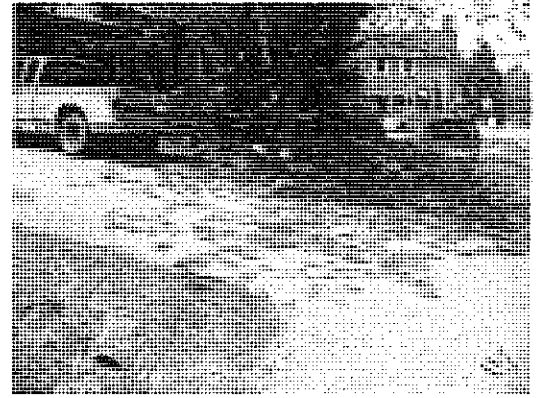
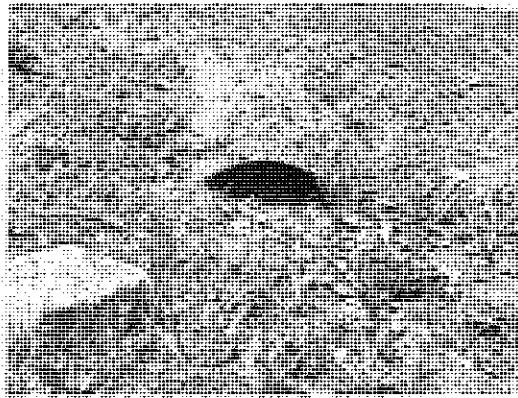
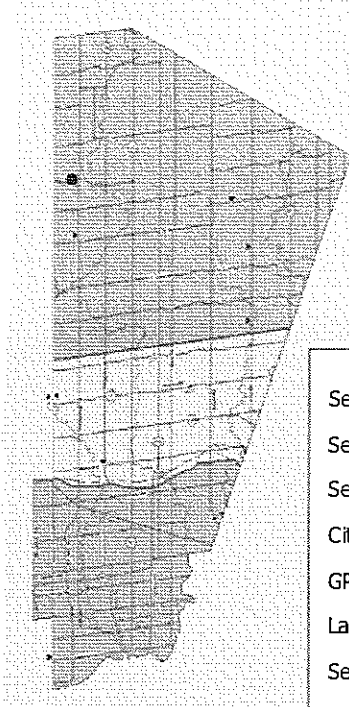
Effective Cross-Section: 60 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 3 m
 Ditching on Private Prop: 0 m
 Volume of HW South: m³
 Volume of HW North: 0.1 m³
 Headwall Repair South: m³
 Headwall Repair North: 0 m³
 Pre-Fab HW SA South: m²
 Pre-Fab HW SA North: m²
 Gabions Req. at South: m³
 Gabions Req. at North: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset South: 8 m
 Centre-Line Offset North: 8 m
 Exposed Length South: 0 m
 Exposed Length North: 0 m
 Maximum Overburden: 0.8 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean	\$2,000
2		
3	Do Nothing	\$0
4	Ditching	\$450
5		
6		
Total Incl. Mobilization and Contingency :		\$3,188

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 306



Section - Road: 14240 - MISSISSAUGA ROAD
 Section Start: S.LIMITS, BELFOUNTAIN
 Section End: REG. RD. # 11
 City/Town: CALEDON
 GPS Coord: 579325 E 4849450 N
 Last Inspected: 5/27/2005
 Service Type: Entrance
 Address/Cross Road: 17266
 Side of Road: West

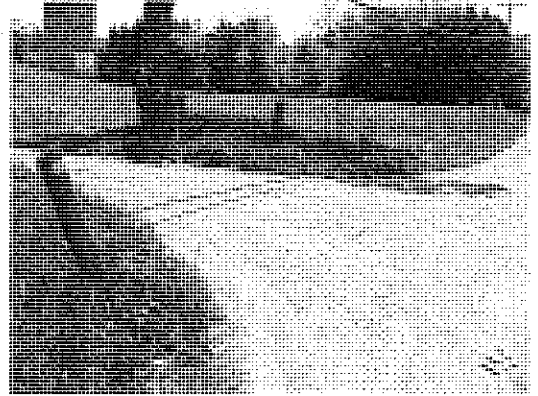
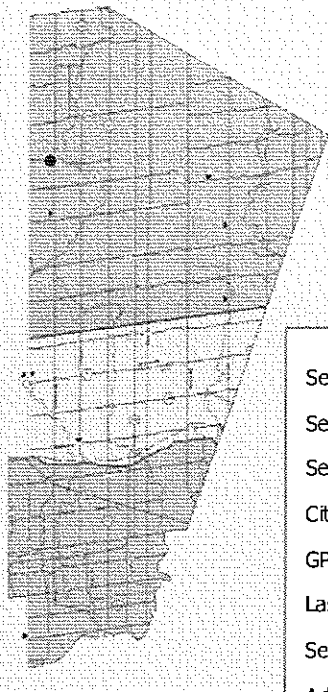
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$975
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,094

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 25 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 4 m
 Ditching on Private Prop: 0 m
 Volume of HW South m³
 Volume of HW North m³
 Headwall Repair South m³
 Headwall Repair North m³
 Pre-Fab HW SA South m²
 Pre-Fab HW SA North m²
 Gabions Req. at South m³
 Gabions Req. at North m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset South: 2.95 m
 Centre-Line Offset North: 3.25 m
 Exposed Length South: 0 m
 Exposed Length North: 0.3 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 307



Section - Road:	14240 -	MISSISSAUGA ROAD
Section Start:	S.LIMITS, BELFOUNTAIN	
Section End:	REG. RD. # 11	
City/Town:	CALEDON	
GPS Coord:	579723 E	4849445 N
Last Inspected:	5/27/2005	
Service Type:	Entrance	
Address/Cross Road:	N/A	
Side of Road:	West	

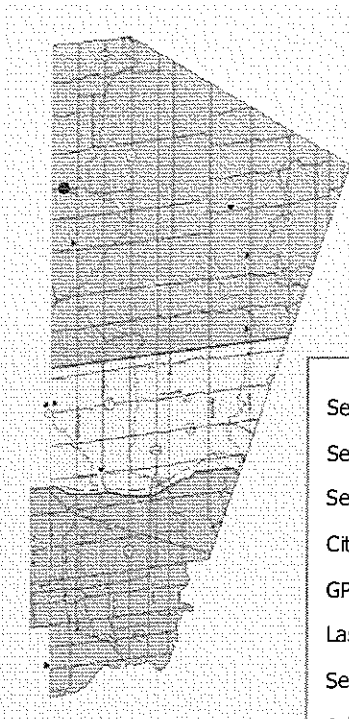
Effective Cross-Section:	10	%
% Req. Replacement:	0	%
Cross Section:		
Area Req. Erosion Cntrl:	0	m ²
Total Ditching Required :	8	m
Ditching on Private Prop:	0	m
Volume of HW South		m ³
Volume of HW North		m ³
Headwall Repair South		m ³
Headwall Repair North		m ³
Pre-Fab HW SA South		m ²
Pre-Fab HW SA North		m ²
Gabions Req. at South		m ³
Gabions Req. at North		m ³
Total Barrier Length:		m
Barriers Req. Repair:		m
Barriers Replace/Install:	0	m
Number of Marker Posts:		
Markers Req. Straight:		
Markers Replace/Install:	0	
Centre-Line Offset South	5	m
Centre-Line Offset North	5	m
Exposed Length South	0	m
Exposed Length North	0	m
Maximum Overburden:	0.5	m
Nominal Diameter:	0.4	m
Maximum Span:		m
Interior Height:		m

Shape/Type:	Round	
Material:	Corrugated Steel	
Surface:	A <input type="checkbox"/>	B <input type="checkbox"/> C <input checked="" type="checkbox"/>
No Headwall Present at South	<input checked="" type="checkbox"/>	Pre-Fab Headwall at South <input type="checkbox"/>
No Headwall Present at North	<input checked="" type="checkbox"/>	Pre-Fab Headwall at North <input type="checkbox"/>
Concrete Headwall at South	<input type="checkbox"/>	Gabion Headwall at South <input type="checkbox"/>
Concrete Headwall at North	<input type="checkbox"/>	Gabion Headwall at North <input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts <input type="checkbox"/>

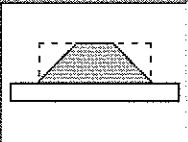
1	Flush/Clean	\$1,250
2		
3		
4	Ditching	\$1,200
5		
6		
Total Incl. Mobilization and Contingency :		\$3,188

Immediately	<input type="checkbox"/>
This Year	<input checked="" type="checkbox"/>
1 - 2 Years	<input type="checkbox"/>
3 - 5 Years	<input type="checkbox"/>
6 - 10 Years	<input type="checkbox"/>
11+ Years	<input type="checkbox"/>
N/A	<input type="checkbox"/>

CULVERT NO. 1734



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAWS CREEK RD.
 City/Town: CALEDON
 GPS Coord: 578880 E 4848967 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 523
 Side of Road: South

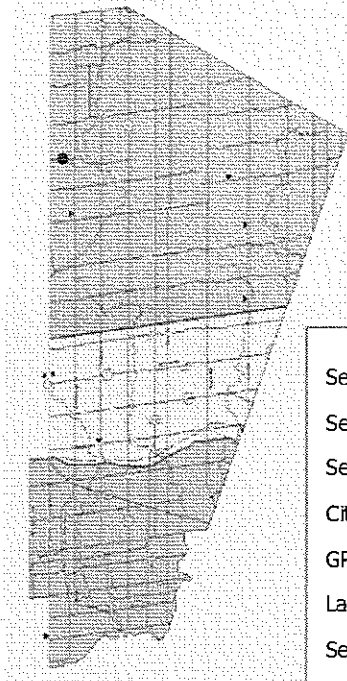
Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section: 
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW West m3
 Volume of HW East m3
 Headwall Repair West m3
 Headwall Repair East m3
 Pre-Fab HW SA West m2
 Pre-Fab HW SA East m2
 Gabions Req. at West m3
 Gabions Req. at East m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset West 4.25 m
 Centre-Line Offset East 4.35 m
 Exposed Length West 0 m
 Exposed Length East 0.1 m
 Maximum Overburden: 0.6 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11 + Years
 N/A

CULVERT NO. 1735



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAW'S CREEK RD.
 City/Town: CALEDON
 GPS Coord: 578961 E 4849065 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 593
 Side of Road: South

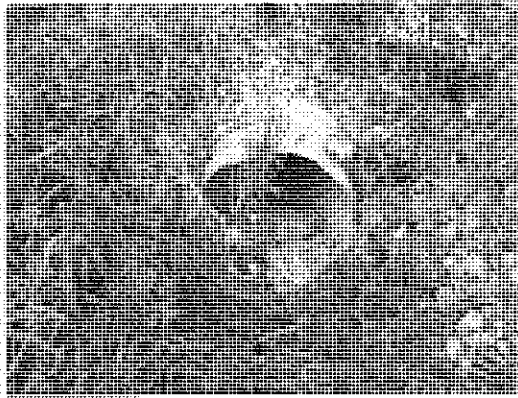
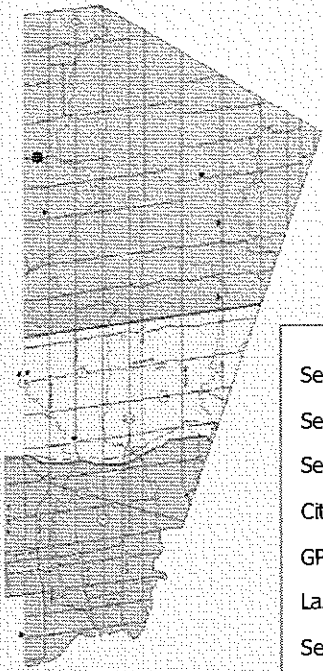
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,138
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,548

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW West m³
 Volume of HW East m³
 Headwall Repair West m³
 Headwall Repair East m³
 Pre-Fab HW SA West m²
 Pre-Fab HW SA East m²
 Gabions Req. at West m³
 Gabions Req. at East m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset West 4.55 m
 Centre-Line Offset East 4.55 m
 Exposed Length West 0 m
 Exposed Length East 0 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 1736



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAW'S CREEK RD.
 City/Town: CALEDON
 GPS Coord: 578971 E 4849075 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 595
 Side of Road: South

Effective Cross-Section:	95 %
% Req. Replacement:	0 %
Cross Section:	
Area Req. Erosion Cntrl:	0 m ²
Total Ditching Required :	0 m
Ditching on Private Prop:	m
Volume of HW West	m ³
Volume of HW East	m ³
Headwall Repair West	m ³
Headwall Repair East	m ³
Pre-Fab HW SA West	m ²
Pre-Fab HW SA East	m ²
Gabions Req. at West	m ³
Gabions Req. at East	m ³
Total Barrier Length:	m
Barriers Req. Repair:	m
Barriers Replace/Install:	0 m
Number of Marker Posts:	
Markers Req. Straight:	
Markers Replace/Install:	0
Centre-Line Offset West	4.75 m
Centre-Line Offset East	4.65 m
Exposed Length West	0.2 m
Exposed Length East	0.1 m
Maximum Overburden:	0.3 m
Nominal Diameter:	0.4 m
Maximum Span:	m
Interior Height:	m

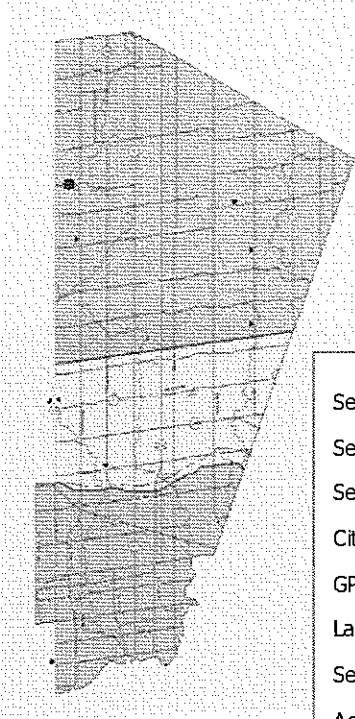
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C

No Headwall Present at West	<input checked="" type="checkbox"/>	Pre-Fab Headwall at West	<input type="checkbox"/>
No Headwall Present at East	<input checked="" type="checkbox"/>	Pre-Fab Headwall at East	<input type="checkbox"/>
Concrete Headwall at West	<input type="checkbox"/>	Gabion Headwall at West	<input type="checkbox"/>
Concrete Headwall at East	<input type="checkbox"/>	Gabion Headwall at East	<input type="checkbox"/>
Barriers Present	<input type="checkbox"/>	Marker Posts	<input type="checkbox"/>

1	Flush/Clean	\$1,175
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$1,594

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 1737



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAW'S CREEK RD.
 City/Town: CALEDON
 GPS Coord: 578995 E 4849105 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 597
 Side of Road: South

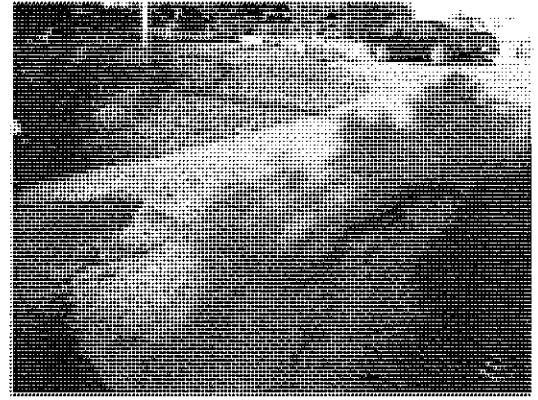
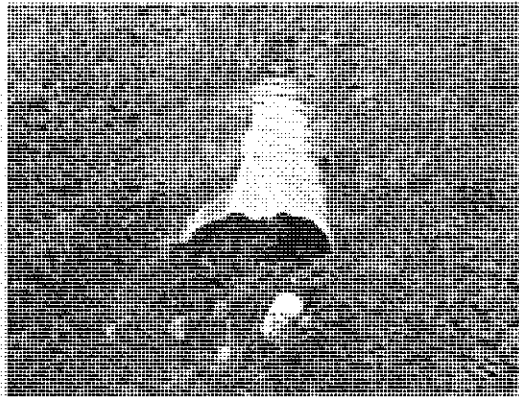
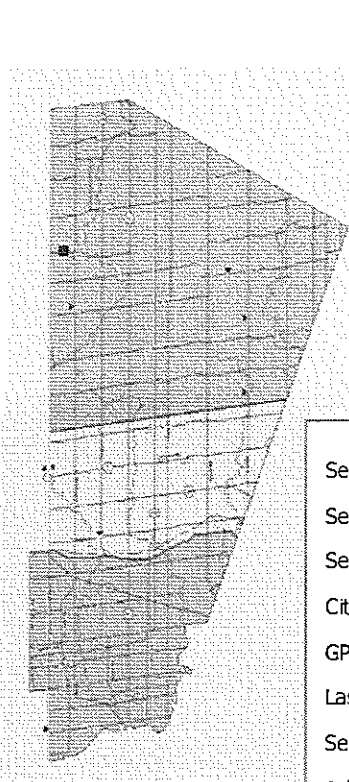
Effective Cross-Section: 30 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 4 m
 Ditching on Private Prop: 0 m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset West: 4.7 m
 Centre-Line Offset East: 4.6 m
 Exposed Length West: 0.5 m
 Exposed Length East: 0.4 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean & Re-Shape Ends	\$1,362
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,578

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 1738



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAWS CREEK RD.
 City/Town: CALEDON
 GPS Coord: 579008 E 4849123 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 599
 Side of Road: South

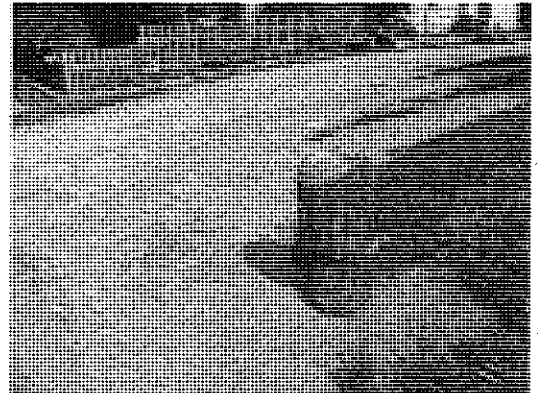
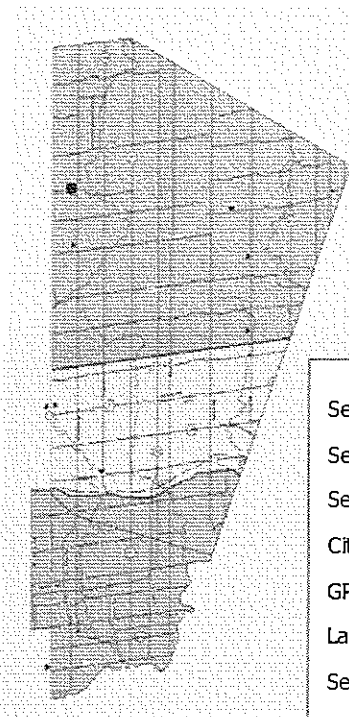
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$950
2		
3		
4	Ditching	\$300
5		
6		
Total Incl. Mobilization and Contingency :		\$1,688

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 40 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required : 2 m
 Ditching on Private Prop: 0 m
 Volume of HW West _____ m³
 Volume of HW East _____ m³
 Headwall Repair West _____ m³
 Headwall Repair East _____ m³
 Pre-Fab HW SA West _____ m²
 Pre-Fab HW SA East _____ m²
 Gabions Req. at West _____ m³
 Gabions Req. at East _____ m³
 Total Barrier Length: _____ m
 Barriers Req. Repair: _____ m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: _____
 Markers Req. Straight: _____
 Markers Replace/Install: 0
 Centre-Line Offset West 4.15 m
 Centre-Line Offset East 3.45 m
 Exposed Length West 0.7 m
 Exposed Length East 0 m
 Maximum Overburden: 0.6 m
 Nominal Diameter: 0.4 m
 Maximum Span: _____ m
 Interior Height: _____ m

CULVERT NO. 1739



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAWS CREEK RD.
 City/Town: CALEDON
 GPS Coord: 579298 E 4849577 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 779
 Side of Road: South

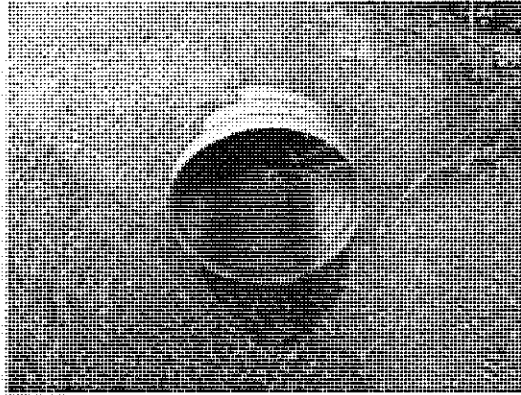
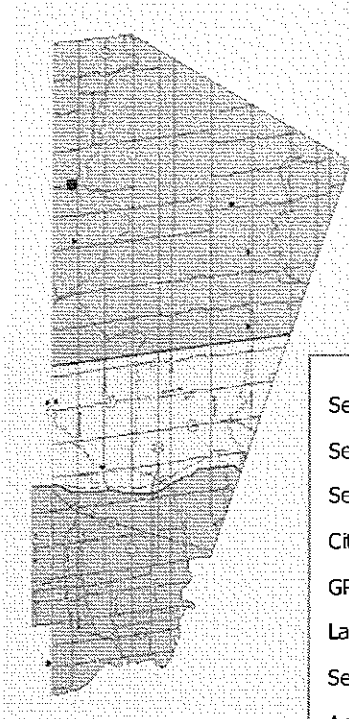
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 0 m
 Ditching on Private Prop: m
 Volume of HW West m3
 Volume of HW East m3
 Headwall Repair West m3
 Headwall Repair East m3
 Pre-Fab HW SA West m2
 Pre-Fab HW SA East m2
 Gabions Req. at West m3
 Gabions Req. at East m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset West 4.65 m
 Centre-Line Offset East 4.55 m
 Exposed Length West 0.1 m
 Exposed Length East 0 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 1740



Section - Road: 110700 - BUSH STREET
 Section Start: MISSISSAUGA RD. (REG. RD. # 1)
 Section End: SHAW'S CREEK RD.
 City/Town: CALEDON
 GPS Coord: 579301 E 4849583 N
 Last Inspected: 8/23/2005
 Service Type: Entrance
 Address/Cross Road: 779
 Side of Road: South

Effective Cross-Section: 100 %
 % Req. Replacement: 0 %
 Cross Section:

Area Req. Erosion Cntrl: 0 m²
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW West: m³
 Volume of HW East: m³
 Headwall Repair West: m³
 Headwall Repair East: m³
 Pre-Fab HW SA West: m²
 Pre-Fab HW SA East: m²
 Gabions Req. at West: m³
 Gabions Req. at East: m³
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: m
 Markers Req. Straight: m
 Markers Replace/Install: 0 m
 Centre-Line Offset West: 4.5 m
 Centre-Line Offset East: 4.5 m
 Exposed Length West: 0.2 m
 Exposed Length East: 0.2 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

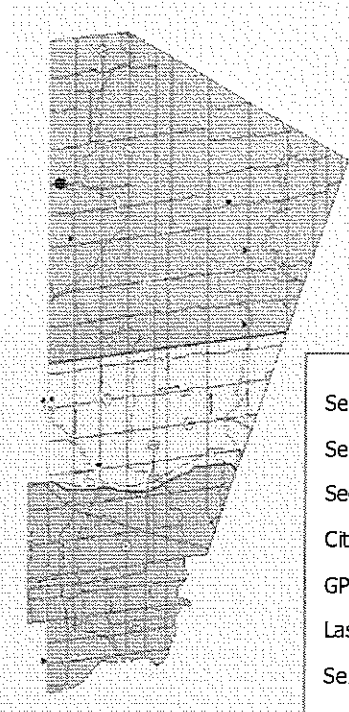
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C

No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6		
Total Incl. Mobilization and Contingency :		\$0

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

CULVERT NO. 1741



Section - Road: 110820 - BUSH STREET
 Section Start: SHAWS CREEK RD.
 Section End: WINSTON CHURCHILL BLVD. (REG. RD. :)
 City/Town: CALEDON
 GPS Coord: 578762 E 4848842 N
 Last Inspected: 8/23/2005
 Service Type: Other Parallel
 Address/Cross Road: N/A
 Side of Road: North

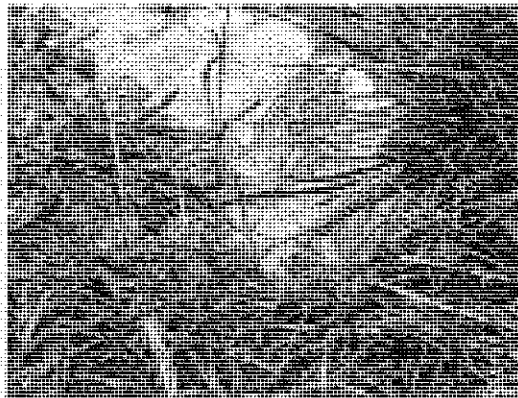
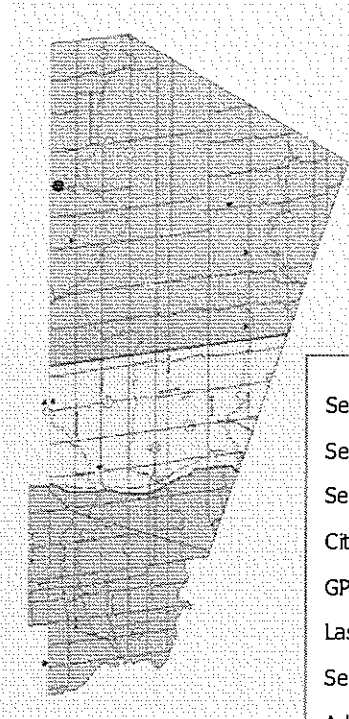
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,150
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$2,313

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 60 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 4 m
 Ditching on Private Prop: 0 m
 Volume of HW West m3
 Volume of HW East m3
 Headwall Repair West m3
 Headwall Repair East m3
 Pre-Fab HW SA West m2
 Pre-Fab HW SA East m2
 Gabions Req. at West m3
 Gabions Req. at East m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset West 4.5 m
 Centre-Line Offset East 4.7 m
 Exposed Length West 0.2 m
 Exposed Length East 0.4 m
 Maximum Overburden: 0.4 m
 Nominal Diameter: 0.46 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 1742



Section - Road: 110820 - BUSH STREET
 Section Start: SHAWS CREEK RD.
 Section End: WINSTON CHURCHILL BLVD. (REG. RD. #)
 City/Town: CALEDON
 GPS Coord: 578576 E 4848582 N
 Last Inspected: 8/23/2005
 Service Type: Field Entrance
 Address/Cross Road: N/A
 Side of Road: South

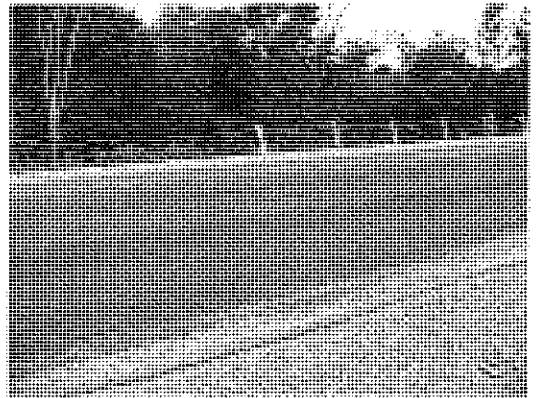
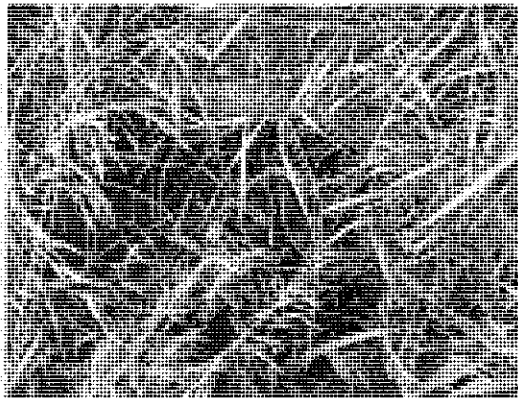
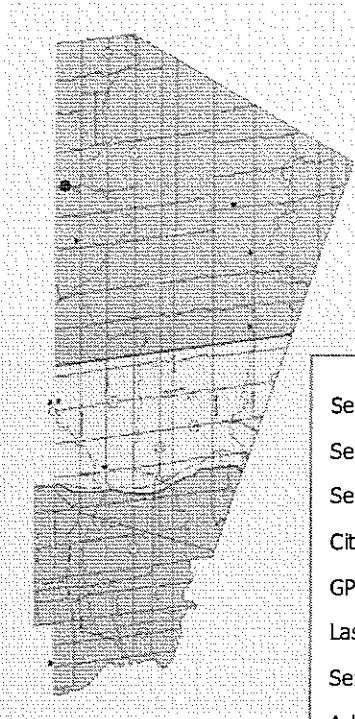
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$775
2		
3		
4	Ditching	\$600
5		
6		
Total Incl. Mobilization and Contingency :		\$1,844

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 0 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 4 m
 Ditching on Private Prop: 0 m
 Volume of HW West m3
 Volume of HW East m3
 Headwall Repair West m3
 Headwall Repair East m3
 Pre-Fab HW SA West m2
 Pre-Fab HW SA East m2
 Gabions Req. at West m3
 Gabions Req. at East m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts:
 Markers Req. Straight:
 Markers Replace/Install: 0
 Centre-Line Offset West 3.15 m
 Centre-Line Offset East 3.05 m
 Exposed Length West 0.1 m
 Exposed Length East 0 m
 Maximum Overburden: 0.2 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 1743



Section - Road: 110820 - BUSH STREET
 Section Start: SHAWS CREEK RD.
 Section End: WINSTON CHURCHILL BLVD. (REG. RD. #)
 City/Town: CALEDON
 GPS Coord: 578712 E 4848736 N
 Last Inspected: 8/23/2005
 Service Type: Cross
 Address/Cross Road: N/A
 Side of Road: N/A

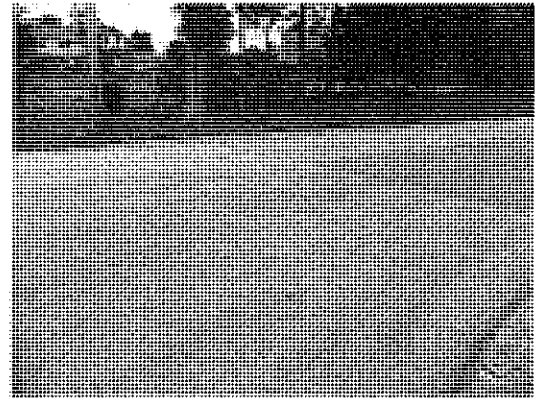
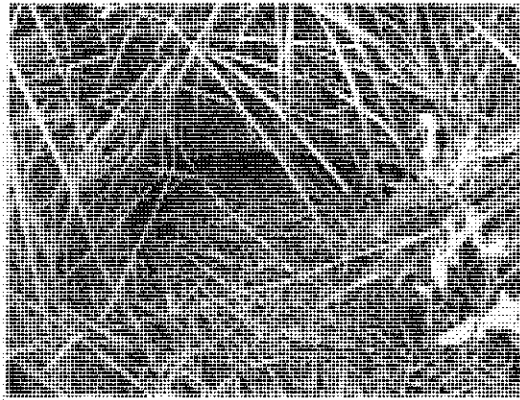
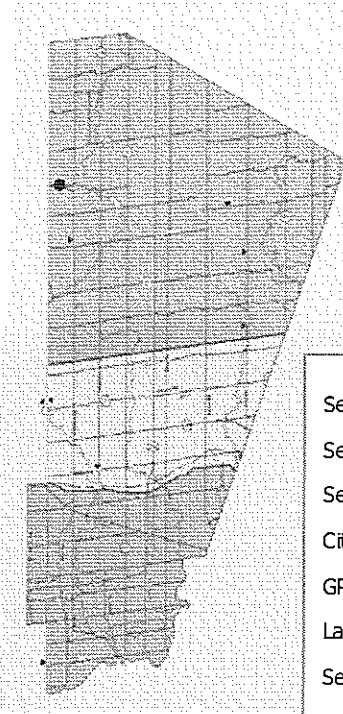
Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at South Pre-Fab Headwall at South
 No Headwall Present at North Pre-Fab Headwall at North
 Concrete Headwall at South Gabion Headwall at South
 Concrete Headwall at North Gabion Headwall at North
 Barriers Present Marker Posts

1	Do Nothing	\$0
2		
3		
4		
5		
6	Replace/Install Marker Posts	\$20
Total Incl. Mobilization and Contingency :		\$150

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 90 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required: 0 m
 Ditching on Private Prop: m
 Volume of HW South: m3
 Volume of HW North: m3
 Headwall Repair South: m3
 Headwall Repair North: m3
 Pre-Fab HW SA South: m2
 Pre-Fab HW SA North: m2
 Gabions Req. at South: m3
 Gabions Req. at North: m3
 Total Barrier Length: 100 m
 Barriers Req. Repair: 0 m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 1
 Markers Req. Straight: 0
 Markers Replace/Install: 2
 Centre-Line Offset South: 15 m
 Centre-Line Offset North: 15 m
 Exposed Length South: 0.1 m
 Exposed Length North: 0.1 m
 Maximum Overburden: 6.9 m
 Nominal Diameter: 0.9 m
 Maximum Span: m
 Interior Height: m

CULVERT NO. 1744



Section - Road: 110820 - BUSH STREET
 Section Start: SHAWS CREEK RD.
 Section End: WINSTON CHURCHILL BLVD. (REG. RD. #)
 City/Town: CALEDON
 GPS Coord: 578825 E 4848890 N
 Last Inspected: 8/23/2005
 Service Type: Intersection
 Address/Cross Road: Shaw Creek Rd
 Side of Road: South

Shape/Type: Round
 Material: Corrugated Steel
 Surface: A B C
 No Headwall Present at West Pre-Fab Headwall at West
 No Headwall Present at East Pre-Fab Headwall at East
 Concrete Headwall at West Gabion Headwall at West
 Concrete Headwall at East Gabion Headwall at East
 Barriers Present Marker Posts

1	Flush/Clean	\$1,800
2		
3		
4	Ditching	\$300
5		
6	Replace/Install Marker Posts	\$10
Total Incl. Mobilization and Contingency :		\$2,763

Immediately
 This Year
 1 - 2 Years
 3 - 5 Years
 6 - 10 Years
 11+ Years
 N/A

Effective Cross-Section: 15 %
 % Req. Replacement: 0 %
 Cross Section:
 Area Req. Erosion Cntrl: 0 m2
 Total Ditching Required : 2 m
 Ditching on Private Prop: 0 m
 Volume of HW West m3
 Volume of HW East m3
 Headwall Repair West m3
 Headwall Repair East m3
 Pre-Fab HW SA West m2
 Pre-Fab HW SA East m2
 Gabions Req. at West m3
 Gabions Req. at East m3
 Total Barrier Length: m
 Barriers Req. Repair: m
 Barriers Replace/Install: 0 m
 Number of Marker Posts: 1
 Markers Req. Straight: 0
 Markers Replace/Install: 1
 Centre-Line Offset West: 7.15 m
 Centre-Line Offset East: 7.25 m
 Exposed Length West: 0 m
 Exposed Length East: 0.1 m
 Maximum Overburden: 0.5 m
 Nominal Diameter: 0.4 m
 Maximum Span: m
 Interior Height: m

Appendix B
VO2 Hydrologic Modelling Input Parameters
for Cross Culverts

Table B-1: VO2 Parameters for Cross Culverts									VO2 Results: Peak Flow (m ³ /s)					
Culvert ID #	VO2 ID #	Area (ha)	Total Area (ha)	CN	la (mm)	Tc (hr)	Tp (hr)	Comments	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
10	21	8.81	8.81	68.3	6.5	2.035	1.357		0.079	0.134	0.177	0.235	0.287	0.333
14	22	3.01	-	71.6	5.2	0.083	0.056	Ineffective Depression Area ¹	-	-	-	-	-	-
14	24	5.03	-	72.5	4.8	0.118	0.079	Ineffective Depression Area ¹	-	-	-	-	-	-
14	27	0.68	-	72.2	4.9	0.083	0.056	Ineffective Depression Area ¹	-	-	-	-	-	-
14	30	5.57	12.27	69.8	6.1	0.083	0.056		0.243	0.432	0.598	0.827	1.019	1.204
14	32	6.71		64.3	8.7	0.480	0.320							
14	31	-		channel routing: length = 477 m, slope = 0.0168 m/m; width = 85 m										
16	34	2.15	4.23	71.9	5.0	0.155	0.103		0.193	0.329	0.438	0.59	0.721	0.845
16	36	2.08		67.6	7.7	0.127	0.085							
16	35	-		channel routing: length = 107 m, slope = 0.0248 m/m; width = 70 m										
17	40	3.95	-	54.0	10.0	0.603	0.402	Ineffective Depression Area ¹	-	-	-	-	-	-
17	39	35.03	35.03	65.5	7.2	1.741	1.161		0.311	0.539	0.719	0.961	1.182	1.376
24	42	0.56	-	70.0	5.0	0.083	0.055	Ineffective Depression Area ¹	-	-	-	-	-	-
24	44	0.87	-	64.6	6.7	0.083	0.055	Ineffective Depression Area ¹	-	-	-	-	-	-
24	47	0.48	-	70.0	5.0	0.083	0.055	Ineffective Depression Area ¹	-	-	-	-	-	-
24	49	2.77	2.77	70.7	5.4	0.167	0.111		0.145	0.241	0.314	0.411	0.49	0.568
37	50	11.96	21.05	66.4	5.7	0.268	0.179	Effective Depression Area ²	0.311	0.504	0.650	1.42	1.875	3.285
37	52	3.90		69.4	4.9	0.107	0.071	Effective Depression Area ²						
37	55	5.19		73.3	4.0	0.167	0.111							
37	56	-		(Roadside ditch) channel routing: length = 354 m, slope = 0.0335 m/m; width = 2.5 m										
43	67	1.52	48.56	62.0	8.0	0.088	0.059	Effective Depression Area ²	0.529	0.918	1.370	2.678	3.366	4.985
43	69	1.80		58.8	8.5	0.103	0.069	Effective Depression Area ²						
43	72	24.19		60.0	8.6	0.553	0.369							
43	66	21.05		Includes area from culvert # 37										
44	76	127.28	127.28	59.9	8.3	1.178	0.785		1.186	2.119	2.872	3.908	4.855	5.701
47	82	0.24	0.24	77.6	3.5	0.167	0.111		0.017	0.027	0.034	0.044	0.052	0.059
48	78	2.66	17.52	59.8	8.6	0.107	0.071	Effective Depression Area ²	0.155	0.282	0.386	0.530	0.661	0.874
48	80	14.63		58.0	9.4	0.858	0.572							
48	83	0.24		Includes area from culvert # 48										
55	84	7.71	7.71	62.5	9.1	0.436	0.291		0.149	0.268	0.365	0.497	0.614	0.722
56	85	0.91	0.91	64.9	8.5	0.167	0.111		0.034	0.06	0.08	0.108	0.131	0.154
2	86	19.15	19.15	71.3	5.8	0.366	0.244		0.654	1.097	1.438	1.9	2.288	2.647

Table B-2: Time of Concentration (T_c) Calculations for Cross Culverts

1) Kirpich's Equation for Estimating T _c : $T_c \text{ (min)} = 0.0195 (L^{0.177}) / (S^{0.385})$ where length (L) in metres, slope (S) in m/m															
Note for using Kirpich's Eqn: For overland flow, grassed surfaces, multiply T _c by 2. For overland flow, concrete or asphalt surfaces, multiply T _c by 0.4. For concrete channels, multiply T _c by 0.2. (Reference: Modern Sewer Design, 1980)															
2) SCS Upland Method of Estimating T _c :															
Code	Description												Velocity (m/s)		
1	Forest with heavy ground litter & hay meadow (overland flow)												$=2.5 \cdot (s^{0.5}) \cdot 0.3048$		
2	Trash fallow or min tillage cultivation; contour or strip cropped & woodland (overland flow)												$=5.0 \cdot (s^{0.5}) \cdot 0.3048$		
3	Short grass pasture (overland flow)												$=7.0 \cdot (s^{0.5}) \cdot 0.3048$		
4	Cultivated, straight row (overland flow)												$=9.0 \cdot (s^{0.5}) \cdot 0.3048$		
5	Nearly bare and untilled (overland flow); & alluvial fans western mountain regions												$=10.0 \cdot (s^{0.5}) \cdot 0.3048$		
6	Grassed waterway												$=15.0 \cdot (s^{0.5}) \cdot 0.3048$		
7	Paved areas (sheet flow); & small upland gullies												$=20.0 \cdot (s^{0.5}) \cdot 0.3048$		
Elevation															
Culvert ID #	Area (ha)	E1 (m)	E2 (m)	change (m)	Length (m)	Overland slope (m/m)	Land Use	Tc Method	Weighted overland slope (m/m)	SCS Upland GND cover - Code	Overland velocity (see chart) (m/s)	Travel time (min)	Time of Conc (min)	Time of Conc (hr)	
10	5.07	403	385.5	17.5	249	0.0703	Crop Field	SCS Upland	0.0703	4	0.73	5.70	122.08	2.035	
	3.74	385.5	384.6	0.9	294	0.0031	Forest	SCS Upland	0.0031	1	0.04	116.4			
14	5.57	406	389	17	152.33	0.1116	Crop Field	SCS Upland	0.1116	4	0.92	2.77	Use 5 min to depression area ²	0.083	
	3.01	404.0	397	7	77	0.0905	Crop Field	SCS Upland	0.0905	4	0.83	1.56	Use 5 min to depression area ²	0.083	
	5.03	405.0	390	15	274	0.0548	Crop Field	SCS Upland	0.0548	4	0.64	7.11	7.11	0.118	
	0.68	394.5	390	4.5	49	0.0924	Crop Field	SCS Upland	0.0924	4	0.83	0.97	Use 5 min to depression area ²	0.083	
	6.71	389	381	8	477	0.0168	Woodland/Pasture	SCS Upland	0.0168	3	0.28	28.8	28.81	0.480	
17	421	410	11	208	0.0528	Woodland	SCS Upland	0.0528	1	0.18	19.85	104.47	1.741		
	35.0	410	404	6	419	0.0143	Crop Field	SCS Upland	0.0143	4	0.33			21.29	
	404	385.1	18.9	541	0.0349	Forest	SCS Upland	0.0349	1	0.14	63.33				
	3.95	430	415	15	345	0.0435	Woodland	SCS Upland	0.0435	1	0.16			36.19	36.19
24	2.77	436	428.4	7.6	139	0.0547	Lawn	SCS Upland	0.0547	3	0.50	4.64	Use minimum 10 minutes inlet time ¹	0.167	
	0.56	n/a	n/a	n/a	n/a	n/a	Lawn	SCS Upland	n/a	n/a	n/a	n/a	Use 5 min to depression area ²	0.083	
	0.87	n/a	n/a	n/a	n/a	n/a	Lawn	SCS Upland	n/a	n/a	n/a	n/a	Use 5 min to depression area ²	0.083	
	0.48	n/a	n/a	n/a	n/a	n/a	Lawn	SCS Upland	n/a	n/a	n/a	n/a	Use 5 min to depression area ²	0.083	
	11.96	434	427	7.0	309	0.0226	Lawn	SCS Upland	0.0226	3	0.32	16.07	16.07	0.268	
37	3.90	434	425	9.0	192	0.0468	Pasture	SCS Upland	0.0468	3	0.46	6.93	6.93	0.116	
	5.19	430	421.6	8.4	209	0.0402	Crop Field	SCS Upland	0.0402	4	0.55	6.34	10.04	0.167	
	n/a	n/a	n/a	155	0.0131	Ditch	SCS Upland	0.0131	7	0.70	3.70				
	1.52	433	427	6	127	0.0472	Pasture	Kirpich's Eqn	0.0472	n/a	n/a	5.26	5.26	0.088	
1.80	432	421	11.0	178	0.0618	Forest	Kirpich's Eqn	0.0618	n/a	n/a	6.16	6.16	0.103		
43	24.19	427	400.2	26.8	1030	0.0260	Forest & Pasture	Kirpich's Eqn	0.0260	n/a	n/a	33.19	33.19	0.553	
	127.27	445	399.7	45.3	2360	0.0192	Woodland & Pasture	Kirpich's Eqn	0.0192	n/a	n/a	70.66	70.66	1.178	
48	2.66	409	398	11	185	0.0595	Pasture	Kirpich's Eqn	0.0595	n/a	n/a	6.44	6.44	0.107	
	14.62	402	398.5	3.5	764	0.0046	Pasture & Woodland	Kirpich's Eqn	0.0046	n/a	n/a	51.47	51.47	0.858	
47	0.24	402	400	2	43	0.0462	Lawn	assume sheet flow	0.0462	3	0.46	1.57	Use minimum 10 minutes inlet time for cross culverts ¹	0.167	
	400	398.5	1.5	45	0.0331	Ditch	assume conc. flow	0.0331	7	1.11	0.68				
55	401	399	2	100	0.0200	Woodland	SCS Upland	0.0200	2	0.22	7.73	26.18	0.436		
	399	391.55	7.45	292	0.0255	Woodland	SCS Upland	0.0171	6	0.60	11.69				
	391.55	390	1.55	127	0.0122	Woodland	SCS Upland								
	389.5	388.8	0.7	162	0.0043	Ditch	SCS Upland							0.0043	7
56	393.3	389.5	3.8	100	0.0380	Woodland	SCS Upland					0.0380	2	0.30	5.61
	389.5	389	0.5	56	0.0089	Woodland	SCS Upland	0.0089	6	0.43	2.17				
	389	387.4	1.6	49	0.0325	Ditch	SCS Upland	0.0325	7	1.10	0.75				
16	405	398	7	185	0.0378	Crop Field	SCS Upland	0.0378	4	0.53	5.80	9.28	0.155		
	398	390	8	59	0.1360	Woodland	SCS Upland	0.1360	1	0.28	3.49				
	390	386.2	3.8	154	0.0248	Meadow/Pasture	SCS Upland	0.0248	3	0.34	7.62			7.62	0.127

2	19.15	411	408	3	96	0.0312	Pasture	SCS Upland	0.0312	3	0.38	4.26	21.98	0.366
		408	405.81	2.2	79	0.0277	Woodland	SCS Upland	0.0277	6	0.76	1.73		
		405.81	389	16.8	687	0.0245	Crop Field	SCS Upland	0.0245	6	0.72	16.0		
Note:														
1. Cross culverts are to be designed with a minimum inlet time of 10 minutes (Region of Peel Standards/Guidelines)														
2. A minimum tc of 5 minutes is assumed for areas draining to depression areas that act as ponds.														

Table B-3: CN and Initial Abstraction (Ia) Parameters for Cross Culverts

CVC Standard Parameters:															
Cover	CN Value for Soil Group AB ¹	CN Value for Soil Group B	Ia (mm)												
Woods	54	60	10												
Meadows	62	66	8												
Cultivated	70	74	4												
Lawns	70	71	5												
Impervious area	100	100	2												
Note: 1. CN Values for Soil Group AB not available from CVC Guidelines; CN values from MTO Drainage Manual, Design Chart 1.09															
Culvert ID #	Area (m ²)	Total Area (m ²)	Soil Group	Land Use	CN	Ia (mm)	Area-weighted CN	Area-weighted Ia (mm)	Comments						
10	50674	88099	B	Crop	74	4	68.28	6.5							
10	36914		B	Forest	60	10									
10	511		B	Road	100	2									
14	20914	30091	B	Crop	74	4	71.56	5.2	Ineffective Depression Area						
14	9177		B	Meadows	66	8									
14	9483		B	Meadows	66	8									
14	40842	50325	B	Crop	74	4	72.49	4.8	Ineffective Depression Area						
14	1550		B	Meadows	66	8									
14	5226		B	Crop	74	4									
14	29493	55677	B	Meadows	66	8	69.76	6.1							
14	26184		B	Crop	74	4									
14	1428		B	Road	100	2									
14	27086	67062	B	Woodland	60	10	64.3	8.7							
14	38548		B	Meadows	66	8									
17	39521		AB	Forest	54	10									
17	58122	350250	AB	Forest	54	10	65.48	7.2	Ineffective Depression Area						
17	28645		AB	Crop	70	4									
17	2884		AB	Forest	54	10									
17	10174		AB	Meadows	62	8									
17	131		AB	Road	100	2									
17	121		AB	Road	100	2									
17	1137		AB	Road	100	2									
17	585		AB	Road	100	2									
17	125541		B	Crop	74	4									
17	119360		B	Woodland	60	10									
17	864		B	Road	100	2									
17	2686		B	Road	100	2									
24	5557		5557	AB	Lawn	70					5	70	5	Ineffective Depression Area	
24	2917		8680	AB	Forest	54					10	64.62	6.7	Ineffective Depression Area	
24	5763			AB	Lawn	70					5				
24	4821	AB		Lawn	70	5									
24	21786	27698	AB	Lawn	70	5	70.73	5.4	Ineffective Depression Area						
24	3414		AB	Forest	54	10									
24	2498		AB	Road	100	2									
37	68926	119566	AB	Crop	70	4	66.44	5.7							
37	33718		AB	Woodland	54	10									
37	13132		AB	Lawn	70	5									
37	3790		AB	Road	100	2									
37	28246	38997	AB	Crop	70	4	69.43	4.9	Effective Depression Area						
37	9077		AB	Meadow	62	8									
37	1674		AB	Impervious	100	2									
37	41999		AB	Crop	70	4									
37	3322	51917	AB	Meadow	62	8	73.30	4							
37	6596		AB	Road	100	2									
43	15215		15215	AB	Meadows	62					8	62	8	Effective Depression Area	
43	12540	17986	AB	Woodland	54	10	58.84	8.49	Effective Depression Area						
43	5446		AB	Lawn	70	5									
43	7568		AB	Road	100	2									
43	97938	241924	AB	Woodland	54	10	59.95	8.62							
43	136418		AB	Meadows	62	8									
44	335578	1272760	AB	Meadows	62	8	59.91	8.29							
44	302202		AB	Lawn	70	5									
44	634980		AB	Woodland	54	10									
47	1768	2368	AB	ImprovedLand	70	4	77.61	3.49							
47	600		AB	Road	100	2									
48	19265	26587	AB	Meadows	62	8	59.80	8.55	Effective Depression Area						
48	7322		AB	Woodland	54	10									
48	2188		AB	Road	100	2									
48	5332	146246	AB	Meadows	62	8	58.04	9.37							
48	12884		AB	Lawn	70	5									
48	85514		AB	Woodland	54	10									
48	40328		B	Woodland	60	10									
55	66654	77101	B	Woodland	60	10	62.45	9.14							
55	8799		B	Cultivated	74	4									
55	1647		B	Road	100	2									
56	7071	9092	B	Woodland	60	10	64.87	8.53							
56	1407		B	Cultivated	74	4									
56	615		B	Road	100	2									
16	5528	21482	B	Woodland	66	8	71.94	5.03							
16	15954		B	Crop	74	4									
16	996	20803	B	Road	100	2	67.63	7.71							
16	19807		B	Meadows	66	8									
2	56550		B	Meadows	66	8									

2	23511	191486	B	Woodland	60	10	71.27	5.81	
2	9951		B	Road	100	2			
2	101475		B	Crop	74	4			

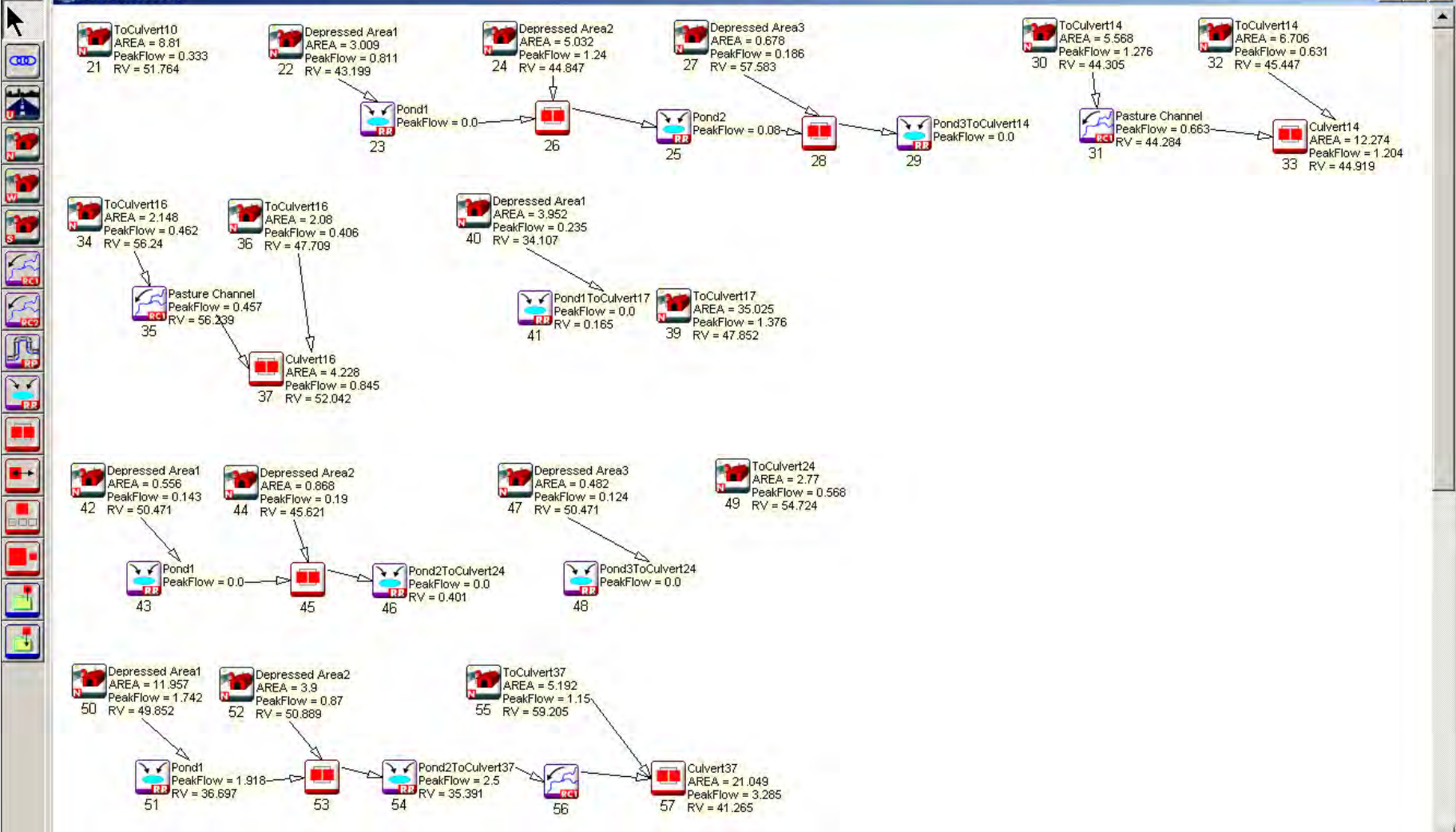
Appendix C
VO2 Hydrologic Modelling Outputs
for Cross Culverts

Visual OTTHYMO 2.0

File Edit View Project Analysis Tools Window Help

100%

Scenario 1

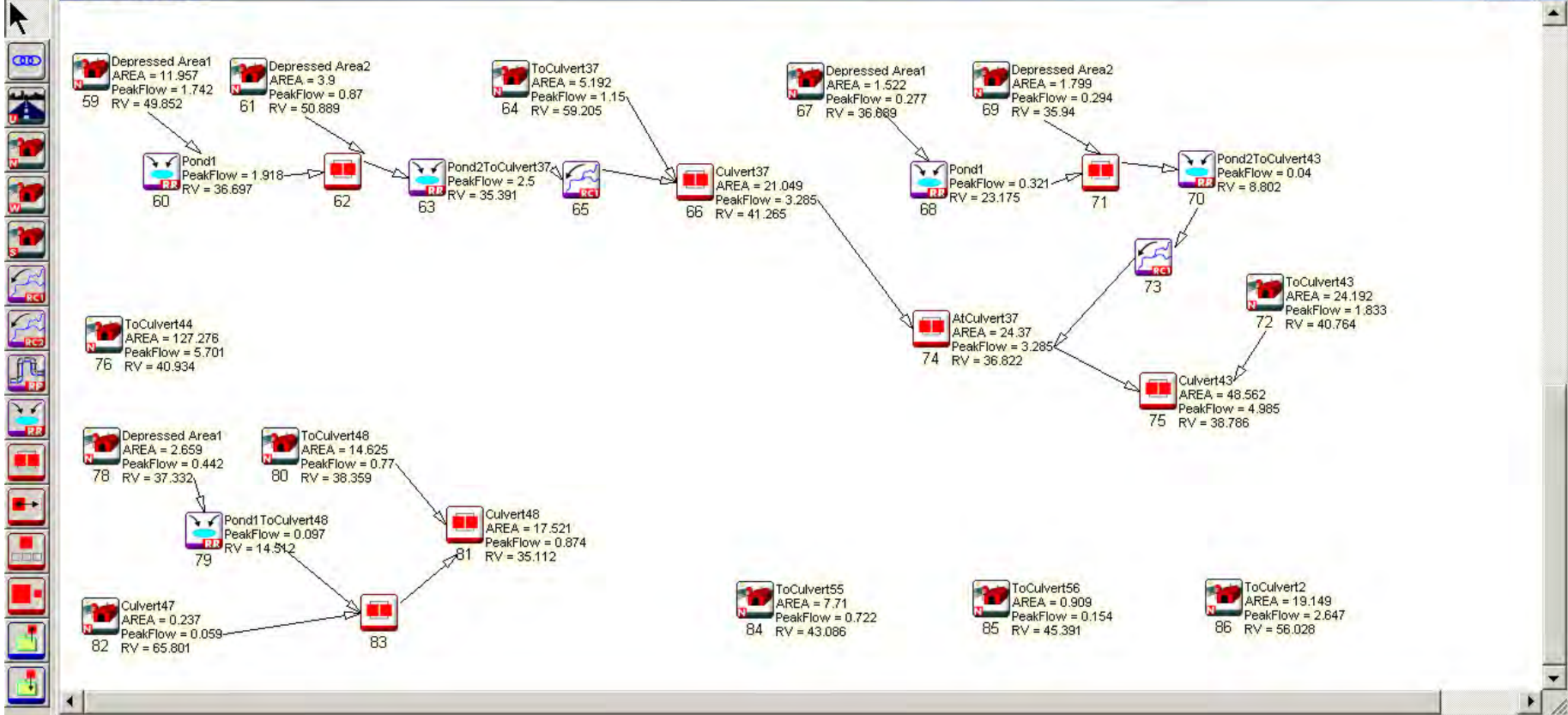


Visual OTTHYMO 2.0

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Scenario1




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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files\visual OTTHYMO v2.0\voin.dat

Output filename: m:\PROJECTS\DRAFT\10\103121 Bush Street and Mississauga
 Rd\SWM\WRmodels\VO2\100602_MajorCrossing\Scenario1.out
 Summary filename: m:\PROJECTS\DRAFT\10\103121 Bush Street and Mississauga
 Rd\SWM\WRmodels\VO2\100602_MajorCrossing\Scenario1.sum

DATE: 6/9/2010 TIME: 9:48:35 AM

USER:

COMMENTS: _____

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*****
** SIMULATION NUMBER: 1 **
*****

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-----
| CHICAGO STORM |
| Ptotal= 55.10 mm |
-----

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```

IDF curve parameters: A= 674.573
                     B= 6.012
                     C= .781
used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
Storm time step = 5.00 min
Time to peak ratio = .49

```

The CORRELATION coefficient is = .9996

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	102.00	103.59
10.	80.00	77.33
15.	64.00	62.54
30.	41.00	41.06
60.	24.00	25.58
120.	16.00	15.44
360.	6.30	6.71
720.	3.90	3.93
1440.	2.40	2.30

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.51	6.08	.91	12.08	11.16	18.08	.87
.17	.51	6.17	.92	12.17	9.01	18.17	.86
.25	.52	6.25	.93	12.25	7.59	18.25	.85
.33	.52	6.33	.94	12.33	6.58	18.33	.84
.42	.52	6.42	.96	12.42	5.82	18.42	.83
.50	.53	6.50	.97	12.50	5.22	18.50	.82
.58	.53	6.58	.98	12.58	4.75	18.58	.81
.67	.53	6.67	.99	12.67	4.36	18.67	.81
.75	.54	6.75	1.01	12.75	4.04	18.75	.80
.83	.54	6.83	1.02	12.83	3.76	18.83	.79
.92	.54	6.92	1.03	12.92	3.53	18.92	.78
1.00	.55	7.00	1.05	13.00	3.32	19.00	.78
1.08	.55	7.08	1.06	13.08	3.14	19.08	.77
1.17	.55	7.17	1.08	13.17	2.98	19.17	.76
1.25	.56	7.25	1.10	13.25	2.84	19.25	.76
1.33	.56	7.33	1.11	13.33	2.71	19.33	.75
1.42	.56	7.42	1.13	13.42	2.59	19.42	.74
1.50	.57	7.50	1.15	13.50	2.49	19.50	.74

1.58	.57	7.58	1.17	13.58	2.39	19.58	.73
1.67	.57	7.67	1.19	13.67	2.30	19.67	.72
1.75	.58	7.75	1.21	13.75	2.22	19.75	.72
1.83	.58	7.83	1.23	13.83	2.15	19.83	.71
1.92	.59	7.92	1.25	13.92	2.08	19.92	.71
2.00	.59	8.00	1.27	14.00	2.01	20.00	.70
2.08	.59	8.08	1.29	14.08	1.95	20.08	.69
2.17	.60	8.17	1.32	14.17	1.90	20.17	.69
2.25	.60	8.25	1.34	14.25	1.84	20.25	.68
2.33	.61	8.33	1.37	14.33	1.80	20.33	.68
2.42	.61	8.42	1.40	14.42	1.75	20.42	.67
2.50	.62	8.50	1.43	14.50	1.70	20.50	.67
2.58	.62	8.58	1.46	14.58	1.66	20.58	.66
2.67	.62	8.67	1.49	14.67	1.62	20.67	.66
2.75	.63	8.75	1.53	14.75	1.59	20.75	.65
2.83	.63	8.83	1.56	14.83	1.55	20.83	.65
2.92	.64	8.92	1.60	14.92	1.52	20.92	.64
3.00	.64	9.00	1.64	15.00	1.49	21.00	.64
3.08	.65	9.08	1.68	15.08	1.46	21.08	.63
3.17	.65	9.17	1.73	15.17	1.43	21.17	.63
3.25	.66	9.25	1.77	15.25	1.40	21.25	.63
3.33	.66	9.33	1.82	15.33	1.37	21.33	.62
3.42	.67	9.42	1.88	15.42	1.35	21.42	.62
3.50	.67	9.50	1.94	15.50	1.32	21.50	.61
3.58	.68	9.58	2.00	15.58	1.30	21.58	.61
3.67	.69	9.67	2.07	15.67	1.28	21.67	.60
3.75	.69	9.75	2.14	15.75	1.25	21.75	.60
3.83	.70	9.83	2.21	15.83	1.23	21.83	.60
3.92	.70	9.92	2.30	15.92	1.21	21.92	.59
4.00	.71	10.00	2.39	16.00	1.19	22.00	.59
4.08	.71	10.08	2.49	16.08	1.17	22.08	.59
4.17	.72	10.17	2.60	16.17	1.16	22.17	.58
4.25	.73	10.25	2.73	16.25	1.14	22.25	.58
4.33	.73	10.33	2.86	16.33	1.12	22.33	.57
4.42	.74	10.42	3.02	16.42	1.11	22.42	.57
4.50	.75	10.50	3.19	16.50	1.09	22.50	.57
4.58	.75	10.58	3.39	16.58	1.08	22.58	.56
4.67	.76	10.67	3.61	16.67	1.06	22.67	.56
4.75	.77	10.75	3.88	16.75	1.05	22.75	.56
4.83	.78	10.83	4.19	16.83	1.03	22.83	.55
4.92	.78	10.92	4.56	16.92	1.02	22.92	.55
5.00	.79	11.00	5.01	17.00	1.01	23.00	.55
5.08	.80	11.08	5.58	17.08	.99	23.08	.54
5.17	.81	11.17	6.31	17.17	.98	23.17	.54
5.25	.82	11.25	7.28	17.25	.97	23.25	.54
5.33	.82	11.33	8.65	17.33	.96	23.33	.53
5.42	.83	11.42	10.72	17.42	.95	23.42	.53
5.50	.84	11.50	14.20	17.50	.93	23.50	.53
5.58	.85	11.58	21.19	17.58	.92	23.58	.53
5.67	.86	11.67	41.67	17.67	.91	23.67	.52
5.75	.87	11.75	103.59	17.75	.90	23.75	.52
5.83	.88	11.83	42.36	17.83	.89	23.83	.52
5.92	.89	11.92	21.91	17.92	.88	23.92	.51
6.00	.90	12.00	14.75	18.00	.87	24.00	.51

CALIB							
NASHYD	(0021)	Area	(ha)= 8.81	Curve Number	(CN)= 68.3		
ID= 1 DT= 5.0 min		Ia	(mm)= 6.50	# of Linear Res.(N)=	3.00		
		U.H. Tp(hrs)=	1.36				

Unit Hyd Qpeak (cms)= .248

PEAK FLOW (cms)= .079 (i)
 TIME TO PEAK (hrs)= 13.333
 RUNOFF VOLUME (mm)= 14.177
 TOTAL RAINFALL (mm)= 55.099
 RUNOFF COEFFICIENT = .257

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD	(0027)	Area	(ha)= .68	Curve Number	(CN)= 72.2		
ID= 1 DT= 2.0 min		Ia	(mm)= 4.91	# of Linear Res.(N)=	3.00		
		U.H. Tp(hrs)=	.06				

NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.033	.51	6.033	.91	12.033	11.16	18.03	.87
.067	.51	6.067	.91	12.067	11.16	18.07	.87
.100	.51	6.100	.92	12.100	10.08	18.10	.86

.133	.51	6.133	.92	12.133	9.01	18.13	.86
.167	.51	6.167	.92	12.167	9.01	18.17	.86
.200	.52	6.200	.93	12.200	7.59	18.20	.85
.233	.52	6.233	.93	12.233	7.59	18.23	.85
.267	.52	6.267	.94	12.267	7.08	18.27	.84
.300	.52	6.300	.94	12.300	6.58	18.30	.84
.333	.52	6.333	.94	12.333	6.57	18.33	.84
.367	.52	6.367	.96	12.367	5.82	18.37	.83
.400	.52	6.400	.96	12.400	5.82	18.40	.83
.433	.53	6.433	.96	12.433	5.52	18.43	.83
.467	.53	6.467	.97	12.467	5.22	18.47	.82
.500	.53	6.500	.97	12.500	5.22	18.50	.82
.533	.53	6.533	.98	12.533	4.75	18.53	.81
.567	.53	6.567	.98	12.567	4.75	18.57	.81
.600	.53	6.600	.99	12.600	4.56	18.60	.81
.633	.53	6.633	.99	12.633	4.36	18.63	.81
.667	.53	6.667	.99	12.667	4.36	18.67	.81
.700	.54	6.700	1.01	12.700	4.04	18.70	.80
.733	.54	6.733	1.01	12.733	4.04	18.73	.80
.767	.54	6.767	1.01	12.767	3.90	18.77	.79
.800	.54	6.800	1.02	12.800	3.76	18.80	.79
.833	.54	6.833	1.02	12.833	3.76	18.83	.79
.867	.54	6.867	1.03	12.867	3.53	18.87	.78
.900	.54	6.900	1.03	12.900	3.53	18.90	.78
.933	.54	6.933	1.04	12.933	3.42	18.93	.78
.967	.55	6.967	1.05	12.967	3.32	18.97	.78
1.000	.55	7.000	1.05	13.000	3.32	19.00	.78
1.033	.55	7.033	1.06	13.033	3.14	19.03	.77
1.067	.55	7.067	1.06	13.067	3.14	19.07	.77
1.100	.55	7.100	1.07	13.100	3.06	19.10	.77
1.133	.55	7.133	1.08	13.133	2.98	19.13	.76
1.167	.55	7.167	1.08	13.167	2.98	19.17	.76
1.200	.56	7.200	1.10	13.200	2.84	19.20	.76
1.233	.56	7.233	1.10	13.233	2.84	19.23	.76
1.267	.56	7.267	1.10	13.267	2.77	19.27	.75
1.300	.56	7.300	1.11	13.300	2.71	19.30	.75
1.333	.56	7.333	1.11	13.333	2.71	19.33	.75
1.367	.56	7.367	1.13	13.367	2.59	19.37	.74
1.400	.56	7.400	1.13	13.400	2.59	19.40	.74
1.433	.57	7.433	1.14	13.433	2.54	19.43	.74
1.467	.57	7.467	1.15	13.467	2.49	19.47	.74
1.500	.57	7.500	1.15	13.500	2.49	19.50	.74
1.533	.57	7.533	1.17	13.533	2.39	19.53	.73
1.567	.57	7.567	1.17	13.567	2.39	19.57	.73
1.600	.57	7.600	1.18	13.600	2.35	19.60	.73
1.633	.57	7.633	1.19	13.633	2.30	19.63	.72
1.667	.57	7.667	1.19	13.667	2.30	19.67	.72
1.700	.58	7.700	1.21	13.700	2.22	19.70	.72
1.733	.58	7.733	1.21	13.733	2.22	19.73	.72
1.767	.58	7.767	1.22	13.767	2.19	19.77	.71
1.800	.58	7.800	1.23	13.800	2.15	19.80	.71
1.833	.58	7.833	1.23	13.833	2.15	19.83	.71
1.867	.59	7.867	1.25	13.867	2.08	19.87	.71
1.900	.59	7.900	1.25	13.900	2.08	19.90	.71
1.933	.59	7.933	1.26	13.933	2.05	19.93	.70
1.967	.59	7.967	1.27	13.967	2.01	19.97	.70
2.000	.59	8.000	1.27	14.000	2.01	20.00	.70
2.033	.59	8.033	1.29	14.033	1.95	20.03	.69
2.067	.59	8.067	1.29	14.067	1.95	20.07	.69
2.100	.60	8.100	1.31	14.100	1.93	20.10	.69
2.133	.60	8.133	1.32	14.133	1.90	20.13	.69
2.167	.60	8.167	1.32	14.167	1.90	20.17	.69
2.200	.60	8.200	1.34	14.200	1.84	20.20	.68
2.233	.60	8.233	1.34	14.233	1.84	20.23	.68
2.267	.60	8.267	1.36	14.267	1.82	20.27	.68
2.300	.61	8.300	1.37	14.300	1.80	20.30	.68
2.333	.61	8.333	1.37	14.333	1.80	20.33	.68
2.367	.61	8.367	1.40	14.367	1.75	20.37	.67
2.400	.61	8.400	1.40	14.400	1.75	20.40	.67
2.433	.61	8.433	1.41	14.433	1.73	20.43	.67
2.467	.62	8.467	1.43	14.467	1.70	20.47	.67
2.500	.62	8.500	1.43	14.500	1.70	20.50	.67
2.533	.62	8.533	1.46	14.533	1.66	20.53	.66
2.567	.62	8.567	1.46	14.567	1.66	20.57	.66
2.600	.62	8.600	1.48	14.600	1.64	20.60	.66
2.633	.62	8.633	1.49	14.633	1.62	20.63	.66
2.667	.62	8.667	1.49	14.667	1.62	20.67	.66
2.700	.63	8.700	1.53	14.700	1.59	20.70	.65
2.733	.63	8.733	1.53	14.733	1.59	20.73	.65
2.767	.63	8.767	1.54	14.767	1.57	20.77	.65
2.800	.63	8.800	1.56	14.800	1.55	20.80	.65
2.833	.63	8.833	1.56	14.833	1.55	20.83	.65
2.867	.64	8.867	1.60	14.867	1.52	20.87	.64
2.900	.64	8.900	1.60	14.900	1.52	20.90	.64
2.933	.64	8.933	1.62	14.933	1.50	20.93	.64
2.967	.64	8.967	1.64	14.967	1.49	20.97	.64
3.000	.64	9.000	1.64	15.000	1.49	21.00	.64
3.033	.65	9.033	1.68	15.033	1.46	21.03	.63
3.067	.65	9.067	1.68	15.067	1.46	21.07	.63

3.100	.65	9.100	1.70	15.100	1.44	21.10	.63
3.133	.65	9.133	1.73	15.133	1.43	21.13	.63
3.167	.65	9.167	1.73	15.167	1.43	21.17	.63
3.200	.66	9.200	1.77	15.200	1.40	21.20	.63
3.233	.66	9.233	1.77	15.233	1.40	21.23	.63
3.267	.66	9.267	1.80	15.267	1.38	21.27	.62
3.300	.66	9.300	1.82	15.300	1.37	21.30	.62
3.333	.66	9.333	1.82	15.333	1.37	21.33	.62
3.367	.67	9.367	1.88	15.367	1.35	21.37	.62
3.400	.67	9.400	1.88	15.400	1.35	21.40	.62
3.433	.67	9.433	1.91	15.433	1.33	21.43	.62
3.467	.67	9.467	1.94	15.467	1.32	21.47	.61
3.500	.67	9.500	1.94	15.500	1.32	21.50	.61
3.533	.68	9.533	2.00	15.533	1.30	21.53	.61
3.567	.68	9.567	2.00	15.567	1.30	21.57	.61
3.600	.68	9.600	2.03	15.600	1.29	21.60	.61
3.633	.69	9.633	2.07	15.633	1.28	21.63	.60
3.667	.69	9.667	2.07	15.667	1.28	21.67	.60
3.700	.69	9.700	2.14	15.700	1.25	21.70	.60
3.733	.69	9.733	2.14	15.733	1.25	21.73	.60
3.767	.69	9.767	2.18	15.767	1.24	21.77	.60
3.800	.70	9.800	2.21	15.800	1.23	21.80	.60
3.833	.70	9.833	2.21	15.833	1.23	21.83	.60
3.867	.70	9.867	2.30	15.867	1.21	21.87	.59
3.900	.70	9.900	2.30	15.900	1.21	21.90	.59
3.933	.71	9.933	2.35	15.933	1.20	21.93	.59
3.967	.71	9.967	2.39	15.967	1.19	21.97	.59
4.000	.71	10.000	2.39	16.000	1.19	22.00	.59
4.033	.71	10.033	2.49	16.033	1.17	22.03	.59
4.067	.71	10.067	2.49	16.067	1.17	22.07	.59
4.100	.72	10.100	2.55	16.100	1.17	22.10	.58
4.133	.72	10.133	2.60	16.133	1.16	22.13	.58
4.167	.72	10.167	2.60	16.167	1.16	22.17	.58
4.200	.73	10.200	2.73	16.200	1.14	22.20	.58
4.233	.73	10.233	2.73	16.233	1.14	22.23	.58
4.267	.73	10.267	2.80	16.267	1.13	22.27	.58
4.300	.73	10.300	2.86	16.300	1.12	22.30	.57
4.333	.73	10.333	2.86	16.333	1.12	22.33	.57
4.367	.74	10.367	3.02	16.367	1.11	22.37	.57
4.400	.74	10.400	3.02	16.400	1.11	22.40	.57
4.433	.74	10.433	3.10	16.433	1.10	22.43	.57
4.467	.75	10.467	3.19	16.467	1.09	22.47	.57
4.500	.75	10.500	3.19	16.500	1.09	22.50	.57
4.533	.75	10.533	3.39	16.533	1.08	22.53	.56
4.567	.75	10.567	3.39	16.567	1.08	22.57	.56
4.600	.76	10.600	3.50	16.600	1.07	22.60	.56
4.633	.76	10.633	3.61	16.633	1.06	22.63	.56
4.667	.76	10.667	3.61	16.667	1.06	22.67	.56
4.700	.77	10.700	3.88	16.700	1.05	22.70	.56
4.733	.77	10.733	3.88	16.733	1.05	22.73	.56
4.767	.77	10.767	4.03	16.767	1.04	22.77	.56
4.800	.78	10.800	4.19	16.800	1.03	22.80	.55
4.833	.78	10.833	4.19	16.833	1.03	22.83	.55
4.867	.78	10.867	4.56	16.867	1.02	22.87	.55
4.900	.78	10.900	4.56	16.900	1.02	22.90	.55
4.933	.79	10.933	4.79	16.933	1.01	22.93	.55
4.967	.79	10.967	5.01	16.967	1.01	22.97	.55
5.000	.79	11.000	5.01	17.000	1.01	23.00	.55
5.033	.80	11.033	5.58	17.033	.99	23.03	.54
5.067	.80	11.067	5.58	17.067	.99	23.07	.54
5.100	.80	11.100	5.95	17.100	.99	23.10	.54
5.133	.81	11.133	6.31	17.133	.98	23.13	.54
5.167	.81	11.167	6.31	17.167	.98	23.17	.54
5.200	.82	11.200	7.28	17.200	.97	23.20	.54
5.233	.82	11.233	7.28	17.233	.97	23.23	.54
5.267	.82	11.267	7.97	17.267	.96	23.27	.54
5.300	.82	11.300	8.65	17.300	.96	23.30	.53
5.333	.82	11.333	8.66	17.333	.96	23.33	.53
5.367	.83	11.367	10.72	17.367	.95	23.37	.53
5.400	.83	11.400	10.72	17.400	.95	23.40	.53
5.433	.84	11.433	12.46	17.433	.94	23.43	.53
5.467	.84	11.467	14.20	17.467	.93	23.47	.53
5.500	.84	11.500	14.20	17.500	.93	23.50	.53
5.533	.85	11.533	21.19	17.533	.92	23.53	.53
5.567	.85	11.567	21.19	17.567	.92	23.57	.53
5.600	.86	11.600	31.45	17.600	.92	23.60	.52
5.633	.86	11.633	41.67	17.633	.91	23.63	.52
5.667	.86	11.667	41.75	17.667	.91	23.67	.52
5.700	.87	11.700	103.59	17.700	.90	23.70	.52
5.733	.87	11.733	103.59	17.733	.90	23.73	.52
5.767	.87	11.767	72.90	17.767	.90	23.77	.52
5.800	.88	11.800	42.36	17.800	.89	23.80	.52
5.833	.88	11.833	42.33	17.833	.89	23.83	.52
5.867	.89	11.867	21.91	17.867	.88	23.87	.51
5.900	.89	11.900	21.91	17.900	.88	23.90	.51
5.933	.89	11.933	18.32	17.933	.88	23.93	.51
5.967	.90	11.967	14.75	17.967	.87	23.97	.51
6.000	.90	12.000	14.74	18.000	.87	24.00	.51

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .051 (i)
TIME TO PEAK (hrs)= 11.767
RUNOFF VOLUME (mm)= 16.873
TOTAL RAINFALL (mm)= 55.099
RUNOFF COEFFICIENT = .306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0024)	Area (ha)=	5.03	Curve Number (CN)=	72.5
ID= 1 DT= 2.0 min	Ia (mm)=	4.75	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.08		

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= .335 (i)
TIME TO PEAK (hrs)= 11.800
RUNOFF VOLUME (mm)= 11.645
TOTAL RAINFALL (mm)= 55.099
RUNOFF COEFFICIENT = .211

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0022)	Area (ha)=	3.01	Curve Number (CN)=	71.6
ID= 1 DT= 2.0 min	Ia (mm)=	5.22	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.06		

Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .219 (i)
TIME TO PEAK (hrs)= 11.767
RUNOFF VOLUME (mm)= 10.978
TOTAL RAINFALL (mm)= 55.099
RUNOFF COEFFICIENT = .199

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0023)				
IN= 2---> OUT= 1				
DT= 2.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0002	.2156
	.0001	.1117	20.0000	.2166
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0022)	3.01	.22	11.77	10.98
OUTFLOW: ID= 1 (0023)	3.01	.00	13.60	.01
	PEAK FLOW REDUCTION [Qout/Qin](%)=	.01		
	TIME SHIFT OF PEAK FLOW (min)=	110.00		
	MAXIMUM STORAGE USED (ha.m.)=	.0330		

ADD HYD (0026)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0024):	5.03	.335	11.80	11.64
+ ID2= 2 (0023):	3.01	.000	13.60	.01
ID = 3 (0026):	8.04	.335	11.80	7.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0025)				
IN= 2---> OUT= 1				
DT= 2.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0003	.2171
	.0001	.0498	20.0000	.2181
	.0002	.1676	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0026)	8.04	.33	11.80	7.29
OUTFLOW: ID= 1 (0025)	8.04	.00	13.67	.01

PEAK FLOW REDUCTION [Qout/Qin](%)= .03
 TIME SHIFT OF PEAK FLOW (min)=112.00
 MAXIMUM STORAGE USED (ha.m.)= .0585

ADD HYD (0028)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0027):	.68	.051	11.77	16.87
+ ID2= 2 (0025):	8.04	.000	13.67	.01
=====				
ID = 3 (0028):	8.72	.051	11.77	1.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0029)				
IN= 2----> OUT= 1				
DT= 2.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0002	.0898
	.0001	.0455	20.0000	.0908
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0028)	8.72	.05	11.77	1.32
OUTFLOW: ID= 1 (0029)	8.72	.00	24.17	.01

PEAK FLOW REDUCTION [Qout/Qin](%)= .05
 TIME SHIFT OF PEAK FLOW (min)=744.00
 MAXIMUM STORAGE USED (ha.m.)= .0114

CALIB			
NASHYD (0032)			
ID= 1 DT= 5.0 min			
Area	(ha)=	Curve Number	(CN)=
Ia	(mm)=	# of Linear Res.	(N)=
U.H. Tp	(hrs)=		
6.71		64.3	
8.68		3.00	
.32			

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.51	6.083	.91	12.083	11.16	18.08	.87
.167	.51	6.167	.92	12.167	9.01	18.17	.86
.250	.52	6.250	.93	12.250	7.59	18.25	.85
.333	.52	6.333	.94	12.333	6.58	18.33	.84
.417	.52	6.417	.96	12.417	5.82	18.42	.83
.500	.53	6.500	.97	12.500	5.22	18.50	.82
.583	.53	6.583	.98	12.583	4.75	18.58	.81
.667	.53	6.667	.99	12.667	4.36	18.67	.81
.750	.54	6.750	1.01	12.750	4.04	18.75	.80
.833	.54	6.833	1.02	12.833	3.76	18.83	.79
.917	.54	6.917	1.03	12.917	3.53	18.92	.78
1.000	.55	7.000	1.05	13.000	3.32	19.00	.78
1.083	.55	7.083	1.06	13.083	3.14	19.08	.77
1.167	.55	7.167	1.08	13.167	2.98	19.17	.76
1.250	.56	7.250	1.10	13.250	2.84	19.25	.76
1.333	.56	7.333	1.11	13.333	2.71	19.33	.75
1.417	.56	7.417	1.13	13.417	2.59	19.42	.74
1.500	.57	7.500	1.15	13.500	2.49	19.50	.74
1.583	.57	7.583	1.17	13.583	2.39	19.58	.73
1.667	.57	7.667	1.19	13.667	2.30	19.67	.72
1.750	.58	7.750	1.21	13.750	2.22	19.75	.72
1.833	.58	7.833	1.23	13.833	2.15	19.83	.71
1.917	.59	7.917	1.25	13.917	2.08	19.92	.71
2.000	.59	8.000	1.27	14.000	2.01	20.00	.70
2.083	.59	8.083	1.29	14.083	1.95	20.08	.69
2.167	.60	8.167	1.32	14.167	1.90	20.17	.69
2.250	.60	8.250	1.34	14.250	1.84	20.25	.68
2.333	.61	8.333	1.37	14.333	1.80	20.33	.68
2.417	.61	8.417	1.40	14.417	1.75	20.42	.67
2.500	.62	8.500	1.43	14.500	1.70	20.50	.67
2.583	.62	8.583	1.46	14.583	1.66	20.58	.66
2.667	.62	8.667	1.49	14.667	1.62	20.67	.66
2.750	.63	8.750	1.53	14.750	1.59	20.75	.65
2.833	.63	8.833	1.56	14.833	1.55	20.83	.65
2.917	.64	8.917	1.60	14.917	1.52	20.92	.64
3.000	.64	9.000	1.64	15.000	1.49	21.00	.64
3.083	.65	9.083	1.68	15.083	1.46	21.08	.63
3.167	.65	9.167	1.73	15.167	1.43	21.17	.63
3.250	.66	9.250	1.77	15.250	1.40	21.25	.63
3.333	.66	9.333	1.82	15.333	1.37	21.33	.62

3.417	.67	9.417	1.88	15.417	1.35	21.42	.62
3.500	.67	9.500	1.94	15.500	1.32	21.50	.61
3.583	.68	9.583	2.00	15.583	1.30	21.58	.61
3.667	.69	9.667	2.07	15.667	1.28	21.67	.60
3.750	.69	9.750	2.14	15.750	1.25	21.75	.60
3.833	.70	9.833	2.21	15.833	1.23	21.83	.60
3.917	.70	9.917	2.30	15.917	1.21	21.92	.59
4.000	.71	10.000	2.39	16.000	1.19	22.00	.59
4.083	.71	10.083	2.49	16.083	1.17	22.08	.59
4.167	.72	10.167	2.60	16.167	1.16	22.17	.58
4.250	.73	10.250	2.73	16.250	1.14	22.25	.58
4.333	.73	10.333	2.86	16.333	1.12	22.33	.57
4.417	.74	10.417	3.02	16.417	1.11	22.42	.57
4.500	.75	10.500	3.19	16.500	1.09	22.50	.57
4.583	.75	10.583	3.39	16.583	1.08	22.58	.56
4.667	.76	10.667	3.61	16.667	1.06	22.67	.56
4.750	.77	10.750	3.88	16.750	1.05	22.75	.56
4.833	.78	10.833	4.19	16.833	1.03	22.83	.55
4.917	.78	10.917	4.56	16.917	1.02	22.92	.55
5.000	.79	11.000	5.01	17.000	1.01	23.00	.55
5.083	.80	11.083	5.58	17.083	.99	23.08	.54
5.167	.81	11.167	6.31	17.167	.98	23.17	.54
5.250	.82	11.250	7.28	17.250	.97	23.25	.54
5.333	.82	11.333	8.65	17.333	.96	23.33	.53
5.417	.83	11.417	10.72	17.417	.95	23.42	.53
5.500	.84	11.500	14.20	17.500	.93	23.50	.53
5.583	.85	11.583	21.19	17.583	.92	23.58	.53
5.667	.86	11.667	41.67	17.667	.91	23.67	.52
5.750	.87	11.750	103.59	17.750	.90	23.75	.52
5.833	.88	11.833	42.36	17.833	.89	23.83	.52
5.917	.89	11.917	21.91	17.917	.88	23.92	.51
6.000	.90	12.000	14.75	18.000	.87	24.00	.00

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .134 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 11.474
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .208

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0030) Area (ha)= 5.57 Curve Number (CN)= 69.8
 ID= 1 DT= 5.0 min Ia (mm)= 6.12 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= 3.828

PEAK FLOW (cms)= .335 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 12.384
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .225

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ROUTE CHN (0031) Routing time step (min)'= 5.00
 IN= 2----> OUT= 1

<----- DATA FOR SECTION (1.2) ----->
 Distance Elevation Manning
 .00 386.25 .0300
 37.50 385.75 .0300 / .0300 Main Channel
 47.50 385.75 .0300 / .0300 Main Channel
 85.00 386.25 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .03 385.78 .150E+03 .1 .33 23.91
 .05 385.80 .350E+03 .3 .47 16.85
 .08 385.83 .599E+03 .7 .56 14.12
 .11 385.86 .898E+03 1.2 .63 12.62
 .13 385.88 .125E+04 1.8 .68 11.65
 .16 385.91 .164E+04 2.5 .73 10.95
 .18 385.93 .209E+04 3.3 .76 10.42
 .21 385.96 .259E+04 4.3 .80 9.99
 .24 385.99 .313E+04 5.4 .82 9.64
 .26 386.01 .373E+04 6.7 .85 9.33
 .29 386.04 .438E+04 8.0 .88 9.07
 .32 386.07 .507E+04 9.6 .90 8.83
 .34 386.09 .582E+04 11.2 .92 8.62
 .37 386.12 .661E+04 13.1 .94 8.43

.39	386.14	.745E+04	15.1	.96	8.25
.42	386.17	.835E+04	17.2	.98	8.08
.45	386.20	.929E+04	19.5	1.00	7.93
.47	386.22	.103E+05	22.0	1.02	7.79
.50	386.25	.113E+05	24.7	1.04	7.65

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0030)	5.57	.34	11.75	12.38	.05	.46
OUTFLOW: ID= 1 (0031)	5.57	.12	11.92	12.36	.03	.34

ADD HYD (0033)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0032):	6.71	.134	12.08	11.47
+ ID2= 2 (0031):	5.57	.121	11.92	12.36
=====				
ID = 3 (0033):	12.27	.243	12.00	11.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0036)	Area (ha)=	Curve Number (CN)=
ID= 1 DT= 5.0 min	2.08	67.6
	Ia (mm)= 7.71	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .08	

Unit Hyd Qpeak (cms)= .938

PEAK FLOW (cms)= .096 (i)

TIME TO PEAK (hrs)= 11.750

RUNOFF VOLUME (mm)= 12.652

TOTAL RAINFALL (mm)= 55.057

RUNOFF COEFFICIENT = .230

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0034)	Area (ha)=	Curve Number (CN)=
ID= 1 DT= 5.0 min	2.15	71.9
	Ia (mm)= 5.03	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .10	

Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .121 (i)

TIME TO PEAK (hrs)= 11.833

RUNOFF VOLUME (mm)= 16.396

TOTAL RAINFALL (mm)= 55.057

RUNOFF COEFFICIENT = .298

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0035)	Routing time step (min)'=
IN= 2----> OUT= 1	5.00

Distance	Elevation	Manning	
.00	388.25	.0300	
30.00	387.75	.0300 / .0300	Main Channel
40.00	387.75	.0300 / .0300	Main Channel
70.00	388.25	.0300	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	387.78	.327E+02	.1	.41	4.35
.05	387.80	.744E+02	.4	.59	3.03
.08	387.83	.125E+03	.8	.71	2.52
.11	387.86	.185E+03	1.4	.80	2.25
.13	387.88	.253E+03	2.0	.87	2.07
.16	387.91	.330E+03	2.8	.92	1.95
.18	387.93	.417E+03	3.7	.97	1.85
.21	387.96	.512E+03	4.8	1.01	1.78
.24	387.99	.616E+03	6.0	1.04	1.72
.26	388.01	.729E+03	7.3	1.07	1.67
.29	388.04	.851E+03	8.7	1.10	1.63
.32	388.07	.982E+03	10.3	1.13	1.59
.34	388.09	.112E+04	12.0	1.15	1.56
.37	388.12	.127E+04	13.9	1.17	1.53

.39	388.14	.143E+04	15.9	1.19	1.50
.42	388.17	.160E+04	18.0	1.21	1.48
.45	388.20	.177E+04	20.3	1.23	1.45
.47	388.22	.196E+04	22.8	1.25	1.43
.50	388.25	.215E+04	25.4	1.27	1.41

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0034)	2.15	.12	11.83	16.40	.03	.41
OUTFLOW: ID= 1 (0035)	2.15	.10	11.92	16.40	.02	.41

ADD HYD (0037)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0036):	2.08	.096	11.75	12.65
+ ID2= 2 (0035):	2.15	.104	11.92	16.40
=====				
ID = 3 (0037):	4.23	.193	11.83	14.55

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0039)	Area (ha)=	35.03	Curve Number (CN)=	65.5
ID= 1 DT= 5.0 min	Ia (mm)=	7.17	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.16		

Unit Hyd Qpeak (cms)= 1.152
 PEAK FLOW (cms)= .311 (i)
 TIME TO PEAK (hrs)= 13.083
 RUNOFF VOLUME (mm)= 12.614
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .229

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0040)	Area (ha)=	3.95	Curve Number (CN)=	54.0
ID= 1 DT= 5.0 min	Ia (mm)=	10.00	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.40		

Unit Hyd Qpeak (cms)= .375
 PEAK FLOW (cms)= .044 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 7.764
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .141

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0041)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1	.0000	.0000	.0002	.1655
DT= 5.0 min	.0001	.0976	20.0000	.1665

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.04	12.17	7.76
OUTFLOW: ID= 1 (0041)	3.95	.00	25.42	.03

PEAK FLOW REDUCTION [Qout/Qin](%)= .07
 TIME SHIFT OF PEAK FLOW (min)=795.00
 MAXIMUM STORAGE USED (ha.m.)= .0306

CALIB NASHYD (0044)	Area (ha)=	.87	Curve Number (CN)=	64.6
ID= 1 DT= 3.0 min	Ia (mm)=	6.68	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.06		

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.050	.51	6.050	.91	12.050	11.16	18.05	.87
.100	.51	6.100	.91	12.100	10.44	18.10	.86
.150	.51	6.150	.92	12.150	9.01	18.15	.86
.200	.52	6.200	.93	12.200	8.06	18.20	.85
.250	.52	6.250	.93	12.250	7.59	18.25	.85
.300	.52	6.300	.94	12.300	6.58	18.30	.84
.350	.52	6.350	.95	12.350	6.32	18.35	.84
.400	.52	6.400	.96	12.400	5.82	18.40	.83
.450	.53	6.450	.96	12.450	5.42	18.45	.82
.500	.53	6.500	.97	12.500	5.22	18.50	.82
.550	.53	6.550	.98	12.550	4.75	18.55	.81
.600	.53	6.600	.99	12.600	4.62	18.60	.81
.650	.53	6.650	.99	12.650	4.36	18.65	.81
.700	.54	6.700	1.00	12.700	4.15	18.70	.80
.750	.54	6.750	1.01	12.750	4.04	18.75	.80
.800	.54	6.800	1.02	12.800	3.76	18.80	.79
.850	.54	6.850	1.03	12.850	3.68	18.85	.79
.900	.54	6.900	1.03	12.900	3.53	18.90	.78
.950	.55	6.950	1.04	12.950	3.39	18.95	.78
1.000	.55	7.000	1.05	13.000	3.32	19.00	.78
1.050	.55	7.050	1.06	13.050	3.14	19.05	.77
1.100	.55	7.100	1.07	13.100	3.09	19.10	.77
1.150	.55	7.150	1.08	13.150	2.98	19.15	.76
1.200	.56	7.200	1.09	13.200	2.89	19.20	.76
1.250	.56	7.250	1.10	13.250	2.84	19.25	.76
1.300	.56	7.300	1.11	13.300	2.71	19.30	.75
1.350	.56	7.350	1.12	13.350	2.67	19.35	.75
1.400	.56	7.400	1.13	13.400	2.59	19.40	.74
1.450	.57	7.450	1.14	13.450	2.52	19.45	.74
1.500	.57	7.500	1.15	13.500	2.49	19.50	.74
1.550	.57	7.550	1.17	13.550	2.39	19.55	.73
1.600	.57	7.600	1.17	13.600	2.36	19.60	.73
1.650	.57	7.650	1.19	13.650	2.30	19.65	.72
1.700	.58	7.700	1.20	13.700	2.25	19.70	.72
1.750	.58	7.750	1.21	13.750	2.22	19.75	.72
1.800	.58	7.800	1.23	13.800	2.15	19.80	.71
1.850	.58	7.850	1.23	13.850	2.12	19.85	.71
1.900	.59	7.900	1.25	13.900	2.08	19.90	.71
1.950	.59	7.950	1.26	13.950	2.04	19.95	.70
2.000	.59	8.000	1.27	14.000	2.01	20.00	.70
2.050	.59	8.050	1.29	14.050	1.95	20.05	.69
2.100	.60	8.100	1.30	14.100	1.94	20.10	.69
2.150	.60	8.150	1.32	14.150	1.90	20.15	.69
2.200	.60	8.200	1.34	14.200	1.86	20.20	.69
2.250	.60	8.250	1.34	14.250	1.84	20.25	.68
2.300	.61	8.300	1.37	14.300	1.80	20.30	.68
2.350	.61	8.350	1.38	14.350	1.78	20.35	.68
2.400	.61	8.400	1.40	14.400	1.75	20.40	.67
2.450	.61	8.450	1.42	14.450	1.72	20.45	.67
2.500	.62	8.500	1.43	14.500	1.70	20.50	.67
2.550	.62	8.550	1.46	14.550	1.66	20.55	.66
2.600	.62	8.600	1.47	14.600	1.65	20.60	.66
2.650	.62	8.650	1.49	14.650	1.62	20.65	.66
2.700	.63	8.700	1.51	14.700	1.60	20.70	.65
2.750	.63	8.750	1.53	14.750	1.59	20.75	.65
2.800	.63	8.800	1.56	14.800	1.55	20.80	.65
2.850	.64	8.850	1.57	14.850	1.54	20.85	.65
2.900	.64	8.900	1.60	14.900	1.52	20.90	.64
2.950	.64	8.950	1.63	14.950	1.50	20.95	.64
3.000	.64	9.000	1.64	15.000	1.49	21.00	.64
3.050	.65	9.050	1.68	15.050	1.46	21.05	.63
3.100	.65	9.100	1.70	15.100	1.45	21.10	.63
3.150	.65	9.150	1.73	15.150	1.43	21.15	.63
3.200	.66	9.200	1.76	15.200	1.41	21.20	.63
3.250	.66	9.250	1.77	15.250	1.40	21.25	.63
3.300	.66	9.300	1.82	15.300	1.37	21.30	.62
3.350	.67	9.350	1.84	15.350	1.36	21.35	.62
3.400	.67	9.400	1.88	15.400	1.35	21.40	.62
3.450	.67	9.450	1.92	15.450	1.33	21.45	.61
3.500	.67	9.500	1.94	15.500	1.32	21.50	.61
3.550	.68	9.550	2.00	15.550	1.30	21.55	.61
3.600	.68	9.600	2.02	15.600	1.29	21.60	.61
3.650	.69	9.650	2.07	15.650	1.28	21.65	.60
3.700	.69	9.700	2.11	15.700	1.26	21.70	.60
3.750	.69	9.750	2.14	15.750	1.25	21.75	.60
3.800	.70	9.800	2.21	15.800	1.23	21.80	.60
3.850	.70	9.850	2.24	15.850	1.23	21.85	.60
3.900	.70	9.900	2.30	15.900	1.21	21.90	.59
3.950	.71	9.950	2.36	15.950	1.20	21.95	.59
4.000	.71	10.000	2.39	16.000	1.19	22.00	.59
4.050	.71	10.050	2.49	16.050	1.17	22.05	.59
4.100	.72	10.100	2.53	16.100	1.17	22.10	.58
4.150	.72	10.150	2.60	16.150	1.16	22.15	.58
4.200	.73	10.200	2.69	16.200	1.15	22.20	.58
4.250	.73	10.250	2.73	16.250	1.14	22.25	.58
4.300	.73	10.300	2.86	16.300	1.12	22.30	.57
4.350	.74	10.350	2.91	16.350	1.12	22.35	.57

4.400	.74	10.400	3.02	16.400	1.11	22.40	.57
4.450	.75	10.450	3.13	16.450	1.10	22.45	.57
4.500	.75	10.500	3.19	16.500	1.09	22.50	.57
4.550	.75	10.550	3.39	16.550	1.08	22.55	.56
4.600	.76	10.600	3.46	16.600	1.07	22.60	.56
4.650	.76	10.650	3.61	16.650	1.06	22.65	.56
4.700	.77	10.700	3.79	16.700	1.05	22.70	.56
4.750	.77	10.750	3.88	16.750	1.05	22.75	.56
4.800	.78	10.800	4.19	16.800	1.03	22.80	.55
4.850	.78	10.850	4.31	16.850	1.03	22.85	.55
4.900	.78	10.900	4.56	16.900	1.02	22.90	.55
4.950	.79	10.950	4.86	16.950	1.01	22.95	.55
5.000	.79	11.000	5.01	17.000	1.01	23.00	.55
5.050	.80	11.050	5.58	17.050	.99	23.05	.54
5.100	.80	11.100	5.82	17.100	.99	23.10	.54
5.150	.81	11.150	6.31	17.150	.98	23.15	.54
5.200	.81	11.200	6.96	17.200	.97	23.20	.54
5.250	.82	11.250	7.29	17.250	.97	23.25	.54
5.300	.82	11.300	8.65	17.300	.96	23.30	.53
5.350	.83	11.350	9.34	17.350	.95	23.35	.53
5.400	.83	11.400	10.72	17.400	.95	23.40	.53
5.450	.84	11.450	13.04	17.450	.94	23.45	.53
5.500	.84	11.500	14.20	17.500	.93	23.50	.53
5.550	.85	11.550	21.19	17.550	.92	23.55	.53
5.600	.85	11.600	28.03	17.600	.92	23.60	.52
5.650	.86	11.650	41.67	17.650	.91	23.65	.52
5.700	.87	11.700	82.98	17.700	.91	23.70	.52
5.750	.87	11.750	103.56	17.750	.90	23.75	.52
5.800	.88	11.800	42.36	17.800	.89	23.80	.52
5.850	.88	11.850	35.53	17.850	.89	23.85	.52
5.900	.89	11.900	21.91	17.900	.88	23.90	.51
5.950	.90	11.950	17.13	17.950	.88	23.95	.51
6.000	.90	12.000	14.75	18.000	.87	24.00	.51

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .047 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 12.078
 TOTAL RAINFALL (mm)= 55.099
 RUNOFF COEFFICIENT = .219

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB					
NASHYD (0042)	Area (ha)=	.56	Curve Number (CN)=	70.0	
ID= 1 DT= 3.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00	
	U.H. Tp(hrs)=	.06			

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .039 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 14.052
 TOTAL RAINFALL (mm)= 55.099
 RUNOFF COEFFICIENT = .255

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0043)					
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)	
DT= 3.0 min	.0000	.0000	.0002	.0357	
	.0001	.0118	20.0000	.0367	

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0042)	.56	.04	11.75	14.05
OUTFLOW: ID= 1 (0043)	.56	.00	20.10	.30

PEAK FLOW REDUCTION [Qout/Qin](%)= .17
 TIME SHIFT OF PEAK FLOW (min)=501.00
 MAXIMUM STORAGE USED (ha.m.)= .0076

ADD HYD (0045)					
1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0044):	.87	.047	11.75	12.08	
+ ID2= 2 (0043):	.56	.000	20.10	.30	
ID = 3 (0045):	1.42	.047	11.75	7.48	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0046)
IN= 2---> OUT= 1
DT= 3.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.1073
.0001	.0117	20.0000	.1083

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0045)	1.42	.05	11.75	7.48
OUTFLOW: ID= 1 (0046)	1.42	.00	24.10	.23

PEAK FLOW REDUCTION [Qout/Qin](%)= .19
TIME SHIFT OF PEAK FLOW (min)=741.00
MAXIMUM STORAGE USED (ha.m.)= .0103

CALIB NASHYD (0047)
ID= 1 DT= 3.0 min

Area (ha)= .48 Curve Number (CN)= 70.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .033 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 14.052
TOTAL RAINFALL (mm)= 55.099
RUNOFF COEFFICIENT = .255

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0048)
IN= 2---> OUT= 1
DT= 3.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0731
.0001	.0496	20.0000	.0741

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0047)	.48	.03	11.75	14.05
OUTFLOW: ID= 1 (0048)	.48	.00	20.15	.07

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
TIME SHIFT OF PEAK FLOW (min)=504.00
MAXIMUM STORAGE USED (ha.m.)= .0067

CALIB NASHYD (0049)
ID= 1 DT= 5.0 min

Area (ha)= 2.77 Curve Number (CN)= 70.7
Ia (mm)= 5.35 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	.51	6.083	.91	12.083	11.16	18.08	.87
.167	.51	6.167	.92	12.167	9.01	18.17	.86
.250	.52	6.250	.93	12.250	7.59	18.25	.85
.333	.52	6.333	.94	12.333	6.58	18.33	.84
.417	.52	6.417	.96	12.417	5.82	18.42	.83
.500	.53	6.500	.97	12.500	5.22	18.50	.82
.583	.53	6.583	.98	12.583	4.75	18.58	.81
.667	.53	6.667	.99	12.667	4.36	18.67	.81
.750	.54	6.750	1.01	12.750	4.04	18.75	.80
.833	.54	6.833	1.02	12.833	3.76	18.83	.79
.917	.54	6.917	1.03	12.917	3.53	18.92	.78
1.000	.55	7.000	1.05	13.000	3.32	19.00	.78
1.083	.55	7.083	1.06	13.083	3.14	19.08	.77
1.167	.55	7.167	1.08	13.167	2.98	19.17	.76
1.250	.56	7.250	1.10	13.250	2.84	19.25	.76
1.333	.56	7.333	1.11	13.333	2.71	19.33	.75
1.417	.56	7.417	1.13	13.417	2.59	19.42	.74
1.500	.57	7.500	1.15	13.500	2.49	19.50	.74
1.583	.57	7.583	1.17	13.583	2.39	19.58	.73
1.667	.57	7.667	1.19	13.667	2.30	19.67	.72

1.750	.58	7.750	1.21	13.750	2.22	19.75	.72
1.833	.58	7.833	1.23	13.833	2.15	19.83	.71
1.917	.59	7.917	1.25	13.917	2.08	19.92	.71
2.000	.59	8.000	1.27	14.000	2.01	20.00	.70
2.083	.59	8.083	1.29	14.083	1.95	20.08	.69
2.167	.60	8.167	1.32	14.167	1.90	20.17	.69
2.250	.60	8.250	1.34	14.250	1.84	20.25	.68
2.333	.61	8.333	1.37	14.333	1.80	20.33	.68
2.417	.61	8.417	1.40	14.417	1.75	20.42	.67
2.500	.62	8.500	1.43	14.500	1.70	20.50	.67
2.583	.62	8.583	1.46	14.583	1.66	20.58	.66
2.667	.62	8.667	1.49	14.667	1.62	20.67	.66
2.750	.63	8.750	1.53	14.750	1.59	20.75	.65
2.833	.63	8.833	1.56	14.833	1.55	20.83	.65
2.917	.64	8.917	1.60	14.917	1.52	20.92	.64
3.000	.64	9.000	1.64	15.000	1.49	21.00	.64
3.083	.65	9.083	1.68	15.083	1.46	21.08	.63
3.167	.65	9.167	1.73	15.167	1.43	21.17	.63
3.250	.66	9.250	1.77	15.250	1.40	21.25	.63
3.333	.66	9.333	1.82	15.333	1.37	21.33	.62
3.417	.67	9.417	1.88	15.417	1.35	21.42	.62
3.500	.67	9.500	1.94	15.500	1.32	21.50	.61
3.583	.68	9.583	2.00	15.583	1.30	21.58	.61
3.667	.69	9.667	2.07	15.667	1.28	21.67	.60
3.750	.69	9.750	2.14	15.750	1.25	21.75	.60
3.833	.70	9.833	2.21	15.833	1.23	21.83	.60
3.917	.70	9.917	2.30	15.917	1.21	21.92	.59
4.000	.71	10.000	2.39	16.000	1.19	22.00	.59
4.083	.71	10.083	2.49	16.083	1.17	22.08	.59
4.167	.72	10.167	2.60	16.167	1.16	22.17	.58
4.250	.73	10.250	2.73	16.250	1.14	22.25	.58
4.333	.73	10.333	2.86	16.333	1.12	22.33	.57
4.417	.74	10.417	3.02	16.417	1.11	22.42	.57
4.500	.75	10.500	3.19	16.500	1.09	22.50	.57
4.583	.75	10.583	3.39	16.583	1.08	22.58	.56
4.667	.76	10.667	3.61	16.667	1.06	22.67	.56
4.750	.77	10.750	3.88	16.750	1.05	22.75	.56
4.833	.78	10.833	4.19	16.833	1.03	22.83	.55
4.917	.78	10.917	4.56	16.917	1.02	22.92	.55
5.000	.79	11.000	5.01	17.000	1.01	23.00	.55
5.083	.80	11.083	5.58	17.083	.99	23.08	.54
5.167	.81	11.167	6.31	17.167	.98	23.17	.54
5.250	.82	11.250	7.28	17.250	.97	23.25	.54
5.333	.82	11.333	8.65	17.333	.96	23.33	.53
5.417	.83	11.417	10.72	17.417	.95	23.42	.53
5.500	.84	11.500	14.20	17.500	.93	23.50	.53
5.583	.85	11.583	21.19	17.583	.92	23.58	.53
5.667	.86	11.667	41.67	17.667	.91	23.67	.52
5.750	.87	11.750	103.59	17.750	.90	23.75	.52
5.833	.88	11.833	42.36	17.833	.89	23.83	.52
5.917	.89	11.917	21.91	17.917	.88	23.92	.51
6.000	.90	12.000	14.75	18.000	.87	24.00	.50

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .145 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 15.676
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .285

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0055) | Area (ha)= 5.19 | Curve Number (CN)= 73.3
 ID= 1 DT= 5.0 min | Ia (mm)= 4.00 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .311 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 17.839
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .324

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0052) | Area (ha)= 3.90 | Curve Number (CN)= 69.4
 ID= 1 DT= 5.0 min | Ia (mm)= 4.85 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .230 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 14.554
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .264

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0050) | Area (ha)= 11.96 Curve Number (CN)= 66.4
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
 |-----| U.H. Tp(hrs)= .18

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= .416 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 13.653
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .248

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | RESERVOIR (0051) |
 | IN= 2---> OUT= 1 |
DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.1583
	.0001	.1573	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0050)	11.96	.42	11.92	13.65
OUTFLOW: ID= 1 (0051)	11.96	.02	22.42	.50

PEAK FLOW REDUCTION [Qout/Qin](%)= 3.85
 TIME SHIFT OF PEAK FLOW (min)=630.00
 MAXIMUM STORAGE USED (ha.m.)= .1595

 | ADD HYD (0053) |
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0052):	3.90	.230	11.75	14.55
+ ID2= 2 (0051):	11.96	.016	22.42	.50
=====				
ID = 3 (0053):	15.86	.230	11.75	3.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 | RESERVOIR (0054) |
 | IN= 2---> OUT= 1 |
DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0771
	.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0053)	15.86	.23	11.75	3.96
OUTFLOW: ID= 1 (0054)	15.86	.00	24.92	.02

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=790.00
 MAXIMUM STORAGE USED (ha.m.)= .0624

 | ROUTE CHN (0056) |
 | IN= 2---> OUT= 1 |
 |-----| Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.5) ----->
 Distance Elevation Manning
 .00 425.00 .0300
 .75 424.25 .0300 / .0300 Main Channel
 1.75 424.25 .0300 / .0300 Main Channel
 2.50 425.00 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)

.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

```

<---- hydrograph ----> <-pipe / channel-->
                AREA   QPEAK   TPEAK   R.V.   MAX DEPTH   MAX VEL
                (ha)   (cms)   (hrs)   (mm)   (m)         (m/s)
INFLOW : ID= 2 (0054) 15.86   .00   24.92   .02     .00         .68
OUTFLOW: ID= 1 (0056) 15.86   .00   24.92   .02     .00         .68

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| ADD HYD (0057) |
| 1 + 2 = 3 |
-----
ID1= 1 (0055):   AREA   QPEAK   TPEAK   R.V.
                  (ha)   (cms)   (hrs)   (mm)
+ ID2= 2 (0056): 15.86   .000   24.92   .02
-----
ID = 3 (0057):  21.05   .311   11.83   4.41

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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| CALIB
| NASHYD (0058) | Area (ha)= 21.77 Curve Number (CN)= 67.4
| ID= 1 DT= 5.0 min | Ia (mm)= 5.22 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .35

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Unit Hyd Qpeak (cms)= 2.354
PEAK FLOW (cms)= .524 (i)
TIME TO PEAK (hrs)= 12.083
RUNOFF VOLUME (mm)= 14.403
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .262

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

| CALIB
| NASHYD (0059) | Area (ha)= 11.96 Curve Number (CN)= 66.4
| ID= 1 DT= 5.0 min | Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .18

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```

Unit Hyd Qpeak (cms)= 2.557
PEAK FLOW (cms)= .416 (i)
TIME TO PEAK (hrs)= 11.917
RUNOFF VOLUME (mm)= 13.653
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .248

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

| RESERVOIR (0060) |
| IN= 2----> OUT= 1 |
| DT= 5.0 min |
-----
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.0000 .0000 | 20.0000 .1583
.0001 .1573 | .0000 .0000

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                AREA   QPEAK   TPEAK   R.V.
                (ha)   (cms)   (hrs)   (mm)
INFLOW : ID= 2 (0059) 11.96   .42   11.92   13.65
OUTFLOW: ID= 1 (0060) 11.96   .02   22.42   .50

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 3.85

TIME SHIFT OF PEAK FLOW (min)=630.00
 MAXIMUM STORAGE USED (ha.m.)= .1595

CALIB
 NASHYD (0061) Area (ha)= 3.90 Curve Number (CN)= 69.4
 ID= 1 DT= 5.0 min Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .230 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 14.554
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .264

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0062)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0060):	11.96	.016	22.42	.50
+ ID2= 2 (0061):	3.90	.230	11.75	14.55
ID = 3 (0062):	15.86	.230	11.75	3.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0063)
 IN= 2---> OUT= 1
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0771
	.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0062)	15.86	.23	11.75	3.96
OUTFLOW: ID= 1 (0063)	15.86	.00	24.92	.02

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=790.00
 MAXIMUM STORAGE USED (ha.m.)= .0624

ROUTE CHN (0065)
 IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.5) ----->
 Distance Elevation Manning
 .00 425.00 .0300
 .75 424.25 .0300 / .0300 Main Channel
 1.75 424.25 .0300 / .0300 Main Channel
 2.50 425.00 .0300

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

<---- hydrograph ----> <-pipe / channel-->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0063) 15.86 .00 24.92 .02 .00 .68
 OUTFLOW: ID= 1 (0065) 15.86 .00 24.92 .02 .00 .68

CALIB
 NASHYD (0064) Area (ha)= 5.19 Curve Number (CN)= 73.3
 ID= 1 DT= 5.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .311 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 17.839
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .324

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0066)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0065):	15.86	.000	24.92	.02
+ ID2= 2 (0064):	5.19	.311	11.83	17.84
ID = 3 (0066):	21.05	.311	11.83	4.41

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
 NASHYD (0069) Area (ha)= 1.80 Curve Number (CN)= 58.8
 ID= 1 DT= 5.0 min Ia (mm)= 8.49 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .07

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .065 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 8.754
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .159

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 NASHYD (0067) Area (ha)= 1.52 Curve Number (CN)= 62.0
 ID= 1 DT= 5.0 min Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .064 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 9.243
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .168

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0068)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min	.0000	.0000	20.0000	.0207
	.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.06	11.75	9.24
OUTFLOW: ID= 1 (0068)	1.52	.00	24.08	.16

PEAK FLOW REDUCTION [Qout/Qin](%)= .10
 TIME SHIFT OF PEAK FLOW (min)=740.00
 MAXIMUM STORAGE USED (ha.m.)= .0138

ADD HYD (0071)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0069):	1.80	.065	11.75	8.75
+ ID2= 2 (0068):	1.52	.000	24.08	.16
=====				
ID = 3 (0071):	3.32	.065	11.75	4.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0070)	OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1	(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min	.0000	.0000	20.0000	.0708
	.0001	.0707	.0000	.0000
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0071)	3.32	.07	11.75	4.82
OUTFLOW: ID= 1 (0070)	3.32	.00	24.25	.02
PEAK FLOW REDUCTION [Qout/Qin](%)=	.03			
TIME SHIFT OF PEAK FLOW	(min)=750.00			
MAXIMUM STORAGE USED	(ha.m.)= .0159			

ROUTE CHN (0073)	Routing time step (min)'=
IN= 2---> OUT= 1	5.00

<----- DATA FOR SECTION (1.6) ----->				
Distance	Elevation	Manning		
.00	421.26	.0300		
1.10	420.66	.0300 / .0300	Main Channel	
2.00	420.66	.0300 / .0300	Main Channel	
3.10	421.26	.0300		

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0070)	3.32	.00	24.25	.02	.00	.05
OUTFLOW: ID= 1 (0073)	3.32	.00	24.17	.02	.00	.05

ADD HYD (0074)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0066):	21.05	.311	11.83	4.41
+ ID2= 2 (0073):	3.32	.000	24.17	.02
=====				
ID = 3 (0074):	24.37	.311	11.83	3.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	Curve Number
NASHYD (0072)	(ha)= 24.19	(CN)= 60.0
ID= 1 DT= 5.0 min	Ia (mm)= 8.62	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .37	

Unit Hyd Qpeak (cms)= 2.505

PEAK FLOW (cms)= .377 (i)
TIME TO PEAK (hrs)= 12.167
RUNOFF VOLUME (mm)= 9.976
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .181

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0074):	24.37	.311	11.83	3.82
+ ID2= 2 (0072):	24.19	.377	12.17	9.98
ID = 3 (0075):	48.56	.529	11.92	6.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0076)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	127.28	59.9
	Ia (mm)= 8.29	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .79	

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 1.186 (i)
TIME TO PEAK (hrs)= 12.667
RUNOFF VOLUME (mm)= 10.091
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .183

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0077)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	17.28	58.3
	Ia (mm)= 9.24	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .57	

Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .183 (i)
TIME TO PEAK (hrs)= 12.417
RUNOFF VOLUME (mm)= 9.230
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .168

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0082)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	.24	77.6
	Ia (mm)= 3.49	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .11	

Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .017 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 20.920
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .380

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0078)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	2.66	59.8
	Ia (mm)= 8.55	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .07	

Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .098 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 9.141
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .166

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0079) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE   |   OUTFLOW   STORAGE
      (cms)     (ha.m.)   |   (cms)     (ha.m.)
      .0000     .0000     |   20.0000    .0608
      .0001     .0607     |   .0000       .0000

      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0078)  2.66      .10      11.75     9.14
OUTFLOW: ID= 1 (0079)  2.66      .00      24.17     .06

      PEAK FLOW REDUCTION [Qout/Qin](%)= .04
      TIME SHIFT OF PEAK FLOW (min)=745.00
      MAXIMUM STORAGE USED (ha.m.)= .0242
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-----
| ADD HYD (0083) |
| 1 + 2 = 3      |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
      ID1= 1 (0082): .24      .017     11.83     20.92
+ ID2= 2 (0079):  2.66      .000     24.17     .06
=====
      ID = 3 (0083):  2.90      .017     11.83     1.76
-----

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0080) |
| ID= 1 DT= 5.0 min |
-----
      Area (ha)= 14.63   Curve Number (CN)= 58.0
      Ia (mm)= 9.37     # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .57
-----

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Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .152 (i)
TIME TO PEAK (hrs)= 12.417
RUNOFF VOLUME (mm)= 9.102
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .165
-----

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD (0081) |
| 1 + 2 = 3      |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
      ID1= 1 (0083):  2.90      .017     11.83     1.76
+ ID2= 2 (0080):  14.63      .152     12.42     9.10
=====
      ID = 3 (0081):  17.52      .155     12.42     7.89
-----

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0084) |
| ID= 1 DT= 5.0 min |
-----
      Area (ha)= 7.71   Curve Number (CN)= 62.5
      Ia (mm)= 9.14     # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .29
-----

```

```

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .149 (i)
TIME TO PEAK (hrs)= 12.083
RUNOFF VOLUME (mm)= 10.609
TOTAL RAINFALL (mm)= 55.057
RUNOFF COEFFICIENT = .193
-----

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0085) |
| ID= 1 DT= 5.0 min |
-----
      Area (ha)= .91   Curve Number (CN)= 64.9
      Ia (mm)= 8.53   # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .11
-----

```

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Unit Hyd Qpeak (cms)= .313
-----

```


PEAK FLOW (cms)= .034 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 11.551
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .210

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB (0086) Area (ha)= 19.15 Curve Number (CN)= 71.3
 NASHYD (0086) Ia (mm)= 5.81 # of Linear Res.(N)= 3.00
 ID= 1 DT= 5.0 min U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= .654 (i)
 TIME TO PEAK (hrs)= 12.000
 RUNOFF VOLUME (mm)= 15.980
 TOTAL RAINFALL (mm)= 55.057
 RUNOFF COEFFICIENT = .290

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ** SIMULATION NUMBER: 2 **

CHICAGO STORM Ptotal= 70.76 mm
 IDF curve parameters: A=1025.002
 B= 7.559
 C= .804
 used in: INTENSITY = A / (t + B)^C
 Duration of storm = 24.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = .49

The CORRELATION coefficient is = .9997

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	135.00	134.02
10.	100.00	102.36
15.	85.00	83.69
30.	58.00	55.55
60.	34.00	34.65
120.	21.00	20.78
360.	8.30	8.88
720.	5.10	5.13
1440.	3.10	2.95

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.59	6.08	1.08	12.08	15.27	18.08	1.02
.17	.60	6.17	1.09	12.17	12.18	18.17	1.01
.25	.60	6.25	1.10	12.25	10.15	18.25	1.00
.33	.60	6.33	1.12	12.33	8.71	18.33	.99
.42	.61	6.42	1.13	12.42	7.64	18.42	.98
.50	.61	6.50	1.15	12.50	6.81	18.50	.97
.58	.61	6.58	1.16	12.58	6.16	18.58	.96
.67	.62	6.67	1.18	12.67	5.62	18.67	.95
.75	.62	6.75	1.20	12.75	5.18	18.75	.94
.83	.63	6.83	1.21	12.83	4.80	18.83	.93
.92	.63	6.92	1.23	12.92	4.48	18.92	.92
1.00	.63	7.00	1.25	13.00	4.20	19.00	.91
1.08	.64	7.08	1.27	13.08	3.96	19.08	.90
1.17	.64	7.17	1.29	13.17	3.75	19.17	.90
1.25	.65	7.25	1.31	13.25	3.56	19.25	.89
1.33	.65	7.33	1.33	13.33	3.39	19.33	.88
1.42	.65	7.42	1.35	13.42	3.23	19.42	.87
1.50	.66	7.50	1.37	13.50	3.09	19.50	.86
1.58	.66	7.58	1.40	13.58	2.97	19.58	.86
1.67	.67	7.67	1.42	13.67	2.85	19.67	.85
1.75	.67	7.75	1.44	13.75	2.75	19.75	.84
1.83	.68	7.83	1.47	13.83	2.65	19.83	.83
1.92	.68	7.92	1.50	13.92	2.56	19.92	.83
2.00	.69	8.00	1.53	14.00	2.47	20.00	.82
2.08	.69	8.08	1.56	14.08	2.40	20.08	.81
2.17	.70	8.17	1.59	14.17	2.32	20.17	.81
2.25	.70	8.25	1.62	14.25	2.26	20.25	.80
2.33	.71	8.33	1.65	14.33	2.19	20.33	.79
2.42	.71	8.42	1.69	14.42	2.13	20.42	.79
2.50	.72	8.50	1.72	14.50	2.08	20.50	.78
2.58	.72	8.58	1.76	14.58	2.02	20.58	.77

2.67	.73	8.67	1.80	14.67	1.97	20.67	.77
2.75	.73	8.75	1.85	14.75	1.93	20.75	.76
2.83	.74	8.83	1.89	14.83	1.88	20.83	.76
2.92	.74	8.92	1.94	14.92	1.84	20.92	.75
3.00	.75	9.00	1.99	15.00	1.80	21.00	.75
3.08	.76	9.08	2.05	15.08	1.76	21.08	.74
3.17	.76	9.17	2.10	15.17	1.72	21.17	.73
3.25	.77	9.25	2.16	15.25	1.69	21.25	.73
3.33	.77	9.33	2.23	15.33	1.65	21.33	.72
3.42	.78	9.42	2.30	15.42	1.62	21.42	.72
3.50	.79	9.50	2.37	15.50	1.59	21.50	.71
3.58	.79	9.58	2.45	15.58	1.56	21.58	.71
3.67	.80	9.67	2.54	15.67	1.53	21.67	.70
3.75	.81	9.75	2.63	15.75	1.50	21.75	.70
3.83	.82	9.83	2.74	15.83	1.48	21.83	.69
3.92	.82	9.92	2.85	15.92	1.45	21.92	.69
4.00	.83	10.00	2.97	16.00	1.43	22.00	.69
4.08	.84	10.08	3.10	16.08	1.41	22.08	.68
4.17	.84	10.17	3.25	16.17	1.38	22.17	.68
4.25	.85	10.25	3.41	16.25	1.36	22.25	.67
4.33	.86	10.33	3.59	16.33	1.34	22.33	.67
4.42	.87	10.42	3.80	16.42	1.32	22.42	.66
4.50	.88	10.50	4.03	16.50	1.30	22.50	.66
4.58	.89	10.58	4.29	16.58	1.28	22.58	.65
4.67	.89	10.67	4.60	16.67	1.26	22.67	.65
4.75	.90	10.75	4.96	16.75	1.25	22.75	.65
4.83	.91	10.83	5.38	16.83	1.23	22.83	.64
4.92	.92	10.92	5.89	16.92	1.21	22.92	.64
5.00	.93	11.00	6.52	17.00	1.20	23.00	.63
5.08	.94	11.08	7.31	17.08	1.18	23.08	.63
5.17	.95	11.17	8.33	17.17	1.16	23.17	.63
5.25	.96	11.25	9.71	17.25	1.15	23.25	.62
5.33	.97	11.33	11.67	17.33	1.13	23.33	.62
5.42	.98	11.42	14.64	17.42	1.12	23.42	.62
5.50	.99	11.50	19.66	17.50	1.11	23.50	.61
5.58	1.00	11.58	29.72	17.58	1.09	23.58	.61
5.67	1.01	11.67	58.04	17.67	1.08	23.67	.61
5.75	1.03	11.75	134.02	17.75	1.07	23.75	.60
5.83	1.04	11.83	58.98	17.83	1.06	23.83	.60
5.92	1.05	11.92	30.75	17.92	1.04	23.92	.60
6.00	1.06	12.00	20.46	18.00	1.03	24.00	.59

CALIB							
NASHYD	(0021)	Area	(ha)= 8.81	Curve Number	(CN)= 68.3		
ID= 1 DT= 5.0 min		Ia	(mm)= 6.50	# of Linear Res.(N)=	3.00		
		U.H. Tp(hrs)=	1.36				

Unit Hyd Qpeak (cms)= .248

PEAK FLOW (cms)= .134 (i)
TIME TO PEAK (hrs)= 13.333
RUNOFF VOLUME (mm)= 22.656
TOTAL RAINFALL (mm)= 70.759
RUNOFF COEFFICIENT = .320

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD	(0027)	Area	(ha)= .68	Curve Number	(CN)= 72.2		
ID= 1 DT= 2.0 min		Ia	(mm)= 4.91	# of Linear Res.(N)=	3.00		
		U.H. Tp(hrs)=	.06				

NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.033	.59	6.033	1.08	12.033	15.27	18.03	1.02
.067	.59	6.067	1.08	12.067	15.27	18.07	1.02
.100	.59	6.100	1.08	12.100	13.72	18.10	1.02
.133	.60	6.133	1.09	12.133	12.18	18.13	1.01
.167	.60	6.167	1.09	12.167	12.18	18.17	1.01
.200	.60	6.200	1.10	12.200	10.15	18.20	1.00
.233	.60	6.233	1.10	12.233	10.15	18.23	1.00
.267	.60	6.267	1.11	12.267	9.43	18.27	.99
.300	.60	6.300	1.12	12.300	8.71	18.30	.99
.333	.60	6.333	1.12	12.333	8.71	18.33	.99
.367	.61	6.367	1.13	12.367	7.64	18.37	.98
.400	.61	6.400	1.13	12.400	7.64	18.40	.98
.433	.61	6.433	1.14	12.433	7.22	18.43	.97
.467	.61	6.467	1.15	12.467	6.81	18.47	.97
.500	.61	6.500	1.15	12.500	6.81	18.50	.97
.533	.61	6.533	1.16	12.533	6.16	18.53	.96

.567	.61	6.567	1.16	12.567	6.16	18.57	.96
.600	.62	6.600	1.17	12.600	5.89	18.60	.95
.633	.62	6.633	1.18	12.633	5.62	18.63	.95
.667	.62	6.667	1.18	12.667	5.62	18.67	.95
.700	.62	6.700	1.20	12.700	5.18	18.70	.94
.733	.62	6.733	1.20	12.733	5.18	18.73	.94
.767	.62	6.767	1.20	12.767	4.99	18.77	.93
.800	.63	6.800	1.21	12.800	4.80	18.80	.93
.833	.63	6.833	1.21	12.833	4.80	18.83	.93
.867	.63	6.867	1.23	12.867	4.48	18.87	.92
.900	.63	6.900	1.23	12.900	4.48	18.90	.92
.933	.63	6.933	1.24	12.933	4.34	18.93	.92
.967	.63	6.967	1.25	12.967	4.20	18.97	.91
1.000	.63	7.000	1.25	13.000	4.20	19.00	.91
1.033	.64	7.033	1.27	13.033	3.96	19.03	.90
1.067	.64	7.067	1.27	13.067	3.96	19.07	.90
1.100	.64	7.100	1.28	13.100	3.85	19.10	.90
1.133	.64	7.133	1.29	13.133	3.75	19.13	.90
1.167	.64	7.167	1.29	13.167	3.75	19.17	.90
1.200	.65	7.200	1.31	13.200	3.56	19.20	.89
1.233	.65	7.233	1.31	13.233	3.56	19.23	.89
1.267	.65	7.267	1.32	13.267	3.47	19.27	.88
1.300	.65	7.300	1.33	13.300	3.39	19.30	.88
1.333	.65	7.333	1.33	13.333	3.39	19.33	.88
1.367	.65	7.367	1.35	13.367	3.23	19.37	.87
1.400	.65	7.400	1.35	13.400	3.23	19.40	.87
1.433	.66	7.433	1.36	13.433	3.16	19.43	.87
1.467	.66	7.467	1.37	13.467	3.09	19.47	.86
1.500	.66	7.500	1.37	13.500	3.09	19.50	.86
1.533	.66	7.533	1.40	13.533	2.97	19.53	.86
1.567	.66	7.567	1.40	13.567	2.97	19.57	.86
1.600	.67	7.600	1.41	13.600	2.91	19.60	.85
1.633	.67	7.633	1.42	13.633	2.85	19.63	.85
1.667	.67	7.667	1.42	13.667	2.85	19.67	.85
1.700	.67	7.700	1.44	13.700	2.75	19.70	.84
1.733	.67	7.733	1.44	13.733	2.75	19.73	.84
1.767	.67	7.767	1.46	13.767	2.70	19.77	.84
1.800	.68	7.800	1.47	13.800	2.65	19.80	.83
1.833	.68	7.833	1.47	13.833	2.65	19.83	.83
1.867	.68	7.867	1.50	13.867	2.56	19.87	.83
1.900	.68	7.900	1.50	13.900	2.56	19.90	.83
1.933	.68	7.933	1.51	13.933	2.52	19.93	.82
1.967	.69	7.967	1.53	13.967	2.47	19.97	.82
2.000	.69	8.000	1.53	14.000	2.47	20.00	.82
2.033	.69	8.033	1.56	14.033	2.40	20.03	.81
2.067	.69	8.067	1.56	14.067	2.40	20.07	.81
2.100	.69	8.100	1.57	14.100	2.36	20.10	.81
2.133	.70	8.133	1.59	14.133	2.32	20.13	.81
2.167	.70	8.167	1.59	14.167	2.32	20.17	.81
2.200	.70	8.200	1.62	14.200	2.26	20.20	.80
2.233	.70	8.233	1.62	14.233	2.26	20.23	.80
2.267	.70	8.267	1.64	14.267	2.22	20.27	.80
2.300	.71	8.300	1.65	14.300	2.19	20.30	.79
2.333	.71	8.333	1.65	14.333	2.19	20.33	.79
2.367	.71	8.367	1.69	14.367	2.13	20.37	.79
2.400	.71	8.400	1.69	14.400	2.13	20.40	.79
2.433	.71	8.433	1.71	14.433	2.10	20.43	.78
2.467	.72	8.467	1.72	14.467	2.08	20.47	.78
2.500	.72	8.500	1.72	14.500	2.08	20.50	.78
2.533	.72	8.533	1.76	14.533	2.02	20.53	.77
2.567	.72	8.567	1.76	14.567	2.02	20.57	.77
2.600	.72	8.600	1.78	14.600	2.00	20.60	.77
2.633	.73	8.633	1.80	14.633	1.97	20.63	.77
2.667	.73	8.667	1.80	14.667	1.97	20.67	.77
2.700	.73	8.700	1.85	14.700	1.93	20.70	.76
2.733	.73	8.733	1.85	14.733	1.93	20.73	.76
2.767	.74	8.767	1.87	14.767	1.90	20.77	.76
2.800	.74	8.800	1.89	14.800	1.88	20.80	.76
2.833	.74	8.833	1.89	14.833	1.88	20.83	.76
2.867	.74	8.867	1.94	14.867	1.84	20.87	.75
2.900	.74	8.900	1.94	14.900	1.84	20.90	.75
2.933	.75	8.933	1.97	14.933	1.82	20.93	.75
2.967	.75	8.967	1.99	14.967	1.80	20.97	.75
3.000	.75	9.000	1.99	15.000	1.80	21.00	.75
3.033	.76	9.033	2.05	15.033	1.76	21.03	.74
3.067	.76	9.067	2.05	15.067	1.76	21.07	.74
3.100	.76	9.100	2.07	15.100	1.74	21.10	.74
3.133	.76	9.133	2.10	15.133	1.72	21.13	.73
3.167	.76	9.167	2.10	15.167	1.72	21.17	.73
3.200	.77	9.200	2.16	15.200	1.69	21.20	.73
3.233	.77	9.233	2.16	15.233	1.69	21.23	.73
3.267	.77	9.267	2.20	15.267	1.67	21.27	.73
3.300	.77	9.300	2.23	15.300	1.65	21.30	.72
3.333	.77	9.333	2.23	15.333	1.65	21.33	.72
3.367	.78	9.367	2.30	15.367	1.62	21.37	.72
3.400	.78	9.400	2.30	15.400	1.62	21.40	.72
3.433	.78	9.433	2.34	15.433	1.60	21.43	.72
3.467	.79	9.467	2.37	15.467	1.59	21.47	.71
3.500	.79	9.500	2.37	15.500	1.59	21.50	.71

3.533	.79	9.533	2.45	15.533	1.56	21.53	.71
3.567	.79	9.567	2.45	15.567	1.56	21.57	.71
3.600	.80	9.600	2.50	15.600	1.55	21.60	.71
3.633	.80	9.633	2.54	15.633	1.53	21.63	.70
3.667	.80	9.667	2.54	15.667	1.53	21.67	.70
3.700	.81	9.700	2.63	15.700	1.50	21.70	.70
3.733	.81	9.733	2.63	15.733	1.50	21.73	.70
3.767	.81	9.767	2.68	15.767	1.49	21.77	.70
3.800	.82	9.800	2.74	15.800	1.48	21.80	.69
3.833	.82	9.833	2.74	15.833	1.48	21.83	.69
3.867	.82	9.867	2.85	15.867	1.45	21.87	.69
3.900	.82	9.900	2.85	15.900	1.45	21.90	.69
3.933	.83	9.933	2.91	15.933	1.44	21.93	.69
3.967	.83	9.967	2.97	15.967	1.43	21.97	.69
4.000	.83	10.000	2.97	16.000	1.43	22.00	.69
4.033	.84	10.033	3.10	16.033	1.41	22.03	.68
4.067	.84	10.067	3.10	16.067	1.41	22.07	.68
4.100	.84	10.100	3.17	16.100	1.39	22.10	.68
4.133	.84	10.133	3.25	16.133	1.38	22.13	.68
4.167	.84	10.167	3.25	16.167	1.38	22.17	.68
4.200	.85	10.200	3.41	16.200	1.36	22.20	.67
4.233	.85	10.233	3.41	16.233	1.36	22.23	.67
4.267	.86	10.267	3.50	16.267	1.35	22.27	.67
4.300	.86	10.300	3.59	16.300	1.34	22.30	.67
4.333	.86	10.333	3.59	16.333	1.34	22.33	.67
4.367	.87	10.367	3.80	16.367	1.32	22.37	.66
4.400	.87	10.400	3.80	16.400	1.32	22.40	.66
4.433	.87	10.433	3.91	16.433	1.31	22.43	.66
4.467	.88	10.467	4.03	16.467	1.30	22.47	.66
4.500	.88	10.500	4.03	16.500	1.30	22.50	.66
4.533	.89	10.533	4.29	16.533	1.28	22.53	.65
4.567	.89	10.567	4.29	16.567	1.28	22.57	.65
4.600	.89	10.600	4.45	16.600	1.27	22.60	.65
4.633	.89	10.633	4.60	16.633	1.26	22.63	.65
4.667	.89	10.667	4.60	16.667	1.26	22.67	.65
4.700	.90	10.700	4.96	16.700	1.25	22.70	.65
4.733	.90	10.733	4.96	16.733	1.25	22.73	.65
4.767	.91	10.767	5.17	16.767	1.24	22.77	.64
4.800	.91	10.800	5.38	16.800	1.23	22.80	.64
4.833	.91	10.833	5.38	16.833	1.23	22.83	.64
4.867	.92	10.867	5.89	16.867	1.21	22.87	.64
4.900	.92	10.900	5.89	16.900	1.21	22.90	.64
4.933	.93	10.933	6.21	16.933	1.20	22.93	.64
4.967	.93	10.967	6.52	16.967	1.20	22.97	.63
5.000	.93	11.000	6.52	17.000	1.19	23.00	.63
5.033	.94	11.033	7.31	17.033	1.18	23.03	.63
5.067	.94	11.067	7.31	17.067	1.18	23.07	.63
5.100	.95	11.100	7.82	17.100	1.17	23.10	.63
5.133	.95	11.133	8.33	17.133	1.16	23.13	.63
5.167	.95	11.167	8.34	17.167	1.16	23.17	.63
5.200	.96	11.200	9.71	17.200	1.15	23.20	.62
5.233	.96	11.233	9.71	17.233	1.15	23.23	.62
5.267	.97	11.267	10.69	17.267	1.14	23.27	.62
5.300	.97	11.300	11.67	17.300	1.13	23.30	.62
5.333	.97	11.333	11.67	17.333	1.13	23.33	.62
5.367	.98	11.367	14.64	17.367	1.12	23.37	.62
5.400	.98	11.400	14.64	17.400	1.12	23.40	.62
5.433	.99	11.433	17.15	17.433	1.11	23.43	.61
5.467	.99	11.467	19.66	17.467	1.11	23.47	.61
5.500	.99	11.500	19.67	17.500	1.11	23.50	.61
5.533	1.00	11.533	29.72	17.533	1.09	23.53	.61
5.567	1.00	11.567	29.72	17.567	1.09	23.57	.61
5.600	1.01	11.600	43.92	17.600	1.09	23.60	.61
5.633	1.01	11.633	58.04	17.633	1.08	23.63	.61
5.667	1.01	11.667	58.14	17.667	1.08	23.67	.61
5.700	1.03	11.700	134.02	17.700	1.07	23.70	.60
5.733	1.03	11.733	134.02	17.733	1.07	23.73	.60
5.767	1.03	11.767	96.40	17.767	1.06	23.77	.60
5.800	1.04	11.800	58.98	17.800	1.06	23.80	.60
5.833	1.04	11.833	58.95	17.833	1.06	23.83	.60
5.867	1.05	11.867	30.75	17.867	1.04	23.87	.60
5.900	1.05	11.900	30.75	17.900	1.04	23.90	.60
5.933	1.06	11.933	25.59	17.933	1.04	23.93	.59
5.967	1.06	11.967	20.46	17.967	1.03	23.97	.59
6.000	1.06	12.000	20.45	18.000	1.03	24.00	.59

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .082 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 26.268
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .371

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

NASHYD (0024) | Area (ha)= 5.03 | Curve Number (CN)= 72.5
 ID= 1 DT= 2.0 min | Ia (mm)= 4.75 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= .543 (i)
 TIME TO PEAK (hrs)= 11.800
 RUNOFF VOLUME (mm)= 19.056
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .269

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0022) | Area (ha)= 3.01 | Curve Number (CN)= 71.6
 ID= 1 DT= 2.0 min | Ia (mm)= 5.22 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .355 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 18.122
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .256

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0023)
 IN= 2---> OUT= 1
 DT= 2.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.2156
.0001	.1117	20.0000	.2166

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0022)	3.01	.36	11.77	18.12
OUTFLOW: ID= 1 (0023)	3.01	.00	13.60	.01

PEAK FLOW REDUCTION [Qout/Qin](%)= .01
 TIME SHIFT OF PEAK FLOW (min)=110.00
 MAXIMUM STORAGE USED (ha.m.)= .0545

ADD HYD (0026)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0024):	5.03	.543	11.80	19.06
+ ID2= 2 (0023):	3.01	.000	13.60	.01
=====				
ID = 3 (0026):	8.04	.543	11.80	11.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0025)
 IN= 2---> OUT= 1
 DT= 2.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0003	.2171
.0001	.0498	20.0000	.2181
.0002	.1676	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0026)	8.04	.54	11.80	11.93
OUTFLOW: ID= 1 (0025)	8.04	.00	13.70	.01

PEAK FLOW REDUCTION [Qout/Qin](%)= .03
 TIME SHIFT OF PEAK FLOW (min)=114.00
 MAXIMUM STORAGE USED (ha.m.)= .0958

ADD HYD (0028)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0027):	.68	.082	11.77	26.27
+ ID2= 2 (0025):	8.04	.000	13.70	.01

=====

ID = 3 (0028): 8.72 .082 11.77 2.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0029)
 IN= 2----> OUT= 1
 DT= 2.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0898
.0001	.0455	20.0000	.0908

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0028)	8.72	.08	11.77	2.05
OUTFLOW: ID= 1 (0029)	8.72	.00	24.17	.02

PEAK FLOW REDUCTION [Qout/Qin](%)= .05
 TIME SHIFT OF PEAK FLOW (min)=744.00
 MAXIMUM STORAGE USED (ha.m.)= .0178

CALIB
 NASHYD (0032)
 ID= 1 DT= 5.0 min

Area (ha)=	6.71	Curve Number (CN)=	64.3
Ia (mm)=	8.68	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	.32		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	.59	6.083	1.08	12.083	15.27	18.08	1.02
.167	.60	6.167	1.09	12.167	12.18	18.17	1.01
.250	.60	6.250	1.10	12.250	10.15	18.25	1.00
.333	.60	6.333	1.12	12.333	8.71	18.33	.99
.417	.61	6.417	1.13	12.417	7.64	18.42	.98
.500	.61	6.500	1.15	12.500	6.81	18.50	.97
.583	.61	6.583	1.16	12.583	6.16	18.58	.96
.667	.62	6.667	1.18	12.667	5.62	18.67	.95
.750	.62	6.750	1.20	12.750	5.18	18.75	.94
.833	.63	6.833	1.21	12.833	4.80	18.83	.93
.917	.63	6.917	1.23	12.917	4.48	18.92	.92
1.000	.63	7.000	1.25	13.000	4.20	19.00	.91
1.083	.64	7.083	1.27	13.083	3.96	19.08	.90
1.167	.64	7.167	1.29	13.167	3.75	19.17	.90
1.250	.65	7.250	1.31	13.250	3.56	19.25	.89
1.333	.65	7.333	1.33	13.333	3.39	19.33	.88
1.417	.65	7.417	1.35	13.417	3.23	19.42	.87
1.500	.66	7.500	1.37	13.500	3.09	19.50	.86
1.583	.66	7.583	1.40	13.583	2.97	19.58	.86
1.667	.67	7.667	1.42	13.667	2.85	19.67	.85
1.750	.67	7.750	1.44	13.750	2.75	19.75	.84
1.833	.68	7.833	1.47	13.833	2.65	19.83	.83
1.917	.68	7.917	1.50	13.917	2.56	19.92	.83
2.000	.69	8.000	1.53	14.000	2.47	20.00	.82
2.083	.69	8.083	1.56	14.083	2.40	20.08	.81
2.167	.70	8.167	1.59	14.167	2.32	20.17	.81
2.250	.70	8.250	1.62	14.250	2.26	20.25	.80
2.333	.71	8.333	1.65	14.333	2.19	20.33	.79
2.417	.71	8.417	1.69	14.417	2.13	20.42	.79
2.500	.72	8.500	1.72	14.500	2.08	20.50	.78
2.583	.72	8.583	1.76	14.583	2.02	20.58	.77
2.667	.73	8.667	1.80	14.667	1.97	20.67	.77
2.750	.73	8.750	1.85	14.750	1.93	20.75	.76
2.833	.74	8.833	1.89	14.833	1.88	20.83	.76
2.917	.74	8.917	1.94	14.917	1.84	20.92	.75
3.000	.75	9.000	1.99	15.000	1.80	21.00	.75
3.083	.76	9.083	2.05	15.083	1.76	21.08	.74
3.167	.76	9.167	2.10	15.167	1.72	21.17	.73
3.250	.77	9.250	2.16	15.250	1.69	21.25	.73
3.333	.77	9.333	2.23	15.333	1.65	21.33	.72
3.417	.78	9.417	2.30	15.417	1.62	21.42	.72
3.500	.79	9.500	2.37	15.500	1.59	21.50	.71
3.583	.79	9.583	2.45	15.583	1.56	21.58	.71
3.667	.80	9.667	2.54	15.667	1.53	21.67	.70
3.750	.81	9.750	2.63	15.750	1.50	21.75	.70
3.833	.82	9.833	2.74	15.833	1.48	21.83	.69
3.917	.82	9.917	2.85	15.917	1.45	21.92	.69
4.000	.83	10.000	2.97	16.000	1.43	22.00	.69
4.083	.84	10.083	3.10	16.083	1.41	22.08	.68
4.167	.84	10.167	3.25	16.167	1.38	22.17	.68
4.250	.85	10.250	3.41	16.250	1.36	22.25	.67
4.333	.86	10.333	3.59	16.333	1.34	22.33	.67
4.417	.87	10.417	3.80	16.417	1.32	22.42	.66

4.500	.88	10.500	4.03	16.500	1.30	22.50	.66
4.583	.89	10.583	4.29	16.583	1.28	22.58	.65
4.667	.89	10.667	4.60	16.667	1.26	22.67	.65
4.750	.90	10.750	4.96	16.750	1.25	22.75	.65
4.833	.91	10.833	5.38	16.833	1.23	22.83	.64
4.917	.92	10.917	5.89	16.917	1.21	22.92	.64
5.000	.93	11.000	6.52	17.000	1.20	23.00	.63
5.083	.94	11.083	7.31	17.083	1.18	23.08	.63
5.167	.95	11.167	8.33	17.167	1.16	23.17	.63
5.250	.96	11.250	9.71	17.250	1.15	23.25	.62
5.333	.97	11.333	11.67	17.333	1.13	23.33	.62
5.417	.98	11.417	14.64	17.417	1.12	23.42	.62
5.500	.99	11.500	19.66	17.500	1.11	23.50	.61
5.583	1.00	11.583	29.72	17.583	1.09	23.58	.61
5.667	1.01	11.667	58.04	17.667	1.08	23.67	.61
5.750	1.03	11.750	134.01	17.750	1.07	23.75	.60
5.833	1.04	11.833	58.99	17.833	1.06	23.83	.60
5.917	1.05	11.917	30.75	17.917	1.04	23.92	.60
6.000	1.06	12.000	20.46	18.000	1.03	24.00	.60

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .239 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 18.944
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB |
| NASHYD (0030) | Area (ha)= 5.57 Curve Number (CN)= 69.8
| ID= 1 DT= 5.0 min | Ia (mm)= 6.12 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .06

```

Unit Hyd Qpeak (cms)= 3.828

PEAK FLOW (cms)= .550 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 19.641
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .278

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ROUTE CHN (0031) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

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<----- DATA FOR SECTION ( 1.2) ----->
Distance      Elevation      Manning
.00           386.25         .0300
37.50        385.75         .0300 / .0300 Main Channel
47.50        385.75         .0300 / .0300 Main Channel
85.00        386.25         .0300

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<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)        (m)       (cu.m.)     (cms)          (m/s)        (min)
.03      385.78   .150E+03     .1             .33          23.91
.05      385.80   .350E+03     .3             .47          16.85
.08      385.83   .599E+03     .7             .56          14.12
.11      385.86   .898E+03     1.2           .63          12.62
.13      385.88   .125E+04     1.8           .68          11.65
.16      385.91   .164E+04     2.5           .73          10.95
.18      385.93   .209E+04     3.3           .76          10.42
.21      385.96   .259E+04     4.3           .80          9.99
.24      385.99   .313E+04     5.4           .82          9.64
.26      386.01   .373E+04     6.7           .85          9.33
.29      386.04   .438E+04     8.0           .88          9.07
.32      386.07   .507E+04     9.6           .90          8.83
.34      386.09   .582E+04    11.2          .92          8.62
.37      386.12   .661E+04    13.1          .94          8.43
.39      386.14   .745E+04    15.1          .96          8.25
.42      386.17   .835E+04    17.2          .98          8.08
.45      386.20   .929E+04    19.5          1.00         7.93
.47      386.22   .103E+05    22.0          1.02         7.79
.50      386.25   .113E+05    24.7          1.04         7.65

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<---- hydrograph ----> <-pipe / channel->
AREA      QPEAK      TPEAK      R.V.      MAX DEPTH      MAX VEL
(ha)      (cms)      (hrs)      (mm)      (m)            (m/s)
INFLOW : ID= 2 (0030)  5.57      .55      11.75    19.64      .07          .52
OUTFLOW: ID= 1 (0031)  5.57      .23      11.92    19.62      .04          .39

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-----
| ADD HYD (0033) |
| 1 + 2 = 3 |
-----
          AREA   QPEAK   TPEAK   R.V.
          (ha)   (cms)   (hrs)   (mm)
ID1= 1 (0032):  6.71   .239   12.08   18.94
+ ID2= 2 (0031):  5.57   .227   11.92   19.62
=====
ID = 3 (0033):  12.27  .432   12.00   19.25

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB |
| NASHYD (0036) | Area (ha)= 2.08 Curve Number (CN)= 67.6
| ID= 1 DT= 5.0 min | Ia (mm)= 7.71 # of Linear Res.(N)= 3.00
-----
          U.H. Tp(hrs)= .08

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Unit Hyd Qpeak (cms)= .938

PEAK FLOW (cms)= .165 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 20.502
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .290

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB |
| NASHYD (0034) | Area (ha)= 2.15 Curve Number (CN)= 71.9
| ID= 1 DT= 5.0 min | Ia (mm)= 5.03 # of Linear Res.(N)= 3.00
-----
          U.H. Tp(hrs)= .10

```

Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .198 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 25.577
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .362

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ROUTE CHN (0035) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00
-----

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<----- DATA FOR SECTION ( 1.3) ----->
Distance      Elevation      Manning
   .00         388.25         .0300
  30.00        387.75         .0300 / .0300  Main Channel
  40.00        387.75         .0300 / .0300  Main Channel
  70.00        388.25         .0300

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH    ELEV    VOLUME    FLOW RATE    VELOCITY    TRAV.TIME
(m)      (m)      (cu.m.)   (cms)        (m/s)       (min)
.03     387.78   .327E+02   .1            .41         4.35
.05     387.80   .744E+02   .4            .59         3.03
.08     387.83   .125E+03   .8            .71         2.52
.11     387.86   .185E+03   1.4           .80         2.25
.13     387.88   .253E+03   2.0           .87         2.07
.16     387.91   .330E+03   2.8           .92         1.95
.18     387.93   .417E+03   3.7           .97         1.85
.21     387.96   .512E+03   4.8           1.01        1.78
.24     387.99   .616E+03   6.0           1.04        1.72
.26     388.01   .729E+03   7.3           1.07        1.67
.29     388.04   .851E+03   8.7           1.10        1.63
.32     388.07   .982E+03   10.3          1.13        1.59
.34     388.09   .112E+04   12.0          1.15        1.56
.37     388.12   .127E+04   13.9          1.17        1.53
.39     388.14   .143E+04   15.9          1.19        1.50
.42     388.17   .160E+04   18.0          1.21        1.48
.45     388.20   .177E+04   20.3          1.23        1.45
.47     388.22   .196E+04   22.8          1.25        1.43
.50     388.25   .215E+04   25.4          1.27        1.41

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<---- hydrograph ----> <-pipe / channel->
          AREA   QPEAK   TPEAK   R.V.   MAX DEPTH   MAX VEL
          (ha)   (cms)   (hrs)   (mm)   (m)         (m/s)
INFLOW : ID= 2 (0034)  2.15   .20   11.83  25.58   .03         .45
OUTFLOW: ID= 1 (0035)  2.15   .17   11.92  25.58   .03         .43

```


ADD HYD (0037)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0036):	2.08	.165	11.75	20.50
+ ID2= 2 (0035):	2.15	.174	11.92	25.58
=====				
ID = 3 (0037):	4.23	.329	11.83	23.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0039)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	35.03	65.5
	Ia (mm)= 7.17	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 1.16	

Unit Hyd Qpeak (cms)= 1.152

PEAK FLOW (cms)= .539 (i)
 TIME TO PEAK (hrs)= 13.083
 RUNOFF VOLUME (mm)= 20.448
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0040)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	3.95	54.0
	Ia (mm)= 10.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .40	

Unit Hyd Qpeak (cms)= .375

PEAK FLOW (cms)= .082 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 13.300
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .188

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0041)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min	.0000	.0000	.0002	.1655
	.0001	.0976	20.0000	.1665

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.08	12.17	13.30
OUTFLOW: ID= 1 (0041)	3.95	.00	25.42	.06

PEAK FLOW REDUCTION [Qout/Qin](%)= .07
 TIME SHIFT OF PEAK FLOW (min)=795.00
 MAXIMUM STORAGE USED (ha.m.)= .0523

CALIB NASHYD (0044)	Area (ha)	Curve Number (CN)
ID= 1 DT= 3.0 min	.87	64.6
	Ia (mm)= 6.68	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .06	

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.050	.59	6.050	1.08	12.050	15.27	18.05	1.02
.100	.59	6.100	1.08	12.100	14.24	18.10	1.02
.150	.60	6.150	1.09	12.150	12.18	18.15	1.01
.200	.60	6.200	1.10	12.200	10.83	18.20	1.00
.250	.60	6.250	1.10	12.250	10.15	18.25	1.00
.300	.60	6.300	1.12	12.300	8.71	18.30	.99
.350	.60	6.350	1.12	12.350	8.35	18.35	.99
.400	.61	6.400	1.13	12.400	7.64	18.40	.98
.450	.61	6.450	1.14	12.450	7.09	18.45	.97
.500	.61	6.500	1.15	12.500	6.81	18.50	.97
.550	.61	6.550	1.16	12.550	6.16	18.55	.96

.600	.62	6.600	1.17	12.600	5.98	18.60	.96
.650	.62	6.650	1.18	12.650	5.62	18.65	.95
.700	.62	6.700	1.19	12.700	5.32	18.70	.94
.750	.62	6.750	1.20	12.750	5.18	18.75	.94
.800	.63	6.800	1.21	12.800	4.80	18.80	.93
.850	.63	6.850	1.22	12.850	4.69	18.85	.93
.900	.63	6.900	1.23	12.900	4.48	18.90	.92
.950	.63	6.950	1.24	12.950	4.30	18.95	.92
1.000	.63	7.000	1.25	13.000	4.20	19.00	.91
1.050	.64	7.050	1.27	13.050	3.96	19.05	.90
1.100	.64	7.100	1.27	13.100	3.89	19.10	.90
1.150	.64	7.150	1.29	13.150	3.75	19.15	.90
1.200	.64	7.200	1.30	13.200	3.62	19.20	.89
1.250	.65	7.250	1.31	13.250	3.56	19.25	.89
1.300	.65	7.300	1.33	13.300	3.39	19.30	.88
1.350	.65	7.350	1.34	13.350	3.34	19.35	.88
1.400	.65	7.400	1.35	13.400	3.23	19.40	.87
1.450	.66	7.450	1.36	13.450	3.14	19.45	.87
1.500	.66	7.500	1.37	13.500	3.09	19.50	.86
1.550	.66	7.550	1.40	13.550	2.97	19.55	.86
1.600	.66	7.600	1.40	13.600	2.93	19.60	.85
1.650	.67	7.650	1.42	13.650	2.85	19.65	.85
1.700	.67	7.700	1.44	13.700	2.78	19.70	.84
1.750	.67	7.750	1.44	13.750	2.75	19.75	.84
1.800	.68	7.800	1.47	13.800	2.65	19.80	.83
1.850	.68	7.850	1.48	13.850	2.62	19.85	.83
1.900	.68	7.900	1.50	13.900	2.56	19.90	.83
1.950	.68	7.950	1.52	13.950	2.50	19.95	.82
2.000	.69	8.000	1.53	14.000	2.47	20.00	.82
2.050	.69	8.050	1.56	14.050	2.40	20.05	.81
2.100	.69	8.100	1.57	14.100	2.37	20.10	.81
2.150	.70	8.150	1.59	14.150	2.32	20.15	.81
2.200	.70	8.200	1.61	14.200	2.28	20.20	.80
2.250	.70	8.250	1.62	14.250	2.26	20.25	.80
2.300	.71	8.300	1.65	14.300	2.19	20.30	.79
2.350	.71	8.350	1.66	14.350	2.17	20.35	.79
2.400	.71	8.400	1.69	14.400	2.13	20.40	.79
2.450	.72	8.450	1.71	14.450	2.09	20.45	.78
2.500	.72	8.500	1.72	14.500	2.08	20.50	.78
2.550	.72	8.550	1.76	14.550	2.02	20.55	.77
2.600	.72	8.600	1.78	14.600	2.01	20.60	.77
2.650	.73	8.650	1.80	14.650	1.97	20.65	.77
2.700	.73	8.700	1.83	14.700	1.94	20.70	.76
2.750	.73	8.750	1.85	14.750	1.92	20.75	.76
2.800	.74	8.800	1.89	14.800	1.88	20.80	.76
2.850	.74	8.850	1.91	14.850	1.87	20.85	.76
2.900	.74	8.900	1.94	14.900	1.84	20.90	.75
2.950	.75	8.950	1.98	14.950	1.81	20.95	.75
3.000	.75	9.000	1.99	15.000	1.80	21.00	.75
3.050	.76	9.050	2.05	15.050	1.76	21.05	.74
3.100	.76	9.100	2.07	15.100	1.75	21.10	.74
3.150	.76	9.150	2.10	15.150	1.72	21.15	.73
3.200	.77	9.200	2.14	15.200	1.70	21.20	.73
3.250	.77	9.250	2.16	15.250	1.69	21.25	.73
3.300	.77	9.300	2.23	15.300	1.65	21.30	.72
3.350	.78	9.350	2.25	15.350	1.64	21.35	.72
3.400	.78	9.400	2.30	15.400	1.62	21.40	.72
3.450	.79	9.450	2.35	15.450	1.60	21.45	.72
3.500	.79	9.500	2.37	15.500	1.59	21.50	.71
3.550	.79	9.550	2.45	15.550	1.56	21.55	.71
3.600	.80	9.600	2.48	15.600	1.55	21.60	.71
3.650	.80	9.650	2.54	15.650	1.53	21.65	.70
3.700	.81	9.700	2.60	15.700	1.51	21.70	.70
3.750	.81	9.750	2.63	15.750	1.50	21.75	.70
3.800	.82	9.800	2.74	15.800	1.48	21.80	.69
3.850	.82	9.850	2.77	15.850	1.47	21.85	.69
3.900	.82	9.900	2.85	15.900	1.45	21.90	.69
3.950	.83	9.950	2.93	15.950	1.44	21.95	.69
4.000	.83	10.000	2.97	16.000	1.43	22.00	.69
4.050	.84	10.050	3.10	16.050	1.41	22.05	.68
4.100	.84	10.100	3.15	16.100	1.40	22.10	.68
4.150	.84	10.150	3.25	16.150	1.38	22.15	.68
4.200	.85	10.200	3.35	16.200	1.37	22.20	.67
4.250	.85	10.250	3.41	16.250	1.36	22.25	.67
4.300	.86	10.300	3.59	16.300	1.34	22.30	.67
4.350	.86	10.350	3.66	16.350	1.33	22.35	.67
4.400	.87	10.400	3.80	16.400	1.32	22.40	.66
4.450	.87	10.450	3.95	16.450	1.31	22.45	.66
4.500	.88	10.500	4.03	16.500	1.30	22.50	.66
4.550	.89	10.550	4.29	16.550	1.28	22.55	.65
4.600	.89	10.600	4.39	16.600	1.28	22.60	.65
4.650	.89	10.650	4.60	16.650	1.26	22.65	.65
4.700	.90	10.700	4.84	16.700	1.25	22.70	.65
4.750	.90	10.750	4.96	16.750	1.25	22.75	.65
4.800	.91	10.800	5.38	16.800	1.23	22.80	.64
4.850	.91	10.850	5.55	16.850	1.22	22.85	.64
4.900	.92	10.900	5.89	16.900	1.21	22.90	.64
4.950	.93	10.950	6.31	16.950	1.20	22.95	.64
5.000	.93	11.000	6.52	17.000	1.19	23.00	.63

5.050	.94	11.050	7.31	17.050	1.18	23.05	.63
5.100	.94	11.100	7.65	17.100	1.17	23.10	.63
5.150	.95	11.150	8.33	17.150	1.16	23.15	.63
5.200	.96	11.200	9.25	17.200	1.15	23.20	.62
5.250	.96	11.250	9.71	17.250	1.15	23.25	.62
5.300	.97	11.300	11.67	17.300	1.13	23.30	.62
5.350	.97	11.350	12.66	17.350	1.13	23.35	.62
5.400	.98	11.400	14.64	17.400	1.12	23.40	.62
5.450	.99	11.450	17.99	17.450	1.11	23.45	.61
5.500	.99	11.500	19.66	17.500	1.11	23.50	.61
5.550	1.00	11.550	29.72	17.550	1.09	23.55	.61
5.600	1.01	11.600	39.17	17.600	1.09	23.60	.61
5.650	1.01	11.650	58.04	17.650	1.08	23.65	.61
5.700	1.02	11.700	108.73	17.700	1.07	23.70	.60
5.750	1.03	11.750	133.98	17.750	1.07	23.75	.60
5.800	1.04	11.800	58.98	17.800	1.06	23.80	.60
5.850	1.04	11.850	49.56	17.850	1.05	23.85	.60
5.900	1.05	11.900	30.75	17.900	1.04	23.90	.60
5.950	1.06	11.950	23.88	17.950	1.04	23.95	.59
6.000	1.06	12.000	20.45	18.000	1.03	24.00	.59

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .078 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 19.524
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| CALIB          |
| NASHYD (0042) | Area (ha)= .56 Curve Number (CN)= 70.0
| ID= 1 DT= 3.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= .06
-----

```

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .063 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 22.308
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .315

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0043) |
| IN= 2---> OUT= 1 |
| DT= 3.0 min      |
|                |
|                | OUTFLOW   STORAGE   | OUTFLOW   STORAGE
|                | (cms)     (ha.m.)   | (cms)     (ha.m.)
|                | .0000     .0000     | .0002     .0357
|                | .0001     .0118     | 20.0000   .0367
|                |
|                | AREA      QPEAK     TPEAK     R.V.
|                | (ha)      (cms)      (hrs)     (mm)
|                | .56       .06        11.75    22.31
|                | .56       .00        20.10    .49
|                |
|                | INFLOW : ID= 2 (0042)
|                | OUTFLOW: ID= 1 (0043)
|                |
|                | PEAK FLOW REDUCTION [Qout/Qin](%)= .16
|                | TIME SHIFT OF PEAK FLOW (min)=501.00
|                | MAXIMUM STORAGE USED (ha.m.)= .0121
-----

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-----
| ADD HYD (0045) |
| 1 + 2 = 3      |
|                |
|                | AREA      QPEAK     TPEAK     R.V.
|                | (ha)      (cms)      (hrs)     (mm)
|                | .87       .078       11.75    19.52
|                | + ID2= 2 (0043): .56 .000 20.10 .49
|                |
|                | ID = 3 (0045): 1.42 .078 11.75 12.09
-----

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0046) |
| IN= 2---> OUT= 1 |
| DT= 3.0 min      |
|                |
|                | OUTFLOW   STORAGE   | OUTFLOW   STORAGE
|                | (cms)     (ha.m.)   | (cms)     (ha.m.)
|                | .0000     .0000     | .0002     .1073
|                | .0001     .0117     | 20.0000   .1083
|                |
|                | AREA      QPEAK     TPEAK     R.V.
-----

```

INFLOW : ID= 2 (0045) (ha) (cms) (hrs) (mm)
 1.42 .08 11.75 12.09
 OUTFLOW: ID= 1 (0046) 1.42 .00 24.10 .32

PEAK FLOW REDUCTION [Qout/Qin](%)= .13
 TIME SHIFT OF PEAK FLOW (min)=741.00
 MAXIMUM STORAGE USED (ha.m.)= .0168

CALIB NASHYD (0047) Area (ha)= .48 Curve Number (CN)= 70.0
 ID= 1 DT= 3.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .054 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 22.308
 TOTAL RAINFALL (mm)= 70.759
 RUNOFF COEFFICIENT = .315

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0048)
 IN= 2---> OUT= 1
 DT= 3.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0731
.0001	.0496	20.0000	.0741

INFLOW : ID= 2 (0047)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
OUTFLOW: ID= 1 (0048)	.48	.05	11.75	22.31
	.48	.00	20.15	.12

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=504.00
 MAXIMUM STORAGE USED (ha.m.)= .0107

CALIB NASHYD (0049) Area (ha)= 2.77 Curve Number (CN)= 70.7
 ID= 1 DT= 5.0 min Ia (mm)= 5.35 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	.59	6.083	1.08	12.083	15.27	18.08	1.02
.167	.60	6.167	1.09	12.167	12.18	18.17	1.01
.250	.60	6.250	1.10	12.250	10.15	18.25	1.00
.333	.60	6.333	1.12	12.333	8.71	18.33	.99
.417	.61	6.417	1.13	12.417	7.64	18.42	.98
.500	.61	6.500	1.15	12.500	6.81	18.50	.97
.583	.61	6.583	1.16	12.583	6.16	18.58	.96
.667	.62	6.667	1.18	12.667	5.62	18.67	.95
.750	.62	6.750	1.20	12.750	5.18	18.75	.94
.833	.63	6.833	1.21	12.833	4.80	18.83	.93
.917	.63	6.917	1.23	12.917	4.48	18.92	.92
1.000	.63	7.000	1.25	13.000	4.20	19.00	.91
1.083	.64	7.083	1.27	13.083	3.96	19.08	.90
1.167	.64	7.167	1.29	13.167	3.75	19.17	.90
1.250	.65	7.250	1.31	13.250	3.56	19.25	.89
1.333	.65	7.333	1.33	13.333	3.39	19.33	.88
1.417	.65	7.417	1.35	13.417	3.23	19.42	.87
1.500	.66	7.500	1.37	13.500	3.09	19.50	.86
1.583	.66	7.583	1.40	13.583	2.97	19.58	.86
1.667	.67	7.667	1.42	13.667	2.85	19.67	.85
1.750	.67	7.750	1.44	13.750	2.75	19.75	.84
1.833	.68	7.833	1.47	13.833	2.65	19.83	.83
1.917	.68	7.917	1.50	13.917	2.56	19.92	.83
2.000	.69	8.000	1.53	14.000	2.47	20.00	.82
2.083	.69	8.083	1.56	14.083	2.40	20.08	.81
2.167	.70	8.167	1.59	14.167	2.32	20.17	.81
2.250	.70	8.250	1.62	14.250	2.26	20.25	.80
2.333	.71	8.333	1.65	14.333	2.19	20.33	.79
2.417	.71	8.417	1.69	14.417	2.13	20.42	.79
2.500	.72	8.500	1.72	14.500	2.08	20.50	.78
2.583	.72	8.583	1.76	14.583	2.02	20.58	.77
2.667	.73	8.667	1.80	14.667	1.97	20.67	.77
2.750	.73	8.750	1.85	14.750	1.93	20.75	.76

2.833	.74	8.833	1.89	14.833	1.88	20.83	.76
2.917	.74	8.917	1.94	14.917	1.84	20.92	.75
3.000	.75	9.000	1.99	15.000	1.80	21.00	.75
3.083	.76	9.083	2.05	15.083	1.76	21.08	.74
3.167	.76	9.167	2.10	15.167	1.72	21.17	.73
3.250	.77	9.250	2.16	15.250	1.69	21.25	.73
3.333	.77	9.333	2.23	15.333	1.65	21.33	.72
3.417	.78	9.417	2.30	15.417	1.62	21.42	.72
3.500	.79	9.500	2.37	15.500	1.59	21.50	.71
3.583	.79	9.583	2.45	15.583	1.56	21.58	.71
3.667	.80	9.667	2.54	15.667	1.53	21.67	.70
3.750	.81	9.750	2.63	15.750	1.50	21.75	.70
3.833	.82	9.833	2.74	15.833	1.48	21.83	.69
3.917	.82	9.917	2.85	15.917	1.45	21.92	.69
4.000	.83	10.000	2.97	16.000	1.43	22.00	.69
4.083	.84	10.083	3.10	16.083	1.41	22.08	.68
4.167	.84	10.167	3.25	16.167	1.38	22.17	.68
4.250	.85	10.250	3.41	16.250	1.36	22.25	.67
4.333	.86	10.333	3.59	16.333	1.34	22.33	.67
4.417	.87	10.417	3.80	16.417	1.32	22.42	.66
4.500	.88	10.500	4.03	16.500	1.30	22.50	.66
4.583	.89	10.583	4.29	16.583	1.28	22.58	.65
4.667	.89	10.667	4.60	16.667	1.26	22.67	.65
4.750	.90	10.750	4.96	16.750	1.25	22.75	.65
4.833	.91	10.833	5.38	16.833	1.23	22.83	.64
4.917	.92	10.917	5.89	16.917	1.21	22.92	.64
5.000	.93	11.000	6.52	17.000	1.20	23.00	.63
5.083	.94	11.083	7.31	17.083	1.18	23.08	.63
5.167	.95	11.167	8.33	17.167	1.16	23.17	.63
5.250	.96	11.250	9.71	17.250	1.15	23.25	.62
5.333	.97	11.333	11.67	17.333	1.13	23.33	.62
5.417	.98	11.417	14.64	17.417	1.12	23.42	.62
5.500	.99	11.500	19.66	17.500	1.11	23.50	.61
5.583	1.00	11.583	29.72	17.583	1.09	23.58	.61
5.667	1.01	11.667	58.04	17.667	1.08	23.67	.61
5.750	1.03	11.750	134.01	17.750	1.07	23.75	.60
5.833	1.04	11.833	58.99	17.833	1.06	23.83	.60
5.917	1.05	11.917	30.75	17.917	1.04	23.92	.60
6.000	1.06	12.000	20.46	18.000	1.03	24.00	.60

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .241 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 24.615
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .348

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0055) Area (ha)= 5.19 Curve Number (CN)= 73.3
 ID= 1 DT= 5.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .504 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 27.461
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .388

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0052) Area (ha)= 3.90 Curve Number (CN)= 69.4
 ID= 1 DT= 5.0 min Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .374 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 22.838
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .323

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0050) Area (ha)= 11.96 Curve Number (CN)= 66.4
 ID= 1 DT= 5.0 min Ia (mm)= 5.74 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .18

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= .705 (i)
TIME TO PEAK (hrs)= 11.917
RUNOFF VOLUME (mm)= 21.776
TOTAL RAINFALL (mm)= 70.710
RUNOFF COEFFICIENT = .308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0051)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.0000 .0000 | 20.0000 .1583
.0001 .1573 | .0000 .0000

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW : ID= 2 (0050) 11.96 .71 11.92 21.78
OUTFLOW: ID= 1 (0051) 11.96 .19 12.75 8.62

PEAK FLOW REDUCTION [Qout/Qin](%)= 26.85
TIME SHIFT OF PEAK FLOW (min)= 50.00
MAXIMUM STORAGE USED (ha.m.)= .2080

ADD HYD (0053)
1 + 2 = 3

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0052): 3.90 .374 11.75 22.84
+ ID2= 2 (0051): 11.96 .189 12.75 8.62
ID = 3 (0053): 15.86 .374 11.75 12.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0054)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.0000 .0000 | 20.0000 .0771
.0001 .0761 | .0000 .0000

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW : ID= 2 (0053) 15.86 .37 11.75 12.12
OUTFLOW: ID= 1 (0054) 15.86 .12 13.25 7.32

PEAK FLOW REDUCTION [Qout/Qin](%)= 31.89
TIME SHIFT OF PEAK FLOW (min)= 90.00
MAXIMUM STORAGE USED (ha.m.)= .1332

ROUTE CHN (0056)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

DATA FOR SECTION (1.5) ----->
Distance Elevation Manning
.00 425.00 .0300
.75 424.25 .0300 / .0300 Main Channel
1.75 424.25 .0300 / .0300 Main Channel
2.50 425.00 .0300

TRAVEL TIME TABLE

Table with 6 columns: DEPTH (m), ELEV (m), VOLUME (cu.m.), FLOW RATE (cms), VELOCITY (m/s), TRAV.TIME (min). Rows show data for depths from .04 to .51 meters.

.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0054)	15.86	.12	13.25	7.32	.09	1.13
OUTFLOW: ID= 1 (0056)	15.86	.08	13.50	7.32	.07	.96

ADD HYD (0057)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0055):	5.19	.504	11.83	27.46
+ ID2= 2 (0056):	15.86	.079	13.50	7.32
=====				
ID = 3 (0057):	21.05	.504	11.83	12.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0058)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	21.77	5.22	.35	67.4	3.00

Unit Hyd Qpeak (cms)= 2.354
 PEAK FLOW (cms)= .886 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 22.801
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .322

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0059)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	11.96	5.74	.18	66.4	3.00

Unit Hyd Qpeak (cms)= 2.557
 PEAK FLOW (cms)= .705 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 21.776
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .308

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0060)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1 DT= 5.0 min	.0000	.0000	20.0000	.1583
	.0001	.1573	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0059)	11.96	.71	11.92	21.78
OUTFLOW: ID= 1 (0060)	11.96	.19	12.75	8.62

PEAK FLOW REDUCTION [Qout/Qin](%)= 26.85
 TIME SHIFT OF PEAK FLOW (min)= 50.00
 MAXIMUM STORAGE USED (ha.m.)= .2080

CALIB NASHYD (0061)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	3.90	4.85	.08	69.4	3.00

Unit Hyd Qpeak (cms)= 1.935
 PEAK FLOW (cms)= .374 (i)

TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 22.838
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .323

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD (0062) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0060):  11.96      .189      12.75      8.62
+ ID2= 2 (0061):  3.90      .374      11.75      22.84
=====
ID = 3 (0062):  15.86      .374      11.75      12.12
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0063) |
| IN= 2----> OUT= 1 |
| DT= 5.0 min |
-----
      OUTFLOW      STORAGE      OUTFLOW      STORAGE
      (cms)      (ha.m.)      (cms)      (ha.m.)
      .0000      .0000      20.0000      .0771
      .0001      .0761      .0000      .0000

      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0062)  15.86      .37      11.75      12.12
OUTFLOW: ID= 1 (0063)  15.86      .12      13.25      7.32

PEAK FLOW REDUCTION [Qout/Qin](%)= 31.89
TIME SHIFT OF PEAK FLOW (min)= 90.00
MAXIMUM STORAGE USED (ha.m.)= .1332
  
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-----
| ROUTE CHN (0065) |
| IN= 2----> OUT= 1 |
-----
      Routing time step (min)'= 5.00

<----- DATA FOR SECTION ( 1.5) ----->
      Distance      Elevation      Manning
      .00      425.00      .0300
      .75      424.25      .0300 / .0300 Main Channel
      1.75      424.25      .0300 / .0300 Main Channel
      2.50      425.00      .0300
  
```

```

<----- TRAVEL TIME TABLE ----->
      DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
      (m)      (m)      (cu.m.)      (cms)      (m/s)      (min)
      .04      424.29      .145E+02      .0      .68      8.63
      .08      424.33      .302E+02      .1      1.05      5.61
      .12      424.37      .469E+02      .2      1.33      4.42
      .16      424.41      .647E+02      .3      1.57      3.76
      .20      424.45      .837E+02      .4      1.77      3.34
      .24      424.49      .104E+03      .6      1.94      3.04
      .28      424.53      .125E+03      .7      2.10      2.81
      .32      424.57      .147E+03      .9      2.23      2.64
      .36      424.61      .170E+03      1.1      2.36      2.50
      .39      424.64      .195E+03      1.4      2.47      2.39
      .43      424.68      .220E+03      1.6      2.57      2.30
      .47      424.72      .247E+03      1.9      2.66      2.22
      .51      424.76      .275E+03      2.1      2.75      2.15
      .55      424.80      .304E+03      2.4      2.83      2.09
      .59      424.84      .334E+03      2.7      2.90      2.04
      .63      424.88      .365E+03      3.1      2.97      1.99
      .67      424.92      .397E+03      3.4      3.03      1.95
      .71      424.96      .430E+03      3.8      3.09      1.91
      .75      425.00      .465E+03      4.1      3.14      1.88
  
```

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<----- hydrograph -----> <-pipe / channel->
      AREA      QPEAK      TPEAK      R.V.      MAX DEPTH      MAX VEL
      (ha)      (cms)      (hrs)      (mm)      (m)      (m/s)
INFLOW : ID= 2 (0063)  15.86      .12      13.25      7.32      .09      1.13
OUTFLOW: ID= 1 (0065)  15.86      .08      13.50      7.32      .07      .96
  
```

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-----
| CALIB      (0064) |
| NASHYD      (0064) |
| ID= 1 DT= 5.0 min |
-----
      Area (ha)= 5.19      Curve Number (CN)= 73.3
      Ia (mm)= 4.00      # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .11
  
```

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .504 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 27.461
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .388

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0066)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0065):	15.86	.079	13.50	7.32
+ ID2= 2 (0064):	5.19	.504	11.83	27.46
ID = 3 (0066):	21.05	.504	11.83	12.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0069)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	1.80	8.49	.07	58.8	3.00

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .114 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 14.609
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .207

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0067)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	1.52	8.00	.06	62.0	3.00

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .111 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 15.239
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .216

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0068)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1 DT= 5.0 min	.0000	.0000	20.0000	.0207
	.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.11	11.75	15.24
OUTFLOW: ID= 1 (0068)	1.52	.00	18.83	1.71

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.68
 TIME SHIFT OF PEAK FLOW (min)=425.00
 MAXIMUM STORAGE USED (ha.m.)= .0209

ADD HYD (0071)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0069):	1.80	.114	11.75	14.61
+ ID2= 2 (0068):	1.52	.002	18.83	1.71
ID = 3 (0071):	3.32	.114	11.75	8.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0070)

IN= 2---> OUT= 1
DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0708
	.0001	.0707	.0000	.0000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 2 (0071)		3.32	.11	11.75
OUTFLOW: ID= 1 (0070)		3.32	.00	24.25

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
TIME SHIFT OF PEAK FLOW (min)=750.00
MAXIMUM STORAGE USED (ha.m.)= .0287

ROUTE CHN (0073)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.6) ----->

Distance	Elevation	Manning	
.00	421.26	.0300	
1.10	420.66	.0300 / .0300	Main Channel
2.00	420.66	.0300 / .0300	Main Channel
3.10	421.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

<---- hydrograph ----> <-pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	3.32	.00	24.25	.04	.00	.05
OUTFLOW: ID= 1 (0073)	3.32	.00	24.17	.04	.00	.05

ADD HYD (0074)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0066):	21.05	.504	11.83	12.29
+ ID2= 2 (0073):	3.32	.000	24.17	.04
=====				
ID = 3 (0074):	24.37	.504	11.83	10.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0072)
ID= 1 DT= 5.0 min

Area (ha)= 24.19 Curve Number (CN)= 60.0
Ia (mm)= 8.62 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .37

Unit Hyd Qpeak (cms)= 2.505
PEAK FLOW (cms)= .679 (i)
TIME TO PEAK (hrs)= 12.167
RUNOFF VOLUME (mm)= 16.630
TOTAL RAINFALL (mm)= 70.710
RUNOFF COEFFICIENT = .235

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0074):	24.37	.504	11.83	10.62
+ ID2= 2 (0072):	24.19	.679	12.17	16.63
ID = 3 (0075):	48.56	.918	11.92	13.61

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0076)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	127.28	59.9
	Ia (mm)= 8.29	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .79	

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 2.119 (i)
 TIME TO PEAK (hrs)= 12.667
 RUNOFF VOLUME (mm)= 16.766
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .237

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0077)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	17.28	58.3
	Ia (mm)= 9.24	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .57	

Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .333 (i)
 TIME TO PEAK (hrs)= 12.417
 RUNOFF VOLUME (mm)= 15.545
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .220

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0082)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	.24	77.6
	Ia (mm)= 3.49	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .11	

Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .027 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 31.589
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .447

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0078)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	2.66	59.8
	Ia (mm)= 8.55	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .07	

Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .171 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 15.233
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .215

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0079)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1	.0000	.0000	20.0000	.0608
DT= 5.0 min	.0001	.0607	.0000	.0000
	AREA	QPEAK	TPEAK	R.V.

INFLOW : ID= 2 (0078) (ha) (cms) (hrs) (mm)
 2.66 .17 11.75 15.23
 OUTFLOW: ID= 1 (0079) 2.66 .00 24.17 .09

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=745.00
 MAXIMUM STORAGE USED (ha.m.)= .0403

ADD HYD (0083)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0082):	.24	.027	11.83	31.59
+ ID2= 2 (0079):	2.66	.000	24.17	.09
=====				
ID = 3 (0083):	2.90	.027	11.83	2.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0080)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	14.63	9.37	.57	58.0	3.00

Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .278 (i)
 TIME TO PEAK (hrs)= 12.417
 RUNOFF VOLUME (mm)= 15.359
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .217

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0081)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0083):	2.90	.027	11.83	2.67
+ ID2= 2 (0080):	14.63	.278	12.42	15.36
=====				
ID = 3 (0081):	17.52	.282	12.42	13.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0084)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	7.71	9.14	.29	62.5	3.00

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .268 (i)
 TIME TO PEAK (hrs)= 12.000
 RUNOFF VOLUME (mm)= 17.682
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .250

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0085)	Area (ha)	Ia (mm)	U.H. Tp(hrs)	Curve Number (CN)	# of Linear Res.(N)
ID= 1 DT= 5.0 min	.91	8.53	.11	64.9	3.00

Unit Hyd Qpeak (cms)= .313

PEAK FLOW (cms)= .060 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 19.014
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .269

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0086)	Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min	19.15	71.3

|ID= 1 DT= 5.0 min | Ia (mm)= 5.81 # of Linear Res.(N)= 3.00
 ----- U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= 1.097 (i)
 TIME TO PEAK (hrs)= 12.000
 RUNOFF VOLUME (mm)= 25.156
 TOTAL RAINFALL (mm)= 70.710
 RUNOFF COEFFICIENT = .356

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ** SIMULATION NUMBER: 3 **

| CHICAGO STORM |
Ptotal= 81.99 mm

IDF curve parameters: A=1231.993
 B= 7.975
 C= .809
 used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = .49

The CORRELATION coefficient is = .9995

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	155.00	154.92
10.	115.00	119.01
15.	99.00	97.58
30.	70.00	64.98
60.	40.00	40.57
120.	24.00	24.32
360.	9.70	10.35
720.	5.90	5.96
1440.	3.60	3.42

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.67	6.08	1.22	12.08	17.98	18.08	1.16
.17	.67	6.17	1.24	12.17	14.30	18.17	1.15
.25	.68	6.25	1.26	12.25	11.89	18.25	1.14
.33	.68	6.33	1.27	12.33	10.18	18.33	1.12
.42	.69	6.42	1.29	12.42	8.91	18.42	1.11
.50	.69	6.50	1.31	12.50	7.93	18.50	1.10
.58	.69	6.58	1.32	12.58	7.16	18.58	1.09
.67	.70	6.67	1.34	12.67	6.53	18.67	1.08
.75	.70	6.75	1.36	12.75	6.00	18.75	1.07
.83	.71	6.83	1.38	12.83	5.56	18.83	1.06
.92	.71	6.92	1.40	12.92	5.19	18.92	1.05
1.00	.72	7.00	1.42	13.00	4.86	19.00	1.04
1.08	.72	7.08	1.44	13.08	4.58	19.08	1.03
1.17	.73	7.17	1.47	13.17	4.32	19.17	1.02
1.25	.73	7.25	1.49	13.25	4.10	19.25	1.01
1.33	.74	7.33	1.51	13.33	3.90	19.33	1.00
1.42	.74	7.42	1.54	13.42	3.72	19.42	.99
1.50	.75	7.50	1.56	13.50	3.56	19.50	.98
1.58	.75	7.58	1.59	13.58	3.41	19.58	.97
1.67	.76	7.67	1.62	13.67	3.28	19.67	.96
1.75	.76	7.75	1.65	13.75	3.16	19.75	.95
1.83	.77	7.83	1.68	13.83	3.04	19.83	.95
1.92	.77	7.92	1.71	13.92	2.94	19.92	.94
2.00	.78	8.00	1.74	14.00	2.84	20.00	.93
2.08	.78	8.08	1.78	14.08	2.75	20.08	.92
2.17	.79	8.17	1.81	14.17	2.66	20.17	.91
2.25	.79	8.25	1.85	14.25	2.59	20.25	.91
2.33	.80	8.33	1.89	14.33	2.51	20.33	.90
2.42	.81	8.42	1.93	14.42	2.44	20.42	.89
2.50	.81	8.50	1.97	14.50	2.38	20.50	.89
2.58	.82	8.58	2.02	14.58	2.32	20.58	.88
2.67	.82	8.67	2.06	14.67	2.26	20.67	.87
2.75	.83	8.75	2.11	14.75	2.20	20.75	.86
2.83	.84	8.83	2.17	14.83	2.15	20.83	.86
2.92	.84	8.92	2.22	14.92	2.10	20.92	.85
3.00	.85	9.00	2.28	15.00	2.05	21.00	.85
3.08	.86	9.08	2.34	15.08	2.01	21.08	.84
3.17	.86	9.17	2.41	15.17	1.97	21.17	.83
3.25	.87	9.25	2.48	15.25	1.93	21.25	.83
3.33	.88	9.33	2.56	15.33	1.89	21.33	.82
3.42	.89	9.42	2.64	15.42	1.85	21.42	.81
3.50	.89	9.50	2.72	15.50	1.81	21.50	.81
3.58	.90	9.58	2.82	15.58	1.78	21.58	.80
3.67	.91	9.67	2.92	15.67	1.75	21.67	.80

3.75	.92	9.75	3.03	15.75	1.72	21.75	.79
3.83	.92	9.83	3.14	15.83	1.69	21.83	.79
3.92	.93	9.92	3.27	15.92	1.66	21.92	.78
4.00	.94	10.00	3.41	16.00	1.63	22.00	.78
4.08	.95	10.08	3.57	16.08	1.60	22.08	.77
4.17	.96	10.17	3.74	16.17	1.58	22.17	.77
4.25	.97	10.25	3.93	16.25	1.55	22.25	.76
4.33	.98	10.33	4.14	16.33	1.53	22.33	.76
4.42	.99	10.42	4.38	16.42	1.50	22.42	.75
4.50	1.00	10.50	4.65	16.50	1.48	22.50	.75
4.58	1.01	10.58	4.96	16.58	1.46	22.58	.74
4.67	1.01	10.67	5.32	16.67	1.44	22.67	.74
4.75	1.03	10.75	5.75	16.75	1.42	22.75	.73
4.83	1.04	10.83	6.24	16.83	1.40	22.83	.73
4.92	1.05	10.92	6.85	16.92	1.38	22.92	.72
5.00	1.06	11.00	7.59	17.00	1.36	23.00	.72
5.08	1.07	11.08	8.52	17.08	1.34	23.08	.71
5.17	1.08	11.17	9.74	17.17	1.32	23.17	.71
5.25	1.09	11.25	11.37	17.25	1.31	23.25	.71
5.33	1.10	11.33	13.69	17.33	1.29	23.33	.70
5.42	1.11	11.42	17.22	17.42	1.28	23.42	.70
5.50	1.13	11.50	23.19	17.50	1.26	23.50	.69
5.58	1.14	11.58	35.13	17.58	1.24	23.58	.69
5.67	1.15	11.67	68.35	17.67	1.23	23.67	.68
5.75	1.17	11.75	154.92	17.75	1.21	23.75	.68
5.83	1.18	11.83	69.45	17.83	1.20	23.83	.68
5.92	1.20	11.92	36.35	17.92	1.19	23.92	.67
6.00	1.21	12.00	24.14	18.00	1.17	24.00	.67

CALIB (0021) Area (ha)= 8.81 Curve Number (CN)= 68.3
NASHYD (0021) Ia (mm)= 6.50 # of Linear Res.(N)= 3.00
ID= 1 DT= 5.0 min U.H. Tp(hrs)= 1.36

Unit Hyd Qpeak (cms)= .248
PEAK FLOW (cms)= .177 (i)
TIME TO PEAK (hrs)= 13.250
RUNOFF VOLUME (mm)= 29.453
TOTAL RAINFALL (mm)= 81.991
RUNOFF COEFFICIENT = .359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB (0027) Area (ha)= .68 Curve Number (CN)= 72.2
NASHYD (0027) Ia (mm)= 4.91 # of Linear Res.(N)= 3.00
ID= 1 DT= 2.0 min U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.033	.67	6.033	1.22	12.033	17.98	18.03	1.16
.067	.67	6.067	1.22	12.067	17.98	18.07	1.16
.100	.67	6.100	1.23	12.100	16.13	18.10	1.15
.133	.67	6.133	1.24	12.133	14.30	18.13	1.15
.167	.67	6.167	1.24	12.167	14.30	18.17	1.15
.200	.68	6.200	1.26	12.200	11.89	18.20	1.14
.233	.68	6.233	1.26	12.233	11.89	18.23	1.14
.267	.68	6.267	1.26	12.267	11.03	18.27	1.13
.300	.68	6.300	1.27	12.300	10.18	18.30	1.12
.333	.68	6.333	1.27	12.333	10.18	18.33	1.12
.367	.69	6.367	1.29	12.367	8.91	18.37	1.11
.400	.69	6.400	1.29	12.400	8.91	18.40	1.11
.433	.69	6.433	1.30	12.433	8.42	18.43	1.11
.467	.69	6.467	1.31	12.467	7.93	18.47	1.10
.500	.69	6.500	1.31	12.500	7.93	18.50	1.10
.533	.69	6.533	1.32	12.533	7.16	18.53	1.09
.567	.69	6.567	1.32	12.567	7.16	18.57	1.09
.600	.70	6.600	1.33	12.600	6.84	18.60	1.08
.633	.70	6.633	1.34	12.633	6.53	18.63	1.08
.667	.70	6.667	1.34	12.667	6.53	18.67	1.08
.700	.70	6.700	1.36	12.700	6.00	18.70	1.07
.733	.70	6.733	1.36	12.733	6.00	18.73	1.07
.767	.71	6.767	1.37	12.767	5.78	18.77	1.06
.800	.71	6.800	1.38	12.800	5.56	18.80	1.06
.833	.71	6.833	1.38	12.833	5.56	18.83	1.06
.867	.71	6.867	1.40	12.867	5.19	18.87	1.05
.900	.71	6.900	1.40	12.900	5.19	18.90	1.05
.933	.71	6.933	1.41	12.933	5.02	18.93	1.04
.967	.72	6.967	1.42	12.967	4.86	18.97	1.04

1.000	.72	7.000	1.42	13.000	4.86	19.00	1.04
1.033	.72	7.033	1.44	13.033	4.58	19.03	1.03
1.067	.72	7.067	1.44	13.067	4.58	19.07	1.03
1.100	.72	7.100	1.46	13.100	4.45	19.10	1.02
1.133	.73	7.133	1.47	13.133	4.32	19.13	1.02
1.167	.73	7.167	1.47	13.167	4.32	19.17	1.02
1.200	.73	7.200	1.49	13.200	4.10	19.20	1.01
1.233	.73	7.233	1.49	13.233	4.10	19.23	1.01
1.267	.73	7.267	1.50	13.267	4.00	19.27	1.00
1.300	.74	7.300	1.51	13.300	3.90	19.30	1.00
1.333	.74	7.333	1.51	13.333	3.90	19.33	1.00
1.367	.74	7.367	1.54	13.367	3.72	19.37	.99
1.400	.74	7.400	1.54	13.400	3.72	19.40	.99
1.433	.74	7.433	1.55	13.433	3.64	19.43	.98
1.467	.75	7.467	1.56	13.467	3.56	19.47	.98
1.500	.75	7.500	1.56	13.500	3.56	19.50	.98
1.533	.75	7.533	1.59	13.533	3.41	19.53	.97
1.567	.75	7.567	1.59	13.567	3.41	19.57	.97
1.600	.75	7.600	1.60	13.600	3.35	19.60	.97
1.633	.76	7.633	1.62	13.633	3.28	19.63	.96
1.667	.76	7.667	1.62	13.667	3.28	19.67	.96
1.700	.76	7.700	1.65	13.700	3.16	19.70	.95
1.733	.76	7.733	1.65	13.733	3.16	19.73	.95
1.767	.76	7.767	1.66	13.767	3.10	19.77	.95
1.800	.77	7.800	1.68	13.800	3.04	19.80	.95
1.833	.77	7.833	1.68	13.833	3.04	19.83	.95
1.867	.77	7.867	1.71	13.867	2.94	19.87	.94
1.900	.77	7.900	1.71	13.900	2.94	19.90	.94
1.933	.77	7.933	1.73	13.933	2.89	19.93	.93
1.967	.78	7.967	1.74	13.967	2.84	19.97	.93
2.000	.78	8.000	1.74	14.000	2.84	20.00	.93
2.033	.78	8.033	1.78	14.033	2.75	20.03	.92
2.067	.78	8.067	1.78	14.067	2.75	20.07	.92
2.100	.79	8.100	1.79	14.100	2.71	20.10	.92
2.133	.79	8.133	1.81	14.133	2.66	20.13	.91
2.167	.79	8.167	1.81	14.167	2.66	20.17	.91
2.200	.79	8.200	1.85	14.200	2.59	20.20	.91
2.233	.79	8.233	1.85	14.233	2.59	20.23	.91
2.267	.80	8.267	1.87	14.267	2.55	20.27	.90
2.300	.80	8.300	1.89	14.300	2.51	20.30	.90
2.333	.80	8.333	1.89	14.333	2.51	20.33	.90
2.367	.81	8.367	1.93	14.367	2.44	20.37	.89
2.400	.81	8.400	1.93	14.400	2.44	20.40	.89
2.433	.81	8.433	1.95	14.433	2.41	20.43	.89
2.467	.81	8.467	1.97	14.467	2.38	20.47	.89
2.500	.81	8.500	1.97	14.500	2.38	20.50	.89
2.533	.82	8.533	2.02	14.533	2.32	20.53	.88
2.567	.82	8.567	2.02	14.567	2.32	20.57	.88
2.600	.82	8.600	2.04	14.600	2.29	20.60	.87
2.633	.82	8.633	2.06	14.633	2.26	20.63	.87
2.667	.82	8.667	2.06	14.667	2.26	20.67	.87
2.700	.83	8.700	2.11	14.700	2.20	20.70	.86
2.733	.83	8.733	2.11	14.733	2.20	20.73	.86
2.767	.83	8.767	2.14	14.767	2.18	20.77	.86
2.800	.84	8.800	2.17	14.800	2.15	20.80	.86
2.833	.84	8.833	2.17	14.833	2.15	20.83	.86
2.867	.84	8.867	2.22	14.867	2.10	20.87	.85
2.900	.84	8.900	2.22	14.900	2.10	20.90	.85
2.933	.85	8.933	2.25	14.933	2.08	20.93	.85
2.967	.85	8.967	2.28	14.967	2.05	20.97	.85
3.000	.85	9.000	2.28	15.000	2.05	21.00	.85
3.033	.86	9.033	2.34	15.033	2.01	21.03	.84
3.067	.86	9.067	2.34	15.067	2.01	21.07	.84
3.100	.86	9.100	2.38	15.100	1.99	21.10	.84
3.133	.86	9.133	2.41	15.133	1.97	21.13	.83
3.167	.86	9.167	2.41	15.167	1.97	21.17	.83
3.200	.87	9.200	2.48	15.200	1.93	21.20	.83
3.233	.87	9.233	2.48	15.233	1.93	21.23	.83
3.267	.88	9.267	2.52	15.267	1.91	21.27	.82
3.300	.88	9.300	2.56	15.300	1.89	21.30	.82
3.333	.88	9.333	2.56	15.333	1.89	21.33	.82
3.367	.89	9.367	2.64	15.367	1.85	21.37	.81
3.400	.89	9.400	2.64	15.400	1.85	21.40	.81
3.433	.89	9.433	2.68	15.433	1.83	21.43	.81
3.467	.89	9.467	2.72	15.467	1.81	21.47	.81
3.500	.89	9.500	2.72	15.500	1.81	21.50	.81
3.533	.90	9.533	2.82	15.533	1.78	21.53	.80
3.567	.90	9.567	2.82	15.567	1.78	21.57	.80
3.600	.90	9.600	2.87	15.600	1.76	21.60	.80
3.633	.91	9.633	2.92	15.633	1.75	21.63	.80
3.667	.91	9.667	2.92	15.667	1.75	21.67	.80
3.700	.92	9.700	3.03	15.700	1.72	21.70	.79
3.733	.92	9.733	3.03	15.733	1.72	21.73	.79
3.767	.92	9.767	3.08	15.767	1.70	21.77	.79
3.800	.92	9.800	3.14	15.800	1.69	21.80	.79
3.833	.92	9.833	3.14	15.833	1.69	21.83	.79
3.867	.93	9.867	3.27	15.867	1.66	21.87	.78
3.900	.93	9.900	3.27	15.900	1.66	21.90	.78
3.933	.94	9.933	3.34	15.933	1.64	21.93	.78

3.967	.94	9.967	3.41	15.967	1.63	21.97	.78
4.000	.94	10.000	3.41	16.000	1.63	22.00	.78
4.033	.95	10.033	3.57	16.033	1.60	22.03	.77
4.067	.95	10.067	3.57	16.067	1.60	22.07	.77
4.100	.95	10.100	3.65	16.100	1.59	22.10	.77
4.133	.96	10.133	3.74	16.133	1.58	22.13	.77
4.167	.96	10.167	3.74	16.167	1.58	22.17	.77
4.200	.97	10.200	3.93	16.200	1.55	22.20	.76
4.233	.97	10.233	3.93	16.233	1.55	22.23	.76
4.267	.97	10.267	4.04	16.267	1.54	22.27	.76
4.300	.98	10.300	4.14	16.300	1.53	22.30	.76
4.333	.98	10.333	4.14	16.333	1.53	22.33	.76
4.367	.99	10.367	4.38	16.367	1.50	22.37	.75
4.400	.99	10.400	4.38	16.400	1.50	22.40	.75
4.433	.99	10.433	4.52	16.433	1.49	22.43	.75
4.467	1.00	10.467	4.65	16.467	1.48	22.47	.75
4.500	1.00	10.500	4.65	16.500	1.48	22.50	.75
4.533	1.01	10.533	4.96	16.533	1.46	22.53	.74
4.567	1.01	10.567	4.96	16.567	1.46	22.57	.74
4.600	1.01	10.600	5.14	16.600	1.45	22.60	.74
4.633	1.01	10.633	5.32	16.633	1.44	22.63	.74
4.667	1.01	10.667	5.32	16.667	1.44	22.67	.74
4.700	1.03	10.700	5.75	16.700	1.42	22.70	.73
4.733	1.03	10.733	5.75	16.733	1.42	22.73	.73
4.767	1.03	10.767	6.00	16.767	1.41	22.77	.73
4.800	1.04	10.800	6.24	16.800	1.40	22.80	.73
4.833	1.04	10.833	6.25	16.833	1.40	22.83	.73
4.867	1.05	10.867	6.85	16.867	1.38	22.87	.72
4.900	1.05	10.900	6.85	16.900	1.38	22.90	.72
4.933	1.05	10.933	7.22	16.933	1.37	22.93	.72
4.967	1.06	10.967	7.59	16.967	1.36	22.97	.72
5.000	1.06	11.000	7.59	17.000	1.36	23.00	.72
5.033	1.07	11.033	8.52	17.033	1.34	23.03	.71
5.067	1.07	11.067	8.52	17.067	1.34	23.07	.71
5.100	1.07	11.100	9.13	17.100	1.33	23.10	.71
5.133	1.08	11.133	9.74	17.133	1.32	23.13	.71
5.167	1.08	11.167	9.74	17.167	1.32	23.17	.71
5.200	1.09	11.200	11.37	17.200	1.31	23.20	.71
5.233	1.09	11.233	11.37	17.233	1.31	23.23	.71
5.267	1.10	11.267	12.53	17.267	1.30	23.27	.70
5.300	1.10	11.300	13.69	17.300	1.29	23.30	.70
5.333	1.10	11.333	13.69	17.333	1.29	23.33	.70
5.367	1.11	11.367	17.22	17.367	1.28	23.37	.70
5.400	1.11	11.400	17.22	17.400	1.28	23.40	.70
5.433	1.12	11.433	20.21	17.433	1.27	23.43	.69
5.467	1.13	11.467	23.19	17.467	1.26	23.47	.69
5.500	1.13	11.500	23.21	17.500	1.26	23.50	.69
5.533	1.14	11.533	35.13	17.533	1.24	23.53	.69
5.567	1.14	11.567	35.13	17.567	1.24	23.57	.69
5.600	1.15	11.600	51.78	17.600	1.24	23.60	.69
5.633	1.15	11.633	68.35	17.633	1.23	23.63	.68
5.667	1.15	11.667	68.46	17.667	1.23	23.67	.68
5.700	1.17	11.700	154.92	17.700	1.21	23.70	.68
5.733	1.17	11.733	154.92	17.733	1.21	23.73	.68
5.767	1.17	11.767	112.07	17.767	1.21	23.77	.68
5.800	1.18	11.800	69.45	17.800	1.20	23.80	.68
5.833	1.18	11.833	69.40	17.833	1.20	23.83	.68
5.867	1.20	11.867	36.35	17.867	1.19	23.87	.67
5.900	1.20	11.900	36.35	17.900	1.19	23.90	.67
5.933	1.20	11.933	30.23	17.933	1.18	23.93	.67
5.967	1.21	11.967	24.14	17.967	1.17	23.97	.67
6.000	1.21	12.000	24.13	18.000	1.17	24.00	.67

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .106 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 33.683
 TOTAL RAINFALL (mm)= 81.990
 RUNOFF COEFFICIENT = .411

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0024) | Area (ha)= 5.03 Curve Number (CN)= 72.5
 | ID= 1 DT= 2.0 min | Ia (mm)= 4.75 # of Linear Res.(N)= 3.00
 |-----| U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= .703 (i)
 TIME TO PEAK (hrs)= 11.800
 RUNOFF VOLUME (mm)= 24.837
 TOTAL RAINFALL (mm)= 81.990
 RUNOFF COEFFICIENT = .303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB (0022) |
| NASHYD (0022) | Area (ha)= 3.01 Curve Number (CN)= 71.6
| ID= 1 DT= 2.0 min | Ia (mm)= 5.22 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .06

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Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .461 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 23.720
 TOTAL RAINFALL (mm)= 81.990
 RUNOFF COEFFICIENT = .289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR (0023) |
| IN= 2----> OUT= 1 |
| DT= 2.0 min |
|-----|
| OUTFLOW STORAGE | OUTFLOW STORAGE |
| (cms) (ha.m.) | (cms) (ha.m.) |
| .0000 .0000 | .0002 .2156 |
| .0001 .1117 | 20.0000 .2166 |
|-----|
| AREA QPEAK TPEAK R.V. |
| (ha) (cms) (hrs) (mm) |
| INFLOW : ID= 2 (0022) 3.01 .46 11.77 23.72 |
| OUTFLOW: ID= 1 (0023) 3.01 .00 13.60 .01 |
|-----|
| PEAK FLOW REDUCTION [Qout/Qin](%)= .01 |
| TIME SHIFT OF PEAK FLOW (min)=110.00 |
| MAXIMUM STORAGE USED (ha.m.)= .0713 |

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-----
| ADD HYD (0026) |
| 1 + 2 = 3 |
|-----|
| AREA QPEAK TPEAK R.V. |
| (ha) (cms) (hrs) (mm) |
| ID1= 1 (0024): 5.03 .703 11.80 24.84 |
| + ID2= 2 (0023): 3.01 .000 13.60 .01 |
|-----|
| ID = 3 (0026): 8.04 .703 11.80 15.55 |

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| RESERVOIR (0025) |
| IN= 2----> OUT= 1 |
| DT= 2.0 min |
|-----|
| OUTFLOW STORAGE | OUTFLOW STORAGE |
| (cms) (ha.m.) | (cms) (ha.m.) |
| .0000 .0000 | .0003 .2171 |
| .0001 .0498 | 20.0000 .2181 |
| .0002 .1676 | .0000 .0000 |
|-----|
| AREA QPEAK TPEAK R.V. |
| (ha) (cms) (hrs) (mm) |
| INFLOW : ID= 2 (0026) 8.04 .70 11.80 15.55 |
| OUTFLOW: ID= 1 (0025) 8.04 .00 13.70 .02 |
|-----|
| PEAK FLOW REDUCTION [Qout/Qin](%)= .02 |
| TIME SHIFT OF PEAK FLOW (min)=114.00 |
| MAXIMUM STORAGE USED (ha.m.)= .1249 |

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-----
| ADD HYD (0028) |
| 1 + 2 = 3 |
|-----|
| AREA QPEAK TPEAK R.V. |
| (ha) (cms) (hrs) (mm) |
| ID1= 1 (0027): .68 .106 11.77 33.68 |
| + ID2= 2 (0025): 8.04 .000 13.70 .02 |
|-----|
| ID = 3 (0028): 8.72 .106 11.77 2.63 |

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| RESERVOIR (0029) |
| IN= 2----> OUT= 1 |
| DT= 2.0 min |
|-----|
| OUTFLOW STORAGE | OUTFLOW STORAGE |
| (cms) (ha.m.) | (cms) (ha.m.) |
| .0000 .0000 | .0002 .0898 |
| .0001 .0455 | 20.0000 .0908 |

```


INFLOW : ID= 2 (0028) AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)
 OUTFLOW: ID= 1 (0029) 8.72 .11 11.77 2.63
 8.72 .00 24.17 .02

PEAK FLOW REDUCTION [Qout/Qin](%)= .05
 TIME SHIFT OF PEAK FLOW (min)=744.00
 MAXIMUM STORAGE USED (ha.m.)= .0228

 CALIB Area (ha)= 6.71 Curve Number (CN)= 64.3
 NASHYD (0032) Ia (mm)= 8.68 # of Linear Res.(N)= 3.00
 ID= 1 DT= 5.0 min U.H. Tp(hrs)= .32

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.67	6.083	1.22	12.083	17.98	18.08	1.16
.167	.67	6.167	1.24	12.167	14.30	18.17	1.15
.250	.68	6.250	1.26	12.250	11.89	18.25	1.14
.333	.68	6.333	1.27	12.333	10.18	18.33	1.12
.417	.69	6.417	1.29	12.417	8.91	18.42	1.11
.500	.69	6.500	1.31	12.500	7.93	18.50	1.10
.583	.69	6.583	1.32	12.583	7.16	18.58	1.09
.667	.70	6.667	1.34	12.667	6.53	18.67	1.08
.750	.70	6.750	1.36	12.750	6.00	18.75	1.07
.833	.71	6.833	1.38	12.833	5.56	18.83	1.06
.917	.71	6.917	1.40	12.917	5.19	18.92	1.05
1.000	.72	7.000	1.42	13.000	4.86	19.00	1.04
1.083	.72	7.083	1.44	13.083	4.58	19.08	1.03
1.167	.73	7.167	1.47	13.167	4.32	19.17	1.02
1.250	.73	7.250	1.49	13.250	4.10	19.25	1.01
1.333	.74	7.333	1.51	13.333	3.90	19.33	1.00
1.417	.74	7.417	1.54	13.417	3.72	19.42	.99
1.500	.75	7.500	1.56	13.500	3.56	19.50	.98
1.583	.75	7.583	1.59	13.583	3.41	19.58	.97
1.667	.76	7.667	1.62	13.667	3.28	19.67	.96
1.750	.76	7.750	1.65	13.750	3.16	19.75	.95
1.833	.77	7.833	1.68	13.833	3.04	19.83	.95
1.917	.77	7.917	1.71	13.917	2.94	19.92	.94
2.000	.78	8.000	1.74	14.000	2.84	20.00	.93
2.083	.78	8.083	1.78	14.083	2.75	20.08	.92
2.167	.79	8.167	1.81	14.167	2.66	20.17	.91
2.250	.79	8.250	1.85	14.250	2.59	20.25	.91
2.333	.80	8.333	1.89	14.333	2.51	20.33	.90
2.417	.81	8.417	1.93	14.417	2.44	20.42	.89
2.500	.81	8.500	1.97	14.500	2.38	20.50	.89
2.583	.82	8.583	2.02	14.583	2.32	20.58	.88
2.667	.82	8.667	2.06	14.667	2.26	20.67	.87
2.750	.83	8.750	2.11	14.750	2.20	20.75	.86
2.833	.84	8.833	2.17	14.833	2.15	20.83	.86
2.917	.84	8.917	2.22	14.917	2.10	20.92	.85
3.000	.85	9.000	2.28	15.000	2.05	21.00	.85
3.083	.86	9.083	2.34	15.083	2.01	21.08	.84
3.167	.86	9.167	2.41	15.167	1.97	21.17	.83
3.250	.87	9.250	2.48	15.250	1.93	21.25	.83
3.333	.88	9.333	2.56	15.333	1.89	21.33	.82
3.417	.89	9.417	2.64	15.417	1.85	21.42	.81
3.500	.89	9.500	2.72	15.500	1.81	21.50	.81
3.583	.90	9.583	2.82	15.583	1.78	21.58	.80
3.667	.91	9.667	2.92	15.667	1.75	21.67	.80
3.750	.92	9.750	3.03	15.750	1.72	21.75	.79
3.833	.92	9.833	3.14	15.833	1.69	21.83	.79
3.917	.93	9.917	3.27	15.917	1.66	21.92	.78
4.000	.94	10.000	3.41	16.000	1.63	22.00	.78
4.083	.95	10.083	3.57	16.083	1.60	22.08	.77
4.167	.96	10.167	3.74	16.167	1.58	22.17	.77
4.250	.97	10.250	3.93	16.250	1.55	22.25	.76
4.333	.98	10.333	4.14	16.333	1.53	22.33	.76
4.417	.99	10.417	4.38	16.417	1.50	22.42	.75
4.500	1.00	10.500	4.65	16.500	1.48	22.50	.75
4.583	1.01	10.583	4.96	16.583	1.46	22.58	.74
4.667	1.01	10.667	5.32	16.667	1.44	22.67	.74
4.750	1.03	10.750	5.75	16.750	1.42	22.75	.73
4.833	1.04	10.833	6.24	16.833	1.40	22.83	.73
4.917	1.05	10.917	6.85	16.917	1.38	22.92	.72
5.000	1.06	11.000	7.59	17.000	1.36	23.00	.72
5.083	1.07	11.083	8.52	17.083	1.34	23.08	.71
5.167	1.08	11.167	9.74	17.167	1.32	23.17	.71
5.250	1.09	11.250	11.37	17.250	1.31	23.25	.71
5.333	1.10	11.333	13.69	17.333	1.29	23.33	.70
5.417	1.11	11.417	17.22	17.417	1.28	23.42	.70
5.500	1.13	11.500	23.19	17.500	1.26	23.50	.69

5.583	1.14	11.583	35.13	17.583	1.24	23.58	.69
5.667	1.15	11.667	68.35	17.667	1.23	23.67	.68
5.750	1.17	11.750	154.91	17.750	1.21	23.75	.68
5.833	1.18	11.833	69.46	17.833	1.20	23.83	.68
5.917	1.20	11.917	36.35	17.917	1.19	23.92	.67
6.000	1.21	12.000	24.14	18.000	1.17	24.00	.00

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .322 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 25.036
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0030) | Area (ha)= 5.57 Curve Number (CN)= 69.8
| ID= 1 DT= 5.0 min | Ia (mm)= 6.12 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .06
  
```

Unit Hyd Qpeak (cms)= 3.828

PEAK FLOW (cms)= .719 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 25.427
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .310

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ROUTE CHN (0031) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00
|-----|
<----- DATA FOR SECTION ( 1.2) ----->
Distance Elevation Manning
.00 386.25 .0300
37.50 385.75 .0300 / .0300 Main Channel
47.50 385.75 .0300 / .0300 Main Channel
85.00 386.25 .0300
  
```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 385.78 .150E+03 .1 .33 23.91
.05 385.80 .350E+03 .3 .47 16.85
.08 385.83 .599E+03 .7 .56 14.12
.11 385.86 .898E+03 1.2 .63 12.62
.13 385.88 .125E+04 1.8 .68 11.65
.16 385.91 .164E+04 2.5 .73 10.95
.18 385.93 .209E+04 3.3 .76 10.42
.21 385.96 .259E+04 4.3 .80 9.99
.24 385.99 .313E+04 5.4 .82 9.64
.26 386.01 .373E+04 6.7 .85 9.33
.29 386.04 .438E+04 8.0 .88 9.07
.32 386.07 .507E+04 9.6 .90 8.83
.34 386.09 .582E+04 11.2 .92 8.62
.37 386.12 .661E+04 13.1 .94 8.43
.39 386.14 .745E+04 15.1 .96 8.25
.42 386.17 .835E+04 17.2 .98 8.08
.45 386.20 .929E+04 19.5 1.00 7.93
.47 386.22 .103E+05 22.0 1.02 7.79
.50 386.25 .113E+05 24.7 1.04 7.65
  
```

```

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0030) 5.57 .72 11.75 25.43 .08 .56
OUTFLOW: ID= 1 (0031) 5.57 .32 11.92 25.41 .05 .45
  
```

```

-----
| ADD HYD (0033) |
| 1 + 2 = 3 |
|-----|
ID1= 1 (0032): 6.71 .322 12.08 25.04
+ ID2= 2 (0031): 5.57 .323 11.92 25.41
=====
ID = 3 (0033): 12.27 .598 11.92 25.20
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0036) | Area (ha)= 2.08 Curve Number (CN)= 67.6
| ID= 1 DT= 5.0 min | Ia (mm)= 7.71 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .08

```

Unit Hyd Qpeak (cms)= .938

PEAK FLOW (cms)= .219 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 26.826
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .327

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0034) | Area (ha)= 2.15 Curve Number (CN)= 71.9
| ID= 1 DT= 5.0 min | Ia (mm)= 5.03 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .10

```

Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .258 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 32.829
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .401

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ROUTE CHN (0035) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

```

```

-----
<----- DATA FOR SECTION ( 1.3) ----->
Distance Elevation Manning
.00 388.25 .0300
30.00 387.75 .0300 / .0300 Main Channel
40.00 387.75 .0300 / .0300 Main Channel
70.00 388.25 .0300

```

```

-----
<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 387.78 .327E+02 .1 .41 4.35
.05 387.80 .744E+02 .4 .59 3.03
.08 387.83 .125E+03 .8 .71 2.52
.11 387.86 .185E+03 1.4 .80 2.25
.13 387.88 .253E+03 2.0 .87 2.07
.16 387.91 .330E+03 2.8 .92 1.95
.18 387.93 .417E+03 3.7 .97 1.85
.21 387.96 .512E+03 4.8 1.01 1.78
.24 387.99 .616E+03 6.0 1.04 1.72
.26 388.01 .729E+03 7.3 1.07 1.67
.29 388.04 .851E+03 8.7 1.10 1.63
.32 388.07 .982E+03 10.3 1.13 1.59
.34 388.09 .112E+04 12.0 1.15 1.56
.37 388.12 .127E+04 13.9 1.17 1.53
.39 388.14 .143E+04 15.9 1.19 1.50
.42 388.17 .160E+04 18.0 1.21 1.48
.45 388.20 .177E+04 20.3 1.23 1.45
.47 388.22 .196E+04 22.8 1.25 1.43
.50 388.25 .215E+04 25.4 1.27 1.41

```

```

-----
<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0034) 2.15 .26 11.83 32.83 .04 .48
OUTFLOW: ID= 1 (0035) 2.15 .23 11.83 32.83 .04 .46

```

```

-----
| ADD HYD (0037) |
| 1 + 2 = 3 |
-----
AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0036): 2.08 .219 11.75 26.83
+ ID2= 2 (0035): 2.15 .231 11.83 32.83
=====
ID = 3 (0037): 4.23 .438 11.83 29.88

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 CALIB
 NASHYD (0039) Area (ha)= 35.03 Curve Number (CN)= 65.5
 ID= 1 DT= 5.0 min Ia (mm)= 7.17 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.16

Unit Hyd Qpeak (cms)= 1.152

PEAK FLOW (cms)= .719 (i)
 TIME TO PEAK (hrs)= 13.083
 RUNOFF VOLUME (mm)= 26.788
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .327

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0040) Area (ha)= 3.95 Curve Number (CN)= 54.0
 ID= 1 DT= 5.0 min Ia (mm)= 10.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .40

Unit Hyd Qpeak (cms)= .375

PEAK FLOW (cms)= .114 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 17.946
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .219

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 RESERVOIR (0041)
 IN= 2---> OUT= 1
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0002	.1655
	.0001	.0976	20.0000	.1665

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.11	12.17	17.95
OUTFLOW: ID= 1 (0041)	3.95	.00	25.33	.08

PEAK FLOW REDUCTION [Qout/Qin](%)= .06
 TIME SHIFT OF PEAK FLOW (min)=790.00
 MAXIMUM STORAGE USED (ha.m.)= .0706

 CALIB
 NASHYD (0044) Area (ha)= .87 Curve Number (CN)= 64.6
 ID= 1 DT= 3.0 min Ia (mm)= 6.68 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.050	.67	6.050	1.22	12.050	17.98	18.05	1.16
.100	.67	6.100	1.23	12.100	16.75	18.10	1.16
.150	.67	6.150	1.24	12.150	14.30	18.15	1.15
.200	.68	6.200	1.25	12.200	12.69	18.20	1.14
.250	.68	6.250	1.26	12.250	11.88	18.25	1.14
.300	.68	6.300	1.27	12.300	10.18	18.30	1.12
.350	.68	6.350	1.28	12.350	9.75	18.35	1.12
.400	.69	6.400	1.29	12.400	8.91	18.40	1.11
.450	.69	6.450	1.30	12.450	8.26	18.45	1.10
.500	.69	6.500	1.31	12.500	7.93	18.50	1.10
.550	.69	6.550	1.32	12.550	7.16	18.55	1.09
.600	.70	6.600	1.33	12.600	6.95	18.60	1.09
.650	.70	6.650	1.34	12.650	6.53	18.65	1.08
.700	.70	6.700	1.36	12.700	6.18	18.70	1.07
.750	.70	6.750	1.36	12.750	6.00	18.75	1.07
.800	.71	6.800	1.38	12.800	5.56	18.80	1.06
.850	.71	6.850	1.39	12.850	5.44	18.85	1.05
.900	.71	6.900	1.40	12.900	5.19	18.90	1.05
.950	.72	6.950	1.42	12.950	4.97	18.95	1.04
1.000	.72	7.000	1.42	13.000	4.86	19.00	1.04
1.050	.72	7.050	1.44	13.050	4.58	19.05	1.03
1.100	.72	7.100	1.45	13.100	4.49	19.10	1.02
1.150	.73	7.150	1.47	13.150	4.32	19.15	1.02
1.200	.73	7.200	1.48	13.200	4.18	19.20	1.01

1.250	.73	7.250	1.49	13.250	4.10	19.25	1.01
1.300	.74	7.300	1.51	13.300	3.90	19.30	1.00
1.350	.74	7.350	1.52	13.350	3.84	19.35	.99
1.400	.74	7.400	1.54	13.400	3.72	19.40	.99
1.450	.74	7.450	1.56	13.450	3.62	19.45	.98
1.500	.75	7.500	1.56	13.500	3.56	19.50	.98
1.550	.75	7.550	1.59	13.550	3.41	19.55	.97
1.600	.75	7.600	1.60	13.600	3.37	19.60	.97
1.650	.76	7.650	1.62	13.650	3.28	19.65	.96
1.700	.76	7.700	1.64	13.700	3.20	19.70	.96
1.750	.76	7.750	1.65	13.750	3.16	19.75	.95
1.800	.77	7.800	1.68	13.800	3.04	19.80	.95
1.850	.77	7.850	1.69	13.850	3.01	19.85	.94
1.900	.77	7.900	1.71	13.900	2.94	19.90	.94
1.950	.78	7.950	1.73	13.950	2.87	19.95	.93
2.000	.78	8.000	1.74	14.000	2.84	20.00	.93
2.050	.78	8.050	1.78	14.050	2.75	20.05	.92
2.100	.78	8.100	1.79	14.100	2.72	20.10	.92
2.150	.79	8.150	1.81	14.150	2.66	20.15	.91
2.200	.79	8.200	1.84	14.200	2.61	20.20	.91
2.250	.79	8.250	1.85	14.250	2.59	20.25	.91
2.300	.80	8.300	1.89	14.300	2.51	20.30	.90
2.350	.80	8.350	1.90	14.350	2.49	20.35	.90
2.400	.81	8.400	1.93	14.400	2.44	20.40	.89
2.450	.81	8.450	1.96	14.450	2.40	20.45	.89
2.500	.81	8.500	1.97	14.500	2.38	20.50	.89
2.550	.82	8.550	2.02	14.550	2.32	20.55	.88
2.600	.82	8.600	2.03	14.600	2.30	20.60	.88
2.650	.82	8.650	2.06	14.650	2.26	20.65	.87
2.700	.83	8.700	2.10	14.700	2.22	20.70	.87
2.750	.83	8.750	2.11	14.750	2.20	20.75	.86
2.800	.84	8.800	2.17	14.800	2.15	20.80	.86
2.850	.84	8.850	2.18	14.850	2.13	20.85	.86
2.900	.84	8.900	2.22	14.900	2.10	20.90	.85
2.950	.85	8.950	2.26	14.950	2.07	20.95	.85
3.000	.85	9.000	2.28	15.000	2.05	21.00	.85
3.050	.86	9.050	2.34	15.050	2.01	21.05	.84
3.100	.86	9.100	2.37	15.100	2.00	21.10	.84
3.150	.86	9.150	2.41	15.150	1.97	21.15	.83
3.200	.87	9.200	2.46	15.200	1.94	21.20	.83
3.250	.87	9.250	2.48	15.250	1.93	21.25	.83
3.300	.88	9.300	2.56	15.300	1.89	21.30	.82
3.350	.88	9.350	2.58	15.350	1.87	21.35	.82
3.400	.89	9.400	2.64	15.400	1.85	21.40	.81
3.450	.89	9.450	2.69	15.450	1.83	21.45	.81
3.500	.89	9.500	2.72	15.500	1.81	21.50	.81
3.550	.90	9.550	2.82	15.550	1.78	21.55	.80
3.600	.90	9.600	2.85	15.600	1.77	21.60	.80
3.650	.91	9.650	2.92	15.650	1.75	21.65	.80
3.700	.91	9.700	2.99	15.700	1.73	21.70	.79
3.750	.92	9.750	3.03	15.750	1.72	21.75	.79
3.800	.92	9.800	3.14	15.800	1.69	21.80	.79
3.850	.93	9.850	3.19	15.850	1.68	21.85	.78
3.900	.93	9.900	3.27	15.900	1.66	21.90	.78
3.950	.94	9.950	3.37	15.950	1.64	21.95	.78
4.000	.94	10.000	3.41	16.000	1.63	22.00	.78
4.050	.95	10.050	3.57	16.050	1.60	22.05	.77
4.100	.95	10.100	3.63	16.100	1.59	22.10	.77
4.150	.96	10.150	3.74	16.150	1.58	22.15	.77
4.200	.96	10.200	3.87	16.200	1.56	22.20	.76
4.250	.97	10.250	3.93	16.250	1.55	22.25	.76
4.300	.98	10.300	4.14	16.300	1.53	22.30	.76
4.350	.98	10.350	4.22	16.350	1.52	22.35	.75
4.400	.99	10.400	4.38	16.400	1.50	22.40	.75
4.450	.99	10.450	4.56	16.450	1.49	22.45	.75
4.500	1.00	10.500	4.65	16.500	1.48	22.50	.75
4.550	1.01	10.550	4.96	16.550	1.46	22.55	.74
4.600	1.01	10.600	5.08	16.600	1.45	22.60	.74
4.650	1.01	10.650	5.32	16.650	1.44	22.65	.74
4.700	1.02	10.700	5.61	16.700	1.42	22.70	.73
4.750	1.03	10.750	5.75	16.750	1.42	22.75	.73
4.800	1.04	10.800	6.24	16.800	1.40	22.80	.73
4.850	1.04	10.850	6.45	16.850	1.39	22.85	.73
4.900	1.05	10.900	6.85	16.900	1.38	22.90	.72
4.950	1.05	10.950	7.34	16.950	1.37	22.95	.72
5.000	1.06	11.000	7.59	17.000	1.36	23.00	.72
5.050	1.07	11.050	8.52	17.050	1.34	23.05	.71
5.100	1.07	11.100	8.93	17.100	1.34	23.10	.71
5.150	1.08	11.150	9.74	17.150	1.32	23.15	.71
5.200	1.09	11.200	10.83	17.200	1.31	23.20	.71
5.250	1.09	11.250	11.37	17.250	1.31	23.25	.71
5.300	1.10	11.300	13.69	17.300	1.29	23.30	.70
5.350	1.11	11.350	14.87	17.350	1.29	23.35	.70
5.400	1.11	11.400	17.22	17.400	1.28	23.40	.70
5.450	1.12	11.450	21.21	17.450	1.26	23.45	.69
5.500	1.13	11.500	23.20	17.500	1.26	23.50	.69
5.550	1.14	11.550	35.13	17.550	1.24	23.55	.69
5.600	1.14	11.600	46.22	17.600	1.24	23.60	.69
5.650	1.15	11.650	68.35	17.650	1.23	23.65	.68

5.700	1.16	11.700	126.11	17.700	1.22	23.70	.68
5.750	1.17	11.750	154.87	17.750	1.21	23.75	.68
5.800	1.18	11.800	69.45	17.800	1.20	23.80	.68
5.850	1.19	11.850	58.40	17.850	1.20	23.85	.68
5.900	1.20	11.900	36.35	17.900	1.19	23.90	.67
5.950	1.20	11.950	28.21	17.950	1.18	23.95	.67
6.000	1.21	12.000	24.14	18.000	1.17	24.00	.67

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .104 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 25.555
 TOTAL RAINFALL (mm)= 81.990
 RUNOFF COEFFICIENT = .312

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0042)	Area (ha)=	.56	Curve Number (CN)=	70.0			
ID= 1 DT= 3.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.06					

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .081 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 28.843
 TOTAL RAINFALL (mm)= 81.990
 RUNOFF COEFFICIENT = .352

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0043)							
IN= 2---> OUT= 1							
DT= 3.0 min							
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)			
	.0000	.0000	.0002	.0357			
	.0001	.0118	20.0000	.0367			
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)			
INFLOW : ID= 2 (0042)	.56	.08	11.75	28.84			
OUTFLOW: ID= 1 (0043)	.56	.00	20.10	.60			
	PEAK FLOW REDUCTION [Qout/Qin](%)=	.14					
	TIME SHIFT OF PEAK FLOW (min)=	501.00					
	MAXIMUM STORAGE USED (ha.m.)=	.0157					

ADD HYD (0045)							
1 + 2 = 3							
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)			
ID1= 1 (0044):	.87	.104	11.75	25.55			
+ ID2= 2 (0043):	.56	.000	20.10	.60			
ID = 3 (0045):	1.42	.104	11.75	15.81			

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0046)							
IN= 2---> OUT= 1							
DT= 3.0 min							
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)			
	.0000	.0000	.0002	.1073			
	.0001	.0117	20.0000	.1083			
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)			
INFLOW : ID= 2 (0045)	1.42	.10	11.75	15.81			
OUTFLOW: ID= 1 (0046)	1.42	.00	24.10	.34			
	PEAK FLOW REDUCTION [Qout/Qin](%)=	.11					
	TIME SHIFT OF PEAK FLOW (min)=	741.00					
	MAXIMUM STORAGE USED (ha.m.)=	.0220					

CALIB							
NASHYD (0047)	Area (ha)=	.48	Curve Number (CN)=	70.0			
ID= 1 DT= 3.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00			

U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .070 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 28.843
TOTAL RAINFALL (mm)= 81.990
RUNOFF COEFFICIENT = .352

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0048)
IN= 2---> OUT= 1
DT= 3.0 min

OUTFLOW (cms) STORAGE (ha.m.)
.0000 .0000
.0001 .0496

OUTFLOW (cms) STORAGE (ha.m.)
.0002 .0731
20.0000 .0741

AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)
INFLOW : ID= 2 (0047) .48 .07 11.75 28.84
OUTFLOW: ID= 1 (0048) .48 .00 20.15 .15

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
TIME SHIFT OF PEAK FLOW (min)=504.00
MAXIMUM STORAGE USED (ha.m.)= .0138

CALIB (0049)
NASHYD (0049)
ID= 1 DT= 5.0 min

Area (ha)= 2.77 Curve Number (CN)= 70.7
Ia (mm)= 5.35 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH

Table with 8 columns: TIME hrs, RAIN mm/hr, TIME hrs, RAIN mm/hr, TIME hrs, RAIN mm/hr, TIME hrs, RAIN mm/hr. It lists transformed rainfall data at 5-minute intervals.

3.917	.93	9.917	3.27	15.917	1.66	21.92	.78
4.000	.94	10.000	3.41	16.000	1.63	22.00	.78
4.083	.95	10.083	3.57	16.083	1.60	22.08	.77
4.167	.96	10.167	3.74	16.167	1.58	22.17	.77
4.250	.97	10.250	3.93	16.250	1.55	22.25	.76
4.333	.98	10.333	4.14	16.333	1.53	22.33	.76
4.417	.99	10.417	4.38	16.417	1.50	22.42	.75
4.500	1.00	10.500	4.65	16.500	1.48	22.50	.75
4.583	1.01	10.583	4.96	16.583	1.46	22.58	.74
4.667	1.01	10.667	5.32	16.667	1.44	22.67	.74
4.750	1.03	10.750	5.75	16.750	1.42	22.75	.73
4.833	1.04	10.833	6.24	16.833	1.40	22.83	.73
4.917	1.05	10.917	6.85	16.917	1.38	22.92	.72
5.000	1.06	11.000	7.59	17.000	1.36	23.00	.72
5.083	1.07	11.083	8.52	17.083	1.34	23.08	.71
5.167	1.08	11.167	9.74	17.167	1.32	23.17	.71
5.250	1.09	11.250	11.37	17.250	1.31	23.25	.71
5.333	1.10	11.333	13.69	17.333	1.29	23.33	.70
5.417	1.11	11.417	17.22	17.417	1.28	23.42	.70
5.500	1.13	11.500	23.19	17.500	1.26	23.50	.69
5.583	1.14	11.583	35.13	17.583	1.24	23.58	.69
5.667	1.15	11.667	68.35	17.667	1.23	23.67	.68
5.750	1.17	11.750	154.91	17.750	1.21	23.75	.68
5.833	1.18	11.833	69.46	17.833	1.20	23.83	.68
5.917	1.20	11.917	36.35	17.917	1.19	23.92	.67
6.000	1.21	12.000	24.14	18.000	1.17	24.00	.60

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .314 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 31.708
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .387

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0055) Area (ha)= 5.19 Curve Number (CN)= 73.3
 ID= 1 DT= 5.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .650 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 35.011
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0052) Area (ha)= 3.90 Curve Number (CN)= 69.4
 ID= 1 DT= 5.0 min Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .488 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 29.428
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0050) Area (ha)= 11.96 Curve Number (CN)= 66.4
 ID= 1 DT= 5.0 min Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .18

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= .931 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 28.306
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .345

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

RESERVOIR (0051)
IN= 2----> OUT= 1
DT= 5.0 min

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.1583
.0001	.1573	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0050)	11.96	.93	11.92	28.31
OUTFLOW: ID= 1 (0051)	11.96	.82	12.25	15.15

PEAK FLOW REDUCTION [Qout/Qin](%)= 88.17
 TIME SHIFT OF PEAK FLOW (min)= 20.00
 MAXIMUM STORAGE USED (ha.m.)= .2453

```

ADD HYD (0053)
1 + 2 = 3

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0052):	3.90	.488	11.75	29.43
+ ID2= 2 (0051):	11.96	.821	12.25	15.15
=====				
ID = 3 (0053):	15.86	.895	12.25	18.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

RESERVOIR (0054)
IN= 2----> OUT= 1
DT= 5.0 min

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.0771
.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0053)	15.86	.90	12.25	18.66
OUTFLOW: ID= 1 (0054)	15.86	.59	12.33	13.86

PEAK FLOW REDUCTION [Qout/Qin](%)= 65.67
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .2569

```

ROUTE CHN (0056)
IN= 2----> OUT= 1

```

Routing time step (min)'= 5.00

```

<----- DATA FOR SECTION ( 1.5) ----->
Distance      Elevation      Manning
.00           425.00         .0300
.75           424.25         .0300 / .0300  Main Channel
1.75         424.25         .0300 / .0300  Main Channel
2.50         425.00         .0300

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)        (m)        (cu.m.)     (cms)          (m/s)        (min)
.04        424.29     .145E+02     .0              .68           8.63
.08        424.33     .302E+02     .1              1.05          5.61
.12        424.37     .469E+02     .2              1.33          4.42
.16        424.41     .647E+02     .3              1.57          3.76
.20        424.45     .837E+02     .4              1.77          3.34
.24        424.49     .104E+03     .6              1.94          3.04
.28        424.53     .125E+03     .7              2.10          2.81
.32        424.57     .147E+03     .9              2.23          2.64
.36        424.61     .170E+03     1.1             2.36          2.50
.39        424.64     .195E+03     1.4             2.47          2.39
.43        424.68     .220E+03     1.6             2.57          2.30
.47        424.72     .247E+03     1.9             2.66          2.22
.51        424.76     .275E+03     2.1             2.75          2.15
.55        424.80     .304E+03     2.4             2.83          2.09
.59        424.84     .334E+03     2.7             2.90          2.04
.63        424.88     .365E+03     3.1             2.97          1.99
.67        424.92     .397E+03     3.4             3.03          1.95
.71        424.96     .430E+03     3.8             3.09          1.91
.75        425.00     .465E+03     4.1             3.14          1.88

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0054)	15.86	.59	12.33	13.86	.24	1.96
OUTFLOW: ID= 1 (0056)	15.86	.45	12.33	13.86	.20	1.80

```

-----
| ADD HYD (0057) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0055):  5.19      .650      11.83      35.01
+ ID2= 2 (0056): 15.86      .446      12.33      13.86
=====
ID = 3 (0057):  21.05      .650      11.83      19.08

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0058) |
| ID= 1 DT= 5.0 min |
-----
      Area      (ha)= 21.77      Curve Number (CN)= 67.4
      Ia      (mm)= 5.22      # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .35

```

Unit Hyd Qpeak (cms)= 2.354

PEAK FLOW (cms)= 1.168 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 29.525
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .360

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0059) |
| ID= 1 DT= 5.0 min |
-----
      Area      (ha)= 11.96      Curve Number (CN)= 66.4
      Ia      (mm)= 5.74      # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .18

```

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= .931 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 28.306
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .345

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0060) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
      OUTFLOW      STORAGE      OUTFLOW      STORAGE
      (cms)      (ha.m.)      (cms)      (ha.m.)
      .0000      .0000      20.0000      .1583
      .0001      .1573      .0000      .0000

      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0059)  11.96      .93      11.92      28.31
OUTFLOW: ID= 1 (0060)  11.96      .82      12.25      15.15

      PEAK FLOW REDUCTION [Qout/Qin](%)= 88.17
      TIME SHIFT OF PEAK FLOW (min)= 20.00
      MAXIMUM STORAGE USED (ha.m.)= .2453

```

```

-----
| CALIB |
| NASHYD (0061) |
| ID= 1 DT= 5.0 min |
-----
      Area      (ha)= 3.90      Curve Number (CN)= 69.4
      Ia      (mm)= 4.85      # of Linear Res.(N)= 3.00
      U.H. Tp(hrs)= .08

```

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .488 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 29.428
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD (0062) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)

```



```

ID1= 1 (0060):    11.96    .821    12.25    15.15
+ ID2= 2 (0061):    3.90    .488    11.75    29.43
=====
ID = 3 (0062):    15.86    .895    12.25    18.66

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

| RESERVOIR (0063) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0771
	.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0062)	15.86	.90	12.25	18.66
OUTFLOW: ID= 1 (0063)	15.86	.59	12.33	13.86

PEAK FLOW REDUCTION	[Qout/Qin](%)=
TIME SHIFT OF PEAK FLOW	(min)= 5.00
MAXIMUM STORAGE USED	(ha.m.)= .2569

```

| ROUTE CHN (0065) |
| IN= 2---> OUT= 1 |

```

Routing time step (min)'= 5.00

```

<----- DATA FOR SECTION ( 1.5) ----->
Distance      Elevation      Manning
.00           425.00         .0300
.75           424.25         .0300 / .0300  Main Channel
1.75         424.25         .0300 / .0300  Main Channel
2.50         425.00         .0300

```

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0063)	15.86	.59	12.33	13.86	.24	1.96
OUTFLOW: ID= 1 (0065)	15.86	.45	12.33	13.86	.20	1.80

```

| CALIB NASHYD (0064) |
| ID= 1 DT= 5.0 min |

```

Area (ha)= 5.19 Curve Number (CN)= 73.3
Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .650 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 35.011
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

| ADD HYD (0066) |
| 1 + 2 = 3 |

```

AREA QPEAK TPEAK R.V.

	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0065):	15.86	.446	12.33	13.86
+ ID2= 2 (0064):	5.19	.650	11.83	35.01
=====				
ID = 3 (0066):	21.05	.650	11.83	19.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD (0069)	1.80	58.8
ID= 1 DT= 5.0 min	Ia (mm)= 8.49	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .07	

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .154 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 19.445
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .237

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD (0067)	1.52	62.0
ID= 1 DT= 5.0 min	Ia (mm)= 8.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .06	

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .148 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 20.147
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .246

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0068)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1	.0000	.0000	20.0000	.0207
DT= 5.0 min	.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.15	11.75	20.15
OUTFLOW: ID= 1 (0068)	1.52	.01	13.17	6.62

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.16
 TIME SHIFT OF PEAK FLOW (min)= 85.00
 MAXIMUM STORAGE USED (ha.m.)= .0210

ADD HYD (0071)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0069):	1.80	.154	11.75	19.44
+ ID2= 2 (0068):	1.52	.008	13.17	6.62
=====				
ID = 3 (0071):	3.32	.154	11.75	13.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0070)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1	.0000	.0000	20.0000	.0708
DT= 5.0 min	.0001	.0707	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0071)	3.32	.15	11.75	13.57
OUTFLOW: ID= 1 (0070)	3.32	.00	24.17	.07

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=745.00

ROUTE CHN (0073)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.6) ----->

Distance	Elevation	Manning	
.00	421.26	.0300	
1.10	420.66	.0300 / .0300	Main Channel
2.00	420.66	.0300 / .0300	Main Channel
3.10	421.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

<---- hydrograph ----> <-pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	3.32	.00	24.17	.07	.00	.05
OUTFLOW: ID= 1 (0073)	3.32	.00	24.17	.06	.00	.05

ADD HYD (0074)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0066):	21.05	.650	11.83	19.08
+ ID2= 2 (0073):	3.32	.000	24.17	.06
=====				
ID = 3 (0074):	24.37	.650	11.83	16.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0072)
ID= 1 DT= 5.0 min

Area (ha)= 24.19 Curve Number (CN)= 60.0
Ia (mm)= 8.62 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .37

Unit Hyd Qpeak (cms)= 2.505

PEAK FLOW (cms)= .921 (i)
TIME TO PEAK (hrs)= 12.167
RUNOFF VOLUME (mm)= 22.116
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .270

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0074):	24.37	.650	11.83	16.49
+ ID2= 2 (0072):	24.19	.921	12.17	22.12
=====				
ID = 3 (0075):	48.56	1.370	12.33	19.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area (ha)=	127.28	Curve Number (CN)=	59.9
NASHYD (0076)		Ia (mm)=	8.29	# of Linear Res.(N)=	3.00
ID= 1 DT= 5.0 min		U.H. Tp(hrs)=	.79		

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 2.872 (i)
 TIME TO PEAK (hrs)= 12.667
 RUNOFF VOLUME (mm)= 22.263
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .272

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area (ha)=	17.28	Curve Number (CN)=	58.3
NASHYD (0077)		Ia (mm)=	9.24	# of Linear Res.(N)=	3.00
ID= 1 DT= 5.0 min		U.H. Tp(hrs)=	.57		

Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .455 (i)
 TIME TO PEAK (hrs)= 12.417
 RUNOFF VOLUME (mm)= 20.780
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .254

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area (ha)=	.24	Curve Number (CN)=	77.6
NASHYD (0082)		Ia (mm)=	3.49	# of Linear Res.(N)=	3.00
ID= 1 DT= 5.0 min		U.H. Tp(hrs)=	.11		

Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .034 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 39.838
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .486

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area (ha)=	2.66	Curve Number (CN)=	59.8
NASHYD (0078)		Ia (mm)=	8.55	# of Linear Res.(N)=	3.00
ID= 1 DT= 5.0 min		U.H. Tp(hrs)=	.07		

Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .231 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 20.255
 TOTAL RAINFALL (mm)= 81.935
 RUNOFF COEFFICIENT = .247

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0079)		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1		.0000	.0000	20.0000	.0608
DT= 5.0 min		.0001	.0607	.0000	.0000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0078)		2.66	.23	11.75	20.25
OUTFLOW: ID= 1 (0079)		2.66	.00	24.17	.13
		PEAK FLOW REDUCTION [Qout/Qin] (%)=	.04		
		TIME SHIFT OF PEAK FLOW (min)=	745.00		
		MAXIMUM STORAGE USED (ha.m.)=	.0535		

ADD HYD (0083)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3					

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-----
ID1= 1 (0082):      (ha)   (cms)   (hrs)   (mm)
+ ID2= 2 (0079):    2.66   .000   24.17   .13
=====
ID = 3 (0083):      2.90   .034   11.83   3.38

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB
| NASHYD (0080) | Area (ha)= 14.63 Curve Number (CN)= 58.0
| ID= 1 DT= 5.0 min | Ia (mm)= 9.37 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .57

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Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .381 (i)
TIME TO PEAK (hrs)= 12.417
RUNOFF VOLUME (mm)= 20.553
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .251

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ADD HYD (0081) |
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
|-----| (ha) (cms) (hrs) (mm)
ID1= 1 (0083): 2.90 .034 11.83 3.38
+ ID2= 2 (0080): 14.63 .381 12.42 20.55
=====
ID = 3 (0081): 17.52 .386 12.33 17.71

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB
| NASHYD (0084) | Area (ha)= 7.71 Curve Number (CN)= 62.5
| ID= 1 DT= 5.0 min | Ia (mm)= 9.14 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .29

```

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .365 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 23.487
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .287

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB
| NASHYD (0085) | Area (ha)= .91 Curve Number (CN)= 64.9
| ID= 1 DT= 5.0 min | Ia (mm)= 8.53 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .11

```

Unit Hyd Qpeak (cms)= .313

PEAK FLOW (cms)= .080 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 25.089
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB
| NASHYD (0086) | Area (ha)= 19.15 Curve Number (CN)= 71.3
| ID= 1 DT= 5.0 min | Ia (mm)= 5.81 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .24

```

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= 1.438 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 32.434
TOTAL RAINFALL (mm)= 81.935
RUNOFF COEFFICIENT = .396

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ** SIMULATION NUMBER: 4 **

CHICAGO STORM
 Ptotal= 94.15 mm

IDF curve parameters: A=1649.671
 B= 9.457
 C= .830

used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = .49

The CORRELATION coefficient is = .9992

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	180.00	179.69
10.	135.00	140.43
15.	117.00	116.15
30.	85.00	78.09
60.	49.00	48.84
120.	29.00	29.13
360.	11.00	12.20
720.	6.90	6.94
1440.	4.20	3.92

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.69	6.08	1.29	12.08	21.88	18.08	1.22
.17	.69	6.17	1.31	12.17	17.23	18.17	1.21
.25	.70	6.25	1.33	12.25	14.18	18.25	1.19
.33	.70	6.33	1.34	12.33	12.04	18.33	1.18
.42	.71	6.42	1.36	12.42	10.46	18.42	1.17
.50	.71	6.50	1.38	12.50	9.25	18.50	1.15
.58	.72	6.58	1.40	12.58	8.29	18.58	1.14
.67	.72	6.67	1.42	12.67	7.52	18.67	1.13
.75	.73	6.75	1.44	12.75	6.88	18.75	1.12
.83	.73	6.83	1.46	12.83	6.34	18.83	1.11
.92	.74	6.92	1.49	12.92	5.89	18.92	1.10
1.00	.74	7.00	1.51	13.00	5.50	19.00	1.08
1.08	.75	7.08	1.53	13.08	5.16	19.08	1.07
1.17	.75	7.17	1.56	13.17	4.86	19.17	1.06
1.25	.76	7.25	1.58	13.25	4.59	19.25	1.05
1.33	.76	7.33	1.61	13.33	4.36	19.33	1.04
1.42	.77	7.42	1.64	13.42	4.15	19.42	1.03
1.50	.77	7.50	1.67	13.50	3.96	19.50	1.02
1.58	.78	7.58	1.70	13.58	3.78	19.58	1.01
1.67	.78	7.67	1.73	13.67	3.63	19.67	1.00
1.75	.79	7.75	1.76	13.75	3.48	19.75	1.00
1.83	.79	7.83	1.79	13.83	3.35	19.83	.99
1.92	.80	7.92	1.83	13.92	3.23	19.92	.98
2.00	.81	8.00	1.86	14.00	3.11	20.00	.97
2.08	.81	8.08	1.90	14.08	3.01	20.08	.96
2.17	.82	8.17	1.94	14.17	2.91	20.17	.95
2.25	.82	8.25	1.98	14.25	2.82	20.25	.94
2.33	.83	8.33	2.03	14.33	2.74	20.33	.94
2.42	.84	8.42	2.07	14.42	2.66	20.42	.93
2.50	.84	8.50	2.12	14.50	2.58	20.50	.92
2.58	.85	8.58	2.17	14.58	2.51	20.58	.91
2.67	.86	8.67	2.23	14.67	2.45	20.67	.91
2.75	.86	8.75	2.28	14.75	2.38	20.75	.90
2.83	.87	8.83	2.34	14.83	2.32	20.83	.89
2.92	.88	8.92	2.41	14.92	2.27	20.92	.89
3.00	.88	9.00	2.47	15.00	2.22	21.00	.88
3.08	.89	9.08	2.54	15.08	2.16	21.08	.87
3.17	.90	9.17	2.62	15.17	2.12	21.17	.86
3.25	.91	9.25	2.70	15.25	2.07	21.25	.86
3.33	.91	9.33	2.79	15.33	2.03	21.33	.85
3.42	.92	9.42	2.88	15.42	1.99	21.42	.85
3.50	.93	9.50	2.98	15.50	1.95	21.50	.84
3.58	.94	9.58	3.09	15.58	1.91	21.58	.83
3.67	.95	9.67	3.20	15.67	1.87	21.67	.83
3.75	.96	9.75	3.33	15.75	1.84	21.75	.82
3.83	.96	9.83	3.47	15.83	1.80	21.83	.82
3.92	.97	9.92	3.62	15.92	1.77	21.92	.81
4.00	.98	10.00	3.78	16.00	1.74	22.00	.80
4.08	.99	10.08	3.96	16.08	1.71	22.08	.80
4.17	1.00	10.17	4.16	16.17	1.68	22.17	.79
4.25	1.01	10.25	4.39	16.25	1.65	22.25	.79
4.33	1.02	10.33	4.64	16.33	1.62	22.33	.78
4.42	1.03	10.42	4.93	16.42	1.60	22.42	.78
4.50	1.04	10.50	5.25	16.50	1.57	22.50	.77
4.58	1.05	10.58	5.62	16.58	1.55	22.58	.77
4.67	1.06	10.67	6.06	16.67	1.53	22.67	.76
4.75	1.07	10.75	6.57	16.75	1.50	22.75	.76

4.83	1.08	10.83	7.17	16.83	1.48	22.83	.75
4.92	1.10	10.92	7.91	16.92	1.46	22.92	.75
5.00	1.11	11.00	8.82	17.00	1.44	23.00	.74
5.08	1.12	11.08	9.98	17.08	1.42	23.08	.74
5.17	1.13	11.17	11.49	17.17	1.40	23.17	.73
5.25	1.14	11.25	13.53	17.25	1.38	23.25	.73
5.33	1.16	11.33	16.46	17.33	1.36	23.33	.72
5.42	1.17	11.42	20.92	17.42	1.35	23.42	.72
5.50	1.18	11.50	28.48	17.50	1.33	23.50	.71
5.58	1.20	11.58	43.48	17.58	1.31	23.58	.71
5.67	1.21	11.67	83.71	17.67	1.30	23.67	.71
5.75	1.23	11.75	179.69	17.75	1.28	23.75	.70
5.83	1.24	11.83	85.03	17.83	1.26	23.83	.70
5.92	1.26	11.92	45.00	17.92	1.25	23.92	.69
6.00	1.27	12.00	29.68	18.00	1.23	24.00	.69

 CALIB
 NASHYD (0021) Area (ha)= 8.81 Curve Number (CN)= 68.3
 ID= 1 DT= 5.0 min Ia (mm)= 6.50 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.36

Unit Hyd Qpeak (cms)= .248

PEAK FLOW (cms)= .235 (i)
 TIME TO PEAK (hrs)= 13.250
 RUNOFF VOLUME (mm)= 37.356
 TOTAL RAINFALL (mm)= 94.147
 RUNOFF COEFFICIENT = .397

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0027) Area (ha)= .68 Curve Number (CN)= 72.2
 ID= 1 DT= 2.0 min Ia (mm)= 4.91 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.033	.69	6.033	1.29	12.033	21.88	18.03	1.22
.067	.69	6.067	1.29	12.067	21.88	18.07	1.22
.100	.69	6.100	1.30	12.100	19.55	18.10	1.21
.133	.69	6.133	1.31	12.133	17.23	18.13	1.21
.167	.69	6.167	1.31	12.167	17.23	18.17	1.21
.200	.70	6.200	1.33	12.200	14.18	18.20	1.19
.233	.70	6.233	1.33	12.233	14.18	18.23	1.19
.267	.70	6.267	1.33	12.267	13.11	18.27	1.19
.300	.70	6.300	1.34	12.300	12.04	18.30	1.18
.333	.70	6.333	1.34	12.333	12.04	18.33	1.18
.367	.71	6.367	1.36	12.367	10.46	18.37	1.17
.400	.71	6.400	1.36	12.400	10.46	18.40	1.17
.433	.71	6.433	1.37	12.433	9.85	18.43	1.16
.467	.71	6.467	1.38	12.467	9.25	18.47	1.15
.500	.71	6.500	1.38	12.500	9.25	18.50	1.15
.533	.72	6.533	1.40	12.533	8.29	18.53	1.14
.567	.72	6.567	1.40	12.567	8.29	18.57	1.14
.600	.72	6.600	1.41	12.600	7.90	18.60	1.14
.633	.72	6.633	1.42	12.633	7.52	18.63	1.13
.667	.72	6.667	1.42	12.667	7.52	18.67	1.13
.700	.73	6.700	1.44	12.700	6.88	18.70	1.12
.733	.73	6.733	1.44	12.733	6.88	18.73	1.12
.767	.73	6.767	1.45	12.767	6.61	18.77	1.11
.800	.73	6.800	1.46	12.800	6.34	18.80	1.11
.833	.73	6.833	1.46	12.833	6.34	18.83	1.11
.867	.74	6.867	1.49	12.867	5.89	18.87	1.10
.900	.74	6.900	1.49	12.900	5.89	18.90	1.10
.933	.74	6.933	1.50	12.933	5.69	18.93	1.09
.967	.74	6.967	1.51	12.967	5.50	18.97	1.08
1.000	.74	7.000	1.51	13.000	5.50	19.00	1.08
1.033	.75	7.033	1.53	13.033	5.16	19.03	1.07
1.067	.75	7.067	1.53	13.067	5.16	19.07	1.07
1.100	.75	7.100	1.54	13.100	5.01	19.10	1.07
1.133	.75	7.133	1.56	13.133	4.86	19.13	1.06
1.167	.75	7.167	1.56	13.167	4.86	19.17	1.06
1.200	.76	7.200	1.58	13.200	4.59	19.20	1.05
1.233	.76	7.233	1.58	13.233	4.59	19.23	1.05
1.267	.76	7.267	1.60	13.267	4.47	19.27	1.05
1.300	.76	7.300	1.61	13.300	4.36	19.30	1.04
1.333	.76	7.333	1.61	13.333	4.36	19.33	1.04
1.367	.77	7.367	1.64	13.367	4.15	19.37	1.03
1.400	.77	7.400	1.64	13.400	4.15	19.40	1.03

1.433	.77	7.433	1.65	13.433	4.05	19.43	1.03
1.467	.77	7.467	1.67	13.467	3.96	19.47	1.02
1.500	.77	7.500	1.67	13.500	3.96	19.50	1.02
1.533	.78	7.533	1.70	13.533	3.78	19.53	1.01
1.567	.78	7.567	1.70	13.567	3.78	19.57	1.01
1.600	.78	7.600	1.71	13.600	3.70	19.60	1.01
1.633	.78	7.633	1.73	13.633	3.63	19.63	1.00
1.667	.78	7.667	1.73	13.667	3.62	19.67	1.00
1.700	.79	7.700	1.76	13.700	3.48	19.70	1.00
1.733	.79	7.733	1.76	13.733	3.48	19.73	1.00
1.767	.79	7.767	1.78	13.767	3.41	19.77	.99
1.800	.79	7.800	1.79	13.800	3.35	19.80	.99
1.833	.79	7.833	1.79	13.833	3.35	19.83	.99
1.867	.80	7.867	1.83	13.867	3.23	19.87	.98
1.900	.80	7.900	1.83	13.900	3.23	19.90	.98
1.933	.80	7.933	1.85	13.933	3.17	19.93	.97
1.967	.81	7.967	1.86	13.967	3.11	19.97	.97
2.000	.81	8.000	1.86	14.000	3.11	20.00	.97
2.033	.81	8.033	1.90	14.033	3.01	20.03	.96
2.067	.81	8.067	1.90	14.067	3.01	20.07	.96
2.100	.81	8.100	1.92	14.100	2.96	20.10	.96
2.133	.82	8.133	1.94	14.133	2.91	20.13	.95
2.167	.82	8.167	1.94	14.167	2.91	20.17	.95
2.200	.82	8.200	1.98	14.200	2.82	20.20	.94
2.233	.82	8.233	1.98	14.233	2.82	20.23	.94
2.267	.83	8.267	2.01	14.267	2.78	20.27	.94
2.300	.83	8.300	2.03	14.300	2.74	20.30	.94
2.333	.83	8.333	2.03	14.333	2.74	20.33	.94
2.367	.84	8.367	2.07	14.367	2.66	20.37	.93
2.400	.84	8.400	2.07	14.400	2.66	20.40	.93
2.433	.84	8.433	2.10	14.433	2.62	20.43	.93
2.467	.84	8.467	2.12	14.467	2.58	20.47	.92
2.500	.84	8.500	2.12	14.500	2.58	20.50	.92
2.533	.85	8.533	2.17	14.533	2.51	20.53	.91
2.567	.85	8.567	2.17	14.567	2.51	20.57	.91
2.600	.85	8.600	2.20	14.600	2.48	20.60	.91
2.633	.86	8.633	2.23	14.633	2.45	20.63	.91
2.667	.86	8.667	2.23	14.667	2.45	20.67	.91
2.700	.86	8.700	2.28	14.700	2.38	20.70	.90
2.733	.86	8.733	2.28	14.733	2.38	20.73	.90
2.767	.87	8.767	2.31	14.767	2.35	20.77	.90
2.800	.87	8.800	2.34	14.800	2.32	20.80	.89
2.833	.87	8.833	2.34	14.833	2.32	20.83	.89
2.867	.88	8.867	2.41	14.867	2.27	20.87	.89
2.900	.88	8.900	2.41	14.900	2.27	20.90	.89
2.933	.88	8.933	2.44	14.933	2.24	20.93	.88
2.967	.88	8.967	2.47	14.967	2.22	20.97	.88
3.000	.88	9.000	2.47	15.000	2.22	21.00	.88
3.033	.89	9.033	2.54	15.033	2.16	21.03	.87
3.067	.89	9.067	2.54	15.067	2.16	21.07	.87
3.100	.90	9.100	2.58	15.100	2.14	21.10	.87
3.133	.90	9.133	2.62	15.133	2.12	21.13	.86
3.167	.90	9.167	2.62	15.167	2.12	21.17	.86
3.200	.91	9.200	2.70	15.200	2.07	21.20	.86
3.233	.91	9.233	2.70	15.233	2.07	21.23	.86
3.267	.91	9.267	2.74	15.267	2.05	21.27	.85
3.300	.91	9.300	2.79	15.300	2.03	21.30	.85
3.333	.91	9.333	2.79	15.333	2.03	21.33	.85
3.367	.92	9.367	2.88	15.367	1.99	21.37	.85
3.400	.92	9.400	2.88	15.400	1.99	21.40	.85
3.433	.93	9.433	2.93	15.433	1.97	21.43	.84
3.467	.93	9.467	2.98	15.467	1.95	21.47	.84
3.500	.93	9.500	2.98	15.500	1.95	21.50	.84
3.533	.94	9.533	3.09	15.533	1.91	21.53	.83
3.567	.94	9.567	3.09	15.567	1.91	21.57	.83
3.600	.94	9.600	3.15	15.600	1.89	21.60	.83
3.633	.95	9.633	3.20	15.633	1.87	21.63	.83
3.667	.95	9.667	3.20	15.667	1.87	21.67	.83
3.700	.96	9.700	3.33	15.700	1.84	21.70	.82
3.733	.96	9.733	3.33	15.733	1.84	21.73	.82
3.767	.96	9.767	3.40	15.767	1.82	21.77	.82
3.800	.96	9.800	3.47	15.800	1.80	21.80	.82
3.833	.96	9.833	3.47	15.833	1.80	21.83	.82
3.867	.97	9.867	3.62	15.867	1.77	21.87	.81
3.900	.97	9.900	3.62	15.900	1.77	21.90	.81
3.933	.98	9.933	3.70	15.933	1.75	21.93	.81
3.967	.98	9.967	3.78	15.967	1.74	21.97	.80
4.000	.98	10.000	3.78	16.000	1.74	22.00	.80
4.033	.99	10.033	3.96	16.033	1.71	22.03	.80
4.067	.99	10.067	3.96	16.067	1.71	22.07	.80
4.100	1.00	10.100	4.06	16.100	1.69	22.10	.80
4.133	1.00	10.133	4.16	16.133	1.68	22.13	.79
4.167	1.00	10.167	4.16	16.167	1.68	22.17	.79
4.200	1.01	10.200	4.39	16.200	1.65	22.20	.79
4.233	1.01	10.233	4.39	16.233	1.65	22.23	.79
4.267	1.02	10.267	4.52	16.267	1.64	22.27	.78
4.300	1.02	10.300	4.64	16.300	1.62	22.30	.78
4.333	1.02	10.333	4.64	16.333	1.62	22.33	.78
4.367	1.03	10.367	4.93	16.367	1.60	22.37	.78

4.400	1.03	10.400	4.93	16.400	1.60	22.40	.78
4.433	1.04	10.433	5.09	16.433	1.59	22.43	.77
4.467	1.04	10.467	5.25	16.467	1.57	22.47	.77
4.500	1.04	10.500	5.25	16.500	1.57	22.50	.77
4.533	1.05	10.533	5.62	16.533	1.55	22.53	.77
4.567	1.05	10.567	5.62	16.567	1.55	22.57	.77
4.600	1.06	10.600	5.84	16.600	1.54	22.60	.76
4.633	1.06	10.633	6.06	16.633	1.53	22.63	.76
4.667	1.06	10.667	6.06	16.667	1.53	22.67	.76
4.700	1.07	10.700	6.57	16.700	1.50	22.70	.76
4.733	1.07	10.733	6.57	16.733	1.50	22.73	.76
4.767	1.08	10.767	6.87	16.767	1.49	22.77	.75
4.800	1.08	10.800	7.17	16.800	1.48	22.80	.75
4.833	1.08	10.833	7.17	16.833	1.48	22.83	.75
4.867	1.10	10.867	7.91	16.867	1.46	22.87	.75
4.900	1.10	10.900	7.91	16.900	1.46	22.90	.75
4.933	1.10	10.933	8.37	16.933	1.45	22.93	.74
4.967	1.11	10.967	8.82	16.967	1.44	22.97	.74
5.000	1.11	11.000	8.82	17.000	1.44	23.00	.74
5.033	1.12	11.033	9.98	17.033	1.42	23.03	.74
5.067	1.12	11.067	9.98	17.067	1.42	23.07	.74
5.100	1.13	11.100	10.73	17.100	1.41	23.10	.74
5.133	1.13	11.133	11.49	17.133	1.40	23.13	.73
5.167	1.13	11.167	11.49	17.167	1.40	23.17	.73
5.200	1.14	11.200	13.53	17.200	1.38	23.20	.73
5.233	1.14	11.233	13.53	17.233	1.38	23.23	.73
5.267	1.15	11.267	15.00	17.267	1.37	23.27	.73
5.300	1.16	11.300	16.46	17.300	1.36	23.30	.72
5.333	1.16	11.333	16.46	17.333	1.36	23.33	.72
5.367	1.17	11.367	20.92	17.367	1.35	23.37	.72
5.400	1.17	11.400	20.92	17.400	1.35	23.40	.72
5.433	1.18	11.433	24.71	17.433	1.34	23.43	.72
5.467	1.18	11.467	28.48	17.467	1.33	23.47	.71
5.500	1.18	11.500	28.50	17.500	1.33	23.50	.71
5.533	1.20	11.533	43.48	17.533	1.31	23.53	.71
5.567	1.20	11.567	43.48	17.567	1.31	23.57	.71
5.600	1.21	11.600	63.65	17.600	1.30	23.60	.71
5.633	1.21	11.633	83.71	17.633	1.30	23.63	.71
5.667	1.21	11.667	83.83	17.667	1.30	23.67	.71
5.700	1.23	11.700	179.69	17.700	1.28	23.70	.70
5.733	1.23	11.733	179.69	17.733	1.28	23.73	.70
5.767	1.24	11.767	132.24	17.767	1.27	23.77	.70
5.800	1.24	11.800	85.03	17.800	1.26	23.80	.70
5.833	1.24	11.833	84.97	17.833	1.26	23.83	.70
5.867	1.26	11.867	45.00	17.867	1.25	23.87	.69
5.900	1.26	11.900	45.00	17.900	1.25	23.90	.69
5.933	1.27	11.933	37.32	17.933	1.24	23.93	.69
5.967	1.27	11.967	29.68	17.967	1.23	23.97	.69
6.000	1.27	12.000	29.67	18.000	1.23	24.00	.69

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .137 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 42.213
 TOTAL RAINFALL (mm)= 94.146
 RUNOFF COEFFICIENT = .448

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	5.03	Curve Number (CN)=	72.5
NASHYD (0024)	Ia (mm)=	4.75	# of Linear Res.(N)=	3.00
ID= 1 DT= 2.0 min	U.H. Tp(hrs)=	.08		

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= .908 (i)
 TIME TO PEAK (hrs)= 11.800
 RUNOFF VOLUME (mm)= 32.210
 TOTAL RAINFALL (mm)= 94.146
 RUNOFF COEFFICIENT = .342

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	3.01	Curve Number (CN)=	71.6
NASHYD (0022)	Ia (mm)=	5.22	# of Linear Res.(N)=	3.00
ID= 1 DT= 2.0 min	U.H. Tp(hrs)=	.06		

Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .594 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 30.881

TOTAL RAINFALL (mm)= 94.146
 RUNOFF COEFFICIENT = .328

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0023)		OUTFLOW		STORAGE	
IN= 2---> OUT= 1		(cms)		(ha.m.)	
DT= 2.0 min					
		.0000	.0000	.0002	.2156
		.0001	.1117	20.0000	.2166
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW :	ID= 2 (0022)	3.01	.59	11.77	30.88
OUTFLOW:	ID= 1 (0023)	3.01	.00	13.60	.02
		PEAK FLOW REDUCTION [Qout/Qin](%)=	.01		
		TIME SHIFT OF PEAK FLOW (min)=	110.00		
		MAXIMUM STORAGE USED (ha.m.)=	.0929		

ADD HYD (0026)		AREA		QPEAK		TPEAK		R.V.	
1 + 2 = 3		(ha)		(cms)		(hrs)		(mm)	
	ID1= 1 (0024):	5.03	.908	11.80	32.21				
	+ ID2= 2 (0023):	3.01	.000	13.60	.02				
	ID = 3 (0026):	8.04	.908	11.80	20.16				

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0025)		OUTFLOW		STORAGE	
IN= 2---> OUT= 1		(cms)		(ha.m.)	
DT= 2.0 min					
		.0000	.0000	.0003	.2171
		.0001	.0498	20.0000	.2181
		.0002	.1676	.0000	.0000
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW :	ID= 2 (0026)	8.04	.91	11.80	20.16
OUTFLOW:	ID= 1 (0025)	8.04	.00	13.70	.02
		PEAK FLOW REDUCTION [Qout/Qin](%)=	.02		
		TIME SHIFT OF PEAK FLOW (min)=	114.00		
		MAXIMUM STORAGE USED (ha.m.)=	.1620		

ADD HYD (0028)		AREA		QPEAK		TPEAK		R.V.	
1 + 2 = 3		(ha)		(cms)		(hrs)		(mm)	
	ID1= 1 (0027):	.68	.137	11.77	42.21				
	+ ID2= 2 (0025):	8.04	.000	13.70	.02				
	ID = 3 (0028):	8.72	.137	11.77	3.30				

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0029)		OUTFLOW		STORAGE	
IN= 2---> OUT= 1		(cms)		(ha.m.)	
DT= 2.0 min					
		.0000	.0000	.0002	.0898
		.0001	.0455	20.0000	.0908
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW :	ID= 2 (0028)	8.72	.14	11.77	3.30
OUTFLOW:	ID= 1 (0029)	8.72	.00	24.13	.03
		PEAK FLOW REDUCTION [Qout/Qin](%)=	.05		
		TIME SHIFT OF PEAK FLOW (min)=	742.00		
		MAXIMUM STORAGE USED (ha.m.)=	.0285		

CALIB

NASHYD (0032) | Area (ha)= 6.71 Curve Number (CN)= 64.3
 ID= 1 DT= 5.0 min | Ia (mm)= 8.68 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .32

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.69	6.083	1.29	12.083	21.88	18.08	1.22
.167	.69	6.167	1.31	12.167	17.23	18.17	1.21
.250	.70	6.250	1.33	12.250	14.18	18.25	1.19
.333	.70	6.333	1.34	12.333	12.04	18.33	1.18
.417	.71	6.417	1.36	12.417	10.46	18.42	1.17
.500	.71	6.500	1.38	12.500	9.25	18.50	1.15
.583	.72	6.583	1.40	12.583	8.29	18.58	1.14
.667	.72	6.667	1.42	12.667	7.52	18.67	1.13
.750	.73	6.750	1.44	12.750	6.88	18.75	1.12
.833	.73	6.833	1.46	12.833	6.34	18.83	1.11
.917	.74	6.917	1.49	12.917	5.89	18.92	1.10
1.000	.74	7.000	1.51	13.000	5.50	19.00	1.08
1.083	.75	7.083	1.53	13.083	5.16	19.08	1.07
1.167	.75	7.167	1.56	13.167	4.86	19.17	1.06
1.250	.76	7.250	1.58	13.250	4.59	19.25	1.05
1.333	.76	7.333	1.61	13.333	4.36	19.33	1.04
1.417	.77	7.417	1.64	13.417	4.15	19.42	1.03
1.500	.77	7.500	1.67	13.500	3.96	19.50	1.02
1.583	.78	7.583	1.70	13.583	3.78	19.58	1.01
1.667	.78	7.667	1.73	13.667	3.63	19.67	1.00
1.750	.79	7.750	1.76	13.750	3.48	19.75	1.00
1.833	.79	7.833	1.79	13.833	3.35	19.83	.99
1.917	.80	7.917	1.83	13.917	3.23	19.92	.98
2.000	.81	8.000	1.86	14.000	3.11	20.00	.97
2.083	.81	8.083	1.90	14.083	3.01	20.08	.96
2.167	.82	8.167	1.94	14.167	2.91	20.17	.95
2.250	.82	8.250	1.98	14.250	2.82	20.25	.94
2.333	.83	8.333	2.03	14.333	2.74	20.33	.94
2.417	.84	8.417	2.07	14.417	2.66	20.42	.93
2.500	.84	8.500	2.12	14.500	2.58	20.50	.92
2.583	.85	8.583	2.17	14.583	2.51	20.58	.91
2.667	.86	8.667	2.23	14.667	2.45	20.67	.91
2.750	.86	8.750	2.28	14.750	2.38	20.75	.90
2.833	.87	8.833	2.34	14.833	2.32	20.83	.89
2.917	.88	8.917	2.41	14.917	2.27	20.92	.89
3.000	.88	9.000	2.47	15.000	2.22	21.00	.88
3.083	.89	9.083	2.54	15.083	2.16	21.08	.87
3.167	.90	9.167	2.62	15.167	2.12	21.17	.86
3.250	.91	9.250	2.70	15.250	2.07	21.25	.86
3.333	.91	9.333	2.79	15.333	2.03	21.33	.85
3.417	.92	9.417	2.88	15.417	1.99	21.42	.85
3.500	.93	9.500	2.98	15.500	1.95	21.50	.84
3.583	.94	9.583	3.09	15.583	1.91	21.58	.83
3.667	.95	9.667	3.20	15.667	1.87	21.67	.83
3.750	.96	9.750	3.33	15.750	1.84	21.75	.82
3.833	.96	9.833	3.47	15.833	1.80	21.83	.82
3.917	.97	9.917	3.62	15.917	1.77	21.92	.81
4.000	.98	10.000	3.78	16.000	1.74	22.00	.80
4.083	.99	10.083	3.96	16.083	1.71	22.08	.80
4.167	1.00	10.167	4.16	16.167	1.68	22.17	.79
4.250	1.01	10.250	4.39	16.250	1.65	22.25	.79
4.333	1.02	10.333	4.64	16.333	1.62	22.33	.78
4.417	1.03	10.417	4.93	16.417	1.60	22.42	.78
4.500	1.04	10.500	5.25	16.500	1.57	22.50	.77
4.583	1.05	10.583	5.62	16.583	1.55	22.58	.77
4.667	1.06	10.667	6.06	16.667	1.53	22.67	.76
4.750	1.07	10.750	6.57	16.750	1.50	22.75	.76
4.833	1.08	10.833	7.17	16.833	1.48	22.83	.75
4.917	1.10	10.917	7.91	16.917	1.46	22.92	.75
5.000	1.11	11.000	8.82	17.000	1.44	23.00	.74
5.083	1.12	11.083	9.98	17.083	1.42	23.08	.74
5.167	1.13	11.167	11.49	17.167	1.40	23.17	.73
5.250	1.14	11.250	13.53	17.250	1.38	23.25	.73
5.333	1.16	11.333	16.46	17.333	1.36	23.33	.72
5.417	1.17	11.417	20.92	17.417	1.35	23.42	.72
5.500	1.18	11.500	28.48	17.500	1.33	23.50	.71
5.583	1.20	11.583	43.48	17.583	1.31	23.58	.71
5.667	1.21	11.667	83.71	17.667	1.30	23.67	.71
5.750	1.23	11.750	179.68	17.750	1.28	23.75	.70
5.833	1.24	11.833	85.04	17.833	1.26	23.83	.70
5.917	1.26	11.917	45.01	17.917	1.25	23.92	.69
6.000	1.27	12.000	29.69	18.000	1.23	24.00	.60

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .437 (i)

TIME TO PEAK (hrs)= 12.083

RUNOFF VOLUME (mm)= 32.207

TOTAL RAINFALL (mm)= 94.090

RUNOFF COEFFICIENT = .342

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB |
| NASHYD (0030) | Area (ha)= 5.57 Curve Number (CN)= 69.8
| ID= 1 DT= 5.0 min | Ia (mm)= 6.12 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .06

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Unit Hyd Qpeak (cms)= 3.828

PEAK FLOW (cms)= .929 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 32.133
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .342

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ROUTE CHN (0031) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

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<----- DATA FOR SECTION ( 1.2) ----->
Distance Elevation Manning
.00 386.25 .0300
37.50 385.75 .0300 / .0300 Main Channel
47.50 385.75 .0300 / .0300 Main Channel
85.00 386.25 .0300

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<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 385.78 .150E+03 .1 .33 23.91
.05 385.80 .350E+03 .3 .47 16.85
.08 385.83 .599E+03 .7 .56 14.12
.11 385.86 .898E+03 1.2 .63 12.62
.13 385.88 .125E+04 1.8 .68 11.65
.16 385.91 .164E+04 2.5 .73 10.95
.18 385.93 .209E+04 3.3 .76 10.42
.21 385.96 .259E+04 4.3 .80 9.99
.24 385.99 .313E+04 5.4 .82 9.64
.26 386.01 .373E+04 6.7 .85 9.33
.29 386.04 .438E+04 8.0 .88 9.07
.32 386.07 .507E+04 9.6 .90 8.83
.34 386.09 .582E+04 11.2 .92 8.62
.37 386.12 .661E+04 13.1 .94 8.43
.39 386.14 .745E+04 15.1 .96 8.25
.42 386.17 .835E+04 17.2 .98 8.08
.45 386.20 .929E+04 19.5 1.00 7.93
.47 386.22 .103E+05 22.0 1.02 7.79
.50 386.25 .113E+05 24.7 1.04 7.65

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<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0030) 5.57 .93 11.75 32.13 .09 .59
OUTFLOW: ID= 1 (0031) 5.57 .45 11.92 32.11 .06 .50

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-----
| ADD HYD (0033) |
| 1 + 2 = 3 |
|-----|
| ID1= 1 (0032): | AREA QPEAK TPEAK R.V.
| + ID2= 2 (0031): | (ha) (cms) (hrs) (mm)
| ID = 3 (0033): | 12.27 .827 11.92 32.16

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB |
| NASHYD (0036) | Area (ha)= 2.08 Curve Number (CN)= 67.6
| ID= 1 DT= 5.0 min | Ia (mm)= 7.71 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .08

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Unit Hyd Qpeak (cms)= .938

PEAK FLOW (cms)= .289 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 34.208
 TOTAL RAINFALL (mm)= 94.090

RUNOFF COEFFICIENT = .364

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB |
| NASHYD (0034) | Area (ha)= 2.15 Curve Number (CN)= 71.9
| ID= 1 DT= 5.0 min | Ia (mm)= 5.03 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .10

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Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .336 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 41.182
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .438

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ROUTE CHN (0035) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

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<----- DATA FOR SECTION ( 1.3) ----->
Distance Elevation Manning
.00 388.25 .0300
30.00 387.75 .0300 / .0300 Main Channel
40.00 387.75 .0300 / .0300 Main Channel
70.00 388.25 .0300

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<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 387.78 .327E+02 .1 .41 4.35
.05 387.80 .744E+02 .4 .59 3.03
.08 387.83 .125E+03 .8 .71 2.52
.11 387.86 .185E+03 1.4 .80 2.25
.13 387.88 .253E+03 2.0 .87 2.07
.16 387.91 .330E+03 2.8 .92 1.95
.18 387.93 .417E+03 3.7 .97 1.85
.21 387.96 .512E+03 4.8 1.01 1.78
.24 387.99 .616E+03 6.0 1.04 1.72
.26 388.01 .729E+03 7.3 1.07 1.67
.29 388.04 .851E+03 8.7 1.10 1.63
.32 388.07 .982E+03 10.3 1.13 1.59
.34 388.09 .112E+04 12.0 1.15 1.56
.37 388.12 .127E+04 13.9 1.17 1.53
.39 388.14 .143E+04 15.9 1.19 1.50
.42 388.17 .160E+04 18.0 1.21 1.48
.45 388.20 .177E+04 20.3 1.23 1.45
.47 388.22 .196E+04 22.8 1.25 1.43
.50 388.25 .215E+04 25.4 1.27 1.41

```

```

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0034) 2.15 .34 11.83 41.18 .05 .53
OUTFLOW: ID= 1 (0035) 2.15 .31 11.83 41.18 .04 .52

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-----
| ADD HYD (0037) |
| 1 + 2 = 3 |
|-----|
| ID1= 1 (0036): | AREA QPEAK TPEAK R.V.
| + ID2= 2 (0035): | (ha) (cms) (hrs) (mm)
|=====|
| ID = 3 (0037): | 4.23 .590 11.83 37.75

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB |
| NASHYD (0039) | Area (ha)= 35.03 Curve Number (CN)= 65.5
| ID= 1 DT= 5.0 min | Ia (mm)= 7.17 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= 1.16

```

Unit Hyd Qpeak (cms)= 1.152

PEAK FLOW (cms)= .961 (i)
 TIME TO PEAK (hrs)= 13.083
 RUNOFF VOLUME (mm)= 34.213
 TOTAL RAINFALL (mm)= 94.090

RUNOFF COEFFICIENT = .364

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB          |
| NASHYD (0040) | Area (ha)= 3.95 Curve Number (CN)= 54.0
| ID= 1 DT= 5.0 min | Ia (mm)= 10.00 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .40

```

Unit Hyd Qpeak (cms)= .375

PEAK FLOW (cms)= .158 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 23.531
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .250

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0041) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
|-----|
| OUTFLOW          | STORAGE          | OUTFLOW          | STORAGE          |
| (cms)            | (ha.m.)         | (cms)            | (ha.m.)         |
| .0000            | .0000           | .0002            | .1655           |
| .0001            | .0976           | 20.0000         | .1665           |

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.16	12.17	23.53
OUTFLOW: ID= 1 (0041)	3.95	.00	25.33	.10

PEAK FLOW REDUCTION [Qout/Qin](%)= .06
 TIME SHIFT OF PEAK FLOW (min)=790.00
 MAXIMUM STORAGE USED (ha.m.)= .0926

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-----
| CALIB          |
| NASHYD (0044) | Area (ha)= .87 Curve Number (CN)= 64.6
| ID= 1 DT= 3.0 min | Ia (mm)= 6.68 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .06

```

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.050	.69	6.050	1.29	12.050	21.88	18.05	1.22
.100	.69	6.100	1.30	12.100	20.33	18.10	1.22
.150	.69	6.150	1.31	12.150	17.23	18.15	1.21
.200	.70	6.200	1.32	12.200	15.20	18.20	1.20
.250	.70	6.250	1.33	12.250	14.18	18.25	1.19
.300	.70	6.300	1.34	12.300	12.04	18.30	1.18
.350	.70	6.350	1.35	12.350	11.51	18.35	1.18
.400	.71	6.400	1.36	12.400	10.46	18.40	1.17
.450	.71	6.450	1.37	12.450	9.65	18.45	1.16
.500	.71	6.500	1.38	12.500	9.25	18.50	1.15
.550	.72	6.550	1.40	12.550	8.29	18.55	1.14
.600	.72	6.600	1.41	12.600	8.03	18.60	1.14
.650	.72	6.650	1.42	12.650	7.52	18.65	1.13
.700	.72	6.700	1.43	12.700	7.09	18.70	1.12
.750	.73	6.750	1.44	12.750	6.88	18.75	1.12
.800	.73	6.800	1.46	12.800	6.34	18.80	1.11
.850	.73	6.850	1.47	12.850	6.19	18.85	1.10
.900	.74	6.900	1.49	12.900	5.89	18.90	1.10
.950	.74	6.950	1.50	12.950	5.63	18.95	1.09
1.000	.74	7.000	1.51	13.000	5.50	19.00	1.08
1.050	.75	7.050	1.53	13.050	5.16	19.05	1.07
1.100	.75	7.100	1.54	13.100	5.06	19.10	1.07
1.150	.75	7.150	1.56	13.150	4.86	19.15	1.06
1.200	.75	7.200	1.57	13.200	4.68	19.20	1.06
1.250	.76	7.250	1.58	13.250	4.59	19.25	1.05
1.300	.76	7.300	1.61	13.300	4.36	19.30	1.04
1.350	.76	7.350	1.62	13.350	4.29	19.35	1.04
1.400	.77	7.400	1.64	13.400	4.15	19.40	1.03
1.450	.77	7.450	1.66	13.450	4.02	19.45	1.03
1.500	.77	7.500	1.67	13.500	3.96	19.50	1.02
1.550	.78	7.550	1.70	13.550	3.78	19.55	1.01
1.600	.78	7.600	1.71	13.600	3.73	19.60	1.01
1.650	.78	7.650	1.73	13.650	3.63	19.65	1.00
1.700	.79	7.700	1.75	13.700	3.53	19.70	1.00
1.750	.79	7.750	1.76	13.750	3.48	19.75	1.00
1.800	.79	7.800	1.79	13.800	3.35	19.80	.99
1.850	.80	7.850	1.80	13.850	3.31	19.85	.98

1.900	.80	7.900	1.83	13.900	3.23	19.90	.98
1.950	.80	7.950	1.85	13.950	3.15	19.95	.97
2.000	.81	8.000	1.86	14.000	3.11	20.00	.97
2.050	.81	8.050	1.90	14.050	3.01	20.05	.96
2.100	.81	8.100	1.92	14.100	2.98	20.10	.96
2.150	.82	8.150	1.94	14.150	2.91	20.15	.95
2.200	.82	8.200	1.97	14.200	2.85	20.20	.95
2.250	.82	8.250	1.98	14.250	2.82	20.25	.94
2.300	.83	8.300	2.03	14.300	2.74	20.30	.94
2.350	.83	8.350	2.04	14.350	2.71	20.35	.93
2.400	.84	8.400	2.07	14.400	2.66	20.40	.93
2.450	.84	8.450	2.11	14.450	2.61	20.45	.92
2.500	.84	8.500	2.12	14.500	2.58	20.50	.92
2.550	.85	8.550	2.17	14.550	2.51	20.55	.91
2.600	.85	8.600	2.19	14.600	2.49	20.60	.91
2.650	.86	8.650	2.23	14.650	2.45	20.65	.91
2.700	.86	8.700	2.26	14.700	2.40	20.70	.90
2.750	.86	8.750	2.28	14.750	2.38	20.75	.90
2.800	.87	8.800	2.34	14.800	2.32	20.80	.89
2.850	.87	8.850	2.36	14.850	2.31	20.85	.89
2.900	.88	8.900	2.41	14.900	2.27	20.90	.89
2.950	.88	8.950	2.45	14.950	2.23	20.95	.88
3.000	.88	9.000	2.47	15.000	2.22	21.00	.88
3.050	.89	9.050	2.54	15.050	2.16	21.05	.87
3.100	.89	9.100	2.57	15.100	2.15	21.10	.87
3.150	.90	9.150	2.62	15.150	2.12	21.15	.86
3.200	.90	9.200	2.67	15.200	2.09	21.20	.86
3.250	.91	9.250	2.70	15.250	2.07	21.25	.86
3.300	.91	9.300	2.79	15.300	2.03	21.30	.85
3.350	.92	9.350	2.82	15.350	2.01	21.35	.85
3.400	.92	9.400	2.88	15.400	1.99	21.40	.85
3.450	.93	9.450	2.95	15.450	1.96	21.45	.84
3.500	.93	9.500	2.98	15.500	1.95	21.50	.84
3.550	.94	9.550	3.09	15.550	1.91	21.55	.83
3.600	.94	9.600	3.13	15.600	1.89	21.60	.83
3.650	.95	9.650	3.20	15.650	1.87	21.65	.83
3.700	.95	9.700	3.29	15.700	1.85	21.70	.82
3.750	.96	9.750	3.33	15.750	1.84	21.75	.82
3.800	.96	9.800	3.47	15.800	1.80	21.80	.82
3.850	.97	9.850	3.52	15.850	1.79	21.85	.81
3.900	.97	9.900	3.62	15.900	1.77	21.90	.81
3.950	.98	9.950	3.73	15.950	1.75	21.95	.81
4.000	.98	10.000	3.78	16.000	1.74	22.00	.80
4.050	.99	10.050	3.96	16.050	1.71	22.05	.80
4.100	.99	10.100	4.03	16.100	1.70	22.10	.80
4.150	1.00	10.150	4.16	16.150	1.68	22.15	.79
4.200	1.01	10.200	4.31	16.200	1.66	22.20	.79
4.250	1.01	10.250	4.39	16.250	1.65	22.25	.79
4.300	1.02	10.300	4.64	16.300	1.62	22.30	.78
4.350	1.02	10.350	4.74	16.350	1.62	22.35	.78
4.400	1.03	10.400	4.93	16.400	1.60	22.40	.78
4.450	1.04	10.450	5.14	16.450	1.58	22.45	.77
4.500	1.04	10.500	5.25	16.500	1.57	22.50	.77
4.550	1.05	10.550	5.62	16.550	1.55	22.55	.77
4.600	1.05	10.600	5.77	16.600	1.54	22.60	.76
4.650	1.06	10.650	6.06	16.650	1.53	22.65	.76
4.700	1.07	10.700	6.40	16.700	1.51	22.70	.76
4.750	1.07	10.750	6.57	16.750	1.50	22.75	.76
4.800	1.08	10.800	7.17	16.800	1.48	22.80	.75
4.850	1.09	10.850	7.42	16.850	1.47	22.85	.75
4.900	1.10	10.900	7.91	16.900	1.46	22.90	.75
4.950	1.10	10.950	8.52	16.950	1.45	22.95	.74
5.000	1.11	11.000	8.82	17.000	1.44	23.00	.74
5.050	1.12	11.050	9.98	17.050	1.42	23.05	.74
5.100	1.12	11.100	10.48	17.100	1.41	23.10	.74
5.150	1.13	11.150	11.49	17.150	1.40	23.15	.73
5.200	1.14	11.200	12.85	17.200	1.39	23.20	.73
5.250	1.14	11.250	13.54	17.250	1.38	23.25	.73
5.300	1.16	11.300	16.46	17.300	1.36	23.30	.72
5.350	1.16	11.350	17.95	17.350	1.36	23.35	.72
5.400	1.17	11.400	20.92	17.400	1.35	23.40	.72
5.450	1.18	11.450	25.96	17.450	1.33	23.45	.72
5.500	1.18	11.500	28.49	17.500	1.33	23.50	.71
5.550	1.20	11.550	43.48	17.550	1.31	23.55	.71
5.600	1.20	11.600	56.91	17.600	1.31	23.60	.71
5.650	1.21	11.650	83.71	17.650	1.30	23.65	.71
5.700	1.22	11.700	147.75	17.700	1.29	23.70	.70
5.750	1.23	11.750	179.64	17.750	1.28	23.75	.70
5.800	1.24	11.800	85.03	17.800	1.26	23.80	.70
5.850	1.25	11.850	71.66	17.850	1.26	23.85	.70
5.900	1.26	11.900	45.00	17.900	1.25	23.90	.69
5.950	1.27	11.950	34.78	17.950	1.24	23.95	.69
6.000	1.27	12.000	29.68	18.000	1.23	24.00	.69

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .136 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 32.621

TOTAL RAINFALL (mm)= 94.147
 RUNOFF COEFFICIENT = .346

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0042) ID= 1 DT= 3.0 min	Area (ha)= .56 Ia (mm)= 5.00 U.H. Tp(hrs)= .06	Curve Number (CN)= 70.0 # of Linear Res.(N)= 3.00
---	--	--

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .105 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 36.603
 TOTAL RAINFALL (mm)= 94.147
 RUNOFF COEFFICIENT = .389

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0043) IN= 2---> OUT= 1 DT= 3.0 min	OUTFLOW (cms) .0000 .0001	STORAGE (ha.m.) .0000 .0118	OUTFLOW (cms) .0002 20.0000	STORAGE (ha.m.) .0357 .0367
---	---------------------------------	-----------------------------------	-----------------------------------	-----------------------------------

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0042)	.56	.10	11.75	36.60
OUTFLOW: ID= 1 (0043)	.56	.00	20.10	.70

PEAK FLOW REDUCTION [Qout/Qin](%)= .13
 TIME SHIFT OF PEAK FLOW (min)=501.00
 MAXIMUM STORAGE USED (ha.m.)= .0200

ADD HYD (0045) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0044):	.87	.136	11.75	32.62
+ ID2= 2 (0043):	.56	.000	20.10	.70
<hr/>				
ID = 3 (0045):	1.42	.136	11.75	20.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0046) IN= 2---> OUT= 1 DT= 3.0 min	OUTFLOW (cms) .0000 .0001	STORAGE (ha.m.) .0000 .0117	OUTFLOW (cms) .0002 20.0000	STORAGE (ha.m.) .1073 .1083
---	---------------------------------	-----------------------------------	-----------------------------------	-----------------------------------

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0045)	1.42	.14	11.75	20.16
OUTFLOW: ID= 1 (0046)	1.42	.00	24.10	.36

PEAK FLOW REDUCTION [Qout/Qin](%)= .09
 TIME SHIFT OF PEAK FLOW (min)=741.00
 MAXIMUM STORAGE USED (ha.m.)= .0282

CALIB NASHYD (0047) ID= 1 DT= 3.0 min	Area (ha)= .48 Ia (mm)= 5.00 U.H. Tp(hrs)= .06	Curve Number (CN)= 70.0 # of Linear Res.(N)= 3.00
---	--	--

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .091 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 36.603
 TOTAL RAINFALL (mm)= 94.147
 RUNOFF COEFFICIENT = .389

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0048)
 IN= 2----> OUT= 1
 DT= 3.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0731
.0001	.0496	20.0000	.0741

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0047)	.48	.09	11.75	36.60
OUTFLOW: ID= 1 (0048)	.48	.00	20.15	.20

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=504.00
 MAXIMUM STORAGE USED (ha.m.)= .0175

CALIB
 NASHYD (0049)
 ID= 1 DT= 5.0 min

Area (ha)=	2.77	Curve Number (CN)=	70.7
Ia (mm)=	5.35	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	.11		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.69	6.083	1.29	12.083	21.88	18.08	1.22
.167	.69	6.167	1.31	12.167	17.23	18.17	1.21
.250	.70	6.250	1.33	12.250	14.18	18.25	1.19
.333	.70	6.333	1.34	12.333	12.04	18.33	1.18
.417	.71	6.417	1.36	12.417	10.46	18.42	1.17
.500	.71	6.500	1.38	12.500	9.25	18.50	1.15
.583	.72	6.583	1.40	12.583	8.29	18.58	1.14
.667	.72	6.667	1.42	12.667	7.52	18.67	1.13
.750	.73	6.750	1.44	12.750	6.88	18.75	1.12
.833	.73	6.833	1.46	12.833	6.34	18.83	1.11
.917	.74	6.917	1.49	12.917	5.89	18.92	1.10
1.000	.74	7.000	1.51	13.000	5.50	19.00	1.08
1.083	.75	7.083	1.53	13.083	5.16	19.08	1.07
1.167	.75	7.167	1.56	13.167	4.86	19.17	1.06
1.250	.76	7.250	1.58	13.250	4.59	19.25	1.05
1.333	.76	7.333	1.61	13.333	4.36	19.33	1.04
1.417	.77	7.417	1.64	13.417	4.15	19.42	1.03
1.500	.77	7.500	1.67	13.500	3.96	19.50	1.02
1.583	.78	7.583	1.70	13.583	3.78	19.58	1.01
1.667	.78	7.667	1.73	13.667	3.63	19.67	1.00
1.750	.79	7.750	1.76	13.750	3.48	19.75	1.00
1.833	.79	7.833	1.79	13.833	3.35	19.83	.99
1.917	.80	7.917	1.83	13.917	3.23	19.92	.98
2.000	.81	8.000	1.86	14.000	3.11	20.00	.97
2.083	.81	8.083	1.90	14.083	3.01	20.08	.96
2.167	.82	8.167	1.94	14.167	2.91	20.17	.95
2.250	.82	8.250	1.98	14.250	2.82	20.25	.94
2.333	.83	8.333	2.03	14.333	2.74	20.33	.94
2.417	.84	8.417	2.07	14.417	2.66	20.42	.93
2.500	.84	8.500	2.12	14.500	2.58	20.50	.92
2.583	.85	8.583	2.17	14.583	2.51	20.58	.91
2.667	.86	8.667	2.23	14.667	2.45	20.67	.91
2.750	.86	8.750	2.28	14.750	2.38	20.75	.90
2.833	.87	8.833	2.34	14.833	2.32	20.83	.89
2.917	.88	8.917	2.41	14.917	2.27	20.92	.89
3.000	.88	9.000	2.47	15.000	2.22	21.00	.88
3.083	.89	9.083	2.54	15.083	2.16	21.08	.87
3.167	.90	9.167	2.62	15.167	2.12	21.17	.86
3.250	.91	9.250	2.70	15.250	2.07	21.25	.86
3.333	.91	9.333	2.79	15.333	2.03	21.33	.85
3.417	.92	9.417	2.88	15.417	1.99	21.42	.85
3.500	.93	9.500	2.98	15.500	1.95	21.50	.84
3.583	.94	9.583	3.09	15.583	1.91	21.58	.83
3.667	.95	9.667	3.20	15.667	1.87	21.67	.83
3.750	.96	9.750	3.33	15.750	1.84	21.75	.82
3.833	.96	9.833	3.47	15.833	1.80	21.83	.82
3.917	.97	9.917	3.62	15.917	1.77	21.92	.81
4.000	.98	10.000	3.78	16.000	1.74	22.00	.80
4.083	.99	10.083	3.96	16.083	1.71	22.08	.80
4.167	1.00	10.167	4.16	16.167	1.68	22.17	.79
4.250	1.01	10.250	4.39	16.250	1.65	22.25	.79
4.333	1.02	10.333	4.64	16.333	1.62	22.33	.78
4.417	1.03	10.417	4.93	16.417	1.60	22.42	.78
4.500	1.04	10.500	5.25	16.500	1.57	22.50	.77
4.583	1.05	10.583	5.62	16.583	1.55	22.58	.77
4.667	1.06	10.667	6.06	16.667	1.53	22.67	.76
4.750	1.07	10.750	6.57	16.750	1.50	22.75	.76
4.833	1.08	10.833	7.17	16.833	1.48	22.83	.75
4.917	1.10	10.917	7.91	16.917	1.46	22.92	.75

5.000	1.11	11.000	8.82	17.000	1.44	23.00	.74
5.083	1.12	11.083	9.98	17.083	1.42	23.08	.74
5.167	1.13	11.167	11.49	17.167	1.40	23.17	.73
5.250	1.14	11.250	13.53	17.250	1.38	23.25	.73
5.333	1.16	11.333	16.46	17.333	1.36	23.33	.72
5.417	1.17	11.417	20.92	17.417	1.35	23.42	.72
5.500	1.18	11.500	28.48	17.500	1.33	23.50	.71
5.583	1.20	11.583	43.48	17.583	1.31	23.58	.71
5.667	1.21	11.667	83.71	17.667	1.30	23.67	.71
5.750	1.23	11.750	179.68	17.750	1.28	23.75	.70
5.833	1.24	11.833	85.04	17.833	1.26	23.83	.70
5.917	1.26	11.917	45.01	17.917	1.25	23.92	.69
6.000	1.27	12.000	29.69	18.000	1.23	24.00	.60

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .411 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 39.902
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .424

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0055)	Area (ha)=	5.19	Curve Number (CN)=	73.3			
ID= 1 DT= 5.0 min	Ia (mm)=	4.00	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.11					

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .843 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 43.670
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .464

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0052)	Area (ha)=	3.90	Curve Number (CN)=	69.4			
ID= 1 DT= 5.0 min	Ia (mm)=	4.85	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.08					

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .632 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 37.056
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .394

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0050)	Area (ha)=	11.96	Curve Number (CN)=	66.4			
ID= 1 DT= 5.0 min	Ia (mm)=	5.74	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.18					

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.238 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 35.923
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .382

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0051)							
IN= 2---> OUT= 1							
DT= 5.0 min							
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)			
	.0000	.0000	20.0000	.1583			
	.0001	.1573	.0000	.0000			
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)			
INFLOW : ID= 2 (0050)	11.96	1.24	11.92	35.92			
OUTFLOW: ID= 1 (0051)	11.96	1.97	12.08	22.77			

PEAK FLOW REDUCTION [Qout/Qin](%)=159.41
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= .2904

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ADD HYD (0053)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0052):	3.90	.632	11.75	37.06
+ ID2= 2 (0051):	11.96	1.973	12.08	22.77
ID = 3 (0053):	15.86	2.133	12.08	26.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0054)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1	.0000	.0000	20.0000	.0771
DT= 5.0 min	.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0053)	15.86	2.13	12.08	26.28
OUTFLOW: ID= 1 (0054)	15.86	2.24	12.08	21.48

PEAK FLOW REDUCTION [Qout/Qin](%)=104.96
 TIME SHIFT OF PEAK FLOW (min)= .00
 MAXIMUM STORAGE USED (ha.m.)= .0988

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ROUTE CHN (0056)	ROUTING TIME STEP (min)
IN= 2---> OUT= 1	5.00

<----- DATA FOR SECTION (1.5) ----->

Distance	Elevation	Manning	
.00	425.00	.0300	
.75	424.25	.0300 / .0300	Main Channel
1.75	424.25	.0300 / .0300	Main Channel
2.50	425.00	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0054)	15.86	2.24	12.08	21.48	.53	2.77
OUTFLOW: ID= 1 (0056)	15.86	1.19	12.17	21.48	.36	2.38

ADD HYD (0057)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0055):	5.19	.843	11.83	43.67
+ ID2= 2 (0056):	15.86	1.186	12.17	21.48

=====
ID = 3 (0057): 21.05 1.420 12.17 26.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0058) Area (ha)= 21.77 Curve Number (CN)= 67.4
ID= 1 DT= 5.0 min Ia (mm)= 5.22 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= 2.354

PEAK FLOW (cms)= 1.553 (i)
TIME TO PEAK (hrs)= 12.083
RUNOFF VOLUME (mm)= 37.344
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .397

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
NASHYD (0059) Area (ha)= 11.96 Curve Number (CN)= 66.4
ID= 1 DT= 5.0 min Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .18

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.238 (i)
TIME TO PEAK (hrs)= 11.917
RUNOFF VOLUME (mm)= 35.923
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .382

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0060)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.1583
.0001	.1573	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0059)	11.96	1.24	11.92	35.92
OUTFLOW: ID= 1 (0060)	11.96	1.97	12.08	22.77

PEAK FLOW REDUCTION [Qout/Qin](%)=159.41
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= .2904

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

CALIB
NASHYD (0061) Area (ha)= 3.90 Curve Number (CN)= 69.4
ID= 1 DT= 5.0 min Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .632 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 37.056
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .394

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0062)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0060):	11.96	1.973	12.08	22.77
+ ID2= 2 (0061):	3.90	.632	11.75	37.06
=====				
ID = 3 (0062):	15.86	2.133	12.08	26.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.


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-----
| RESERVOIR (0063) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.0771
.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0062)	15.86	2.13	12.08	26.28
OUTFLOW: ID= 1 (0063)	15.86	2.24	12.08	21.48

PEAK FLOW REDUCTION [Qout/Qin](%)=104.96
 TIME SHIFT OF PEAK FLOW (min)= .00
 MAXIMUM STORAGE USED (ha.m.)= .0988

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

```

-----
| ROUTE CHN (0065) |
| IN= 2---> OUT= 1 |
-----

```

Routing time step (min)'= 5.00

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<----- DATA FOR SECTION ( 1.5) ----->
Distance      Elevation      Manning
.00           425.00         .0300
.75           424.25         .0300 / .0300 Main Channel
1.75         424.25         .0300 / .0300 Main Channel
2.50         425.00         .0300

```

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0063)	15.86	2.24	12.08	21.48	.53	2.77
OUTFLOW: ID= 1 (0065)	15.86	1.19	12.17	21.48	.36	2.38

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-----
| CALIB NASHYD (0064) |
| ID= 1 DT= 5.0 min  |
-----

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Area (ha)= 5.19 Curve Number (CN)= 73.3
 Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .843 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 43.670
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .464

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ADD HYD (0066) |
| 1 + 2 = 3      |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0065):	15.86	1.186	12.17	21.48
+ ID2= 2 (0064):	5.19	.843	11.83	43.67
=====	=====	=====	=====	=====
ID = 3 (0066):	21.05	1.420	12.17	26.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB
| NASHYD (0069) | Area (ha)= 1.80 Curve Number (CN)= 58.8
| ID= 1 DT= 5.0 min | Ia (mm)= 8.49 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .07

```

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .205 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 25.194
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB
| NASHYD (0067) | Area (ha)= 1.52 Curve Number (CN)= 62.0
| ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .06

```

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .196 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 25.942
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0068)
| IN= 2---> OUT= 1
| DT= 5.0 min

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0207
	.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.20	11.75	25.94
OUTFLOW: ID= 1 (0068)	1.52	.04	12.17	12.42

PEAK FLOW REDUCTION [Qout/Qin](%)= 21.69
 TIME SHIFT OF PEAK FLOW (min)= 25.00
 MAXIMUM STORAGE USED (ha.m.)= .0282

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-----
| ADD HYD (0071)
| 1 + 2 = 3

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0069):	1.80	.205	11.75	25.19
+ ID2= 2 (0068):	1.52	.042	12.17	12.42
=====				
ID = 3 (0071):	3.32	.205	11.75	19.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| RESERVOIR (0070)
| IN= 2---> OUT= 1
| DT= 5.0 min

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0708
	.0001	.0707	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0071)	3.32	.21	11.75	19.34
OUTFLOW: ID= 1 (0070)	3.32	.00	24.17	.10

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=745.00
 MAXIMUM STORAGE USED (ha.m.)= .0639

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-----
| ROUTE CHN (0073) |

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| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.6) ----->

Distance	Elevation	Manning	
.00	421.26	.0300	
1.10	420.66	.0300 / .0300	Main Channel
2.00	420.66	.0300 / .0300	Main Channel
3.10	421.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

<---- hydrograph ----> <-pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	3.32	.00	24.17	.10	.00	.05
OUTFLOW: ID= 1 (0073)	3.32	.00	24.17	.09	.00	.05

ADD HYD (0074)

1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0066):	21.05	1.420	12.17	26.96
+ ID2= 2 (0073):	3.32	.000	24.17	.09
=====	=====	=====	=====	=====
ID = 3 (0074):	24.37	1.420	12.17	23.30

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0072)

ID= 1 DT= 5.0 min

Area (ha)=	24.19	Curve Number (CN)=	60.0
Ia (mm)=	8.62	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	.37		

Unit Hyd Qpeak (cms)= 2.505

PEAK FLOW (cms)= 1.258 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 28.625
 TOTAL RAINFALL (mm)= 94.090
 RUNOFF COEFFICIENT = .304

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)

1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0074):	24.37	1.420	12.17	23.30
+ ID2= 2 (0072):	24.19	1.258	12.17	28.63
=====	=====	=====	=====	=====
ID = 3 (0075):	48.56	2.678	12.17	25.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0076)

ID= 1 DT= 5.0 min

Area (ha)=	127.28	Curve Number (CN)=	59.9
Ia (mm)=	8.29	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	.79		

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 3.908 (i)
TIME TO PEAK (hrs)= 12.583
RUNOFF VOLUME (mm)= 28.782
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .306

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0077)	Area (ha)= 17.28	Curve Number (CN)= 58.3	
ID= 1 DT= 5.0 min	Ia (mm)= 9.24	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .57		

Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .625 (i)
TIME TO PEAK (hrs)= 12.417
RUNOFF VOLUME (mm)= 27.019
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .287

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0082)	Area (ha)= .24	Curve Number (CN)= 77.6	
ID= 1 DT= 5.0 min	Ia (mm)= 3.49	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .11		

Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .044 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 49.199
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .523

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0078)	Area (ha)= 2.66	Curve Number (CN)= 59.8	
ID= 1 DT= 5.0 min	Ia (mm)= 8.55	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .07		

Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .308 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 26.215
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .279

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0079)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0608
	.0001	.0607	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0078)	2.66	.31	11.75	26.21
OUTFLOW: ID= 1 (0079)	2.66	.01	17.17	3.40

PEAK FLOW REDUCTION [Qout/Qin](%)= 2.97
TIME SHIFT OF PEAK FLOW (min)=325.00
MAXIMUM STORAGE USED (ha.m.)= .0649

ADD HYD (0083)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0082):	.24	.044	11.83	49.20
+ ID2= 2 (0079):	2.66	.009	17.17	3.40
=====	=====	=====	=====	=====
ID = 3 (0083):	2.90	.044	11.83	7.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0080) Area (ha)= 14.63 Curve Number (CN)= 58.0
ID= 1 DT= 5.0 min Ia (mm)= 9.37 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .57

Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .523 (i)
TIME TO PEAK (hrs)= 12.417
RUNOFF VOLUME (mm)= 26.746
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .284

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0081)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0083):	2.90	.044	11.83	7.15
+ ID2= 2 (0080):	14.63	.523	12.42	26.75
=====				
ID = 3 (0081):	17.52	.530	12.33	23.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0084) Area (ha)= 7.71 Curve Number (CN)= 62.5
ID= 1 DT= 5.0 min Ia (mm)= 9.14 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .29

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .497 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 30.350
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .323

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
NASHYD (0085) Area (ha)= .91 Curve Number (CN)= 64.9
ID= 1 DT= 5.0 min Ia (mm)= 8.53 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= .313

PEAK FLOW (cms)= .108 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 32.229
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .343

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
NASHYD (0086) Area (ha)= 19.15 Curve Number (CN)= 71.3
ID= 1 DT= 5.0 min Ia (mm)= 5.81 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= 1.900 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 40.838
TOTAL RAINFALL (mm)= 94.090
RUNOFF COEFFICIENT = .434

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

** SIMULATION NUMBER: 5 **

CHICAGO STORM
 Ptotal=105.44 mm

IDF curve parameters: A=1931.219
 B= 10.500
 C= .836
 used in: INTENSITY = A / (t + B)^{AC}

Duration of storm = 24.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = .49

The CORRELATION coefficient is = .9993

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	200.00	195.31
10.	145.00	154.60
15.	130.00	128.81
30.	96.00	87.50
60.	55.00	55.05
120.	32.00	32.90
360.	13.00	13.75
720.	7.60	7.80
1440.	4.70	4.39

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.75	6.08	1.41	12.08	25.27	18.08	1.34
.17	.75	6.17	1.43	12.17	19.86	18.17	1.32
.25	.76	6.25	1.45	12.25	16.30	18.25	1.30
.33	.76	6.33	1.47	12.33	13.80	18.33	1.29
.42	.77	6.42	1.49	12.42	11.96	18.42	1.28
.50	.77	6.50	1.51	12.50	10.55	18.50	1.26
.58	.78	6.58	1.54	12.58	9.43	18.58	1.25
.67	.78	6.67	1.56	12.67	8.53	18.67	1.23
.75	.79	6.75	1.58	12.75	7.79	18.75	1.22
.83	.79	6.83	1.61	12.83	7.18	18.83	1.21
.92	.80	6.92	1.63	12.92	6.65	18.92	1.20
1.00	.80	7.00	1.66	13.00	6.20	19.00	1.18
1.08	.81	7.08	1.68	13.08	5.80	19.08	1.17
1.17	.82	7.17	1.71	13.17	5.46	19.17	1.16
1.25	.82	7.25	1.74	13.25	5.16	19.25	1.15
1.33	.83	7.33	1.77	13.33	4.89	19.33	1.14
1.42	.83	7.42	1.80	13.42	4.64	19.42	1.13
1.50	.84	7.50	1.83	13.50	4.43	19.50	1.12
1.58	.84	7.58	1.86	13.58	4.23	19.58	1.11
1.67	.85	7.67	1.90	13.67	4.05	19.67	1.10
1.75	.86	7.75	1.94	13.75	3.88	19.75	1.09
1.83	.86	7.83	1.97	13.83	3.73	19.83	1.08
1.92	.87	7.92	2.01	13.92	3.59	19.92	1.07
2.00	.88	8.00	2.05	14.00	3.47	20.00	1.06
2.08	.88	8.08	2.10	14.08	3.35	20.08	1.05
2.17	.89	8.17	2.14	14.17	3.24	20.17	1.04
2.25	.90	8.25	2.19	14.25	3.13	20.25	1.03
2.33	.90	8.33	2.24	14.33	3.04	20.33	1.02
2.42	.91	8.42	2.29	14.42	2.95	20.42	1.01
2.50	.92	8.50	2.34	14.50	2.86	20.50	1.00
2.58	.92	8.58	2.40	14.58	2.78	20.58	1.00
2.67	.93	8.67	2.46	14.67	2.71	20.67	.99
2.75	.94	8.75	2.52	14.75	2.64	20.75	.98
2.83	.95	8.83	2.59	14.83	2.57	20.83	.97
2.92	.95	8.92	2.66	14.92	2.51	20.92	.96
3.00	.96	9.00	2.74	15.00	2.45	21.00	.96
3.08	.97	9.08	2.82	15.08	2.39	21.08	.95
3.17	.98	9.17	2.90	15.17	2.34	21.17	.94
3.25	.99	9.25	3.00	15.25	2.29	21.25	.93
3.33	1.00	9.33	3.09	15.33	2.24	21.33	.93
3.42	1.00	9.42	3.20	15.42	2.19	21.42	.92
3.50	1.01	9.50	3.31	15.50	2.14	21.50	.91
3.58	1.02	9.58	3.43	15.58	2.10	21.58	.91
3.67	1.03	9.67	3.57	15.67	2.06	21.67	.90
3.75	1.04	9.75	3.71	15.75	2.02	21.75	.89
3.83	1.05	9.83	3.87	15.83	1.98	21.83	.89
3.92	1.06	9.92	4.04	15.92	1.95	21.92	.88
4.00	1.07	10.00	4.23	16.00	1.91	22.00	.87
4.08	1.08	10.08	4.43	16.08	1.88	22.08	.87
4.17	1.09	10.17	4.66	16.17	1.85	22.17	.86
4.25	1.10	10.25	4.92	16.25	1.82	22.25	.86
4.33	1.11	10.33	5.21	16.33	1.79	22.33	.85
4.42	1.12	10.42	5.54	16.42	1.76	22.42	.84
4.50	1.14	10.50	5.91	16.50	1.73	22.50	.84
4.58	1.15	10.58	6.34	16.58	1.70	22.58	.83
4.67	1.16	10.67	6.84	16.67	1.68	22.67	.83
4.75	1.17	10.75	7.43	16.75	1.65	22.75	.82
4.83	1.18	10.83	8.14	16.83	1.63	22.83	.82
4.92	1.20	10.92	8.99	16.92	1.60	22.92	.81
5.00	1.21	11.00	10.05	17.00	1.58	23.00	.81
5.08	1.22	11.08	11.40	17.08	1.56	23.08	.80
5.17	1.24	11.17	13.16	17.17	1.54	23.17	.80

5.25	1.25	11.25	15.55	17.25	1.51	23.25	.79
5.33	1.27	11.33	18.96	17.33	1.49	23.33	.79
5.42	1.28	11.42	24.16	17.42	1.47	23.42	.78
5.50	1.30	11.50	32.93	17.50	1.46	23.50	.78
5.58	1.31	11.58	50.12	17.58	1.44	23.58	.77
5.67	1.33	11.67	94.83	17.67	1.42	23.67	.77
5.75	1.34	11.75	195.31	17.75	1.40	23.75	.76
5.83	1.36	11.83	96.28	17.83	1.38	23.83	.76
5.92	1.38	11.92	51.86	17.92	1.37	23.92	.75
6.00	1.39	12.00	34.32	18.00	1.35	24.00	.75

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| CALIB          |
| NASHYD (0021) | Area (ha)= 8.81 Curve Number (CN)= 68.3
| ID= 1 DT= 5.0 min | Ia (mm)= 6.50 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= 1.36

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Unit Hyd Qpeak (cms)= .248

PEAK FLOW (cms)= .287 (i)
TIME TO PEAK (hrs)= 13.250
RUNOFF VOLUME (mm)= 45.125
TOTAL RAINFALL (mm)= 105.442
RUNOFF COEFFICIENT = .428

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| CALIB          |
| NASHYD (0027) | Area (ha)= .68 Curve Number (CN)= 72.2
| ID= 1 DT= 2.0 min | Ia (mm)= 4.91 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= .06

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NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.033	.75	6.033	1.41	12.033	25.27	18.03	1.34
.067	.75	6.067	1.41	12.067	25.27	18.07	1.34
.100	.75	6.100	1.42	12.100	22.56	18.10	1.33
.133	.75	6.133	1.43	12.133	19.86	18.13	1.32
.167	.75	6.167	1.43	12.167	19.85	18.17	1.32
.200	.76	6.200	1.45	12.200	16.30	18.20	1.30
.233	.76	6.233	1.45	12.233	16.30	18.23	1.30
.267	.76	6.267	1.46	12.267	15.05	18.27	1.30
.300	.76	6.300	1.47	12.300	13.80	18.30	1.29
.333	.76	6.333	1.47	12.333	13.80	18.33	1.29
.367	.77	6.367	1.49	12.367	11.96	18.37	1.28
.400	.77	6.400	1.49	12.400	11.96	18.40	1.28
.433	.77	6.433	1.50	12.433	11.25	18.43	1.27
.467	.77	6.467	1.51	12.467	10.55	18.47	1.26
.500	.77	6.500	1.51	12.500	10.54	18.50	1.26
.533	.78	6.533	1.54	12.533	9.43	18.53	1.25
.567	.78	6.567	1.54	12.567	9.43	18.57	1.25
.600	.78	6.600	1.55	12.600	8.98	18.60	1.24
.633	.78	6.633	1.56	12.633	8.53	18.63	1.23
.667	.78	6.667	1.56	12.667	8.53	18.67	1.23
.700	.79	6.700	1.58	12.700	7.79	18.70	1.22
.733	.79	6.733	1.58	12.733	7.79	18.73	1.22
.767	.79	6.767	1.59	12.767	7.48	18.77	1.22
.800	.79	6.800	1.61	12.800	7.18	18.80	1.21
.833	.79	6.833	1.61	12.833	7.17	18.83	1.21
.867	.80	6.867	1.63	12.867	6.65	18.87	1.20
.900	.80	6.900	1.63	12.900	6.65	18.90	1.20
.933	.80	6.933	1.64	12.933	6.42	18.93	1.19
.967	.80	6.967	1.66	12.967	6.20	18.97	1.18
1.000	.80	7.000	1.66	13.000	6.20	19.00	1.18
1.033	.81	7.033	1.68	13.033	5.80	19.03	1.17
1.067	.81	7.067	1.68	13.067	5.80	19.07	1.17
1.100	.81	7.100	1.70	13.100	5.63	19.10	1.17
1.133	.82	7.133	1.71	13.133	5.46	19.13	1.16
1.167	.82	7.167	1.71	13.167	5.46	19.17	1.16
1.200	.82	7.200	1.74	13.200	5.16	19.20	1.15
1.233	.82	7.233	1.74	13.233	5.16	19.23	1.15
1.267	.82	7.267	1.75	13.267	5.02	19.27	1.14
1.300	.83	7.300	1.77	13.300	4.89	19.30	1.14
1.333	.83	7.333	1.77	13.333	4.89	19.33	1.14
1.367	.83	7.367	1.80	13.367	4.64	19.37	1.13
1.400	.83	7.400	1.80	13.400	4.64	19.40	1.13
1.433	.84	7.433	1.82	13.433	4.53	19.43	1.12
1.467	.84	7.467	1.83	13.467	4.43	19.47	1.12
1.500	.84	7.500	1.83	13.500	4.42	19.50	1.12
1.533	.84	7.533	1.86	13.533	4.23	19.53	1.11
1.567	.84	7.567	1.86	13.567	4.23	19.57	1.11

1.600	.85	7.600	1.88	13.600	4.14	19.60	1.10
1.633	.85	7.633	1.90	13.633	4.05	19.63	1.10
1.667	.85	7.667	1.90	13.667	4.05	19.67	1.10
1.700	.86	7.700	1.94	13.700	3.88	19.70	1.09
1.733	.86	7.733	1.94	13.733	3.88	19.73	1.09
1.767	.86	7.767	1.95	13.767	3.81	19.77	1.08
1.800	.86	7.800	1.97	13.800	3.73	19.80	1.08
1.833	.86	7.833	1.97	13.833	3.73	19.83	1.08
1.867	.87	7.867	2.01	13.867	3.59	19.87	1.07
1.900	.87	7.900	2.01	13.900	3.59	19.90	1.07
1.933	.87	7.933	2.03	13.933	3.53	19.93	1.06
1.967	.88	7.967	2.05	13.967	3.47	19.97	1.06
2.000	.88	8.000	2.05	14.000	3.47	20.00	1.06
2.033	.88	8.033	2.10	14.033	3.35	20.03	1.05
2.067	.88	8.067	2.10	14.067	3.35	20.07	1.05
2.100	.89	8.100	2.12	14.100	3.29	20.10	1.04
2.133	.89	8.133	2.14	14.133	3.24	20.13	1.04
2.167	.89	8.167	2.14	14.167	3.24	20.17	1.04
2.200	.90	8.200	2.19	14.200	3.13	20.20	1.03
2.233	.90	8.233	2.19	14.233	3.13	20.23	1.03
2.267	.90	8.267	2.21	14.267	3.09	20.27	1.03
2.300	.90	8.300	2.24	14.300	3.04	20.30	1.02
2.333	.90	8.333	2.24	14.333	3.04	20.33	1.02
2.367	.91	8.367	2.29	14.367	2.95	20.37	1.01
2.400	.91	8.400	2.29	14.400	2.95	20.40	1.01
2.433	.91	8.433	2.32	14.433	2.91	20.43	1.01
2.467	.92	8.467	2.34	14.467	2.86	20.47	1.00
2.500	.92	8.500	2.34	14.500	2.86	20.50	1.00
2.533	.92	8.533	2.40	14.533	2.78	20.53	1.00
2.567	.92	8.567	2.40	14.567	2.78	20.57	1.00
2.600	.93	8.600	2.43	14.600	2.75	20.60	.99
2.633	.93	8.633	2.46	14.633	2.71	20.63	.99
2.667	.93	8.667	2.46	14.667	2.71	20.67	.99
2.700	.94	8.700	2.52	14.700	2.64	20.70	.98
2.733	.94	8.733	2.52	14.733	2.64	20.73	.98
2.767	.94	8.767	2.56	14.767	2.60	20.77	.98
2.800	.95	8.800	2.59	14.800	2.57	20.80	.97
2.833	.95	8.833	2.59	14.833	2.57	20.83	.97
2.867	.95	8.867	2.66	14.867	2.51	20.87	.96
2.900	.95	8.900	2.66	14.900	2.51	20.90	.96
2.933	.96	8.933	2.70	14.933	2.48	20.93	.96
2.967	.96	8.967	2.74	14.967	2.45	20.97	.96
3.000	.96	9.000	2.74	15.000	2.45	21.00	.96
3.033	.97	9.033	2.82	15.033	2.39	21.03	.95
3.067	.97	9.067	2.82	15.067	2.39	21.07	.95
3.100	.98	9.100	2.86	15.100	2.36	21.10	.95
3.133	.98	9.133	2.90	15.133	2.34	21.13	.94
3.167	.98	9.167	2.90	15.167	2.34	21.17	.94
3.200	.99	9.200	3.00	15.200	2.29	21.20	.93
3.233	.99	9.233	3.00	15.233	2.29	21.23	.93
3.267	.99	9.267	3.05	15.267	2.26	21.27	.93
3.300	1.00	9.300	3.09	15.300	2.24	21.30	.93
3.333	1.00	9.333	3.09	15.333	2.24	21.33	.93
3.367	1.00	9.367	3.20	15.367	2.19	21.37	.92
3.400	1.00	9.400	3.20	15.400	2.19	21.40	.92
3.433	1.01	9.433	3.26	15.433	2.17	21.43	.92
3.467	1.01	9.467	3.31	15.467	2.14	21.47	.91
3.500	1.01	9.500	3.31	15.500	2.14	21.50	.91
3.533	1.02	9.533	3.43	15.533	2.10	21.53	.91
3.567	1.02	9.567	3.43	15.567	2.10	21.57	.91
3.600	1.03	9.600	3.50	15.600	2.08	21.60	.90
3.633	1.03	9.633	3.57	15.633	2.06	21.63	.90
3.667	1.03	9.667	3.57	15.667	2.06	21.67	.90
3.700	1.04	9.700	3.71	15.700	2.02	21.70	.89
3.733	1.04	9.733	3.71	15.733	2.02	21.73	.89
3.767	1.05	9.767	3.79	15.767	2.00	21.77	.89
3.800	1.05	9.800	3.87	15.800	1.98	21.80	.89
3.833	1.05	9.833	3.87	15.833	1.98	21.83	.89
3.867	1.06	9.867	4.04	15.867	1.95	21.87	.88
3.900	1.06	9.900	4.04	15.900	1.95	21.90	.88
3.933	1.07	9.933	4.13	15.933	1.93	21.93	.88
3.967	1.07	9.967	4.23	15.967	1.91	21.97	.87
4.000	1.07	10.000	4.23	16.000	1.91	22.00	.87
4.033	1.08	10.033	4.43	16.033	1.88	22.03	.87
4.067	1.08	10.067	4.43	16.067	1.88	22.07	.87
4.100	1.09	10.100	4.55	16.100	1.86	22.10	.87
4.133	1.09	10.133	4.66	16.133	1.85	22.13	.86
4.167	1.09	10.167	4.66	16.167	1.85	22.17	.86
4.200	1.10	10.200	4.92	16.200	1.82	22.20	.86
4.233	1.10	10.233	4.92	16.233	1.82	22.23	.86
4.267	1.11	10.267	5.07	16.267	1.80	22.27	.85
4.300	1.11	10.300	5.21	16.300	1.79	22.30	.85
4.333	1.11	10.333	5.21	16.333	1.79	22.33	.85
4.367	1.12	10.367	5.54	16.367	1.76	22.37	.84
4.400	1.12	10.400	5.54	16.400	1.76	22.40	.84
4.433	1.13	10.433	5.73	16.433	1.74	22.43	.84
4.467	1.14	10.467	5.91	16.467	1.73	22.47	.84
4.500	1.14	10.500	5.91	16.500	1.73	22.50	.84
4.533	1.15	10.533	6.34	16.533	1.70	22.53	.83

4.567	1.15	10.567	6.34	16.567	1.70	22.57	.83
4.600	1.15	10.600	6.59	16.600	1.69	22.60	.83
4.633	1.16	10.633	6.84	16.633	1.68	22.63	.83
4.667	1.16	10.667	6.84	16.667	1.68	22.67	.83
4.700	1.17	10.700	7.43	16.700	1.65	22.70	.82
4.733	1.17	10.733	7.43	16.733	1.65	22.73	.82
4.767	1.18	10.767	7.78	16.767	1.64	22.77	.82
4.800	1.18	10.800	8.14	16.800	1.63	22.80	.82
4.833	1.18	10.833	8.14	16.833	1.63	22.83	.82
4.867	1.20	10.867	8.99	16.867	1.60	22.87	.81
4.900	1.20	10.900	8.99	16.900	1.60	22.90	.81
4.933	1.20	10.933	9.52	16.933	1.59	22.93	.81
4.967	1.21	10.967	10.05	16.967	1.58	22.97	.81
5.000	1.21	11.000	10.05	17.000	1.58	23.00	.81
5.033	1.22	11.033	11.40	17.033	1.56	23.03	.80
5.067	1.22	11.067	11.40	17.067	1.56	23.07	.80
5.100	1.23	11.100	12.28	17.100	1.55	23.10	.80
5.133	1.24	11.133	13.16	17.133	1.54	23.13	.80
5.167	1.24	11.167	13.16	17.167	1.54	23.17	.80
5.200	1.25	11.200	15.55	17.200	1.51	23.20	.79
5.233	1.25	11.233	15.55	17.233	1.51	23.23	.79
5.267	1.26	11.267	17.25	17.267	1.50	23.27	.79
5.300	1.27	11.300	18.96	17.300	1.49	23.30	.79
5.333	1.27	11.333	18.96	17.333	1.49	23.33	.79
5.367	1.28	11.367	24.16	17.367	1.47	23.37	.78
5.400	1.28	11.400	24.16	17.400	1.47	23.40	.78
5.433	1.29	11.433	28.55	17.433	1.47	23.43	.78
5.467	1.30	11.467	32.93	17.467	1.46	23.47	.78
5.500	1.30	11.500	32.95	17.500	1.46	23.50	.78
5.533	1.31	11.533	50.12	17.533	1.44	23.53	.77
5.567	1.31	11.567	50.12	17.567	1.44	23.57	.77
5.600	1.32	11.600	72.53	17.600	1.43	23.60	.77
5.633	1.33	11.633	94.83	17.633	1.42	23.63	.77
5.667	1.33	11.667	94.96	17.667	1.42	23.67	.77
5.700	1.34	11.700	195.31	17.700	1.40	23.70	.76
5.733	1.34	11.733	195.31	17.733	1.40	23.73	.76
5.767	1.35	11.767	145.66	17.767	1.39	23.77	.76
5.800	1.36	11.800	96.28	17.800	1.38	23.80	.76
5.833	1.36	11.833	96.22	17.833	1.38	23.83	.76
5.867	1.38	11.867	51.86	17.867	1.37	23.87	.75
5.900	1.38	11.900	51.86	17.900	1.37	23.90	.75
5.933	1.39	11.933	43.06	17.933	1.36	23.93	.75
5.967	1.39	11.967	34.32	17.967	1.35	23.97	.75
6.000	1.39	12.000	34.30	18.000	1.35	24.00	.75

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .161 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 50.527
 TOTAL RAINFALL (mm)= 105.441
 RUNOFF COEFFICIENT = .479

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0024) Area (ha)= 5.03 Curve Number (CN)= 72.5
 ID= 1 DT= 2.0 min Ia (mm)= 4.75 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= 1.073 (i)
 TIME TO PEAK (hrs)= 11.800
 RUNOFF VOLUME (mm)= 39.018
 TOTAL RAINFALL (mm)= 105.441
 RUNOFF COEFFICIENT = .370

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0022) Area (ha)= 3.01 Curve Number (CN)= 71.6
 ID= 1 DT= 2.0 min Ia (mm)= 5.22 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .700 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 37.512
 TOTAL RAINFALL (mm)= 105.441
 RUNOFF COEFFICIENT = .356

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR (0023) |
| IN= 2---> OUT= 1 |
| DT= 2.0 min      |
-----

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OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.2156
.0001	.1117	20.0000	.2166

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0022)	3.01	.70	11.77	37.51
OUTFLOW: ID= 1 (0023)	3.01	.00	13.60	.02

```

PEAK FLOW REDUCTION [Qout/Qin](%)= .01
TIME SHIFT OF PEAK FLOW (min)=110.00
MAXIMUM STORAGE USED (ha.m.)= .1128

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-----
| ADD HYD (0026) |
| 1 + 2 = 3      |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0024):	5.03	1.073	11.80	39.02
+ ID2= 2 (0023):	3.01	.000	13.60	.02
=====				
ID = 3 (0026):	8.04	1.073	11.80	24.43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0025) |
| IN= 2---> OUT= 1 |
| DT= 2.0 min      |
-----

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0003	.2171
.0001	.0498	20.0000	.2181
.0002	.1676	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0026)	8.04	1.07	11.80	24.43
OUTFLOW: ID= 1 (0025)	8.04	.00	13.70	.21

```

PEAK FLOW REDUCTION [Qout/Qin](%)= .02
TIME SHIFT OF PEAK FLOW (min)=114.00
MAXIMUM STORAGE USED (ha.m.)= .1962

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-----
| ADD HYD (0028) |
| 1 + 2 = 3      |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0027):	.68	.161	11.77	50.53
+ ID2= 2 (0025):	8.04	.000	13.70	.21
=====				
ID = 3 (0028):	8.72	.161	11.77	4.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0029) |
| IN= 2---> OUT= 1 |
| DT= 2.0 min      |
-----

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0898
.0001	.0455	20.0000	.0908

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0028)	8.72	.16	11.77	4.12
OUTFLOW: ID= 1 (0029)	8.72	.00	29.77	.05

```

PEAK FLOW REDUCTION [Qout/Qin](%)= .05
TIME SHIFT OF PEAK FLOW (min)=*****
MAXIMUM STORAGE USED (ha.m.)= .0355

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| CALIB |
| NASHYD (0032) |
| ID= 1 DT= 5.0 min |
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Area (ha)=	6.71	Curve Number (CN)=	64.3
Ia (mm)=	8.68	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	.32		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.75	6.083	1.41	12.083	25.27	18.08	1.34
.167	.75	6.167	1.43	12.167	19.86	18.17	1.32
.250	.76	6.250	1.45	12.250	16.30	18.25	1.30
.333	.76	6.333	1.47	12.333	13.80	18.33	1.29
.417	.77	6.417	1.49	12.417	11.96	18.42	1.28
.500	.77	6.500	1.51	12.500	10.55	18.50	1.26
.583	.78	6.583	1.54	12.583	9.43	18.58	1.25
.667	.78	6.667	1.56	12.667	8.53	18.67	1.23
.750	.79	6.750	1.58	12.750	7.79	18.75	1.22
.833	.79	6.833	1.61	12.833	7.18	18.83	1.21
.917	.80	6.917	1.63	12.917	6.65	18.92	1.20
1.000	.80	7.000	1.66	13.000	6.20	19.00	1.18
1.083	.81	7.083	1.68	13.083	5.80	19.08	1.17
1.167	.82	7.167	1.71	13.167	5.46	19.17	1.16
1.250	.82	7.250	1.74	13.250	5.16	19.25	1.15
1.333	.83	7.333	1.77	13.333	4.89	19.33	1.14
1.417	.83	7.417	1.80	13.417	4.64	19.42	1.13
1.500	.84	7.500	1.83	13.500	4.43	19.50	1.12
1.583	.84	7.583	1.86	13.583	4.23	19.58	1.11
1.667	.85	7.667	1.90	13.667	4.05	19.67	1.10
1.750	.86	7.750	1.94	13.750	3.88	19.75	1.09
1.833	.86	7.833	1.97	13.833	3.73	19.83	1.08
1.917	.87	7.917	2.01	13.917	3.59	19.92	1.07
2.000	.88	8.000	2.05	14.000	3.47	20.00	1.06
2.083	.88	8.083	2.10	14.083	3.35	20.08	1.05
2.167	.89	8.167	2.14	14.167	3.24	20.17	1.04
2.250	.90	8.250	2.19	14.250	3.13	20.25	1.03
2.333	.90	8.333	2.24	14.333	3.04	20.33	1.02
2.417	.91	8.417	2.29	14.417	2.95	20.42	1.01
2.500	.92	8.500	2.34	14.500	2.86	20.50	1.00
2.583	.92	8.583	2.40	14.583	2.78	20.58	1.00
2.667	.93	8.667	2.46	14.667	2.71	20.67	.99
2.750	.94	8.750	2.52	14.750	2.64	20.75	.98
2.833	.95	8.833	2.59	14.833	2.57	20.83	.97
2.917	.95	8.917	2.66	14.917	2.51	20.92	.96
3.000	.96	9.000	2.74	15.000	2.45	21.00	.96
3.083	.97	9.083	2.82	15.083	2.39	21.08	.95
3.167	.98	9.167	2.90	15.167	2.34	21.17	.94
3.250	.99	9.250	3.00	15.250	2.29	21.25	.93
3.333	1.00	9.333	3.09	15.333	2.24	21.33	.93
3.417	1.00	9.417	3.20	15.417	2.19	21.42	.92
3.500	1.01	9.500	3.31	15.500	2.14	21.50	.91
3.583	1.02	9.583	3.43	15.583	2.10	21.58	.91
3.667	1.03	9.667	3.57	15.667	2.06	21.67	.90
3.750	1.04	9.750	3.71	15.750	2.02	21.75	.89
3.833	1.05	9.833	3.87	15.833	1.98	21.83	.89
3.917	1.06	9.917	4.04	15.917	1.95	21.92	.88
4.000	1.07	10.000	4.23	16.000	1.91	22.00	.87
4.083	1.08	10.083	4.43	16.083	1.88	22.08	.87
4.167	1.09	10.167	4.66	16.167	1.85	22.17	.86
4.250	1.10	10.250	4.92	16.250	1.82	22.25	.86
4.333	1.11	10.333	5.21	16.333	1.79	22.33	.85
4.417	1.12	10.417	5.54	16.417	1.76	22.42	.84
4.500	1.14	10.500	5.91	16.500	1.73	22.50	.84
4.583	1.15	10.583	6.34	16.583	1.70	22.58	.83
4.667	1.16	10.667	6.84	16.667	1.68	22.67	.83
4.750	1.17	10.750	7.43	16.750	1.65	22.75	.82
4.833	1.18	10.833	8.14	16.833	1.63	22.83	.82
4.917	1.20	10.917	8.99	16.917	1.60	22.92	.81
5.000	1.21	11.000	10.05	17.000	1.58	23.00	.81
5.083	1.22	11.083	11.40	17.083	1.56	23.08	.80
5.167	1.24	11.167	13.16	17.167	1.54	23.17	.80
5.250	1.25	11.250	15.55	17.250	1.51	23.25	.79
5.333	1.27	11.333	18.96	17.333	1.49	23.33	.79
5.417	1.28	11.417	24.16	17.417	1.47	23.42	.78
5.500	1.30	11.500	32.93	17.500	1.46	23.50	.78
5.583	1.31	11.583	50.12	17.583	1.44	23.58	.77
5.667	1.33	11.667	94.83	17.667	1.42	23.67	.77
5.750	1.34	11.750	195.29	17.750	1.40	23.75	.76
5.833	1.36	11.833	96.29	17.833	1.38	23.83	.76
5.917	1.38	11.917	51.86	17.917	1.37	23.92	.75
6.000	1.39	12.000	34.32	18.000	1.35	24.00	.00

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .538 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 39.323
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .373

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB          |
| NASHYD (0030) |
| ID= 1 DT= 5.0 min |
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```

Area (ha)= 5.57 Curve Number (CN)= 69.8
Ia (mm)= 6.12 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .06

```

Unit Hyd Qpeak (cms)= 3.828

```

PEAK FLOW (cms)= 1.096 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 38.704
TOTAL RAINFALL (mm)= 105.380
RUNOFF COEFFICIENT = .367

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ROUTE CHN (0031) |
| IN= 2----> OUT= 1 |
-----

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Routing time step (min)'= 5.00

```

<----- DATA FOR SECTION ( 1.2) ----->
Distance Elevation Manning
.00 386.25 .0300
37.50 385.75 .0300 / .0300 Main Channel
47.50 385.75 .0300 / .0300 Main Channel
85.00 386.25 .0300

```

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	385.78	.150E+03	.1	.33	23.91
.05	385.80	.350E+03	.3	.47	16.85
.08	385.83	.599E+03	.7	.56	14.12
.11	385.86	.898E+03	1.2	.63	12.62
.13	385.88	.125E+04	1.8	.68	11.65
.16	385.91	.164E+04	2.5	.73	10.95
.18	385.93	.209E+04	3.3	.76	10.42
.21	385.96	.259E+04	4.3	.80	9.99
.24	385.99	.313E+04	5.4	.82	9.64
.26	386.01	.373E+04	6.7	.85	9.33
.29	386.04	.438E+04	8.0	.88	9.07
.32	386.07	.507E+04	9.6	.90	8.83
.34	386.09	.582E+04	11.2	.92	8.62
.37	386.12	.661E+04	13.1	.94	8.43
.39	386.14	.745E+04	15.1	.96	8.25
.42	386.17	.835E+04	17.2	.98	8.08
.45	386.20	.929E+04	19.5	1.00	7.93
.47	386.22	.103E+05	22.0	1.02	7.79
.50	386.25	.113E+05	24.7	1.04	7.65

```

<---- hydrograph ----> <-pipe / channel-->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0030) 5.57 1.10 11.75 38.70 .10 .62
OUTFLOW: ID= 1 (0031) 5.57 .56 11.92 38.68 .07 .52

```

```

-----
| ADD HYD (0033) |
| 1 + 2 = 3 |
-----

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```

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
ID1= 1 (0032): 6.71 .538 12.08 39.32
+ ID2= 2 (0031): 5.57 .560 11.92 38.68
=====
ID = 3 (0033): 12.27 1.019 11.92 39.03

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB          |
| NASHYD (0036) |
| ID= 1 DT= 5.0 min |
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```

Area (ha)= 2.08 Curve Number (CN)= 67.6
Ia (mm)= 7.71 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .08

```

Unit Hyd Qpeak (cms)= .938

```

PEAK FLOW (cms)= .347 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 41.483
TOTAL RAINFALL (mm)= 105.380
RUNOFF COEFFICIENT = .394

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB          |
| NASHYD (0034) | Area (ha)= 2.15 Curve Number (CN)= 71.9
| ID= 1 DT= 5.0 min | Ia (mm)= 5.03 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= .10

```

Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .400 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 49.325
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .468

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ROUTE CHN (0035) |
| IN= 2----> OUT= 1 | Routing time step (min)'= 5.00
|-----|

```

```

<----- DATA FOR SECTION ( 1.3) ----->
Distance Elevation Manning
.00 388.25 .0300
30.00 387.75 .0300 / .0300 Main Channel
40.00 387.75 .0300 / .0300 Main Channel
70.00 388.25 .0300

```

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	387.78	.327E+02	.1	.41	4.35
.05	387.80	.744E+02	.4	.59	3.03
.08	387.83	.125E+03	.8	.71	2.52
.11	387.86	.185E+03	1.4	.80	2.25
.13	387.88	.253E+03	2.0	.87	2.07
.16	387.91	.330E+03	2.8	.92	1.95
.18	387.93	.417E+03	3.7	.97	1.85
.21	387.96	.512E+03	4.8	1.01	1.78
.24	387.99	.616E+03	6.0	1.04	1.72
.26	388.01	.729E+03	7.3	1.07	1.67
.29	388.04	.851E+03	8.7	1.10	1.63
.32	388.07	.982E+03	10.3	1.13	1.59
.34	388.09	.112E+04	12.0	1.15	1.56
.37	388.12	.127E+04	13.9	1.17	1.53
.39	388.14	.143E+04	15.9	1.19	1.50
.42	388.17	.160E+04	18.0	1.21	1.48
.45	388.20	.177E+04	20.3	1.23	1.45
.47	388.22	.196E+04	22.8	1.25	1.43
.50	388.25	.215E+04	25.4	1.27	1.41

```

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0034) 2.15 .40 11.83 49.32 .05 .58
OUTFLOW: ID= 1 (0035) 2.15 .39 11.83 49.32 .05 .57

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-----
| ADD HYD (0037) |
| 1 + 2 = 3 |
|-----|
| ID1= 1 (0036): | AREA QPEAK TPEAK R.V.
| + ID2= 2 (0035): | (ha) (cms) (hrs) (mm)
| ID = 3 (0037): | 4.23 .721 11.83 45.47

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB          |
| NASHYD (0039) | Area (ha)= 35.03 Curve Number (CN)= 65.5
| ID= 1 DT= 5.0 min | Ia (mm)= 7.17 # of Linear Res.(N)= 3.00
|-----|
| U.H. Tp(hrs)= 1.16

```

Unit Hyd Qpeak (cms)= 1.152

PEAK FLOW (cms)= 1.182 (i)
 TIME TO PEAK (hrs)= 13.083
 RUNOFF VOLUME (mm)= 41.553
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .394

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
NASHYD (0040)
ID= 1 DT= 5.0 min

Area (ha)= 3.95 Curve Number (CN)= 54.0
Ia (mm)= 10.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .40

Unit Hyd Qpeak (cms)= .375

PEAK FLOW (cms)= .198 (i)
TIME TO PEAK (hrs)= 12.167
RUNOFF VOLUME (mm)= 29.178
TOTAL RAINFALL (mm)= 105.380
RUNOFF COEFFICIENT = .277

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0041)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.1655
.0001	.0976	20.0000	.1665

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.20	12.17	29.18
OUTFLOW: ID= 1 (0041)	3.95	.00	25.25	.13

PEAK FLOW REDUCTION [Qout/Qin](%)= .06
TIME SHIFT OF PEAK FLOW (min)=785.00
MAXIMUM STORAGE USED (ha.m.)= .1148

CALIB
NASHYD (0044)
ID= 1 DT= 3.0 min

Area (ha)= .87 Curve Number (CN)= 64.6
Ia (mm)= 6.68 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.050	.75	6.050	1.41	12.050	25.27	18.05	1.34
.100	.75	6.100	1.42	12.100	23.46	18.10	1.33
.150	.75	6.150	1.43	12.150	19.86	18.15	1.32
.200	.76	6.200	1.44	12.200	17.49	18.20	1.31
.250	.76	6.250	1.45	12.250	16.30	18.25	1.30
.300	.76	6.300	1.47	12.300	13.80	18.30	1.29
.350	.77	6.350	1.48	12.350	13.19	18.35	1.29
.400	.77	6.400	1.49	12.400	11.96	18.40	1.28
.450	.77	6.450	1.51	12.450	11.02	18.45	1.27
.500	.77	6.500	1.51	12.500	10.55	18.50	1.26
.550	.78	6.550	1.54	12.550	9.43	18.55	1.25
.600	.78	6.600	1.54	12.600	9.13	18.60	1.24
.650	.78	6.650	1.56	12.650	8.53	18.65	1.23
.700	.79	6.700	1.57	12.700	8.04	18.70	1.23
.750	.79	6.750	1.58	12.750	7.79	18.75	1.22
.800	.79	6.800	1.61	12.800	7.18	18.80	1.21
.850	.79	6.850	1.61	12.850	7.00	18.85	1.21
.900	.80	6.900	1.63	12.900	6.65	18.90	1.20
.950	.80	6.950	1.65	12.950	6.35	18.95	1.19
1.000	.80	7.000	1.66	13.000	6.20	19.00	1.18
1.050	.81	7.050	1.68	13.050	5.80	19.05	1.17
1.100	.81	7.100	1.69	13.100	5.69	19.10	1.17
1.150	.82	7.150	1.71	13.150	5.46	19.15	1.16
1.200	.82	7.200	1.73	13.200	5.26	19.20	1.15
1.250	.82	7.250	1.74	13.250	5.16	19.25	1.15
1.300	.83	7.300	1.77	13.300	4.89	19.30	1.14
1.350	.83	7.350	1.78	13.350	4.80	19.35	1.13
1.400	.83	7.400	1.80	13.400	4.64	19.40	1.13
1.450	.84	7.450	1.82	13.450	4.50	19.45	1.12
1.500	.84	7.500	1.83	13.500	4.43	19.50	1.12
1.550	.84	7.550	1.86	13.550	4.23	19.55	1.11
1.600	.85	7.600	1.88	13.600	4.17	19.60	1.10
1.650	.85	7.650	1.90	13.650	4.05	19.65	1.10
1.700	.85	7.700	1.92	13.700	3.94	19.70	1.09
1.750	.86	7.750	1.94	13.750	3.88	19.75	1.09
1.800	.86	7.800	1.97	13.800	3.73	19.80	1.08
1.850	.87	7.850	1.99	13.850	3.69	19.85	1.07
1.900	.87	7.900	2.01	13.900	3.59	19.90	1.07
1.950	.87	7.950	2.04	13.950	3.51	19.95	1.06
2.000	.88	8.000	2.05	14.000	3.47	20.00	1.06
2.050	.88	8.050	2.10	14.050	3.35	20.05	1.05
2.100	.88	8.100	2.11	14.100	3.31	20.10	1.04

2.150	.89	8.150	2.14	14.150	3.24	20.15	1.04
2.200	.89	8.200	2.17	14.200	3.17	20.20	1.03
2.250	.90	8.250	2.19	14.250	3.13	20.25	1.03
2.300	.90	8.300	2.24	14.300	3.04	20.30	1.02
2.350	.91	8.350	2.25	14.350	3.01	20.35	1.02
2.400	.91	8.400	2.29	14.400	2.95	20.40	1.01
2.450	.91	8.450	2.32	14.450	2.89	20.45	1.01
2.500	.92	8.500	2.34	14.500	2.86	20.50	1.00
2.550	.92	8.550	2.40	14.550	2.78	20.55	1.00
2.600	.93	8.600	2.42	14.600	2.76	20.60	.99
2.650	.93	8.650	2.46	14.650	2.71	20.65	.99
2.700	.94	8.700	2.50	14.700	2.66	20.70	.98
2.750	.94	8.750	2.52	14.750	2.64	20.75	.98
2.800	.95	8.800	2.59	14.800	2.57	20.80	.97
2.850	.95	8.850	2.62	14.850	2.55	20.85	.97
2.900	.95	8.900	2.66	14.900	2.51	20.90	.96
2.950	.96	8.950	2.71	14.950	2.47	20.95	.96
3.000	.96	9.000	2.74	15.000	2.45	21.00	.96
3.050	.97	9.050	2.82	15.050	2.39	21.05	.95
3.100	.97	9.100	2.85	15.100	2.37	21.10	.95
3.150	.98	9.150	2.90	15.150	2.34	21.15	.94
3.200	.98	9.200	2.97	15.200	2.30	21.20	.94
3.250	.99	9.250	3.00	15.250	2.29	21.25	.93
3.300	1.00	9.300	3.09	15.300	2.24	21.30	.93
3.350	1.00	9.350	3.13	15.350	2.22	21.35	.92
3.400	1.00	9.400	3.20	15.400	2.19	21.40	.92
3.450	1.01	9.450	3.27	15.450	2.16	21.45	.92
3.500	1.01	9.500	3.31	15.500	2.14	21.50	.91
3.550	1.02	9.550	3.43	15.550	2.10	21.55	.91
3.600	1.03	9.600	3.48	15.600	2.09	21.60	.90
3.650	1.03	9.650	3.57	15.650	2.06	21.65	.90
3.700	1.04	9.700	3.66	15.700	2.03	21.70	.90
3.750	1.04	9.750	3.71	15.750	2.02	21.75	.89
3.800	1.05	9.800	3.87	15.800	1.98	21.80	.89
3.850	1.05	9.850	3.92	15.850	1.97	21.85	.88
3.900	1.06	9.900	4.04	15.900	1.95	21.90	.88
3.950	1.07	9.950	4.16	15.950	1.92	21.95	.88
4.000	1.07	10.000	4.23	16.000	1.91	22.00	.87
4.050	1.08	10.050	4.43	16.050	1.88	22.05	.87
4.100	1.08	10.100	4.51	16.100	1.87	22.10	.87
4.150	1.09	10.150	4.66	16.150	1.85	22.15	.86
4.200	1.10	10.200	4.84	16.200	1.83	22.20	.86
4.250	1.10	10.250	4.92	16.250	1.82	22.25	.86
4.300	1.11	10.300	5.21	16.300	1.79	22.30	.85
4.350	1.12	10.350	5.32	16.350	1.78	22.35	.85
4.400	1.12	10.400	5.54	16.400	1.76	22.40	.84
4.450	1.13	10.450	5.79	16.450	1.74	22.45	.84
4.500	1.14	10.500	5.91	16.500	1.73	22.50	.84
4.550	1.15	10.550	6.34	16.550	1.70	22.55	.83
4.600	1.15	10.600	6.51	16.600	1.69	22.60	.83
4.650	1.16	10.650	6.84	16.650	1.68	22.65	.83
4.700	1.17	10.700	7.24	16.700	1.66	22.70	.82
4.750	1.17	10.750	7.43	16.750	1.65	22.75	.82
4.800	1.18	10.800	8.14	16.800	1.63	22.80	.82
4.850	1.19	10.850	8.42	16.850	1.62	22.85	.82
4.900	1.20	10.900	8.99	16.900	1.60	22.90	.81
4.950	1.21	10.950	9.70	16.950	1.59	22.95	.81
5.000	1.21	11.000	10.05	17.000	1.58	23.00	.81
5.050	1.22	11.050	11.40	17.050	1.56	23.05	.80
5.100	1.23	11.100	11.98	17.100	1.55	23.10	.80
5.150	1.24	11.150	13.16	17.150	1.54	23.15	.80
5.200	1.25	11.200	14.75	17.200	1.52	23.20	.79
5.250	1.25	11.250	15.55	17.250	1.51	23.25	.79
5.300	1.27	11.300	18.96	17.300	1.49	23.30	.79
5.350	1.27	11.350	20.69	17.350	1.49	23.35	.78
5.400	1.28	11.400	24.16	17.400	1.47	23.40	.78
5.450	1.29	11.450	30.01	17.450	1.46	23.45	.78
5.500	1.30	11.500	32.93	17.500	1.46	23.50	.78
5.550	1.31	11.550	50.12	17.550	1.44	23.55	.77
5.600	1.32	11.600	65.05	17.600	1.43	23.60	.77
5.650	1.33	11.650	94.83	17.650	1.42	23.65	.77
5.700	1.34	11.700	161.87	17.700	1.41	23.70	.76
5.750	1.34	11.750	195.25	17.750	1.40	23.75	.76
5.800	1.36	11.800	96.28	17.800	1.38	23.80	.76
5.850	1.37	11.850	81.45	17.850	1.38	23.85	.76
5.900	1.38	11.900	51.86	17.900	1.37	23.90	.75
5.950	1.39	11.950	40.15	17.950	1.36	23.95	.75
6.000	1.39	12.000	34.31	18.000	1.35	24.00	.75

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .162 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 39.615
 TOTAL RAINFALL (mm)= 105.442
 RUNOFF COEFFICIENT = .376

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.


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-----
| CALIB |
| NASHYD (0042) | Area (ha)= .56 Curve Number (CN)= 70.0
| ID= 1 DT= 3.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .06

```

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .124 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 44.093
 TOTAL RAINFALL (mm)= 105.442
 RUNOFF COEFFICIENT = .418

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0043) |
| IN= 2----> OUT= 1 |
| DT= 3.0 min |
|-----|

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	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0002	.0357
	.0001	.0118	20.0000	.0367

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0042)	.56	.12	11.75	44.09
OUTFLOW: ID= 1 (0043)	.56	.00	20.10	.79

PEAK FLOW REDUCTION [Qout/Qin](%)= .12
 TIME SHIFT OF PEAK FLOW (min)=501.00
 MAXIMUM STORAGE USED (ha.m.)= .0241

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-----
| ADD HYD (0045) |
| 1 + 2 = 3 |
|-----|

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0044):	.87	.162	11.75	39.61
+ ID2= 2 (0043):	.56	.000	20.10	.79
=====				
ID = 3 (0045):	1.42	.162	11.75	24.45

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0046) |
| IN= 2----> OUT= 1 |
| DT= 3.0 min |
|-----|

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.0002	.1073
	.0001	.0117	20.0000	.1083

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0045)	1.42	.16	11.75	24.45
OUTFLOW: ID= 1 (0046)	1.42	.00	24.15	.38

PEAK FLOW REDUCTION [Qout/Qin](%)= .08
 TIME SHIFT OF PEAK FLOW (min)=744.00
 MAXIMUM STORAGE USED (ha.m.)= .0343

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-----
| CALIB |
| NASHYD (0047) | Area (ha)= .48 Curve Number (CN)= 70.0
| ID= 1 DT= 3.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .06

```

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .107 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 44.093
 TOTAL RAINFALL (mm)= 105.442
 RUNOFF COEFFICIENT = .418

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR (0048) |
| IN= 2----> OUT= 1 |
| DT= 3.0 min |
|-----|

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)

.0000 .0000 | .0002 .0731
 .0001 .0496 | 20.0000 .0741

INFLOW : ID= 2 (0047) AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)
 .48 .11 11.75 44.09
 OUTFLOW: ID= 1 (0048) .48 .00 20.15 .24

PEAK FLOW REDUCTION [Qout/Qin] (%) = .04
 TIME SHIFT OF PEAK FLOW (min) = 504.00
 MAXIMUM STORAGE USED (ha.m.) = .0211

 CALIB (0049) Area (ha) = 2.77 Curve Number (CN) = 70.7
 NASHYD (0049) Ia (mm) = 5.35 # of Linear Res. (N) = 3.00
 ID= 1 DT= 5.0 min U.H. Tp(hrs) = .11

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	.75	6.083	1.41	12.083	25.27	18.08	1.34
.167	.75	6.167	1.43	12.167	19.86	18.17	1.32
.250	.76	6.250	1.45	12.250	16.30	18.25	1.30
.333	.76	6.333	1.47	12.333	13.80	18.33	1.29
.417	.77	6.417	1.49	12.417	11.96	18.42	1.28
.500	.77	6.500	1.51	12.500	10.55	18.50	1.26
.583	.78	6.583	1.54	12.583	9.43	18.58	1.25
.667	.78	6.667	1.56	12.667	8.53	18.67	1.23
.750	.79	6.750	1.58	12.750	7.79	18.75	1.22
.833	.79	6.833	1.61	12.833	7.18	18.83	1.21
.917	.80	6.917	1.63	12.917	6.65	18.92	1.20
1.000	.80	7.000	1.66	13.000	6.20	19.00	1.18
1.083	.81	7.083	1.68	13.083	5.80	19.08	1.17
1.167	.82	7.167	1.71	13.167	5.46	19.17	1.16
1.250	.82	7.250	1.74	13.250	5.16	19.25	1.15
1.333	.83	7.333	1.77	13.333	4.89	19.33	1.14
1.417	.83	7.417	1.80	13.417	4.64	19.42	1.13
1.500	.84	7.500	1.83	13.500	4.43	19.50	1.12
1.583	.84	7.583	1.86	13.583	4.23	19.58	1.11
1.667	.85	7.667	1.90	13.667	4.05	19.67	1.10
1.750	.86	7.750	1.94	13.750	3.88	19.75	1.09
1.833	.86	7.833	1.97	13.833	3.73	19.83	1.08
1.917	.87	7.917	2.01	13.917	3.59	19.92	1.07
2.000	.88	8.000	2.05	14.000	3.47	20.00	1.06
2.083	.88	8.083	2.10	14.083	3.35	20.08	1.05
2.167	.89	8.167	2.14	14.167	3.24	20.17	1.04
2.250	.90	8.250	2.19	14.250	3.13	20.25	1.03
2.333	.90	8.333	2.24	14.333	3.04	20.33	1.02
2.417	.91	8.417	2.29	14.417	2.95	20.42	1.01
2.500	.92	8.500	2.34	14.500	2.86	20.50	1.00
2.583	.92	8.583	2.40	14.583	2.78	20.58	1.00
2.667	.93	8.667	2.46	14.667	2.71	20.67	.99
2.750	.94	8.750	2.52	14.750	2.64	20.75	.98
2.833	.95	8.833	2.59	14.833	2.57	20.83	.97
2.917	.95	8.917	2.66	14.917	2.51	20.92	.96
3.000	.96	9.000	2.74	15.000	2.45	21.00	.96
3.083	.97	9.083	2.82	15.083	2.39	21.08	.95
3.167	.98	9.167	2.90	15.167	2.34	21.17	.94
3.250	.99	9.250	3.00	15.250	2.29	21.25	.93
3.333	1.00	9.333	3.09	15.333	2.24	21.33	.93
3.417	1.00	9.417	3.20	15.417	2.19	21.42	.92
3.500	1.01	9.500	3.31	15.500	2.14	21.50	.91
3.583	1.02	9.583	3.43	15.583	2.10	21.58	.91
3.667	1.03	9.667	3.57	15.667	2.06	21.67	.90
3.750	1.04	9.750	3.71	15.750	2.02	21.75	.89
3.833	1.05	9.833	3.87	15.833	1.98	21.83	.89
3.917	1.06	9.917	4.04	15.917	1.95	21.92	.88
4.000	1.07	10.000	4.23	16.000	1.91	22.00	.87
4.083	1.08	10.083	4.43	16.083	1.88	22.08	.87
4.167	1.09	10.167	4.66	16.167	1.85	22.17	.86
4.250	1.10	10.250	4.92	16.250	1.82	22.25	.86
4.333	1.11	10.333	5.21	16.333	1.79	22.33	.85
4.417	1.12	10.417	5.54	16.417	1.76	22.42	.84
4.500	1.14	10.500	5.91	16.500	1.73	22.50	.84
4.583	1.15	10.583	6.34	16.583	1.70	22.58	.83
4.667	1.16	10.667	6.84	16.667	1.68	22.67	.83
4.750	1.17	10.750	7.43	16.750	1.65	22.75	.82
4.833	1.18	10.833	8.14	16.833	1.63	22.83	.82
4.917	1.20	10.917	8.99	16.917	1.60	22.92	.81
5.000	1.21	11.000	10.05	17.000	1.58	23.00	.81
5.083	1.22	11.083	11.40	17.083	1.56	23.08	.80
5.167	1.24	11.167	13.16	17.167	1.54	23.17	.80
5.250	1.25	11.250	15.55	17.250	1.51	23.25	.79
5.333	1.27	11.333	18.96	17.333	1.49	23.33	.79

5.417	1.28	11.417	24.16	17.417	1.47	23.42	.78
5.500	1.30	11.500	32.93	17.500	1.46	23.50	.78
5.583	1.31	11.583	50.12	17.583	1.44	23.58	.77
5.667	1.33	11.667	94.83	17.667	1.42	23.67	.77
5.750	1.34	11.750	195.29	17.750	1.40	23.75	.76
5.833	1.36	11.833	96.29	17.833	1.38	23.83	.76
5.917	1.38	11.917	51.86	17.917	1.37	23.92	.75
6.000	1.39	12.000	34.32	18.000	1.35	24.00	.00

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .490 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 47.911
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .455

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0055)	Area (ha)=	5.19	Curve Number (CN)=	73.3			
ID= 1 DT= 5.0 min	Ia (mm)=	4.00	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.11					

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= .998 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 52.081
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .494

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0052)	Area (ha)=	3.90	Curve Number (CN)=	69.4			
ID= 1 DT= 5.0 min	Ia (mm)=	4.85	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.08					

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .748 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 44.525
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .423

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB							
NASHYD (0050)	Area (ha)=	11.96	Curve Number (CN)=	66.4			
ID= 1 DT= 5.0 min	Ia (mm)=	5.74	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	.18					

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.496 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 43.427
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .412

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0051)							
IN= 2---> OUT= 1							
DT= 5.0 min							
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)			
	.0000	.0000	20.0000	.1583			
	.0001	.1573	.0000	.0000			
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)			
INFLOW : ID= 2 (0050)	11.96	1.50	11.92	43.43			
OUTFLOW: ID= 1 (0051)	11.96	2.44	12.00	30.27			

PEAK FLOW REDUCTION [Qout/Qin](%)=163.13
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .3292

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.

 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ADD HYD (0053)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0052):		3.90	.748	11.75	44.52
+ ID2= 2 (0051):		11.96	2.441	12.00	30.27
=====					
ID = 3 (0053):		15.86	2.722	12.00	33.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0054)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	20.0000	.0771
		.0001	.0761	.0000	.0000
=====					
INFLOW : ID= 2 (0053)	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
OUTFLOW: ID= 1 (0054)	15.86	2.72	12.00	33.78	
	15.86	2.89	12.00	28.98	
PEAK FLOW REDUCTION [Qout/Qin](%)=106.21					
TIME SHIFT OF PEAK FLOW (min)= .00					
MAXIMUM STORAGE USED (ha.m.)= .1044					

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ROUTE CHN (0056)		Routing time step (min)'= 5.00			
IN= 2---> OUT= 1					
----- DATA FOR SECTION (1.5) ----->					
Distance	Elevation	Manning			
.00	425.00	.0300			
.75	424.25	.0300 / .0300	Main Channel		
1.75	424.25	.0300 / .0300	Main Channel		
2.50	425.00	.0300			
----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88
----- hydrograph ----->					
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH
	(ha)	(cms)	(hrs)	(mm)	(m)
INFLOW : ID= 2 (0054)	15.86	2.89	12.00	28.98	.61
OUTFLOW: ID= 1 (0056)	15.86	1.42	12.08	28.98	.40
					MAX VEL
					(m/s)
					2.93
					2.49

ADD HYD (0057)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0055):		5.19	.998	11.83	52.08
+ ID2= 2 (0056):		15.86	1.422	12.08	28.98
=====					
ID = 3 (0057):		21.05	1.875	12.00	34.68

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD (0058) | Area (ha)= 21.77 Curve Number (CN)= 67.4
| ID= 1 DT= 5.0 min | Ia (mm)= 5.22 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .35

```

Unit Hyd Qpeak (cms)= 2.354

PEAK FLOW (cms)= 1.885 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 45.031
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD (0059) | Area (ha)= 11.96 Curve Number (CN)= 66.4
| ID= 1 DT= 5.0 min | Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .18

```

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.496 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 43.427
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .412

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR (0060) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.1583
	.0001	.1573	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0059)	11.96	1.50	11.92	43.43
OUTFLOW: ID= 1 (0060)	11.96	2.44	12.00	30.27

PEAK FLOW REDUCTION [Qout/Qin](%)=163.13
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .3292

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

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-----
| CALIB |
| NASHYD (0061) | Area (ha)= 3.90 Curve Number (CN)= 69.4
| ID= 1 DT= 5.0 min | Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .08

```

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .748 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 44.525
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .423

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD (0062) |
| 1 + 2 = 3 |

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0060):	11.96	2.441	12.00	30.27
+ ID2= 2 (0061):	3.90	.748	11.75	44.52
=====	=====	=====	=====	=====
ID = 3 (0062):	15.86	2.722	12.00	33.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0063) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |

```

	OUTFLOW	STORAGE	OUTFLOW	STORAGE


```

-----
                (cms)      (ha.m.) |      (cms)      (ha.m.)
                .0000      .0000 |      20.0000     .0771
                .0001      .0761 |      .0000       .0000

```

```

                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0062)  15.86      2.72      12.00     33.78
OUTFLOW: ID= 1 (0063)  15.86      2.89      12.00     28.98

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)=106.21
TIME SHIFT OF PEAK FLOW (min)= .00
MAXIMUM STORAGE USED (ha.m.)= .1044

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**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.
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| ROUTE CHN (0065) |
| IN= 2---> OUT= 1 |
-----

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Routing time step (min)'= 5.00

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<----- DATA FOR SECTION ( 1.5) ----->
Distance      Elevation      Manning
.00            425.00          .0300
.75            424.25          .0300 / .0300  Main Channel
1.75          424.25          .0300 / .0300  Main Channel
2.50          425.00          .0300

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)        (m)        (cu.m.)      (cms)          (m/s)         (min)
.04        424.29    .145E+02     .0              .68            8.63
.08        424.33    .302E+02     .1              1.05           5.61
.12        424.37    .469E+02     .2              1.33           4.42
.16        424.41    .647E+02     .3              1.57           3.76
.20        424.45    .837E+02     .4              1.77           3.34
.24        424.49    .104E+03     .6              1.94           3.04
.28        424.53    .125E+03     .7              2.10           2.81
.32        424.57    .147E+03     .9              2.23           2.64
.36        424.61    .170E+03     1.1             2.36           2.50
.39        424.64    .195E+03     1.4             2.47           2.39
.43        424.68    .220E+03     1.6             2.57           2.30
.47        424.72    .247E+03     1.9             2.66           2.22
.51        424.76    .275E+03     2.1             2.75           2.15
.55        424.80    .304E+03     2.4             2.83           2.09
.59        424.84    .334E+03     2.7             2.90           2.04
.63        424.88    .365E+03     3.1             2.97           1.99
.67        424.92    .397E+03     3.4             3.03           1.95
.71        424.96    .430E+03     3.8             3.09           1.91
.75        425.00    .465E+03     4.1             3.14           1.88

```

```

<---- hydrograph ----> <-pipe / channel->
                AREA      QPEAK      TPEAK      R.V.      MAX DEPTH      MAX VEL
                (ha)      (cms)      (hrs)      (mm)      (m)            (m/s)
INFLOW : ID= 2 (0063)  15.86      2.89      12.00     28.98      .61            2.93
OUTFLOW: ID= 1 (0065)  15.86      1.42      12.08     28.98      .40            2.49

```

```

| CALIB      (0064) |
| NASHYD     (0064) |
| ID= 1 DT= 5.0 min |
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Area (ha)= 5.19      Curve Number (CN)= 73.3
Ia (mm)= 4.00       # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

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Unit Hyd Qpeak (cms)= 1.777

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```

PEAK FLOW (cms)= .998 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 52.081
TOTAL RAINFALL (mm)= 105.380
RUNOFF COEFFICIENT = .494

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(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
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| ADD HYD (0066) |
| 1 + 2 = 3 |
-----

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                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0065):  15.86      1.422     12.08     28.98
+ ID2= 2 (0064):  5.19       .998      11.83     52.08
=====
ID = 3 (0066):  21.05      1.875     12.00     34.68

```

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
-----

```

CALIB
 NASHYD (0069) Area (ha)= 1.80 Curve Number (CN)= 58.8
 ID= 1 DT= 5.0 min Ia (mm)= 8.49 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .07

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .249 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 30.951
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .294

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 NASHYD (0067) Area (ha)= 1.52 Curve Number (CN)= 62.0
 ID= 1 DT= 5.0 min Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .235 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 31.712
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0068)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.0207
.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.24	11.75	31.71
OUTFLOW: ID= 1 (0068)	1.52	.10	12.00	18.20

PEAK FLOW REDUCTION [Qout/Qin](%)= 42.20
 TIME SHIFT OF PEAK FLOW (min)= 15.00
 MAXIMUM STORAGE USED (ha.m.)= .0319

ADD HYD (0071)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0069):	1.80	.249	11.75	30.95
+ ID2= 2 (0068):	1.52	.099	12.00	18.20
=====				
ID = 3 (0071):	3.32	.249	11.75	25.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0070)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	20.0000	.0708
.0001	.0707	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0071)	3.32	.25	11.75	25.11
OUTFLOW: ID= 1 (0070)	3.32	.01	17.17	3.82

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.32
 TIME SHIFT OF PEAK FLOW (min)=325.00
 MAXIMUM STORAGE USED (ha.m.)= .0711

ROUTE CHN (0073)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.6) ----->
 Distance Elevation Manning
 .00 421.26 .0300

1.10 420.66 .0300 / .0300 Main Channel
 2.00 420.66 .0300 / .0300 Main Channel
 3.10 421.26 .0300

----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

<---- hydrograph ----> <-pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	3.32	.01	17.17	3.82	.09	.11
OUTFLOW: ID= 1 (0073)	3.32	.01	19.00	3.67	.06	.08

ADD HYD (0074)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
ID1= 1 (0066):		21.05	1.875	12.00	34.68
+ ID2= 2 (0073):		3.32	.005	19.00	3.67
=====					
ID = 3 (0074):		24.37	1.875	12.00	30.45

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0072)		Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min		24.19	60.0
		Ia (mm)= 8.62	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= .37	

Unit Hyd Qpeak (cms)= 2.505

PEAK FLOW (cms)= 1.558 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 35.132
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .333

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
ID1= 1 (0074):		24.37	1.875	12.00	30.45
+ ID2= 2 (0072):		24.19	1.558	12.17	35.13
=====					
ID = 3 (0075):		48.56	3.366	12.08	32.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0076)		Area (ha)	Curve Number (CN)
ID= 1 DT= 5.0 min		127.28	59.9
		Ia (mm)= 8.29	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= .79	

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 4.855 (i)
 TIME TO PEAK (hrs)= 12.583
 RUNOFF VOLUME (mm)= 35.297

TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .335

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| CALIB
| NASHYD (0077) | Area (ha)= 17.28 Curve Number (CN)= 58.3
| ID= 1 DT= 5.0 min | Ia (mm)= 9.24 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .57
  
```

Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .779 (i)
 TIME TO PEAK (hrs)= 12.333
 RUNOFF VOLUME (mm)= 33.277
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .316

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB
| NASHYD (0082) | Area (ha)= .24 Curve Number (CN)= 77.6
| ID= 1 DT= 5.0 min | Ia (mm)= 3.49 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .11
  
```

Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .051 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 58.214
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .552

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB
| NASHYD (0078) | Area (ha)= 2.66 Curve Number (CN)= 59.8
| ID= 1 DT= 5.0 min | Ia (mm)= 8.55 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .07
  
```

Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .374 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 32.174
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .305

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR (0079) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
|-----|
      OUTFLOW STORAGE | OUTFLOW STORAGE
      (cms) (ha.m.) | (cms) (ha.m.)
      .0000 .0000 | 20.0000 .0608
      .0001 .0607 | .0000 .0000
      AREA QPEAK TPEAK R.V.
      (ha) (cms) (hrs) (mm)
INFLOW : ID= 2 (0078) 2.66 .37 11.75 32.17
OUTFLOW: ID= 1 (0079) 2.66 .03 13.25 9.35
      PEAK FLOW REDUCTION [Qout/Qin](%)= 7.74
      TIME SHIFT OF PEAK FLOW (min)= 90.00
      MAXIMUM STORAGE USED (ha.m.)= .0717
  
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-----
| ADD HYD (0083) |
| 1 + 2 = 3 |
|-----|
      AREA QPEAK TPEAK R.V.
      (ha) (cms) (hrs) (mm)
      ID1= 1 (0082): .24 .051 11.83 58.21
      + ID2= 2 (0079): 2.66 .029 13.25 9.35
      -----
      ID = 3 (0083): 2.90 .051 11.83 13.35
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
NASHYD (0080)	Area (ha)=	14.63	Curve Number (CN)=	58.0
ID= 1 DT= 5.0 min	Ia (mm)=	9.37	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.57		

Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .652 (i)
 TIME TO PEAK (hrs)= 12.417
 RUNOFF VOLUME (mm)= 32.962
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .313

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0081)				
1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0083):	2.90	.051	11.83	13.35
+ ID2= 2 (0080):	14.63	.652	12.42	32.96
ID = 3 (0081):	17.52	.661	12.33	29.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
NASHYD (0084)	Area (ha)=	7.71	Curve Number (CN)=	62.5
ID= 1 DT= 5.0 min	Ia (mm)=	9.14	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.29		

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .614 (i)
 TIME TO PEAK (hrs)= 12.000
 RUNOFF VOLUME (mm)= 37.186
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .353

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0085)	Area (ha)=	.91	Curve Number (CN)=	64.9
ID= 1 DT= 5.0 min	Ia (mm)=	8.53	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.11		

Unit Hyd Qpeak (cms)= .313

PEAK FLOW (cms)= .131 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 39.306
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .373

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0086)	Area (ha)=	19.15	Curve Number (CN)=	71.3
ID= 1 DT= 5.0 min	Ia (mm)=	5.81	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.24		

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= 2.288 (i)
 TIME TO PEAK (hrs)= 12.000
 RUNOFF VOLUME (mm)= 49.047
 TOTAL RAINFALL (mm)= 105.380
 RUNOFF COEFFICIENT = .465

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ** SIMULATION NUMBER: 6 **

CHICAGO STORM	IDF curve parameters: A=2147.367
Ptotal=114.71 mm	B= 10.512
	C= .839
	used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = .49

The CORRELATION coefficient is = .9991

TIME (min)	INPUT INT. (mm/hr)	TAB. INT. (mm/hr)
5.	220.00	215.25
10.	160.00	170.27
15.	140.00	141.79
30.	107.00	96.19
60.	61.00	60.42
120.	35.00	36.05
360.	14.00	15.02
720.	8.30	8.50
1440.	5.10	4.78

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	.80	6.08	1.52	12.08	27.59	18.08	1.43
.17	.81	6.17	1.54	12.17	21.65	18.17	1.41
.25	.81	6.25	1.56	12.25	17.75	18.25	1.40
.33	.82	6.33	1.58	12.33	15.01	18.33	1.38
.42	.82	6.42	1.60	12.42	12.99	18.42	1.37
.50	.83	6.50	1.62	12.50	11.45	18.50	1.35
.58	.83	6.58	1.65	12.58	10.23	18.58	1.34
.67	.84	6.67	1.67	12.67	9.25	18.67	1.32
.75	.84	6.75	1.70	12.75	8.44	18.75	1.31
.83	.85	6.83	1.72	12.83	7.77	18.83	1.30
.92	.85	6.92	1.75	12.92	7.19	18.92	1.28
1.00	.86	7.00	1.78	13.00	6.70	19.00	1.27
1.08	.87	7.08	1.81	13.08	6.27	19.08	1.26
1.17	.87	7.17	1.84	13.17	5.90	19.17	1.24
1.25	.88	7.25	1.87	13.25	5.57	19.25	1.23
1.33	.88	7.33	1.90	13.33	5.28	19.33	1.22
1.42	.89	7.42	1.93	13.42	5.01	19.42	1.21
1.50	.90	7.50	1.97	13.50	4.78	19.50	1.20
1.58	.90	7.58	2.00	13.58	4.56	19.58	1.18
1.67	.91	7.67	2.04	13.67	4.37	19.67	1.17
1.75	.92	7.75	2.08	13.75	4.19	19.75	1.16
1.83	.92	7.83	2.12	13.83	4.02	19.83	1.15
1.92	.93	7.92	2.16	13.92	3.87	19.92	1.14
2.00	.94	8.00	2.21	14.00	3.73	20.00	1.13
2.08	.94	8.08	2.25	14.08	3.61	20.08	1.12
2.17	.95	8.17	2.30	14.17	3.49	20.17	1.11
2.25	.96	8.25	2.35	14.25	3.37	20.25	1.10
2.33	.97	8.33	2.40	14.33	3.27	20.33	1.09
2.42	.97	8.42	2.46	14.42	3.17	20.42	1.08
2.50	.98	8.50	2.52	14.50	3.08	20.50	1.07
2.58	.99	8.58	2.58	14.58	3.00	20.58	1.07
2.67	1.00	8.67	2.65	14.67	2.91	20.67	1.06
2.75	1.01	8.75	2.71	14.75	2.84	20.75	1.05
2.83	1.01	8.83	2.79	14.83	2.77	20.83	1.04
2.92	1.02	8.92	2.86	14.92	2.70	20.92	1.03
3.00	1.03	9.00	2.95	15.00	2.63	21.00	1.02
3.08	1.04	9.08	3.03	15.08	2.57	21.08	1.02
3.17	1.05	9.17	3.13	15.17	2.51	21.17	1.01
3.25	1.06	9.25	3.23	15.25	2.46	21.25	1.00
3.33	1.07	9.33	3.33	15.33	2.40	21.33	.99
3.42	1.08	9.42	3.45	15.42	2.35	21.42	.98
3.50	1.09	9.50	3.57	15.50	2.30	21.50	.98
3.58	1.09	9.58	3.70	15.58	2.26	21.58	.97
3.67	1.10	9.67	3.84	15.67	2.21	21.67	.96
3.75	1.11	9.75	4.00	15.75	2.17	21.75	.96
3.83	1.13	9.83	4.17	15.83	2.13	21.83	.95
3.92	1.14	9.92	4.35	15.92	2.09	21.92	.94
4.00	1.15	10.00	4.56	16.00	2.05	22.00	.94
4.08	1.16	10.08	4.78	16.08	2.02	22.08	.93
4.17	1.17	10.17	5.03	16.17	1.98	22.17	.92
4.25	1.18	10.25	5.31	16.25	1.95	22.25	.92
4.33	1.19	10.33	5.63	16.33	1.92	22.33	.91
4.42	1.20	10.42	5.98	16.42	1.89	22.42	.90
4.50	1.22	10.50	6.39	16.50	1.86	22.50	.90
4.58	1.23	10.58	6.86	16.58	1.83	22.58	.89
4.67	1.24	10.67	7.40	16.67	1.80	22.67	.89
4.75	1.25	10.75	8.05	16.75	1.77	22.75	.88
4.83	1.27	10.83	8.82	16.83	1.74	22.83	.87
4.92	1.28	10.92	9.75	16.92	1.72	22.92	.87
5.00	1.30	11.00	10.91	17.00	1.69	23.00	.86
5.08	1.31	11.08	12.38	17.08	1.67	23.08	.86
5.17	1.33	11.17	14.30	17.17	1.65	23.17	.85
5.25	1.34	11.25	16.92	17.25	1.62	23.25	.85
5.33	1.36	11.33	20.66	17.33	1.60	23.33	.84
5.42	1.37	11.42	26.37	17.42	1.58	23.42	.84
5.50	1.39	11.50	36.00	17.50	1.56	23.50	.83
5.58	1.40	11.58	54.94	17.58	1.54	23.58	.83

5.67	1.42	11.67	104.25	17.67	1.52	23.67	.82
5.75	1.44	11.75	215.25	17.75	1.50	23.75	.82
5.83	1.46	11.83	105.85	17.83	1.48	23.83	.81
5.92	1.48	11.92	56.85	17.92	1.47	23.92	.81
6.00	1.50	12.00	37.53	18.00	1.45	24.00	.80

 CALIB
 NASHYD (0021) Area (ha)= 8.81 Curve Number (CN)= 68.3
 ID= 1 DT= 5.0 min Ia (mm)= 6.50 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.36

Unit Hyd Qpeak (cms)= .248

PEAK FLOW (cms)= .333 (i)
 TIME TO PEAK (hrs)= 13.250
 RUNOFF VOLUME (mm)= 51.764
 TOTAL RAINFALL (mm)= 114.710
 RUNOFF COEFFICIENT = .451

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0027) Area (ha)= .68 Curve Number (CN)= 72.2
 ID= 1 DT= 2.0 min Ia (mm)= 4.91 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 2.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.033	.80	6.033	1.52	12.033	27.59	18.03	1.43
.067	.80	6.067	1.52	12.067	27.59	18.07	1.43
.100	.80	6.100	1.53	12.100	24.61	18.10	1.42
.133	.81	6.133	1.54	12.133	21.65	18.13	1.41
.167	.81	6.167	1.54	12.167	21.64	18.17	1.41
.200	.81	6.200	1.56	12.200	17.75	18.20	1.40
.233	.81	6.233	1.56	12.233	17.75	18.23	1.40
.267	.81	6.267	1.57	12.267	16.37	18.27	1.39
.300	.82	6.300	1.58	12.300	15.01	18.30	1.38
.333	.82	6.333	1.58	12.333	15.00	18.33	1.38
.367	.82	6.367	1.60	12.367	12.99	18.37	1.37
.400	.82	6.400	1.60	12.400	12.99	18.40	1.37
.433	.82	6.433	1.61	12.433	12.22	18.43	1.36
.467	.83	6.467	1.62	12.467	11.45	18.47	1.35
.500	.83	6.500	1.62	12.500	11.45	18.50	1.35
.533	.83	6.533	1.65	12.533	10.23	18.53	1.34
.567	.83	6.567	1.65	12.567	10.23	18.57	1.34
.600	.84	6.600	1.66	12.600	9.74	18.60	1.33
.633	.84	6.633	1.67	12.633	9.25	18.63	1.32
.667	.84	6.667	1.67	12.667	9.25	18.67	1.32
.700	.84	6.700	1.70	12.700	8.44	18.70	1.31
.733	.84	6.733	1.70	12.733	8.44	18.73	1.31
.767	.85	6.767	1.71	12.767	8.10	18.77	1.30
.800	.85	6.800	1.72	12.800	7.77	18.80	1.30
.833	.85	6.833	1.72	12.833	7.77	18.83	1.30
.867	.85	6.867	1.75	12.867	7.19	18.87	1.28
.900	.85	6.900	1.75	12.900	7.19	18.90	1.28
.933	.86	6.933	1.76	12.933	6.95	18.93	1.28
.967	.86	6.967	1.78	12.967	6.70	18.97	1.27
1.000	.86	7.000	1.78	13.000	6.70	19.00	1.27
1.033	.87	7.033	1.81	13.033	6.27	19.03	1.26
1.067	.87	7.067	1.81	13.067	6.27	19.07	1.26
1.100	.87	7.100	1.82	13.100	6.09	19.10	1.25
1.133	.87	7.133	1.84	13.133	5.90	19.13	1.24
1.167	.87	7.167	1.84	13.167	5.90	19.17	1.24
1.200	.88	7.200	1.87	13.200	5.57	19.20	1.23
1.233	.88	7.233	1.87	13.233	5.57	19.23	1.23
1.267	.88	7.267	1.88	13.267	5.42	19.27	1.23
1.300	.88	7.300	1.90	13.300	5.28	19.30	1.22
1.333	.88	7.333	1.90	13.333	5.27	19.33	1.22
1.367	.89	7.367	1.93	13.367	5.01	19.37	1.21
1.400	.89	7.400	1.93	13.400	5.01	19.40	1.21
1.433	.89	7.433	1.95	13.433	4.89	19.43	1.20
1.467	.90	7.467	1.97	13.467	4.78	19.47	1.20
1.500	.90	7.500	1.97	13.500	4.77	19.50	1.20
1.533	.90	7.533	2.00	13.533	4.56	19.53	1.18
1.567	.90	7.567	2.00	13.567	4.56	19.57	1.18
1.600	.91	7.600	2.02	13.600	4.46	19.60	1.18
1.633	.91	7.633	2.04	13.633	4.37	19.63	1.17
1.667	.91	7.667	2.04	13.667	4.37	19.67	1.17
1.700	.92	7.700	2.08	13.700	4.19	19.70	1.16
1.733	.92	7.733	2.08	13.733	4.19	19.73	1.16

1.767	.92	7.767	2.10	13.767	4.11	19.77	1.16
1.800	.92	7.800	2.12	13.800	4.02	19.80	1.15
1.833	.92	7.833	2.12	13.833	4.02	19.83	1.15
1.867	.93	7.867	2.16	13.867	3.87	19.87	1.14
1.900	.93	7.900	2.16	13.900	3.87	19.90	1.14
1.933	.93	7.933	2.18	13.933	3.80	19.93	1.14
1.967	.94	7.967	2.21	13.967	3.73	19.97	1.13
2.000	.94	8.000	2.21	14.000	3.73	20.00	1.13
2.033	.94	8.033	2.25	14.033	3.61	20.03	1.12
2.067	.94	8.067	2.25	14.067	3.61	20.07	1.12
2.100	.95	8.100	2.28	14.100	3.55	20.10	1.12
2.133	.95	8.133	2.30	14.133	3.49	20.13	1.11
2.167	.95	8.167	2.30	14.167	3.49	20.17	1.11
2.200	.96	8.200	2.35	14.200	3.37	20.20	1.10
2.233	.96	8.233	2.35	14.233	3.37	20.23	1.10
2.267	.96	8.267	2.38	14.267	3.32	20.27	1.10
2.300	.97	8.300	2.40	14.300	3.27	20.30	1.09
2.333	.97	8.333	2.40	14.333	3.27	20.33	1.09
2.367	.97	8.367	2.46	14.367	3.17	20.37	1.08
2.400	.97	8.400	2.46	14.400	3.17	20.40	1.08
2.433	.98	8.433	2.49	14.433	3.13	20.43	1.08
2.467	.98	8.467	2.52	14.467	3.08	20.47	1.07
2.500	.98	8.500	2.52	14.500	3.08	20.50	1.07
2.533	.99	8.533	2.58	14.533	3.00	20.53	1.07
2.567	.99	8.567	2.58	14.567	3.00	20.57	1.07
2.600	.99	8.600	2.61	14.600	2.95	20.60	1.06
2.633	1.00	8.633	2.65	14.633	2.91	20.63	1.06
2.667	1.00	8.667	2.65	14.667	2.91	20.67	1.06
2.700	1.01	8.700	2.71	14.700	2.84	20.70	1.05
2.733	1.01	8.733	2.71	14.733	2.84	20.73	1.05
2.767	1.01	8.767	2.75	14.767	2.80	20.77	1.04
2.800	1.01	8.800	2.79	14.800	2.77	20.80	1.04
2.833	1.01	8.833	2.79	14.833	2.77	20.83	1.04
2.867	1.02	8.867	2.86	14.867	2.70	20.87	1.03
2.900	1.02	8.900	2.86	14.900	2.70	20.90	1.03
2.933	1.03	8.933	2.91	14.933	2.66	20.93	1.03
2.967	1.03	8.967	2.95	14.967	2.63	20.97	1.02
3.000	1.03	9.000	2.95	15.000	2.63	21.00	1.02
3.033	1.04	9.033	3.03	15.033	2.57	21.03	1.02
3.067	1.04	9.067	3.03	15.067	2.57	21.07	1.02
3.100	1.04	9.100	3.08	15.100	2.54	21.10	1.01
3.133	1.05	9.133	3.13	15.133	2.51	21.13	1.01
3.167	1.05	9.167	3.13	15.167	2.51	21.17	1.01
3.200	1.06	9.200	3.23	15.200	2.46	21.20	1.00
3.233	1.06	9.233	3.23	15.233	2.46	21.23	1.00
3.267	1.06	9.267	3.28	15.267	2.43	21.27	1.00
3.300	1.07	9.300	3.33	15.300	2.40	21.30	.99
3.333	1.07	9.333	3.33	15.333	2.40	21.33	.99
3.367	1.08	9.367	3.45	15.367	2.35	21.37	.98
3.400	1.08	9.400	3.45	15.400	2.35	21.40	.98
3.433	1.08	9.433	3.51	15.433	2.33	21.43	.98
3.467	1.09	9.467	3.57	15.467	2.30	21.47	.98
3.500	1.09	9.500	3.57	15.500	2.30	21.50	.98
3.533	1.09	9.533	3.70	15.533	2.26	21.53	.97
3.567	1.09	9.567	3.70	15.567	2.26	21.57	.97
3.600	1.10	9.600	3.77	15.600	2.24	21.60	.97
3.633	1.10	9.633	3.84	15.633	2.21	21.63	.96
3.667	1.10	9.667	3.84	15.667	2.21	21.67	.96
3.700	1.11	9.700	4.00	15.700	2.17	21.70	.96
3.733	1.11	9.733	4.00	15.733	2.17	21.73	.96
3.767	1.12	9.767	4.08	15.767	2.15	21.77	.95
3.800	1.13	9.800	4.17	15.800	2.13	21.80	.95
3.833	1.13	9.833	4.17	15.833	2.13	21.83	.95
3.867	1.14	9.867	4.35	15.867	2.09	21.87	.94
3.900	1.14	9.900	4.35	15.900	2.09	21.90	.94
3.933	1.14	9.933	4.46	15.933	2.07	21.93	.94
3.967	1.15	9.967	4.56	15.967	2.05	21.97	.94
4.000	1.15	10.000	4.56	16.000	2.05	22.00	.94
4.033	1.16	10.033	4.78	16.033	2.02	22.03	.93
4.067	1.16	10.067	4.78	16.067	2.02	22.07	.93
4.100	1.16	10.100	4.91	16.100	2.00	22.10	.93
4.133	1.17	10.133	5.03	16.133	1.98	22.13	.92
4.167	1.17	10.167	5.04	16.167	1.98	22.17	.92
4.200	1.18	10.200	5.31	16.200	1.95	22.20	.92
4.233	1.18	10.233	5.31	16.233	1.95	22.23	.92
4.267	1.19	10.267	5.47	16.267	1.93	22.27	.91
4.300	1.19	10.300	5.63	16.300	1.92	22.30	.91
4.333	1.19	10.333	5.63	16.333	1.92	22.33	.91
4.367	1.20	10.367	5.98	16.367	1.89	22.37	.90
4.400	1.20	10.400	5.98	16.400	1.89	22.40	.90
4.433	1.21	10.433	6.19	16.433	1.87	22.43	.90
4.467	1.22	10.467	6.39	16.467	1.86	22.47	.90
4.500	1.22	10.500	6.39	16.500	1.85	22.50	.90
4.533	1.23	10.533	6.86	16.533	1.83	22.53	.89
4.567	1.23	10.567	6.86	16.567	1.83	22.57	.89
4.600	1.24	10.600	7.13	16.600	1.81	22.60	.89
4.633	1.24	10.633	7.40	16.633	1.80	22.63	.89
4.667	1.24	10.667	7.41	16.667	1.80	22.67	.89
4.700	1.25	10.700	8.05	16.700	1.77	22.70	.88

4.733	1.25	10.733	8.05	16.733	1.77	22.73	.88
4.767	1.26	10.767	8.43	16.767	1.76	22.77	.88
4.800	1.27	10.800	8.82	16.800	1.74	22.80	.87
4.833	1.27	10.833	8.82	16.833	1.74	22.83	.87
4.867	1.28	10.867	9.75	16.867	1.72	22.87	.87
4.900	1.28	10.900	9.75	16.900	1.72	22.90	.87
4.933	1.29	10.933	10.33	16.933	1.71	22.93	.87
4.967	1.30	10.967	10.91	16.967	1.69	22.97	.86
5.000	1.30	11.000	10.91	17.000	1.69	23.00	.86
5.033	1.31	11.033	12.38	17.033	1.67	23.03	.86
5.067	1.31	11.067	12.38	17.067	1.67	23.07	.86
5.100	1.32	11.100	13.34	17.100	1.66	23.10	.85
5.133	1.33	11.133	14.30	17.133	1.65	23.13	.85
5.167	1.33	11.167	14.30	17.167	1.65	23.17	.85
5.200	1.34	11.200	16.92	17.200	1.62	23.20	.85
5.233	1.34	11.233	16.92	17.233	1.62	23.23	.85
5.267	1.35	11.267	18.79	17.267	1.61	23.27	.84
5.300	1.36	11.300	20.66	17.300	1.60	23.30	.84
5.333	1.36	11.333	20.66	17.333	1.60	23.33	.84
5.367	1.37	11.367	26.37	17.367	1.58	23.37	.84
5.400	1.37	11.400	26.37	17.400	1.58	23.40	.84
5.433	1.38	11.433	31.20	17.433	1.57	23.43	.83
5.467	1.39	11.467	36.00	17.467	1.56	23.47	.83
5.500	1.39	11.500	36.03	17.500	1.56	23.50	.83
5.533	1.40	11.533	54.94	17.533	1.54	23.53	.83
5.567	1.40	11.567	54.94	17.567	1.54	23.57	.83
5.600	1.41	11.600	79.66	17.600	1.53	23.60	.82
5.633	1.42	11.633	104.25	17.633	1.52	23.63	.82
5.667	1.42	11.667	104.39	17.667	1.52	23.67	.82
5.700	1.44	11.700	215.25	17.700	1.50	23.70	.82
5.733	1.44	11.733	215.25	17.733	1.50	23.73	.82
5.767	1.45	11.767	160.41	17.767	1.49	23.77	.81
5.800	1.46	11.800	105.85	17.800	1.48	23.80	.81
5.833	1.46	11.833	105.78	17.833	1.48	23.83	.81
5.867	1.48	11.867	56.85	17.867	1.47	23.87	.81
5.900	1.48	11.900	56.85	17.900	1.47	23.90	.81
5.933	1.49	11.933	47.16	17.933	1.46	23.93	.80
5.967	1.50	11.967	37.53	17.967	1.45	23.97	.80
6.000	1.50	12.000	37.52	18.000	1.45	24.00	.80

Unit Hyd Qpeak (cms)= .466

PEAK FLOW (cms)= .186 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 57.583
 TOTAL RAINFALL (mm)= 114.709
 RUNOFF COEFFICIENT = .502

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0024) | Area (ha)= 5.03 | Curve Number (CN)= 72.5
 ID= 1 DT= 2.0 min | Ia (mm)= 4.75 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 2.433

PEAK FLOW (cms)= 1.240 (i)
 TIME TO PEAK (hrs)= 11.800
 RUNOFF VOLUME (mm)= 44.847
 TOTAL RAINFALL (mm)= 114.709
 RUNOFF COEFFICIENT = .391

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0022) | Area (ha)= 3.01 | Curve Number (CN)= 71.6
 ID= 1 DT= 2.0 min | Ia (mm)= 5.22 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= 2.069

PEAK FLOW (cms)= .811 (i)
 TIME TO PEAK (hrs)= 11.767
 RUNOFF VOLUME (mm)= 43.199
 TOTAL RAINFALL (mm)= 114.709
 RUNOFF COEFFICIENT = .377

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 RESERVOIR (0023)
 IN= 2---> OUT= 1
 DT= 2.0 min | OUTFLOW STORAGE | OUTFLOW STORAGE

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-----
                (cms)      (ha.m.) |      (cms)      (ha.m.)
                .0000      .0000 |      .0002      .2156
                .0001      .1117 |      20.0000     .2166

                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0022)  3.01      .81      11.77     43.20
OUTFLOW: ID= 1 (0023)  3.01      .00      13.60     .03

                PEAK FLOW REDUCTION [Qout/Qin](%)= .01
                TIME SHIFT OF PEAK FLOW (min)=110.00
                MAXIMUM STORAGE USED (ha.m.)= .1299

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-----
| ADD HYD (0026) |
| 1 + 2 = 3 |
-----
                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0024):      5.03      1.240     11.80     44.85
+ ID2= 2 (0023):      3.01      .000      13.60     .03
=====
ID = 3 (0026):      8.04      1.240     11.80     28.07

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| RESERVOIR (0025) |
| IN= 2--> OUT= 1 |
| DT= 2.0 min |
-----
                OUTFLOW      STORAGE      OUTFLOW      STORAGE
                (cms)      (ha.m.) |      (cms)      (ha.m.)
                .0000      .0000 |      .0003      .2171
                .0001      .0498 |      20.0000     .2181
                .0002      .1676 |      .0000      .0000

                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0026)  8.04      1.24      11.80     28.07
OUTFLOW: ID= 1 (0025)  8.04      .08      13.07     1.77

                PEAK FLOW REDUCTION [Qout/Qin](%)= 6.42
                TIME SHIFT OF PEAK FLOW (min)= 76.00
                MAXIMUM STORAGE USED (ha.m.)= .2180

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-----
| ADD HYD (0028) |
| 1 + 2 = 3 |
-----
                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0027):      .68      .186     11.77     57.58
+ ID2= 2 (0025):      8.04      .080     13.07     1.77
=====
ID = 3 (0028):      8.72      .186     11.77     6.11

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| RESERVOIR (0029) |
| IN= 2--> OUT= 1 |
| DT= 2.0 min |
-----
                OUTFLOW      STORAGE      OUTFLOW      STORAGE
                (cms)      (ha.m.) |      (cms)      (ha.m.)
                .0000      .0000 |      .0002      .0898
                .0001      .0455 |      20.0000     .0908

                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 (0028)  8.72      .19      11.77     6.11
OUTFLOW: ID= 1 (0029)  8.72      .00      66.63     .24

                PEAK FLOW REDUCTION [Qout/Qin](%)= .06
                TIME SHIFT OF PEAK FLOW (min)=*****
                MAXIMUM STORAGE USED (ha.m.)= .0512

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-----
| CALIB |
| NASHYD (0032) |
| ID= 1 DT= 5.0 min |
-----
                Area (ha)= 6.71 Curve Number (CN)= 64.3
                Ia (mm)= 8.68 # of Linear Res.(N)= 3.00
                U.H. Tp(hrs)= .32

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NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

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----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr

```

.083	.80	6.083	1.52	12.083	27.59	18.08	1.43
.167	.81	6.167	1.54	12.167	21.65	18.17	1.41
.250	.81	6.250	1.56	12.250	17.75	18.25	1.40
.333	.82	6.333	1.58	12.333	15.01	18.33	1.38
.417	.82	6.417	1.60	12.417	12.99	18.42	1.37
.500	.83	6.500	1.62	12.500	11.45	18.50	1.35
.583	.83	6.583	1.65	12.583	10.23	18.58	1.34
.667	.84	6.667	1.67	12.667	9.25	18.67	1.32
.750	.84	6.750	1.70	12.750	8.44	18.75	1.31
.833	.85	6.833	1.72	12.833	7.77	18.83	1.30
.917	.85	6.917	1.75	12.917	7.19	18.92	1.28
1.000	.86	7.000	1.78	13.000	6.70	19.00	1.27
1.083	.87	7.083	1.81	13.083	6.27	19.08	1.26
1.167	.87	7.167	1.84	13.167	5.90	19.17	1.24
1.250	.88	7.250	1.87	13.250	5.57	19.25	1.23
1.333	.88	7.333	1.90	13.333	5.28	19.33	1.22
1.417	.89	7.417	1.93	13.417	5.01	19.42	1.21
1.500	.90	7.500	1.97	13.500	4.78	19.50	1.20
1.583	.90	7.583	2.00	13.583	4.56	19.58	1.18
1.667	.91	7.667	2.04	13.667	4.37	19.67	1.17
1.750	.92	7.750	2.08	13.750	4.19	19.75	1.16
1.833	.92	7.833	2.12	13.833	4.02	19.83	1.15
1.917	.93	7.917	2.16	13.917	3.87	19.92	1.14
2.000	.94	8.000	2.21	14.000	3.73	20.00	1.13
2.083	.94	8.083	2.25	14.083	3.61	20.08	1.12
2.167	.95	8.167	2.30	14.167	3.49	20.17	1.11
2.250	.96	8.250	2.35	14.250	3.37	20.25	1.10
2.333	.97	8.333	2.40	14.333	3.27	20.33	1.09
2.417	.97	8.417	2.46	14.417	3.17	20.42	1.08
2.500	.98	8.500	2.52	14.500	3.08	20.50	1.07
2.583	.99	8.583	2.58	14.583	3.00	20.58	1.07
2.667	1.00	8.667	2.65	14.667	2.91	20.67	1.06
2.750	1.01	8.750	2.71	14.750	2.84	20.75	1.05
2.833	1.01	8.833	2.79	14.833	2.77	20.83	1.04
2.917	1.02	8.917	2.86	14.917	2.70	20.92	1.03
3.000	1.03	9.000	2.95	15.000	2.63	21.00	1.02
3.083	1.04	9.083	3.03	15.083	2.57	21.08	1.02
3.167	1.05	9.167	3.13	15.167	2.51	21.17	1.01
3.250	1.06	9.250	3.23	15.250	2.46	21.25	1.00
3.333	1.07	9.333	3.33	15.333	2.40	21.33	.99
3.417	1.08	9.417	3.45	15.417	2.35	21.42	.98
3.500	1.09	9.500	3.57	15.500	2.30	21.50	.98
3.583	1.09	9.583	3.70	15.583	2.26	21.58	.97
3.667	1.10	9.667	3.84	15.667	2.21	21.67	.96
3.750	1.11	9.750	4.00	15.750	2.17	21.75	.96
3.833	1.13	9.833	4.17	15.833	2.13	21.83	.95
3.917	1.14	9.917	4.35	15.917	2.09	21.92	.94
4.000	1.15	10.000	4.56	16.000	2.05	22.00	.94
4.083	1.16	10.083	4.78	16.083	2.02	22.08	.93
4.167	1.17	10.167	5.03	16.167	1.98	22.17	.92
4.250	1.18	10.250	5.31	16.250	1.95	22.25	.92
4.333	1.19	10.333	5.63	16.333	1.92	22.33	.91
4.417	1.20	10.417	5.98	16.417	1.89	22.42	.90
4.500	1.22	10.500	6.39	16.500	1.86	22.50	.90
4.583	1.23	10.583	6.86	16.583	1.83	22.58	.89
4.667	1.24	10.667	7.40	16.667	1.80	22.67	.89
4.750	1.25	10.750	8.05	16.750	1.77	22.75	.88
4.833	1.27	10.833	8.82	16.833	1.74	22.83	.87
4.917	1.28	10.917	9.75	16.917	1.72	22.92	.87
5.000	1.30	11.000	10.91	17.000	1.69	23.00	.86
5.083	1.31	11.083	12.38	17.083	1.67	23.08	.86
5.167	1.33	11.167	14.30	17.167	1.65	23.17	.85
5.250	1.34	11.250	16.92	17.250	1.62	23.25	.85
5.333	1.36	11.333	20.66	17.333	1.60	23.33	.84
5.417	1.37	11.417	26.37	17.417	1.58	23.42	.84
5.500	1.39	11.500	36.00	17.500	1.56	23.50	.83
5.583	1.40	11.583	54.93	17.583	1.54	23.58	.83
5.667	1.42	11.667	104.25	17.667	1.52	23.67	.82
5.750	1.44	11.750	215.23	17.750	1.50	23.75	.82
5.833	1.46	11.833	105.86	17.833	1.48	23.83	.81
5.917	1.48	11.917	56.85	17.917	1.47	23.92	.81
6.000	1.50	12.000	37.53	18.000	1.45	24.00	.80

Unit Hyd Qpeak (cms)= .800

PEAK FLOW (cms)= .631 (i)
 TIME TO PEAK (hrs)= 12.083
 RUNOFF VOLUME (mm)= 45.447
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .396

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0030) ID= 1 DT= 5.0 min	Area (ha)= 5.57 Ia (mm)= 6.12 U.H. Tp(hrs)= .06	Curve Number (CN)= 69.8 # of Linear Res.(N)= 3.00
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Unit Hyd Qpeak (cms)= 3.828

PEAK FLOW (cms)= 1.276 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 44.305
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .386

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0031)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

----->
<----- DATA FOR SECTION (1.2) ----->
Distance Elevation Manning
.00 386.25 .0300
37.50 385.75 .0300 / .0300 Main Channel
47.50 385.75 .0300 / .0300 Main Channel
85.00 386.25 .0300

----->
<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	385.78	.150E+03	.1	.33	23.91
.05	385.80	.350E+03	.3	.47	16.85
.08	385.83	.599E+03	.7	.56	14.12
.11	385.86	.898E+03	1.2	.63	12.62
.13	385.88	.125E+04	1.8	.68	11.65
.16	385.91	.164E+04	2.5	.73	10.95
.18	385.93	.209E+04	3.3	.76	10.42
.21	385.96	.259E+04	4.3	.80	9.99
.24	385.99	.313E+04	5.4	.82	9.64
.26	386.01	.373E+04	6.7	.85	9.33
.29	386.04	.438E+04	8.0	.88	9.07
.32	386.07	.507E+04	9.6	.90	8.83
.34	386.09	.582E+04	11.2	.92	8.62
.37	386.12	.661E+04	13.1	.94	8.43
.39	386.14	.745E+04	15.1	.96	8.25
.42	386.17	.835E+04	17.2	.98	8.08
.45	386.20	.929E+04	19.5	1.00	7.93
.47	386.22	.103E+05	22.0	1.02	7.79
.50	386.25	.113E+05	24.7	1.04	7.65

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0030)	5.57	1.28	11.75	44.30	.11	.64
OUTFLOW: ID= 1 (0031)	5.57	.66	11.92	44.28	.08	.55

ADD HYD (0033)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0032):	6.71	.631	12.08	45.45
+ ID2= 2 (0031):	5.57	.663	11.92	44.28
=====	=====	=====	=====	=====
ID = 3 (0033):	12.27	1.204	11.92	44.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0036)
ID= 1 DT= 5.0 min

Area (ha)= 2.08 Curve Number (CN)= 67.6
Ia (mm)= 7.71 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= .938

PEAK FLOW (cms)= .406 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 47.709
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .416

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0034)
ID= 1 DT= 5.0 min

Area (ha)= 2.15 Curve Number (CN)= 71.9
Ia (mm)= 5.03 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .10

Unit Hyd Qpeak (cms)= .795

PEAK FLOW (cms)= .462 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 56.240
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .491

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0035)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

----- DATA FOR SECTION (1.3) ----->
Distance Elevation Manning
.00 388.25 .0300
30.00 387.75 .0300 / .0300 Main Channel
40.00 387.75 .0300 / .0300 Main Channel
70.00 388.25 .0300

----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	387.78	.327E+02	.1	.41	4.35
.05	387.80	.744E+02	.4	.59	3.03
.08	387.83	.125E+03	.8	.71	2.52
.11	387.86	.185E+03	1.4	.80	2.25
.13	387.88	.253E+03	2.0	.87	2.07
.16	387.91	.330E+03	2.8	.92	1.95
.18	387.93	.417E+03	3.7	.97	1.85
.21	387.96	.512E+03	4.8	1.01	1.78
.24	387.99	.616E+03	6.0	1.04	1.72
.26	388.01	.729E+03	7.3	1.07	1.67
.29	388.04	.851E+03	8.7	1.10	1.63
.32	388.07	.982E+03	10.3	1.13	1.59
.34	388.09	.112E+04	12.0	1.15	1.56
.37	388.12	.127E+04	13.9	1.17	1.53
.39	388.14	.143E+04	15.9	1.19	1.50
.42	388.17	.160E+04	18.0	1.21	1.48
.45	388.20	.177E+04	20.3	1.23	1.45
.47	388.22	.196E+04	22.8	1.25	1.43
.50	388.25	.215E+04	25.4	1.27	1.41

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0034)	2.15	.46	11.83	56.24	.06	.60
OUTFLOW: ID= 1 (0035)	2.15	.46	11.83	56.24	.06	.60

ADD HYD (0037)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0036):	2.08	.406	11.75	47.71
+ ID2= 2 (0035):	2.15	.457	11.83	56.24
===== ID = 3 (0037):	4.23	.845	11.83	52.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0039)
ID= 1 DT= 5.0 min

Area (ha)= 35.03 Curve Number (CN)= 65.5
Ia (mm)= 7.17 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.16

Unit Hyd Qpeak (cms)= 1.152

PEAK FLOW (cms)= 1.376 (i)
TIME TO PEAK (hrs)= 13.000
RUNOFF VOLUME (mm)= 47.852
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .417

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0040)
ID= 1 DT= 5.0 min

Area (ha)= 3.95 Curve Number (CN)= 54.0
Ia (mm)= 10.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .40

Unit Hyd Qpeak (cms)= .375

PEAK FLOW (cms)= .235 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 34.107
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .298

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0041)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.1655
.0001	.0976	20.0000	.1665

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0040)	3.95	.23	12.17	34.11
OUTFLOW: ID= 1 (0041)	3.95	.00	25.25	.16

PEAK FLOW REDUCTION [Qout/Qin](%)= .07
 TIME SHIFT OF PEAK FLOW (min)=785.00
 MAXIMUM STORAGE USED (ha.m.)= .1342

CALIB
 NASHYD (0044)
 ID= 1 DT= 3.0 min

Area (ha)= .87 Curve Number (CN)= 64.6
 Ia (mm)= 6.68 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .06

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.050	.80	6.050	1.52	12.050	27.59	18.05	1.43
.100	.80	6.100	1.52	12.100	25.60	18.10	1.43
.150	.81	6.150	1.54	12.150	21.65	18.15	1.41
.200	.81	6.200	1.55	12.200	19.04	18.20	1.40
.250	.81	6.250	1.56	12.250	17.74	18.25	1.40
.300	.82	6.300	1.58	12.300	15.01	18.30	1.38
.350	.82	6.350	1.59	12.350	14.33	18.35	1.38
.400	.82	6.400	1.60	12.400	12.99	18.40	1.37
.450	.83	6.450	1.62	12.450	11.96	18.45	1.36
.500	.83	6.500	1.62	12.500	11.45	18.50	1.35
.550	.83	6.550	1.65	12.550	10.23	18.55	1.34
.600	.83	6.600	1.65	12.600	9.90	18.60	1.33
.650	.84	6.650	1.67	12.650	9.25	18.65	1.32
.700	.84	6.700	1.69	12.700	8.71	18.70	1.31
.750	.84	6.750	1.70	12.750	8.44	18.75	1.31
.800	.85	6.800	1.72	12.800	7.77	18.80	1.30
.850	.85	6.850	1.73	12.850	7.58	18.85	1.29
.900	.85	6.900	1.75	12.900	7.19	18.90	1.28
.950	.86	6.950	1.77	12.950	6.87	18.95	1.27
1.000	.86	7.000	1.78	13.000	6.70	19.00	1.27
1.050	.87	7.050	1.81	13.050	6.27	19.05	1.26
1.100	.87	7.100	1.82	13.100	6.15	19.10	1.25
1.150	.87	7.150	1.84	13.150	5.90	19.15	1.24
1.200	.88	7.200	1.86	13.200	5.68	19.20	1.24
1.250	.88	7.250	1.87	13.250	5.57	19.25	1.23
1.300	.88	7.300	1.90	13.300	5.28	19.30	1.22
1.350	.89	7.350	1.91	13.350	5.19	19.35	1.22
1.400	.89	7.400	1.93	13.400	5.01	19.40	1.21
1.450	.89	7.450	1.95	13.450	4.85	19.45	1.20
1.500	.90	7.500	1.97	13.500	4.77	19.50	1.20
1.550	.90	7.550	2.00	13.550	4.56	19.55	1.18
1.600	.91	7.600	2.01	13.600	4.50	19.60	1.18
1.650	.91	7.650	2.04	13.650	4.37	19.65	1.17
1.700	.91	7.700	2.07	13.700	4.25	19.70	1.17
1.750	.92	7.750	2.08	13.750	4.19	19.75	1.16
1.800	.92	7.800	2.12	13.800	4.02	19.80	1.15
1.850	.93	7.850	2.13	13.850	3.97	19.85	1.15
1.900	.93	7.900	2.16	13.900	3.87	19.90	1.14
1.950	.93	7.950	2.19	13.950	3.78	19.95	1.14
2.000	.94	8.000	2.21	14.000	3.73	20.00	1.13
2.050	.94	8.050	2.25	14.050	3.61	20.05	1.12
2.100	.95	8.100	2.27	14.100	3.57	20.10	1.12
2.150	.95	8.150	2.30	14.150	3.49	20.15	1.11
2.200	.96	8.200	2.33	14.200	3.41	20.20	1.11
2.250	.96	8.250	2.35	14.250	3.37	20.25	1.10
2.300	.97	8.300	2.40	14.300	3.27	20.30	1.09
2.350	.97	8.350	2.42	14.350	3.24	20.35	1.09

2.400	.97	8.400	2.46	14.400	3.17	20.40	1.08
2.450	.98	8.450	2.50	14.450	3.11	20.45	1.08
2.500	.98	8.500	2.52	14.500	3.08	20.50	1.07
2.550	.99	8.550	2.58	14.550	3.00	20.55	1.07
2.600	.99	8.600	2.60	14.600	2.97	20.60	1.06
2.650	1.00	8.650	2.65	14.650	2.91	20.65	1.06
2.700	1.00	8.700	2.69	14.700	2.86	20.70	1.05
2.750	1.01	8.750	2.71	14.750	2.84	20.75	1.05
2.800	1.01	8.800	2.79	14.800	2.77	20.80	1.04
2.850	1.02	8.850	2.81	14.850	2.74	20.85	1.04
2.900	1.02	8.900	2.86	14.900	2.70	20.90	1.03
2.950	1.03	8.950	2.92	14.950	2.65	20.95	1.03
3.000	1.03	9.000	2.95	15.000	2.63	21.00	1.02
3.050	1.04	9.050	3.03	15.050	2.57	21.05	1.02
3.100	1.04	9.100	3.06	15.100	2.55	21.10	1.01
3.150	1.05	9.150	3.13	15.150	2.51	21.15	1.01
3.200	1.05	9.200	3.19	15.200	2.48	21.20	1.00
3.250	1.06	9.250	3.23	15.250	2.46	21.25	1.00
3.300	1.07	9.300	3.33	15.300	2.40	21.30	.99
3.350	1.07	9.350	3.37	15.350	2.39	21.35	.99
3.400	1.08	9.400	3.45	15.400	2.35	21.40	.98
3.450	1.08	9.450	3.53	15.450	2.32	21.45	.98
3.500	1.09	9.500	3.57	15.500	2.30	21.50	.98
3.550	1.09	9.550	3.70	15.550	2.26	21.55	.97
3.600	1.10	9.600	3.75	15.600	2.24	21.60	.97
3.650	1.10	9.650	3.84	15.650	2.21	21.65	.96
3.700	1.11	9.700	3.95	15.700	2.19	21.70	.96
3.750	1.11	9.750	4.00	15.750	2.17	21.75	.96
3.800	1.13	9.800	4.17	15.800	2.13	21.80	.95
3.850	1.13	9.850	4.23	15.850	2.12	21.85	.95
3.900	1.14	9.900	4.35	15.900	2.09	21.90	.94
3.950	1.14	9.950	4.49	15.950	2.07	21.95	.94
4.000	1.15	10.000	4.56	16.000	2.05	22.00	.94
4.050	1.16	10.050	4.78	16.050	2.02	22.05	.93
4.100	1.16	10.100	4.87	16.100	2.01	22.10	.93
4.150	1.17	10.150	5.03	16.150	1.98	22.15	.92
4.200	1.18	10.200	5.22	16.200	1.96	22.20	.92
4.250	1.18	10.250	5.31	16.250	1.95	22.25	.92
4.300	1.19	10.300	5.63	16.300	1.92	22.30	.91
4.350	1.20	10.350	5.75	16.350	1.91	22.35	.91
4.400	1.20	10.400	5.98	16.400	1.89	22.40	.90
4.450	1.21	10.450	6.26	16.450	1.87	22.45	.90
4.500	1.22	10.500	6.39	16.500	1.85	22.50	.90
4.550	1.23	10.550	6.86	16.550	1.83	22.55	.89
4.600	1.23	10.600	7.04	16.600	1.82	22.60	.89
4.650	1.24	10.650	7.40	16.650	1.80	22.65	.89
4.700	1.25	10.700	7.83	16.700	1.78	22.70	.88
4.750	1.25	10.750	8.05	16.750	1.77	22.75	.88
4.800	1.27	10.800	8.82	16.800	1.74	22.80	.87
4.850	1.27	10.850	9.13	16.850	1.74	22.85	.87
4.900	1.28	10.900	9.75	16.900	1.72	22.90	.87
4.950	1.29	10.950	10.52	16.950	1.70	22.95	.86
5.000	1.30	11.000	10.91	17.000	1.69	23.00	.86
5.050	1.31	11.050	12.38	17.050	1.67	23.05	.86
5.100	1.32	11.100	13.02	17.100	1.66	23.10	.85
5.150	1.33	11.150	14.30	17.150	1.65	23.15	.85
5.200	1.34	11.200	16.05	17.200	1.63	23.20	.85
5.250	1.34	11.250	16.92	17.250	1.62	23.25	.85
5.300	1.36	11.300	20.66	17.300	1.60	23.30	.84
5.350	1.36	11.350	22.56	17.350	1.60	23.35	.84
5.400	1.37	11.400	26.37	17.400	1.58	23.40	.84
5.450	1.38	11.450	32.80	17.450	1.57	23.45	.83
5.500	1.39	11.500	36.01	17.500	1.56	23.50	.83
5.550	1.40	11.550	54.94	17.550	1.54	23.55	.83
5.600	1.41	11.600	71.40	17.600	1.53	23.60	.82
5.650	1.42	11.650	104.25	17.650	1.52	23.65	.82
5.700	1.43	11.700	178.31	17.700	1.51	23.70	.82
5.750	1.44	11.750	215.19	17.750	1.50	23.75	.82
5.800	1.46	11.800	105.85	17.800	1.48	23.80	.81
5.850	1.46	11.850	89.49	17.850	1.48	23.85	.81
5.900	1.48	11.900	56.85	17.900	1.47	23.90	.81
5.950	1.49	11.950	43.96	17.950	1.45	23.95	.80
6.000	1.50	12.000	37.53	18.000	1.45	24.00	.80

Unit Hyd Qpeak (cms)= .596

PEAK FLOW (cms)= .190 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 45.621
 TOTAL RAINFALL (mm)= 114.710
 RUNOFF COEFFICIENT = .398

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 CALIB
 NASHYD (0042) Area (ha)= .56 Curve Number (CN)= 70.0
 ID= 1 DT= 3.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

----- U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .382

PEAK FLOW (cms)= .143 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 50.471
TOTAL RAINFALL (mm)= 114.710
RUNOFF COEFFICIENT = .440

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0043) |
| IN= 2---> OUT= 1 |
| DT= 3.0 min |

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0357
.0001	.0118	20.0000	.0367

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0042)	.56	.14	11.75	50.47
OUTFLOW: ID= 1 (0043)	.56	.00	20.10	.86

PEAK FLOW REDUCTION [Qout/Qin](%)= .12
TIME SHIFT OF PEAK FLOW (min)=501.00
MAXIMUM STORAGE USED (ha.m.)= .0276

| ADD HYD (0045) |
| 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0044):	.87	.190	11.75	45.62
+ ID2= 2 (0043):	.56	.000	20.10	.86
=====				
ID = 3 (0045):	1.42	.190	11.75	28.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| RESERVOIR (0046) |
| IN= 2---> OUT= 1 |
| DT= 3.0 min |

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.1073
.0001	.0117	20.0000	.1083

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0045)	1.42	.19	11.75	28.15
OUTFLOW: ID= 1 (0046)	1.42	.00	24.15	.40

PEAK FLOW REDUCTION [Qout/Qin](%)= .07
TIME SHIFT OF PEAK FLOW (min)=744.00
MAXIMUM STORAGE USED (ha.m.)= .0395

| CALIB NASHYD (0047) |
| ID= 1 DT= 3.0 min |

Area (ha)= .48 Curve Number (CN)= 70.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .06

Unit Hyd Qpeak (cms)= .331

PEAK FLOW (cms)= .124 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 50.471
TOTAL RAINFALL (mm)= 114.710
RUNOFF COEFFICIENT = .440

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR (0048) |
| IN= 2---> OUT= 1 |
| DT= 3.0 min |

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.0002	.0731
.0001	.0496	20.0000	.0741

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
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INFLOW : ID= 2 (0047) .48 .12 11.75 50.47
 OUTFLOW: ID= 1 (0048) .48 .00 20.15 .28

PEAK FLOW REDUCTION [Qout/Qin](%)= .04
 TIME SHIFT OF PEAK FLOW (min)=504.00
 MAXIMUM STORAGE USED (ha.m.)= .0242

 CALIB (0049) Area (ha)= 2.77 Curve Number (CN)= 70.7
 NASHYD (0049) Ia (mm)= 5.35 # of Linear Res.(N)= 3.00
 ID= 1 DT= 5.0 min U.H. Tp(hrs)= .11

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.80	6.083	1.52	12.083	27.59	18.08	1.43
.167	.81	6.167	1.54	12.167	21.65	18.17	1.41
.250	.81	6.250	1.56	12.250	17.75	18.25	1.40
.333	.82	6.333	1.58	12.333	15.01	18.33	1.38
.417	.82	6.417	1.60	12.417	12.99	18.42	1.37
.500	.83	6.500	1.62	12.500	11.45	18.50	1.35
.583	.83	6.583	1.65	12.583	10.23	18.58	1.34
.667	.84	6.667	1.67	12.667	9.25	18.67	1.32
.750	.84	6.750	1.70	12.750	8.44	18.75	1.31
.833	.85	6.833	1.72	12.833	7.77	18.83	1.30
.917	.85	6.917	1.75	12.917	7.19	18.92	1.28
1.000	.86	7.000	1.78	13.000	6.70	19.00	1.27
1.083	.87	7.083	1.81	13.083	6.27	19.08	1.26
1.167	.87	7.167	1.84	13.167	5.90	19.17	1.24
1.250	.88	7.250	1.87	13.250	5.57	19.25	1.23
1.333	.88	7.333	1.90	13.333	5.28	19.33	1.22
1.417	.89	7.417	1.93	13.417	5.01	19.42	1.21
1.500	.90	7.500	1.97	13.500	4.78	19.50	1.20
1.583	.90	7.583	2.00	13.583	4.56	19.58	1.18
1.667	.91	7.667	2.04	13.667	4.37	19.67	1.17
1.750	.92	7.750	2.08	13.750	4.19	19.75	1.16
1.833	.92	7.833	2.12	13.833	4.02	19.83	1.15
1.917	.93	7.917	2.16	13.917	3.87	19.92	1.14
2.000	.94	8.000	2.21	14.000	3.73	20.00	1.13
2.083	.94	8.083	2.25	14.083	3.61	20.08	1.12
2.167	.95	8.167	2.30	14.167	3.49	20.17	1.11
2.250	.96	8.250	2.35	14.250	3.37	20.25	1.10
2.333	.97	8.333	2.40	14.333	3.27	20.33	1.09
2.417	.97	8.417	2.46	14.417	3.17	20.42	1.08
2.500	.98	8.500	2.52	14.500	3.08	20.50	1.07
2.583	.99	8.583	2.58	14.583	3.00	20.58	1.07
2.667	1.00	8.667	2.65	14.667	2.91	20.67	1.06
2.750	1.01	8.750	2.71	14.750	2.84	20.75	1.05
2.833	1.01	8.833	2.79	14.833	2.77	20.83	1.04
2.917	1.02	8.917	2.86	14.917	2.70	20.92	1.03
3.000	1.03	9.000	2.95	15.000	2.63	21.00	1.02
3.083	1.04	9.083	3.03	15.083	2.57	21.08	1.02
3.167	1.05	9.167	3.13	15.167	2.51	21.17	1.01
3.250	1.06	9.250	3.23	15.250	2.46	21.25	1.00
3.333	1.07	9.333	3.33	15.333	2.40	21.33	.99
3.417	1.08	9.417	3.45	15.417	2.35	21.42	.98
3.500	1.09	9.500	3.57	15.500	2.30	21.50	.98
3.583	1.09	9.583	3.70	15.583	2.26	21.58	.97
3.667	1.10	9.667	3.84	15.667	2.21	21.67	.96
3.750	1.11	9.750	4.00	15.750	2.17	21.75	.96
3.833	1.13	9.833	4.17	15.833	2.13	21.83	.95
3.917	1.14	9.917	4.35	15.917	2.09	21.92	.94
4.000	1.15	10.000	4.56	16.000	2.05	22.00	.94
4.083	1.16	10.083	4.78	16.083	2.02	22.08	.93
4.167	1.17	10.167	5.03	16.167	1.98	22.17	.92
4.250	1.18	10.250	5.31	16.250	1.95	22.25	.92
4.333	1.19	10.333	5.63	16.333	1.92	22.33	.91
4.417	1.20	10.417	5.98	16.417	1.89	22.42	.90
4.500	1.22	10.500	6.39	16.500	1.86	22.50	.90
4.583	1.23	10.583	6.86	16.583	1.83	22.58	.89
4.667	1.24	10.667	7.40	16.667	1.80	22.67	.89
4.750	1.25	10.750	8.05	16.750	1.77	22.75	.88
4.833	1.27	10.833	8.82	16.833	1.74	22.83	.87
4.917	1.28	10.917	9.75	16.917	1.72	22.92	.87
5.000	1.30	11.000	10.91	17.000	1.69	23.00	.86
5.083	1.31	11.083	12.38	17.083	1.67	23.08	.86
5.167	1.33	11.167	14.30	17.167	1.65	23.17	.85
5.250	1.34	11.250	16.92	17.250	1.62	23.25	.85
5.333	1.36	11.333	20.66	17.333	1.60	23.33	.84
5.417	1.37	11.417	26.37	17.417	1.58	23.42	.84
5.500	1.39	11.500	36.00	17.500	1.56	23.50	.83
5.583	1.40	11.583	54.93	17.583	1.54	23.58	.83
5.667	1.42	11.667	104.25	17.667	1.52	23.67	.82
5.750	1.44	11.750	215.23	17.750	1.50	23.75	.82

5.833	1.46	11.833	105.86	17.833	1.48	23.83	.81
5.917	1.48	11.917	56.85	17.917	1.47	23.92	.81
6.000	1.50	12.000	37.53	18.000	1.45	24.00	.00

Unit Hyd Qpeak (cms)= .952

PEAK FLOW (cms)= .568 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 54.724
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .477

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0055) ID= 1 DT= 5.0 min	Area (ha)= 5.19 Ia (mm)= 4.00 U.H. Tp(hrs)= .11	Curve Number (CN)= 73.3 # of Linear Res.(N)= 3.00
---	---	--

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= 1.150 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 59.205
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .516

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0052) ID= 1 DT= 5.0 min	Area (ha)= 3.90 Ia (mm)= 4.85 U.H. Tp(hrs)= .08	Curve Number (CN)= 69.4 # of Linear Res.(N)= 3.00
---	---	--

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .870 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 50.889
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .444

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0050) ID= 1 DT= 5.0 min	Area (ha)= 11.96 Ia (mm)= 5.74 U.H. Tp(hrs)= .18	Curve Number (CN)= 66.4 # of Linear Res.(N)= 3.00
---	--	--

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.742 (i)
 TIME TO PEAK (hrs)= 11.917
 RUNOFF VOLUME (mm)= 49.852
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .435

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0051) IN= 2---> OUT= 1 DT= 5.0 min	OUTFLOW (cms) .0000 .0001	STORAGE (ha.m.) .0000 .1573	OUTFLOW (cms) 20.0000 .0000	STORAGE (ha.m.) .1583 .0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0050)	11.96	1.74	11.92	49.85
OUTFLOW: ID= 1 (0051)	11.96	1.92	12.00	36.70

PEAK FLOW REDUCTION [Qout/Qin](%)=110.09
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .3041

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

| ADD HYD (0053) |

1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0052):	3.90	.870	11.75	50.89
+ ID2= 2 (0051):	11.96	1.918	12.00	36.70
=====				
ID = 3 (0053):	15.86	2.240	12.00	40.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0054)
IN= 2---> OUT= 1
DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	20.0000	.0771
	.0001	.0761	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0053)	15.86	2.24	12.00	40.19
OUTFLOW: ID= 1 (0054)	15.86	2.50	11.92	35.39

PEAK FLOW REDUCTION [Qout/Qin](%)=111.63
TIME SHIFT OF PEAK FLOW (min)= -5.00
MAXIMUM STORAGE USED (ha.m.)= .3757

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ROUTE CHN (0056)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.5) ----->

Distance	Elevation	Manning	
.00	425.00	.0300	
.75	424.25	.0300 / .0300	Main Channel
1.75	424.25	.0300 / .0300	Main Channel
2.50	425.00	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.04	424.29	.145E+02	.0	.68	8.63
.08	424.33	.302E+02	.1	1.05	5.61
.12	424.37	.469E+02	.2	1.33	4.42
.16	424.41	.647E+02	.3	1.57	3.76
.20	424.45	.837E+02	.4	1.77	3.34
.24	424.49	.104E+03	.6	1.94	3.04
.28	424.53	.125E+03	.7	2.10	2.81
.32	424.57	.147E+03	.9	2.23	2.64
.36	424.61	.170E+03	1.1	2.36	2.50
.39	424.64	.195E+03	1.4	2.47	2.39
.43	424.68	.220E+03	1.6	2.57	2.30
.47	424.72	.247E+03	1.9	2.66	2.22
.51	424.76	.275E+03	2.1	2.75	2.15
.55	424.80	.304E+03	2.4	2.83	2.09
.59	424.84	.334E+03	2.7	2.90	2.04
.63	424.88	.365E+03	3.1	2.97	1.99
.67	424.92	.397E+03	3.4	3.03	1.95
.71	424.96	.430E+03	3.8	3.09	1.91
.75	425.00	.465E+03	4.1	3.14	1.88

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0054)	15.86	2.50	11.92	35.39	.56	2.84
OUTFLOW: ID= 1 (0056)	15.86	2.64	12.00	35.39	.58	2.87

ADD HYD (0057)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0055):	5.19	1.150	11.83	59.20
+ ID2= 2 (0056):	15.86	2.638	12.00	35.39
=====				
ID = 3 (0057):	21.05	3.285	12.00	41.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0058)
ID= 1 DT= 5.0 min

Area (ha)= 21.77 Curve Number (CN)= 67.4
Ia (mm)= 5.22 # of Linear Res.(N)= 3.00

----- U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= 2.354

PEAK FLOW (cms)= 2.189 (i)
TIME TO PEAK (hrs)= 12.083
RUNOFF VOLUME (mm)= 51.600
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .450

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0059) | Area (ha)= 11.96 Curve Number (CN)= 66.4
ID= 1 DT= 5.0 min | Ia (mm)= 5.74 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .18

Unit Hyd Qpeak (cms)= 2.557

PEAK FLOW (cms)= 1.742 (i)
TIME TO PEAK (hrs)= 11.917
RUNOFF VOLUME (mm)= 49.852
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .435

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0060) |
IN= 2---> OUT= 1 |
DT= 5.0 min
OUTFLOW (cms) | STORAGE (ha.m.) | OUTFLOW (cms) | STORAGE (ha.m.)
.0000 | .0000 | 20.0000 | .1583
.0001 | .1573 | .0000 | .0000

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW : ID= 2 (0059) 11.96 1.74 11.92 49.85
OUTFLOW: ID= 1 (0060) 11.96 1.92 12.00 36.70

PEAK FLOW REDUCTION [Qout/Qin](%)=110.09
TIME SHIFT OF PEAK FLOW (min)= 5.00
MAXIMUM STORAGE USED (ha.m.)= .3041

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

CALIB NASHYD (0061) | Area (ha)= 3.90 Curve Number (CN)= 69.4
ID= 1 DT= 5.0 min | Ia (mm)= 4.85 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .08

Unit Hyd Qpeak (cms)= 1.935

PEAK FLOW (cms)= .870 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 50.889
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .444

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0062) |
1 + 2 = 3
ID1= 1 (0060): AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
+ ID2= 2 (0061): 11.96 1.918 12.00 36.70
3.90 .870 11.75 50.89
=====

ID = 3 (0062): 15.86 2.240 12.00 40.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0063) |
IN= 2---> OUT= 1 |
DT= 5.0 min
OUTFLOW (cms) | STORAGE (ha.m.) | OUTFLOW (cms) | STORAGE (ha.m.)
.0000 | .0000 | 20.0000 | .0771
.0001 | .0761 | .0000 | .0000

AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)

INFLOW : ID= 2 (0062) (ha) (cms) (hrs) (mm)
 15.86 2.24 12.00 40.19
 OUTFLOW: ID= 1 (0063) 15.86 2.50 11.92 35.39

PEAK FLOW REDUCTION [Qout/Qin](%)=111.63
 TIME SHIFT OF PEAK FLOW (min)=-5.00
 MAXIMUM STORAGE USED (ha.m.)= .3757

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ROUTE CHN (0065) |
 IN= 2----> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.5) ----->
 Distance Elevation Manning
 .00 425.00 .0300
 .75 424.25 .0300 / .0300 Main Channel
 1.75 424.25 .0300 / .0300 Main Channel
 2.50 425.00 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .04 424.29 .145E+02 .0 .68 8.63
 .08 424.33 .302E+02 .1 1.05 5.61
 .12 424.37 .469E+02 .2 1.33 4.42
 .16 424.41 .647E+02 .3 1.57 3.76
 .20 424.45 .837E+02 .4 1.77 3.34
 .24 424.49 .104E+03 .6 1.94 3.04
 .28 424.53 .125E+03 .7 2.10 2.81
 .32 424.57 .147E+03 .9 2.23 2.64
 .36 424.61 .170E+03 1.1 2.36 2.50
 .39 424.64 .195E+03 1.4 2.47 2.39
 .43 424.68 .220E+03 1.6 2.57 2.30
 .47 424.72 .247E+03 1.9 2.66 2.22
 .51 424.76 .275E+03 2.1 2.75 2.15
 .55 424.80 .304E+03 2.4 2.83 2.09
 .59 424.84 .334E+03 2.7 2.90 2.04
 .63 424.88 .365E+03 3.1 2.97 1.99
 .67 424.92 .397E+03 3.4 3.03 1.95
 .71 424.96 .430E+03 3.8 3.09 1.91
 .75 425.00 .465E+03 4.1 3.14 1.88

<---- hydrograph ----> <-pipe / channel-->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0063) 15.86 2.50 11.92 35.39 .56 2.84
 OUTFLOW: ID= 1 (0065) 15.86 2.64 12.00 35.39 .58 2.87

CALIB NASHYD (0064) | Area (ha)= 5.19 Curve Number (CN)= 73.3
 ID= 1 DT= 5.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= 1.777

PEAK FLOW (cms)= 1.150 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 59.205
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .516

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0066) | AREA QPEAK TPEAK R.V.
 1 + 2 = 3 | (ha) (cms) (hrs) (mm)
 ID1= 1 (0065): 15.86 2.638 12.00 35.39
 + ID2= 2 (0064): 5.19 1.150 11.83 59.20
 ID = 3 (0066): 21.05 3.285 12.00 41.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0069) | Area (ha)= 1.80 Curve Number (CN)= 58.8
 ID= 1 DT= 5.0 min | Ia (mm)= 8.49 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= .07

Unit Hyd Qpeak (cms)= 1.005

PEAK FLOW (cms)= .294 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 35.940
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .313

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
NASHYD (0067)	Area (ha)=	1.52	Curve Number (CN)=	62.0
ID= 1 DT= 5.0 min	Ia (mm)=	8.00	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.06		

Unit Hyd Qpeak (cms)= .995

PEAK FLOW (cms)= .277 (i)
TIME TO PEAK (hrs)= 11.750
RUNOFF VOLUME (mm)= 36.689
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .320

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0068)				
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	.0000	.0000	20.0000	.0207
	.0001	.0206	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0067)	1.52	.28	11.75	36.69
OUTFLOW: ID= 1 (0068)	1.52	.32	11.92	23.18

PEAK FLOW REDUCTION [Qout/Qin](%)=115.72
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= .0383

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ADD HYD (0071)				
1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0069):	1.80	.294	11.75	35.94
+ ID2= 2 (0068):	1.52	.321	11.92	23.18
ID = 3 (0071):	3.32	.478	11.92	30.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0070)				
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	.0000	.0000	20.0000	.0708
	.0001	.0707	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0071)	3.32	.48	11.92	30.09
OUTFLOW: ID= 1 (0070)	3.32	.04	13.75	8.80

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.40
TIME SHIFT OF PEAK FLOW (min)=110.00
MAXIMUM STORAGE USED (ha.m.)= .0915

ROUTE CHN (0073)
IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.6) ----->				
Distance	Elevation	Manning		
.00	421.26	.0300		
1.10	420.66	.0300 / .0300		Main Channel
2.00	420.66	.0300 / .0300		Main Channel
3.10	421.26	.0300		

----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	420.69	.560E+01	.0	.05	59.24
.06	420.72	.119E+02	.0	.09	35.98
.09	420.75	.188E+02	.0	.12	26.61
.13	420.79	.265E+02	.0	.14	21.37
.16	420.82	.348E+02	.0	.17	17.97
.19	420.85	.437E+02	.0	.20	15.58
.22	420.88	.534E+02	.1	.22	13.79
.25	420.91	.637E+02	.1	.25	12.40
.28	420.94	.748E+02	.1	.27	11.29
.32	420.98	.864E+02	.1	.30	10.38
.35	421.01	.988E+02	.2	.32	9.61
.38	421.04	.112E+03	.2	.34	8.96
.41	421.07	.126E+03	.2	.37	8.41
.44	421.10	.140E+03	.3	.39	7.92
.47	421.13	.155E+03	.3	.41	7.50
.51	421.17	.171E+03	.4	.43	7.12
.54	421.20	.187E+03	.5	.45	6.78
.57	421.23	.204E+03	.5	.48	6.48
.60	421.26	.222E+03	.6	.50	6.21

	<---- hydrograph ---->			<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH
	(ha)	(cms)	(hrs)	(mm)	(m)
INFLOW : ID= 2 (0070)	3.32	.04	13.75	8.80	.18
OUTFLOW: ID= 1 (0073)	3.32	.02	14.08	8.66	.18

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

ADD HYD (0074)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0066):	21.05	3.285	12.00	41.26	
+ ID2= 2 (0073):	3.32	.022	14.08	8.66	
=====					
ID = 3 (0074):	24.37	3.285	12.00	36.82	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB					
NASHYD (0072)					
ID= 1 DT= 5.0 min					
	Area	(ha)=	Curve Number	(CN)=	
	Ia	(mm)=	# of Linear Res.(N)=	3.00	
	U.H.	Tp(hrs)=			
	24.19		60.0		
	8.62		3.00		
		.37			

Unit Hyd Qpeak (cms)= 2.505

PEAK FLOW (cms)= 1.833 (i)
 TIME TO PEAK (hrs)= 12.167
 RUNOFF VOLUME (mm)= 40.764
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .356

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0075)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0074):	24.37	3.285	12.00	36.82	
+ ID2= 2 (0072):	24.19	1.833	12.17	40.76	
=====					
ID = 3 (0075):	48.56	4.985	12.00	38.79	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB					
NASHYD (0076)					
ID= 1 DT= 5.0 min					
	Area	(ha)=	Curve Number	(CN)=	
	Ia	(mm)=	# of Linear Res.(N)=	3.00	
	U.H.	Tp(hrs)=			
	127.28		59.9		
	8.29		3.00		
		.79			

Unit Hyd Qpeak (cms)= 6.192

PEAK FLOW (cms)= 5.701 (i)
 TIME TO PEAK (hrs)= 12.583
 RUNOFF VOLUME (mm)= 40.934
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .357

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB          |
| NASHYD (0077) | Area (ha)= 17.28 Curve Number (CN)= 58.3
| ID= 1 DT= 5.0 min | Ia (mm)= 9.24 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= .57
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Unit Hyd Qpeak (cms)= 1.154

PEAK FLOW (cms)= .918 (i)
 TIME TO PEAK (hrs)= 12.333
 RUNOFF VOLUME (mm)= 38.708
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB          |
| NASHYD (0082) | Area (ha)= .24 Curve Number (CN)= 77.6
| ID= 1 DT= 5.0 min | Ia (mm)= 3.49 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= .11
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Unit Hyd Qpeak (cms)= .081

PEAK FLOW (cms)= .059 (i)
 TIME TO PEAK (hrs)= 11.833
 RUNOFF VOLUME (mm)= 65.801
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .574

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB          |
| NASHYD (0078) | Area (ha)= 2.66 Curve Number (CN)= 59.8
| ID= 1 DT= 5.0 min | Ia (mm)= 8.55 # of Linear Res.(N)= 3.00
|                | U.H. Tp(hrs)= .07
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Unit Hyd Qpeak (cms)= 1.418

PEAK FLOW (cms)= .442 (i)
 TIME TO PEAK (hrs)= 11.750
 RUNOFF VOLUME (mm)= 37.332
 TOTAL RAINFALL (mm)= 114.644
 RUNOFF COEFFICIENT = .326

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR (0079) |
| IN= 2--> OUT= 1 |
| DT= 5.0 min      |
|-----|-----|
|                | OUTFLOW | STORAGE | OUTFLOW | STORAGE |
|                | (cms)   | (ha.m.) | (cms)   | (ha.m.) |
|                | .0000   | .0000   | 20.0000 | .0608   |
|                | .0001   | .0607   | .0000   | .0000   |
|-----|-----|
|                | AREA    | QPEAK   | TPEAK   | R.V.    |
|                | (ha)    | (cms)   | (hrs)   | (mm)    |
| INFLOW : ID= 2 (0078) | 2.66   | .44    | 11.75   | 37.33   |
| OUTFLOW: ID= 1 (0079) | 2.66   | .10    | 12.42   | 14.51   |
|                | PEAK FLOW REDUCTION [Qout/Qin](%)= 22.04 |
|                | TIME SHIFT OF PEAK FLOW (min)= 40.00 |
|                | MAXIMUM STORAGE USED (ha.m.)= .0795 |
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| ADD HYD (0083) |
| 1 + 2 = 3      |
|-----|-----|
| ID1= 1 (0082): | AREA    | QPEAK   | TPEAK   | R.V.    |
|                | (ha)    | (cms)   | (hrs)   | (mm)    |
| + ID2= 2 (0079): | .24    | .059    | 11.83   | 65.80   |
|                | 2.66   | .097    | 12.42   | 14.51   |
|-----|-----|
| ID = 3 (0083): | 2.90   | .105    | 12.42   | 18.71   |
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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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| CALIB          |
| NASHYD (0080) | Area (ha)= 14.63 Curve Number (CN)= 58.0
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|ID= 1 DT= 5.0 min | Ia (mm)= 9.37 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .57

Unit Hyd Qpeak (cms)= .977

PEAK FLOW (cms)= .770 (i)
TIME TO PEAK (hrs)= 12.333
RUNOFF VOLUME (mm)= 38.359
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .335

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0081) |
1 + 2 = 3
ID1= 1 (0083): AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)
+ ID2= 2 (0080): 2.90 .105 12.42 18.71
14.63 .770 12.33 38.36
=====

ID = 3 (0081): 17.52 .874 12.42 35.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB |
| NASHYD (0084) | Area (ha)= 7.71 Curve Number (CN)= 62.5
|ID= 1 DT= 5.0 min | Ia (mm)= 9.14 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .29

Unit Hyd Qpeak (cms)= 1.012

PEAK FLOW (cms)= .722 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 43.086
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .376

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0085) | Area (ha)= .91 Curve Number (CN)= 64.9
|ID= 1 DT= 5.0 min | Ia (mm)= 8.53 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .11

Unit Hyd Qpeak (cms)= .313

PEAK FLOW (cms)= .154 (i)
TIME TO PEAK (hrs)= 11.833
RUNOFF VOLUME (mm)= 45.391
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .396

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0086) | Area (ha)= 19.15 Curve Number (CN)= 71.3
|ID= 1 DT= 5.0 min | Ia (mm)= 5.81 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= 2.995

PEAK FLOW (cms)= 2.647 (i)
TIME TO PEAK (hrs)= 12.000
RUNOFF VOLUME (mm)= 56.028
TOTAL RAINFALL (mm)= 114.644
RUNOFF COEFFICIENT = .489

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

FINISH
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Appendix D
Rational Method Calculations
for Roadside Ditches

Table D-1: Peak Flows (Qp) to Roadside Ditches for 10-year Design Storm Event																	
Ditch ID	Ditch Sub-section ID	Total Drainage Area to Ditch (m ²)	Rational Method								Existing Ditch Dimension (estimated)					Maximum Ditch Capacity (m ³ /s) based on Manning's Eqn	Does existing ditch have sufficient capacity? (Yes/No)
			Total Drainage Area to Ditch (ha)	Area-weighted C	IDF Parameter A (10-year)	IDF Parameter b (10-year)	IDF Parameter c (10-year)	t = T _c (min)	Intensity (mm/hr) where I=A/(t + B) ^C	Peak Flow to Ditches Q _p = 0.0027778CiA (m ³ /s)	Estimated Top Width (m)	Estimated Depth	Side Slope (H:V)	Estimated Bottom Width (m)	Long Slope (m/m)		
B10	A	5665	0.57	0.426	1219.9	7.84	0.8073	17.4	90.14	0.06	1.8	0.25	2.5	0.5	0.016	0.34	Yes
B10	B	26705	2.67	0.388	1219.9	7.84	0.8073	19.1	85.39	0.25	1.8	0.25	2.5	0.5	0.035	0.51	Yes
B15	A	4069	0.41	0.406	1219.9	7.84	0.8073	15.9	94.68	0.04	7.0	0.49	4.1	3.0	0.090	12.1	Yes
B18	A	1563	0.16	0.607	1219.9	7.84	0.8073	15.8	95.01	0.03	9.5	0.66	5.0	2.9	0.020	11.0	Yes
B20	A	19120	1.91	0.498	1219.9	7.84	0.8073	17.0	91.09	0.24	3.7	0.84	2.2	0.0	0.035	5.04	Yes
B25	A	4352	0.44	0.446	1219.9	7.84	0.8073	15.4	96.34	0.05	1.9	0.40	1.7	0.6	0.038	1.25	Yes
B25	B	9799	0.98	0.427	1219.9	7.84	0.8073	16.0	94.20	0.11	1.9	0.40	1.7	0.6	0.084	1.85	Yes
B30	A	18397	1.84	0.415	1219.9	7.84	0.8073	16.2	93.75	0.20	2.2	0.55	1.5	0.6	0.004	0.65	Yes
B35	A	7916	0.79	0.435	1219.9	7.84	0.8073	15.0	97.60	0.09	0.4	0.34	0.6	0.0	0.020	0.06	No
M10	A	29457	2.95	0.376	1219.9	7.84	0.8073	18.8	86.31	0.27	2.0	0.30	0.5	1.3	0.060	1.24	Yes
M10	B	204158	20.42	0.364	1219.9	7.84	0.8073	20.1	83.03	1.71	3.1	1.32	1.0	0.0	0.016	4.14	Yes
M10	C	204660	20.47	0.365	1219.9	7.84	0.8073	20.7	81.58	1.69	3.1	1.32	1.0	0.0	0.027	5.37	Yes
M100	A	456	0.05	0.652	1219.9	7.84	0.8073	16.2	93.54	0.01	1.5	0.40	0.0	1.5	0.011	0.84	Yes
M105	A	2534	0.25	0.312	1219.9	7.84	0.8073	15.7	95.21	0.02	2.0	0.24	4.2	0.0	0.005	0.14	Yes
M105	B	4807	0.48	0.318	1219.9	7.84	0.8073	16.4	93.04	0.04	2.0	0.24	4.2	0.0	0.014	0.22	Yes
M110	A	6246	0.62	0.337	1219.9	7.84	0.8073	15.5	95.93	0.06	1.0	0.10	3.0	0.4	0.017	0.05	No
M110	B	7659	0.77	0.345	1219.9	7.84	0.8073	15.9	94.75	0.07	1.0	0.10	3.0	0.4	0.039	0.08	Yes
M110	C	9826	0.98	0.358	1219.9	7.84	0.8073	16.5	92.80	0.09	1.0	0.10	3.0	0.4	0.017	0.05	No
M110	D	22856	2.29	0.361	1219.9	7.84	0.8073	23.6	75.31	0.17	1.0	0.10	3.0	0.4	0.006	0.03	No
M115	A	644	0.06	0.608	1219.9	7.84	0.8073	15.8	94.78	0.01	1.1	0.15	0.3	1.0	0.041	0.26	Yes
M115	B	1405	0.14	0.639	1219.9	7.84	0.8073	17.2	90.65	0.02	1.1	0.15	0.3	1.0	0.022	0.19	Yes
M115	C	77101	7.71	0.301	1219.9	7.84	0.8073	25.6	71.72	0.46	1.1	0.15	0.3	1.0	0.004	0.08	No
M120	A	981	0.10	0.624	1219.9	7.84	0.8073	17.2	90.50	0.02	No ditch evident observed in field					0	No ditch evident
M125	A	9092	0.91	0.307	1219.9	7.84	0.8073	16.3	93.43	0.07	1.2	0.31	1.9	0	0.012	0.18	Yes
M130	A	601	0.06	0.705	1219.9	7.84	0.8073	17.1	90.97	0.01	No ditch evident observed in field					0	No ditch evident
M140	A	2035	0.20	0.746	1219.9	7.84	0.8073	19.1	85.44	0.04	1.0	0.35	0.7	0.5	0.020	0.42	Yes
M145	A	2327	0.23	0.433	1219.9	7.84	0.8073	16.1	93.84	0.03	No ditch evident observed in field					0	No ditch evident
M15	A	3800	0.38	0.607	1219.9	7.84	0.8073	17.3	90.21	0.06	2.0	0.30	2.0	1.3	0.060	1.62	Yes
M15	B	7456	0.75	0.546	1219.9	7.84	0.8073	18.7	86.50	0.10	1.9	0.60	1.0	0.7	0.052	2.82	Yes
M15	C	28256	2.83	0.426	1219.9	7.84	0.8073	23.5	75.50	0.25	2.0	0.68	1.0	0.6	0.018	2.01	Yes
M150	A	2178	0.22	0.661	1219.9	7.84	0.8073	17.7	89.12	0.04	1.7	0.48	1.0	0.7	0.039	1.62	Yes
M155	A	10650	1.07	0.317	1219.9	7.84	0.8073	15.9	94.71	0.09	2.1	0.60	1.3	0.6	0.035	2.38	Yes
M155	B	14048	1.40	0.332	1219.9	7.84	0.8073	16.7	92.12	0.12	2.1	0.60	1.3	0.6	0.053	2.92	Yes
M20	A	815	0.08	0.572	1219.9	7.84	0.8073	15.6	95.59	0.01	1.0	0.70	0.5	0	0.041	0.48	Yes
M20	B	1662	0.17	0.667	1219.9	7.84	0.8073	16.5	92.77	0.03	1.0	0.70	0.5	0	0.037	0.46	Yes
M25	A	15338	1.53	0.380	1219.9	7.84	0.8073	15.6	95.56	0.15	1.7	0.30	2.8	0	0.039	0.46	Yes
M25	B	26607	2.66	0.408	1219.9	7.84	0.8073	18.9	85.88	0.26	1.7	0.30	2.8	0	0.009	0.22	No
M25	C	28466	2.85	0.419	1219.9	7.84	0.8073	19.6	84.26	0.28	1.7	0.30	2.8	0	0.025	0.36	Yes
M25	D	47310	4.73	0.401	1219.9	7.84	0.8073	20.2	82.65	0.44	1.7	0.30	2.8	0	0.014	0.27	No
M30	A	872	0.09	0.538	1219.9	7.84	0.8073	15.0	97.60	0.01	No ditch evident observed in field					0	No ditch evident
M40	A	4705	0.47	0.381	1219.9	7.84	0.8073	16.9	91.56	0.05	1.5	0.30	0.5	1.2	0.020	0.70	Yes
M40	B	5824	0.58	0.419	1219.9	7.84	0.8073	17.9	88.69	0.06	1.5	0.30	0.5	1.2	0.058	1.17	Yes
M40	C	18624	1.86	0.359	1219.9	7.84	0.8073	20.8	81.34	0.15	1.8	0.33	2.7	0	0.010	0.28	Yes
M40	D	21576	2.16	0.399	1219.9	7.84	0.8073	25.4	72.05	0.17	3.1	0.60	1.8	0.9	0.022	2.99	Yes
M45	A	1627	0.16	0.609	1219.9	7.84	0.8073	17.1	90.79	0.02	2.5	0.75	1.0	1.0	0.034	4.49	Yes
M45	B	3296	0.33	0.558	1219.9	7.84	0.8073	17.9	88.68	0.05	4.7	1.26	1.4	1.1	0.024	14.2	Yes
M45	C	201430	20.14	0.355	1219.9	7.84	0.8073	26.3	70.48	1.40	2.1	0.65	0.8	1.0	0.020	2.43	Yes
M45	D	206080	20.61	0.357	1219.9	7.84	0.8073	29.5	65.60	1.34	2.1	0.65	0.8	1.0	0.006	1.31	No

M50	A	5713	0.57	0.434	1219.9	7.84	0.8073	16.8	91.93	0.06	1.9	0.40	1.5	0.7	0.027	1.10	Yes
M55	A	11683	1.17	0.386	1219.9	7.84	0.8073	15.4	96.29	0.12	1.2	0.33	1.2	0.4	0.023	0.43	Yes
M65	A	30449	3.04	0.345	1219.9	7.84	0.8073	16.6	92.32	0.27	2.0	0.60	1.3	0.5	0.010	1.15	Yes
M65	B	173842	17.38	0.325	1219.9	7.84	0.8073	31.7	62.63	0.98	2.0	0.60	1.3	0.5	0.003	0.61	No
M65	C	174445	17.44	0.327	1219.9	7.84	0.8073	32.4	61.82	0.98	2.0	0.60	1.3	0.5	0.054	2.65	Yes
M65	D	175927	17.59	0.329	1219.9	7.84	0.8073	36.4	57.24	0.92	2.0	0.60	1.3	0.5	0.010	1.13	Yes
M75	A	1628	0.16	0.587	1219.9	7.84	0.8073	16.2	93.72	0.02	2.2	0.20	5.5	0	0.020	0.22	Yes
M80	A	1387	0.14	0.443	1219.9	7.84	0.8073	15.0	97.60	0.02	1.6	0.13	6.2	0	0.029	0.10	Yes
M80	B	1721	0.17	0.494	1219.9	7.84	0.8073	15.5	95.95	0.02	1.6	0.13	6.2	0	0.029	0.10	Yes
M85	A	649	0.06	0.655	1219.9	7.84	0.8073	16.6	92.44	0.01	No ditch evident observed in field					0	No ditch evident
M90	A	2424	0.24	0.585	1219.9	7.84	0.8073	17.5	89.66	0.04	2.2	0.32	3.4	0	0.024	0.52	Yes
M95	A	937	0.09	0.597	1219.9	7.84	0.8073	18.2	87.75	0.01	1.4	0.18	0.0	1.4	0.017	0.30	Yes
M95	B	170396	17.04	0.286	1219.9	7.84	0.8073	28.9	66.42	0.90	1.4	0.18	0.0	1.4	0.017	0.30	No
M60	A	21612	2.16	0.467	1219.9	7.84	0.8073	23.7	75.26	0.21	2.1	0.35	2.0	0.7	0.003	0.29	Yes
M60	B	22586	2.26	0.474	1219.9	7.84	0.8073	24.9	72.99	0.22	2.1	0.35	2.0	0.7	0.042	1.20	Yes
M60	C	492954	49.30	0.391	1219.9	7.84	0.8073	54.8	43.24	2.31	2.5	0.60	2.1	0	0.005	0.71	No
M70	A	607	0.06	0.696	1219.9	7.84	0.8073	16.0	94.15	0.01	1.5	0.60	0.6	0.8	0.025	1.12	Yes

Table D-3: Runoff Coefficient C for Areas Draining to Roadside Ditches

Ditch ID	Ditch Sub-section ID	Total Drainage Area to Ditch (m ²)	Total Drainage Area to Ditch (ha)	Land Use Breakdown						Runoff Coefficient C ¹						Area-weighted C
				Pond Area (m ²)	Forest Area (m ²)	Woodland Area (m ²)	Crop Area (m ²)	Grassed Area (m ²)	Impervious Area (m ²)	Pond	Forest	Woodland	Crop	Grassed Area	Impervious Area	
B10	A	5665	0.57	0	0	0	4947	0	719	0.05	0.25	0.25	0.35	0.28	0.95	0.426
B10	B	26705	2.67	0	0	0	25022	0	1670	0.05	0.25	0.25	0.35	0.28	0.95	0.388
B15	A	4069	0.41	0	0	1271	2208	0	591	0.05	0.25	0.25	0.35	0.28	0.95	0.406
B18	A	1563	0.16	0	0	0	0	894	669	0.05	0.30	0.30	0.45	0.35	0.95	0.607
B20	A	19120	1.91	0	0	0	0	14391	4729	0.05	0.30	0.30	0.45	0.35	0.95	0.498
B25	A	4352	0.44	0	0	0	0	3277	1075	0.05	0.25	0.25	0.35	0.28	0.95	0.446
B25	B	9799	0.98	0	0	1349	2435	4050	1959	0.05	0.25	0.25	0.35	0.28	0.95	0.427
B30	A	18397	1.84	0	0	0	0	16398	1999	0.05	0.30	0.30	0.45	0.35	0.95	0.415
B35	A	7916	0.79	0	0	0	0	6085	1831	0.05	0.25	0.25	0.35	0.28	0.95	0.435
M10	A	29457	2.95	0	0	15211	0	11684	2558	0.05	0.30	0.30	0.45	0.35	0.95	0.376
M10	B	204158	20.42	0	0	138450	0	49409	16209	0.05	0.30	0.30	0.45	0.35	0.95	0.364
M10	C	204660	20.47	0	0	138450	0	49628	16486	0.05	0.30	0.30	0.45	0.35	0.95	0.365
M100	A	456	0.05	0	0	209	0	0	247	0.05	0.30	0.30	0.45	0.35	0.95	0.652
M105	A	2534	0.25	0	0	2310	0	0	224	0.05	0.25	0.25	0.45	0.28	0.95	0.312
M105	B	4807	0.48	0	0	2310	0	2137	375	0.05	0.25	0.25	0.45	0.28	0.95	0.318
M110	A	6246	0.62	0	0	5466	0	0	780	0.05	0.25	0.25	0.35	0.28	0.95	0.337
M110	B	7659	0.77	0	0	6616	0	0	1040	0.05	0.25	0.25	0.35	0.28	0.95	0.345
M110	C	9826	0.98	0	0	6616	0	1772	1438	0.05	0.25	0.25	0.35	0.28	0.95	0.358
M110	D	22856	2.29	0	0	12366	0	7162	3334	0.05	0.25	0.25	0.35	0.28	0.95	0.361
M115	A	644	0.06	0	0	315	0	0	329	0.05	0.25	0.25	0.45	0.28	0.95	0.608
M115	B	1405	0.14	0	0	626	0	0	783	0.05	0.25	0.25	0.45	0.28	0.95	0.639
M115	C	77101	7.71	0	0	65265	0	6475	5355	0.05	0.25	0.25	0.45	0.28	0.95	0.301
M120	A	981	0.10	0	0	492	0	0	489	0.05	0.30	0.30	0.45	0.35	0.95	0.624
M125	A	9092	0.91	0	0	8357	0	0	735	0.05	0.30	0.25	0.45	0.35	0.95	0.307
M130	A	601	0.06	0	0	227	0	0	374	0.05	0.30	0.30	0.45	0.35	0.95	0.705
M140	A	2035	0.20	0	0	637	0	0	1398	0.05	0.30	0.30	0.45	0.35	0.95	0.746
M145	A	2327	0.23	0	0	1852	0	0	474	0.05	0.30	0.30	0.45	0.35	0.95	0.433
M15	A	3800	0.38	0	0	0	0	2170	1631	0.05	0.30	0.30	0.45	0.35	0.95	0.607
M15	B	7456	0.75	0	0	0	2870	2170	2451	0.05	0.30	0.30	0.35	0.35	0.95	0.546
M15	C	28256	2.83	0	0	491	21996	2170	3638	0.05	0.30	0.30	0.35	0.35	0.95	0.426
M150	A	2178	0.22	0	0	967	0	0	1211	0.05	0.30	0.30	0.45	0.35	0.95	0.661
M155	A	10650	1.07	0	0	9630	0	0	1020	0.05	0.30	0.25	0.45	0.35	0.95	0.317
M155	B	14048	1.40	0	0	12420	0	0	1642	0.05	0.30	0.25	0.45	0.35	0.95	0.332
M20	A	815	0.08	0	0	474	0	0	341	0.05	0.30	0.30	0.45	0.35	0.95	0.572
M20	B	1662	0.17	0	0	474	0	270	917	0.05	0.30	0.30	0.45	0.35	0.95	0.667
M25	A	15338	1.53	0	0	1493	10042	2906	897	0.05	0.30	0.30	0.35	0.35	0.95	0.380
M25	B	26607	2.66	0	0	1493	10042	12366	2702	0.05	0.30	0.30	0.35	0.35	0.95	0.408
M25	C	28466	2.85	0	0	1493	10042	13548	3377	0.05	0.30	0.30	0.35	0.35	0.95	0.419
M25	D	47310	4.73	801	0	4041	10042	27690	4731	0.05	0.30	0.30	0.35	0.35	0.95	0.401
M30	A	872	0.09	0	0	553	0	0	319	0.05	0.30	0.30	0.45	0.35	0.95	0.538
M40	A	4705	0.47	0	0	2916	0	1060	729	0.05	0.30	0.25	0.45	0.35	0.95	0.381
M40	B	5824	0.58	0	0	3508	0	1060	1255	0.05	0.30	0.25	0.45	0.35	0.95	0.419
M40	C	18624	1.86	0	0	3508	0	12766	2362	0.05	0.30	0.25	0.45	0.28	0.95	0.359
M40	D	21576	2.16	0	0	3508	0	14098	3992	0.05	0.30	0.25	0.45	0.28	0.95	0.399
M45	A	1627	0.16	0	0	854	0	0	773	0.05	0.30	0.30	0.45	0.35	0.95	0.609
M45	B	3296	0.33	0	0	854	0	1230	1212	0.05	0.30	0.30	0.45	0.35	0.95	0.558
M45	C	201430	20.14	3510	0	29582	138562	23752	6034	0.05	0.30	0.30	0.35	0.35	0.95	0.355
M45	D	206080	20.61	3510	0	29582	142676	23752	6560	0.05	0.30	0.30	0.35	0.35	0.95	0.357
M50	A	5713	0.57	0	0	0	4916	0	797	0.05	0.30	0.30	0.35	0.35	0.95	0.434
M55	A	11683	1.17	0	0	0	10981	0	702	0.05	0.30	0.30	0.35	0.35	0.95	0.386
M65	A	30449	3.04	0	0	12274	16371	0	1804	0.05	0.25	0.25	0.35	0.28	0.95	0.345
M65	B	173842	17.38	0	0	59039	104686	6617	3500	0.05	0.25	0.25	0.35	0.28	0.95	0.325
M65	C	174445	17.44	0	0	59039	104686	6902	3815	0.05	0.25	0.25	0.35	0.28	0.95	0.327
M65	D	175927	17.59	0	0	59780	104686	6902	4554	0.05	0.25	0.25	0.35	0.28	0.95	0.329
M75	A	1628	0.16	0	0	0	0	984	644	0.05	0.30	0.30	0.45	0.35	0.95	0.587
M80	A	1387	0.14	0	0	0	0	1049	338	0.05	0.30	0.30	0.45	0.28	0.95	0.443
M80	B	1721	0.17	0	0	0	0	1172	549	0.05	0.30	0.30	0.45	0.28	0.95	0.494
M85	A	649	0.06	0	0	0	0	319	330	0.05	0.30	0.30	0.45	0.35	0.95	0.655
M90	A	2424	0.24	0	0	0	0	1473	951	0.05	0.30	0.30	0.45	0.35	0.95	0.585
M95	A	937	0.09	0	0	0	0	494	443	0.05	0.25	0.25	0.35	0.28	0.95	0.597
M95	B	170396	17.04	1210	0	128315	13353	18895	6254	0.05	0.25	0.25	0.35	0.28	0.95	0.286
M60	A	21612	2.16	0	0	4956	12217	1859	2579	0.05	0.30	0.30	0.45	0.35	0.95	0.467
M60	B	22586	2.26	0	0	5412	12217	1859	3097	0.05	0.30	0.30	0.45	0.35	0.95	0.474
M60	C	492954	49.30	3513	0	143153	167668	160329	19089	0.05	0.30	0.30	0.45	0.35	0.95	0.391
M70	A	607	0.06	0	0	0	0	257	350	0.05	0.30	0.30	0.45	0.35	0.95	0.696

Table D-4: IDF Values (CVC Guidelines)						
IDF Values (ABOVE the escarpment)						
Duration (min)	2yr	5yr	10yr	25yr	50yr	100yr
5	102	135	155	180	200	220
10	80	100	115	135	145	160
15	64	85	99	117	130	140
30	41	58	70	85	96	107
60	24	34	40	49	55	61
120	16	21	24	29	32	35
360	6.3	8.3	9.7	11	13	14
720	3.9	5.1	5.9	6.9	7.6	8.3
1440	2.4	3.1	3.6	4.2	4.7	5.1
$I = A / (t + B)^C$						
Parameter A	637.5921	993.47959	1219.92	1637.321	1871.883	2118.166
Parameter B	5.3	7.14	7.84	9.35	10.04	10.31
Parameter C	0.772434	0.7987811	0.80732	0.828517	0.830688	0.836766

Appendix E
Culvert Master Input Parameters
for Cross Culverts

Table E-1: Culvert Master Parameters for Cross Culverts													
Culvert ID #	Size/Height (m)	Slope (m/m)	Length (m)	Invert Elevation (m)		Obvert Elevation (m)		At U/S Obvert		At Top of Road			Notes
				U/S	D/S	U/S	D/S	Elevation (m)	Modelled Flow (m ³ /s)	Elevation (m)	Modelled Flow (m ³ /s)	Level of Service (Return Period)	
10	0.45	0.0168	13.3	382.71	382.48	383.16	382.93	383.16	0.133	383.34	0.227	10-year	
17	0.30	0.0348	10.3	384.68	384.33	384.98	384.63	384.98	0.048	385.30	0.116	Less than 2-year	
24	0.40	0.0320	15.3	428.30	427.82	428.70	428.22	428.70	0.094	429.24	0.216	2-year	Size modelled as 375mm
37	0.60	0.0306	12.5	418.80	418.41	419.40	419.01	419.40	0.274	419.99	0.639	5-year	
43	0.55	0.0135	12.6	400.13	399.96	400.68	400.51	400.68	0.352	400.88	0.549	2-year	Size modelled as 525mm
44	1.20	0.0138	13.8	399.46	399.27	400.66	400.47	400.66	1.356	400.76	1.687	10-year	
44	1.20	0.0097	13.8	399.44	399.31	400.64	400.51	400.64	1.156	400.76	1.603	10-year	
47	0.40	0.0173	12.2	398.17	397.96	398.57	398.36	398.57	0.098	398.98	0.184	100-year	Size modelled as 375mm
48	0.40	0.0198	12.5	394.08	393.84	394.48	394.24	394.48	0.098	394.95	0.189	2-year	Size modelled as 375mm
55	0.30	0.0261	12.4	388.76	388.43	389.06	388.73	389.06	0.048	389.39	0.106	Less than 2-year	
56	0.30	0.0041	11.5	387.26	387.21	387.56	387.51	387.56	0.044	388.16	0.109	25-year	
14	0.60	0.0285	17.2	380.43	379.94	381.03	380.54	381.03	0.274	381.62	0.639	10-year	
16	0.30	0.0557	16.3	386.15	385.25	386.45	385.55	386.45	0.048	386.86	0.128	Less than 2-year	
2	0.90	0.0172	34.0	387.32	386.73	388.22	387.63	388.22	0.754	394.32	3.486	100-year	

Appendix F
Culvert Master Outputs
for Cross Culverts

Culvert # 2

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	388.39 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	388.30 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	388.39 m	Control Type	Entrance Control
Headwater Depth/Height	1.17		
Grades			
Upstream Invert	387.32 m	Downstream Invert	386.73 m
Length	34.00 m	Constructed Slope	0.017235 m/m
Hydraulic Profile			
Profile	S2	Depth, Downstream	0.59 m
Slope Type	Steep	Normal Depth	0.59 m
Flow Regime	Supercritical	Critical Depth	0.59 m
Velocity Downstream	2.24 m/s	Critical Slope	0.017158 m/m
Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	388.39 m	Upstream Velocity Head	0.26 m
Ke	0.90	Entrance Loss	0.23 m
Inlet Control Properties			
Inlet Control HW Elev.	388.30 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	387.32	394.32	0.10 m

HW Elev. (m)	Discharge (m ³ /s)
387.32	0.0000
387.42	0.0120
387.52	0.0465
387.62	0.1019
387.72	0.1760
387.82	0.2670
387.92	0.3725
388.02	0.4904
388.12	0.6184
388.22	0.7538
388.32	0.8946
388.42	1.0427
388.52	1.2137
388.62	1.3817
388.72	1.4740
388.82	1.5430
388.92	1.5889
389.02	1.6369
389.12	1.6854
389.22	1.7337
389.32	1.7814
389.42	1.8285
389.52	1.8748
389.62	1.9203
389.72	1.9650
389.82	2.0090
389.92	2.0522
390.02	2.0947
390.12	2.1364
390.22	2.1775
390.32	2.2180
390.42	2.2577
390.52	2.2969
390.62	2.3355
390.72	2.3735
390.82	2.4110
390.92	2.4480
391.02	2.4844
391.12	2.5203
391.22	2.5558
391.32	2.5908
391.42	2.6254
391.52	2.6595
391.62	2.6933
391.72	2.7266
391.82	2.7596
391.92	2.7921
392.02	2.8244
392.12	2.8562
392.22	2.8877
392.32	2.9189

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
392.42	2.9498
392.52	2.9804
392.62	3.0106
392.72	3.0406
392.82	3.0703
392.92	3.0997
393.02	3.1288
393.12	3.1576
393.22	3.1862
393.32	3.2146
393.42	3.2427
393.52	3.2706
393.62	3.2982
393.72	3.3256
393.82	3.3528
393.92	3.3798
394.02	3.4066
394.12	3.4331
394.22	3.4595
394.32	3.4856

Culvert # 10

Culvert Analysis Report

Culvert-1

Culvert Summary

Computed Headwater Elev.:	390.09 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	386.04 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	390.09 m	Control Type	Outlet Control
Headwater Depth/Height	16.16		

Grades

Upstream Invert	382.71 m	Downstream Invert	382.48 m
Length	13.30 m	Constructed Slope	0.016767 m/m

Hydraulic Profile

Profile	CompositeM2PressureProfile	Depth, Downstream	0.46 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.46 m
Velocity Downstream	6.09 m/s	Critical Slope	0.256806 m/m

Section

Section Shape	Circular	Mannings Coefficient	0.020
Corrugated Section Material (Corrugated Interior)		Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	390.09 m	Upstream Velocity Head	1.89 m
Ke	0.90	Entrance Loss	1.70 m

Inlet Control Properties

Inlet Control HW Elev.	386.04 m	Flow Control	Submerged
Inlet Type	Beveled ring, 33.7° bevels	Area Full	0.2 m ²
K	0.00180	HDS 5 Chart	3
M	2.50000	HDS 5 Scale	B
C	0.02430	Equation Form	1
Y	0.83000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	382.71	383.34	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
382.71	0.0000
382.72	0.0001
382.73	0.0004
382.74	0.0008
382.75	0.0014
382.76	0.0021
382.77	0.0030
382.78	0.0041
382.79	0.0053
382.80	0.0067
382.81	0.0082
382.82	0.0099
382.83	0.0117
382.84	0.0137
382.85	0.0158
382.86	0.0180
382.87	0.0204
382.88	0.0229
382.89	0.0255
382.90	0.0282
382.91	0.0311
382.92	0.0341
382.93	0.0372
382.94	0.0404
382.95	0.0438
382.96	0.0472
382.97	0.0507
382.98	0.0544
382.99	0.0581
383.00	0.0619
383.01	0.0659
383.02	0.0699
383.03	0.0740
383.04	0.0781
383.05	0.0824
383.06	0.0867
383.07	0.0911
383.08	0.0956
383.09	0.1001
383.10	0.1047
383.11	0.1093
383.12	0.1140
383.13	0.1188
383.14	0.1236
383.15	0.1284
383.16	0.1333
383.17	0.1382
383.18	0.1431
383.19	0.1481
383.20	0.1531
383.21	0.1581

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
383.22	0.1632
383.23	0.1682
383.24	0.1733
383.25	0.1784
383.26	0.1834
383.27	0.1885
383.28	0.1936
383.29	0.1987
383.30	0.2038
383.31	0.2089
383.32	0.2143
383.33	0.2205
383.34	0.2268

Culvert # 14

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev.	383.10 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	382.88 m	Tailwater Elevation	0.00 m
Outlet Control HW Elev.	383.10 m	Control Type	Outlet Control
Headwater Depth/Height	4.37		

Grades			
Upstream Invert	380.43 m	Downstream Invert	379.93 m
Length	17.20 m	Constructed Slope	0.029070 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.59 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.59 m
Velocity Downstream	3.47 m/s	Critical Slope	0.072455 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	383.10 m	Upstream Velocity Head	0.60 m
Ke	0.90	Entrance Loss	0.54 m

Inlet Control Properties			
Inlet Control HW Elev.	382.88 m	Flow Control	Submerged
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	380.43	381.62	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
380.43	0.0000
380.44	0.0001
380.45	0.0004
380.46	0.0009
380.47	0.0016
380.48	0.0024
380.49	0.0035
380.50	0.0048
380.51	0.0062
380.52	0.0078
380.53	0.0096
380.54	0.0116
380.55	0.0138
380.56	0.0161
380.57	0.0186
380.58	0.0212
380.59	0.0240
380.60	0.0270
380.61	0.0302
380.62	0.0335
380.63	0.0370
380.64	0.0406
380.65	0.0444
380.66	0.0483
380.67	0.0523
380.68	0.0565
380.69	0.0609
380.70	0.0654
380.71	0.0700
380.72	0.0748
380.73	0.0797
380.74	0.0847
380.75	0.0898
380.76	0.0951
380.77	0.1005
380.78	0.1060
380.79	0.1116
380.80	0.1173
380.81	0.1232
380.82	0.1291
380.83	0.1352
380.84	0.1413
380.85	0.1476
380.86	0.1539
380.87	0.1604
380.88	0.1669
380.89	0.1735
380.90	0.1803
380.91	0.1870
380.92	0.1939
380.93	0.2008

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
380.94	0.2078
380.95	0.2148
380.96	0.2220
380.97	0.2292
380.98	0.2365
380.99	0.2438
381.00	0.2511
381.01	0.2586
381.02	0.2660
381.03	0.2735
381.04	0.2811
381.05	0.2887
381.06	0.2963
381.07	0.3040
381.08	0.3117
381.09	0.3194
381.10	0.3271
381.11	0.3350
381.12	0.3428
381.13	0.3506
381.14	0.3584
381.15	0.3662
381.16	0.3741
381.17	0.3819
381.18	0.3897
381.19	0.3975
381.20	0.4053
381.21	0.4132
381.22	0.4210
381.23	0.4288
381.24	0.4366
381.25	0.4444
381.26	0.4521
381.27	0.4599
381.28	0.4676
381.29	0.4752
381.30	0.4830
381.31	0.4906
381.32	0.4982
381.33	0.5058
381.34	0.5133
381.35	0.5208
381.36	0.5283
381.37	0.5357
381.38	0.5431
381.39	0.5480
381.40	0.5523
381.41	0.5565
381.42	0.5607
381.43	0.5649
381.44	0.5690
381.45	0.5732
381.46	0.5772
381.47	0.5813
381.48	0.5853

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
381.49	0.5893
381.50	0.5933
381.51	0.5972
381.52	0.6012
381.53	0.6050
381.54	0.6089
381.55	0.6128
381.56	0.6166
381.57	0.6204
381.58	0.6241
381.59	0.6279
381.60	0.6316
381.61	0.6353
381.62	0.6390

Culvert # 16

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	458.34 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	420.39 m	Tailwater Elevation	0.00 m
Outlet Control HW Elev.	458.34 m	Control Type	Outlet Control
Headwater Depth/Height	236.82		
Grades			
Upstream Invert	386.15 m	Downstream Invert	385.25 m
Length	16.30 m	Constructed Slope	0.055521 m/m
Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.30 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.30 m
Velocity Downstream	13.71 m/s	Critical Slope	3.348955 m/m
Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	458.34 m	Upstream Velocity Head	9.58 m
Ke	0.90	Entrance Loss	8.62 m
Inlet Control Properties			
Inlet Control HW Elev.	420.39 m	Flow Control	Submerged
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	386.15	386.86	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
386.15	0.0000
386.16	0.0001
386.17	0.0003
386.18	0.0006
386.19	0.0011
386.20	0.0017
386.21	0.0024
386.22	0.0033
386.23	0.0043
386.24	0.0053
386.25	0.0065
386.26	0.0078
386.27	0.0093
386.28	0.0108
386.29	0.0124
386.30	0.0141
386.31	0.0159
386.32	0.0178
386.33	0.0197
386.34	0.0218
386.35	0.0239
386.36	0.0261
386.37	0.0283
386.38	0.0307
386.39	0.0331
386.40	0.0355
386.41	0.0380
386.42	0.0405
386.43	0.0431
386.44	0.0457
386.45	0.0484
386.46	0.0510
386.47	0.0537
386.48	0.0565
386.49	0.0592
386.50	0.0620
386.51	0.0647
386.52	0.0675
386.53	0.0703
386.54	0.0730
386.55	0.0758
386.56	0.0785
386.57	0.0813
386.58	0.0840
386.59	0.0867
386.60	0.0894
386.61	0.0921
386.62	0.0947
386.63	0.0973
386.64	0.0990
386.65	0.1005

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
386.66	0.1019
386.67	0.1033
386.68	0.1047
386.69	0.1061
386.70	0.1075
386.71	0.1089
386.72	0.1102
386.73	0.1115
386.74	0.1128
386.75	0.1141
386.76	0.1154
386.77	0.1167
386.78	0.1179
386.79	0.1192
386.80	0.1204
386.81	0.1216
386.82	0.1228
386.83	0.1240
386.84	0.1252
386.85	0.1263
386.86	0.1275

Culvert # 17

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev.	437.32 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	418.92 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	437.32 m	Control Type	Outlet Control
Headwater Depth/Height	172.69		

Grades			
Upstream Invert	384.68 m	Downstream Invert	384.33 m
Length	10.30 m	Constructed Slope	0.034854 m/m

Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	0.30 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.30 m
Velocity Downstream	13.71 m/s	Critical Slope	3.348955 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	437.32 m	Upstream Velocity Head	9.58 m
Ke	0.90	Entrance Loss	8.62 m

Inlet Control Properties			
Inlet Control HW Elev.	418.92 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	384.68	385.30	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
384.68	0.0000
384.69	0.0001
384.70	0.0003
384.71	0.0006
384.72	0.0011
384.73	0.0017
384.74	0.0024
384.75	0.0033
384.76	0.0043
384.77	0.0053
384.78	0.0065
384.79	0.0078
384.80	0.0093
384.81	0.0108
384.82	0.0124
384.83	0.0141
384.84	0.0159
384.85	0.0178
384.86	0.0197
384.87	0.0218
384.88	0.0239
384.89	0.0261
384.90	0.0283
384.91	0.0307
384.92	0.0331
384.93	0.0355
384.94	0.0380
384.95	0.0405
384.96	0.0431
384.97	0.0457
384.98	0.0484
384.99	0.0510
385.00	0.0537
385.01	0.0565
385.02	0.0592
385.03	0.0620
385.04	0.0647
385.05	0.0675
385.06	0.0703
385.07	0.0730
385.08	0.0758
385.09	0.0785
385.10	0.0813
385.11	0.0840
385.12	0.0867
385.13	0.0894
385.14	0.0921
385.15	0.0947
385.16	0.0970
385.17	0.0985
385.18	0.1000

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
385.19	0.1014
385.20	0.1029
385.21	0.1043
385.22	0.1057
385.23	0.1071
385.24	0.1084
385.25	0.1098
385.26	0.1111
385.27	0.1124
385.28	0.1137
385.29	0.1150
385.30	0.1159

Culvert # 24

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	451.24 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	442.46 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	451.24 m	Control Type	Outlet Control
Headwater Depth/Height	60.19		

Grades			
Upstream Invert	428.30 m	Downstream Invert	427.82 m
Length	15.30 m	Constructed Slope	0.031895 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.38 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.38 m
Velocity Downstream	8.77 m/s	Critical Slope	1.000129 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.38 m
Section Size	375 mm	Rise	0.38 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	451.24 m	Upstream Velocity Head	3.92 m
Ke	0.90	Entrance Loss	3.53 m

Inlet Control Properties			
Inlet Control HW Elev.	442.46 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	428.30	429.24	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
428.30	0.0000
428.31	0.0000
428.32	0.0003
428.33	0.0007
428.34	0.0012
428.35	0.0019
428.36	0.0027
428.37	0.0037
428.38	0.0048
428.39	0.0061
428.40	0.0074
428.41	0.0089
428.42	0.0106
428.43	0.0123
428.44	0.0142
428.45	0.0162
428.46	0.0183
428.47	0.0205
428.48	0.0228
428.49	0.0252
428.50	0.0277
428.51	0.0304
428.52	0.0331
428.53	0.0359
428.54	0.0388
428.55	0.0417
428.56	0.0448
428.57	0.0479
428.58	0.0511
428.59	0.0544
428.60	0.0578
428.61	0.0612
428.62	0.0646
428.63	0.0681
428.64	0.0717
428.65	0.0753
428.66	0.0789
428.67	0.0826
428.68	0.0863
428.69	0.0901
428.70	0.0939
428.71	0.0977
428.72	0.1015
428.73	0.1054
428.74	0.1092
428.75	0.1131
428.76	0.1169
428.77	0.1208
428.78	0.1247
428.79	0.1286
428.80	0.1324

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
428.81	0.1363
428.82	0.1401
428.83	0.1439
428.84	0.1477
428.85	0.1515
428.86	0.1553
428.87	0.1590
428.88	0.1627
428.89	0.1663
428.90	0.1694
428.91	0.1715
428.92	0.1735
428.93	0.1756
428.94	0.1776
428.95	0.1796
428.96	0.1816
428.97	0.1836
428.98	0.1855
428.99	0.1874
429.00	0.1893
429.01	0.1912
429.02	0.1931
429.03	0.1949
429.04	0.1967
429.05	0.1984
429.06	0.1992
429.07	0.2001
429.08	0.2009
429.09	0.2018
429.10	0.2027
429.11	0.2036
429.12	0.2046
429.13	0.2055
429.14	0.2064
429.15	0.2074
429.16	0.2083
429.17	0.2092
429.18	0.2102
429.19	0.2111
429.20	0.2121
429.21	0.2130
429.22	0.2140
429.23	0.2149
429.24	0.2159

Culvert # 37

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	421.25 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	421.25 m	Tailwater Elevation	419.01 m
Outlet Control HW Elev.	421.19 m	Control Type	Inlet Control
Headwater Depth/Height	4.02		
Grades			
Upstream Invert	418.80 m	Downstream Invert	418.41 m
Length	12.50 m	Constructed Slope	0.030560 m/m
Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.60 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.59 m
Velocity Downstream	3.44 m/s	Critical Slope	0.072455 m/m
Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	421.19 m	Upstream Velocity Head	0.60 m
Ke	0.90	Entrance Loss	0.54 m
Inlet Control Properties			
Inlet Control HW Elev.	421.25 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	418.80	419.99	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
418.80	0.0000
418.81	0.0000
418.82	0.0000
418.83	0.0000
418.84	0.0000
418.85	0.0000
418.86	0.0000
418.87	0.0000
418.88	0.0000
418.89	0.0000
418.90	0.0000
418.91	0.0000
418.92	0.0000
418.93	0.0000
418.94	0.0000
418.95	0.0000
418.96	0.0000
418.97	0.0000
418.98	0.0000
418.99	0.0000
419.00	0.0000
419.01	0.0000
419.02	0.0148
419.03	0.0355
419.04	0.0479
419.05	0.0572
419.06	0.0646
419.07	0.0707
419.08	0.0757
419.09	0.0800
419.10	0.0834
419.11	0.0862
419.12	0.0898
419.13	0.0951
419.14	0.1005
419.15	0.1060
419.16	0.1116
419.17	0.1173
419.18	0.1232
419.19	0.1291
419.20	0.1352
419.21	0.1413
419.22	0.1476
419.23	0.1539
419.24	0.1604
419.25	0.1669
419.26	0.1735
419.27	0.1803
419.28	0.1870
419.29	0.1939
419.30	0.2008

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
419.31	0.2078
419.32	0.2148
419.33	0.2220
419.34	0.2292
419.35	0.2365
419.36	0.2438
419.37	0.2511
419.38	0.2586
419.39	0.2660
419.40	0.2735
419.41	0.2811
419.42	0.2887
419.43	0.2963
419.44	0.3040
419.45	0.3117
419.46	0.3194
419.47	0.3271
419.48	0.3350
419.49	0.3428
419.50	0.3506
419.51	0.3584
419.52	0.3662
419.53	0.3741
419.54	0.3819
419.55	0.3896
419.56	0.3975
419.57	0.4053
419.58	0.4132
419.59	0.4210
419.60	0.4288
419.61	0.4366
419.62	0.4444
419.63	0.4521
419.64	0.4599
419.65	0.4676
419.66	0.4752
419.67	0.4830
419.68	0.4906
419.69	0.4982
419.70	0.5058
419.71	0.5133
419.72	0.5208
419.73	0.5283
419.74	0.5357
419.75	0.5431
419.76	0.5482
419.77	0.5525
419.78	0.5567
419.79	0.5609
419.80	0.5651
419.81	0.5692
419.82	0.5733
419.83	0.5774
419.84	0.5815
419.85	0.5855

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
419.86	0.5895
419.87	0.5935
419.88	0.5974
419.89	0.6013
419.90	0.6052
419.91	0.6091
419.92	0.6129
419.93	0.6167
419.94	0.6205
419.95	0.6243
419.96	0.6281
419.97	0.6318
419.98	0.6355
419.99	0.6392

Culvert # 43

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	401.74 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	401.26 m	Tailwater Elevation	400.51 m
Outlet Control HW Elev.	401.74 m	Control Type	Outlet Control
Headwater Depth/Height	2.95		
Grades			
Upstream Invert	400.13 m	Downstream Invert	399.96 m
Length	12.60 m	Constructed Slope	0.013492 m/m
Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	0.55 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.51 m
Velocity Downstream	2.70 m/s	Critical Slope	0.039100 m/m
Section			
Section Shape	Horizontal Ellipse	Mannings Coefficient	0.024
Section Material	Concrete	Span	0.86 m
Section Size	550 x 860 mm	Rise	0.55 m
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	401.74 m	Upstream Velocity Head	0.37 m
Ke	0.90	Entrance Loss	0.33 m
Inlet Control Properties			
Inlet Control HW Elev.	401.26 m	Flow Control	N/A
Inlet type	projecting (horizontal ellipse)	Area Full	0.4 m ²
K	0.00450	HDS 5 Chart	29
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	400.13	400.88	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
400.13	0.0000
400.14	0.0000
400.15	0.0000
400.16	0.0000
400.17	0.0000
400.18	0.0000
400.19	0.0000
400.20	0.0000
400.21	0.0000
400.22	0.0000
400.23	0.0000
400.24	0.0000
400.25	0.0000
400.26	0.0000
400.27	0.0000
400.28	0.0000
400.29	0.0000
400.30	0.0000
400.31	0.0000
400.32	0.0000
400.33	0.0000
400.34	0.0000
400.35	0.0000
400.36	0.0000
400.37	0.0000
400.38	0.0000
400.39	0.0000
400.40	0.0000
400.41	0.0000
400.42	0.0000
400.43	0.0000
400.44	0.0000
400.45	0.0000
400.46	0.0000
400.47	0.0000
400.48	0.0000
400.49	0.0000
400.50	0.0000
400.51	0.0000
400.52	0.0803
400.53	0.1141
400.54	0.1402
400.55	0.1625
400.56	0.1823
400.57	0.2004
400.58	0.2172
400.59	0.2330
400.60	0.2481
400.61	0.2624
400.62	0.2763
400.63	0.2897

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
400.64	0.3027
400.65	0.3153
400.66	0.3277
400.67	0.3398
400.68	0.3517
400.69	0.3634
400.70	0.3749
400.71	0.3862
400.72	0.3974
400.73	0.4084
400.74	0.4192
400.75	0.4299
400.76	0.4404
400.77	0.4508
400.78	0.4609
400.79	0.4709
400.80	0.4807
400.81	0.4903
400.82	0.4996
400.83	0.5086
400.84	0.5173
400.85	0.5257
400.86	0.5340
400.87	0.5418
400.88	0.5492

Culvert # 44n

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	400.58 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	400.47 m	Tailwater Elevation	400.47 m
Outlet Control HW Elev.	400.58 m	Control Type	Outlet Control
Headwater Depth/Height	0.91		

Grades			
Upstream Invert	399.46 m	Downstream Invert	399.27 m
Length	13.80 m	Constructed Slope	0.013841 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	1.20 m
Slope Type	Steep	Normal Depth	0.53 m
Flow Regime	Subcritical	Critical Depth	0.54 m
Velocity Downstream	0.86 m/s	Critical Slope	0.012636 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	1.22 m
Section Size	1200 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	400.58 m	Upstream Velocity Head	0.05 m
Ke	0.90	Entrance Loss	0.04 m

Inlet Control Properties			
Inlet Control HW Elev.	400.47 m	Flow Control	Unsubmerged
Inlet Type	Projecting	Area Full	1.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	399.46	400.76	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
399.46	0.0000
399.47	0.0000
399.48	0.0000
399.49	0.0000
399.50	0.0000
399.51	0.0000
399.52	0.0000
399.53	0.0000
399.54	0.0000
399.55	0.0000
399.56	0.0000
399.57	0.0000
399.58	0.0000
399.59	0.0000
399.60	0.0000
399.61	0.0000
399.62	0.0000
399.63	0.0000
399.64	0.0000
399.65	0.0000
399.66	0.0000
399.67	0.0000
399.68	0.0000
399.69	0.0000
399.70	0.0000
399.71	0.0000
399.72	0.0000
399.73	0.0000
399.74	0.0000
399.75	0.0000
399.76	0.0000
399.77	0.0000
399.78	0.0000
399.79	0.0000
399.80	0.0000
399.81	0.0000
399.82	0.0000
399.83	0.0000
399.84	0.0000
399.85	0.0000
399.86	0.0000
399.87	0.0000
399.88	0.0000
399.89	0.0000
399.90	0.0000
399.91	0.0000
399.92	0.0000
399.93	0.0000
399.94	0.0000
399.95	0.0000
399.96	0.0000

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
399.97	0.0000
399.98	0.0000
399.99	0.0000
400.00	0.0000
400.01	0.0000
400.02	0.0000
400.03	0.0000
400.04	0.0000
400.05	0.0000
400.06	0.0000
400.07	0.0000
400.08	0.0000
400.09	0.0000
400.10	0.0000
400.11	0.0000
400.12	0.0000
400.13	0.0000
400.14	0.0000
400.15	0.0000
400.16	0.0000
400.17	0.0000
400.18	0.0000
400.19	0.0000
400.20	0.0000
400.21	0.0000
400.22	0.0000
400.23	0.0000
400.24	0.0000
400.25	0.0000
400.26	0.0000
400.27	0.0000
400.28	0.0000
400.29	0.0000
400.30	0.0000
400.31	0.0000
400.32	0.0000
400.33	0.0000
400.34	0.0000
400.35	0.0000
400.36	0.0000
400.37	0.0000
400.38	0.0000
400.39	0.0000
400.40	0.0000
400.41	0.0000
400.42	0.0000
400.43	0.0000
400.44	0.0000
400.45	0.0000
400.46	0.0000
400.47	0.0970
400.48	0.3204
400.49	0.4433
400.50	0.5392
400.51	0.6207

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
400.52	0.6929
400.53	0.7585
400.54	0.8190
400.55	0.8755
400.56	0.9287
400.57	0.9792
400.58	1.0273
400.59	1.0735
400.60	1.1178
400.61	1.1606
400.62	1.2020
400.63	1.2421
400.64	1.2811
400.65	1.3190
400.66	1.3560
400.67	1.3921
400.68	1.4275
400.69	1.4620
400.70	1.4959
400.71	1.5291
400.72	1.5618
400.73	1.5938
400.74	1.6254
400.75	1.6564
400.76	1.6869

Culvert # 44s

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	400.61 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	400.51 m	Tailwater Elevation	400.51 m
Outlet Control HW Elev.	400.61 m	Control Type	Outlet Control
Headwater Depth/Height	0.96		

Grades			
Upstream Invert	399.44 m	Downstream Invert	399.31 m
Length	13.80 m	Constructed Slope	0.009710 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	1.20 m
Slope Type	Mild	Normal Depth	0.58 m
Flow Regime	Subcritical	Critical Depth	0.54 m
Velocity Downstream	0.86 m/s	Critical Slope	0.012636 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	1.22 m
Section Size	1200 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	400.61 m	Upstream Velocity Head	0.04 m
Ke	0.90	Entrance Loss	0.04 m

Inlet Control Properties			
Inlet Control HW Elev.	400.51 m	Flow Control	Unsubmerged
Inlet Type	Projecting	Area Full	1.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	399.44	400.76	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
399.44	0.0000
399.45	0.0000
399.46	0.0000
399.47	0.0000
399.48	0.0000
399.49	0.0000
399.50	0.0000
399.51	0.0000
399.52	0.0000
399.53	0.0000
399.54	0.0000
399.55	0.0000
399.56	0.0000
399.57	0.0000
399.58	0.0000
399.59	0.0000
399.60	0.0000
399.61	0.0000
399.62	0.0000
399.63	0.0000
399.64	0.0000
399.65	0.0000
399.66	0.0000
399.67	0.0000
399.68	0.0000
399.69	0.0000
399.70	0.0000
399.71	0.0000
399.72	0.0000
399.73	0.0000
399.74	0.0000
399.75	0.0000
399.76	0.0000
399.77	0.0000
399.78	0.0000
399.79	0.0000
399.80	0.0000
399.81	0.0000
399.82	0.0000
399.83	0.0000
399.84	0.0000
399.85	0.0000
399.86	0.0000
399.87	0.0000
399.88	0.0000
399.89	0.0000
399.90	0.0000
399.91	0.0000
399.92	0.0000
399.93	0.0000
399.94	0.0000

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
399.95	0.0000
399.96	0.0000
399.97	0.0000
399.98	0.0000
399.99	0.0000
400.00	0.0000
400.01	0.0000
400.02	0.0000
400.03	0.0000
400.04	0.0000
400.05	0.0000
400.06	0.0000
400.07	0.0000
400.08	0.0000
400.09	0.0000
400.10	0.0000
400.11	0.0000
400.12	0.0000
400.13	0.0000
400.14	0.0000
400.15	0.0000
400.16	0.0000
400.17	0.0000
400.18	0.0000
400.19	0.0000
400.20	0.0000
400.21	0.0000
400.22	0.0000
400.23	0.0000
400.24	0.0000
400.25	0.0000
400.26	0.0000
400.27	0.0000
400.28	0.0000
400.29	0.0000
400.30	0.0000
400.31	0.0000
400.32	0.0000
400.33	0.0000
400.34	0.0000
400.35	0.0000
400.36	0.0000
400.37	0.0000
400.38	0.0000
400.39	0.0000
400.40	0.0000
400.41	0.0000
400.42	0.0000
400.43	0.0000
400.44	0.0000
400.45	0.0000
400.46	0.0000
400.47	0.0000
400.48	0.0000
400.49	0.0000

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
400.50	0.0000
400.51	0.1981
400.52	0.3708
400.53	0.4859
400.54	0.5787
400.55	0.6588
400.56	0.7301
400.57	0.7956
400.58	0.8560
400.59	0.9126
400.60	0.9660
400.61	1.0167
400.62	1.0651
400.63	1.1116
400.64	1.1562
400.65	1.1993
400.66	1.2410
400.67	1.2815
400.68	1.3207
400.69	1.3590
400.70	1.3962
400.71	1.4326
400.72	1.4682
400.73	1.5029
400.74	1.5370
400.75	1.5704
400.76	1.6031

Culvert # 47

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev.	418.22 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	412.33 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	418.22 m	Control Type	Outlet Control
Headwater Depth/Height	52.63		

Grades			
Upstream Invert	398.17 m	Downstream Invert	397.96 m
Length	12.20 m	Constructed Slope	0.017295 m/m

Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	0.38 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.38 m
Velocity Downstream	8.77 m/s	Critical Slope	1.000129 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.38 m
Section Size	375 mm	Rise	0.38 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	418.22 m	Upstream Velocity Head	3.92 m
Ke	0.90	Entrance Loss	3.53 m

Inlet Control Properties			
Inlet Control HW Elev.	412.33 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	398.17	398.98	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
398.17	0.0000
398.18	0.0000
398.19	0.0003
398.20	0.0007
398.21	0.0013
398.22	0.0020
398.23	0.0029
398.24	0.0038
398.25	0.0050
398.26	0.0062
398.27	0.0076
398.28	0.0091
398.29	0.0107
398.30	0.0125
398.31	0.0143
398.32	0.0163
398.33	0.0184
398.34	0.0206
398.35	0.0229
398.36	0.0254
398.37	0.0279
398.38	0.0306
398.39	0.0333
398.40	0.0362
398.41	0.0392
398.42	0.0422
398.43	0.0454
398.44	0.0486
398.45	0.0520
398.46	0.0554
398.47	0.0589
398.48	0.0626
398.49	0.0662
398.50	0.0700
398.51	0.0739
398.52	0.0778
398.53	0.0818
398.54	0.0859
398.55	0.0900
398.56	0.0941
398.57	0.0983
398.58	0.1026
398.59	0.1068
398.60	0.1111
398.61	0.1153
398.62	0.1195
398.63	0.1237
398.64	0.1277
398.65	0.1315
398.66	0.1352
398.67	0.1387

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
398.68	0.1418
398.69	0.1447
398.70	0.1472
398.71	0.1494
398.72	0.1504
398.73	0.1517
398.74	0.1529
398.75	0.1542
398.76	0.1555
398.77	0.1568
398.78	0.1582
398.79	0.1595
398.80	0.1608
398.81	0.1622
398.82	0.1635
398.83	0.1648
398.84	0.1662
398.85	0.1675
398.86	0.1688
398.87	0.1701
398.88	0.1715
398.89	0.1728
398.90	0.1741
398.91	0.1754
398.92	0.1767
398.93	0.1780
398.94	0.1793
398.95	0.1806
398.96	0.1818
398.97	0.1831
398.98	0.1844

Culvert # 48

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	414.42 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	408.24 m	Tailwater Elevation	394.24 m
Outlet Control HW Elev.	414.42 m	Control Type	Outlet Control
Headwater Depth/Height	53.39		

Grades			
Upstream Invert	394.08 m	Downstream Invert	393.84 m
Length	12.50 m	Constructed Slope	0.019760 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.40 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.38 m
Velocity Downstream	8.77 m/s	Critical Slope	1.000129 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.38 m
Section Size	375 mm	Rise	0.38 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	414.42 m	Upstream Velocity Head	3.92 m
Ke	0.90	Entrance Loss	3.53 m

Inlet Control Properties			
Inlet Control HW Elev.	408.24 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	394.08	394.95	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
394.08	0.0000
394.09	0.0000
394.10	0.0000
394.11	0.0000
394.12	0.0000
394.13	0.0000
394.14	0.0000
394.15	0.0000
394.16	0.0000
394.17	0.0000
394.18	0.0000
394.19	0.0000
394.20	0.0000
394.21	0.0000
394.22	0.0000
394.23	0.0000
394.24	0.0110
394.25	0.0172
394.26	0.0218
394.27	0.0259
394.28	0.0294
394.29	0.0327
394.30	0.0358
394.31	0.0387
394.32	0.0415
394.33	0.0443
394.34	0.0471
394.35	0.0499
394.36	0.0527
394.37	0.0556
394.38	0.0586
394.39	0.0617
394.40	0.0650
394.41	0.0684
394.42	0.0721
394.43	0.0760
394.44	0.0801
394.45	0.0844
394.46	0.0888
394.47	0.0935
394.48	0.0981
394.49	0.1028
394.50	0.1074
394.51	0.1118
394.52	0.1159
394.53	0.1196
394.54	0.1229
394.55	0.1257
394.56	0.1280
394.57	0.1299
394.58	0.1317

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
394.59	0.1331
394.60	0.1348
394.61	0.1367
394.62	0.1385
394.63	0.1402
394.64	0.1420
394.65	0.1437
394.66	0.1454
394.67	0.1471
394.68	0.1488
394.69	0.1505
394.70	0.1521
394.71	0.1537
394.72	0.1553
394.73	0.1569
394.74	0.1585
394.75	0.1600
394.76	0.1616
394.77	0.1631
394.78	0.1646
394.79	0.1661
394.80	0.1676
394.81	0.1691
394.82	0.1705
394.83	0.1720
394.84	0.1734
394.85	0.1748
394.86	0.1762
394.87	0.1776
394.88	0.1790
394.89	0.1804
394.90	0.1818
394.91	0.1831
394.92	0.1845
394.93	0.1858
394.94	0.1871
394.95	0.1885

Culvert # 55

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev:	448.46 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	422.99 m	Tailwater Elevation	388.73 m
Outlet Control HW Elev.	448.46 m	Control Type	Outlet Control
Headwater Depth/Height	195.88		

Grades			
Upstream Invert	388.76 m	Downstream Invert	388.43 m
Length	12.40 m	Constructed Slope	0.026129 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.30 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.30 m
Velocity Downstream	13.71 m/s	Critical Slope	3.348955 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	448.46 m	Upstream Velocity Head	9.58 m
Ke	0.90	Entrance Loss	8.62 m

Inlet Control Properties			
Inlet Control HW Elev.	422.99 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	388.76	389.39	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
388.76	0.0000
388.77	0.0001
388.78	0.0003
388.79	0.0006
388.80	0.0011
388.81	0.0017
388.82	0.0024
388.83	0.0033
388.84	0.0043
388.85	0.0053
388.86	0.0065
388.87	0.0078
388.87	0.0093
388.88	0.0108
388.90	0.0124
388.90	0.0141
388.91	0.0159
388.92	0.0178
388.94	0.0197
388.95	0.0218
388.96	0.0239
388.96	0.0261
388.97	0.0283
388.99	0.0307
389.00	0.0331
389.01	0.0355
389.02	0.0380
389.03	0.0405
389.04	0.0431
389.05	0.0457
389.06	0.0484
389.07	0.0510
389.08	0.0537
389.09	0.0565
389.09	0.0592
389.10	0.0620
389.11	0.0647
389.12	0.0675
389.14	0.0703
389.15	0.0735
389.15	0.0768
389.16	0.0802
389.17	0.0836
389.19	0.0869
389.20	0.0905
389.21	0.0922
389.21	0.0930
389.23	0.0930
389.24	0.0931
389.25	0.0936
389.26	0.0942

Rating Table Report

Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
389.27	0.0949
389.28	0.0957
389.29	0.0965
389.30	0.0974
389.31	0.0982
389.32	0.0990
389.32	0.0998
389.34	0.1007
389.34	0.1015
389.35	0.1023
389.36	0.1031
389.38	0.1039
389.39	0.1047
389.40	0.1055

Culvert # 56

Culvert Analysis Report

Culvert-1

Culvert Summary			
Computed Headwater Elev.	444.22 m	Discharge	1.0000 m ³ /s
Inlet Control HW Elev.	421.50 m	Tailwater Elevation	N/A m
Outlet Control HW Elev.	444.22 m	Control Type	Outlet Control
Headwater Depth/Height	186.90		

Grades			
Upstream Invert	387.26 m	Downstream Invert	387.21 m
Length	11.50 m	Constructed Slope	0.004087 m/m

Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	0.30 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.30 m
Velocity Downstream	13.71 m/s	Critical Slope	3.348955 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	444.22 m	Upstream Velocity Head	9.58 m
Ke	0.90	Entrance Loss	8.62 m

Inlet Control Properties			
Inlet Control HW Elev.	421.50 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Rating Table Report Culvert-1

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	387.26	388.16	0.01 m

HW Elev. (m)	Discharge (m ³ /s)
387.26	0.0000
387.27	0.0001
387.28	0.0002
387.29	0.0006
387.30	0.0010
387.31	0.0016
387.32	0.0023
387.33	0.0031
387.34	0.0041
387.35	0.0051
387.36	0.0062
387.37	0.0075
387.38	0.0089
387.39	0.0104
387.40	0.0119
387.40	0.0136
387.42	0.0153
387.43	0.0172
387.44	0.0190
387.45	0.0210
387.46	0.0230
387.47	0.0250
387.48	0.0271
387.49	0.0292
387.50	0.0314
387.51	0.0336
387.52	0.0357
387.53	0.0378
387.54	0.0400
387.55	0.0421
387.56	0.0444
387.57	0.0465
387.58	0.0486
387.59	0.0506
387.59	0.0525
387.60	0.0542
387.62	0.0557
387.63	0.0569
387.64	0.0582
387.65	0.0595
387.65	0.0608
387.67	0.0620
387.68	0.0632
387.69	0.0644
387.70	0.0656
387.71	0.0668
387.72	0.0679
387.73	0.0691
387.74	0.0702
387.75	0.0713
387.76	0.0724

Rating Table Report Culvert-1

HW Elev. (m)	Discharge (m ³ /s)
387.77	0.0734
387.78	0.0745
387.79	0.0755
387.80	0.0766
387.81	0.0776
387.82	0.0786
387.83	0.0796
387.84	0.0806
387.84	0.0816
387.85	0.0826
387.87	0.0835
387.88	0.0845
387.89	0.0854
387.90	0.0864
387.91	0.0873
387.92	0.0882
387.93	0.0891
387.94	0.0900
387.95	0.0909
387.96	0.0918
387.97	0.0927
387.98	0.0936
387.99	0.0945
388.00	0.0953
388.01	0.0962
388.02	0.0970
388.03	0.0979
388.04	0.0987
388.04	0.0996
388.06	0.1004
388.07	0.1012
388.08	0.1020
388.09	0.1028
388.09	0.1037
388.11	0.1045
388.12	0.1053
388.13	0.1060
388.14	0.1068
388.15	0.1076
388.16	0.1084
388.17	0.1092

Appendix G
Capacity Rating for Cross Culverts

Table G-1: Capacity Rating for Cross Culverts

Capacity Rating Criteria

Category	Description	Effective Cross-Section (%)
Very Good	Little to no sediment build up in pipe. Culvert ends are undamaged. Little to no debris blocking flow.	100%
Good	Original culvert capacity diminished by 5% or less.	95 % - 99 %
Fair	Original culvert capacity diminished by less than 15%.	85 % - 94 %
Poor	Original culvert capacity diminished by less than 25%.	75 % - 84 %
Below Minimum Tolerable	Original culvert capacity diminished by more than 25%.	0 % - 74 %

Culvert ID #	Culvert Type	Diameter Size / Height (m)	Diameter Size Meets Region's Standard (Minimum 600 mm)	Capacity Rating (CR)
10	cross culvert	0.45	No	Good
17	cross culvert	0.30	No	Below Minimum Tolerable
24	cross culvert	0.40	No	Below Minimum Tolerable
37	cross culvert	0.60	Yes	Below Minimum Tolerable
43	cross culvert	0.9 x 0.55	Yes	Very Good
44 (north)	cross culvert	1.2 x 1.0	Yes	Very Good
44 (south)	cross culvert	1.2 x 1.0	Yes	Very Good
47	cross culvert	0.40	No	Below Minimum Tolerable
48	cross culvert	0.40	No	Poor
55	cross culvert	0.30	No	Below Minimum Tolerable
56	cross culvert	0.30	No	Below Minimum Tolerable
14	cross culvert	0.60	Yes	Fair
16	cross culvert	0.30	No	Fair
2	cross culvert	0.90	Yes	Fair

Appendix H
Capacity Rating for Entrance Culverts

Table H-1: Capacity Rating for Entrance Culverts

Capacity Rating Criteria

Category	Description	Effective Cross-Section (%)
Very Good	Little to no sediment build up in pipe. Culvert ends are undamaged. Little to no debris blocking flow.	100%
Good	Original culvert capacity diminished by 5% or less.	95 % - 99 %
Fair	Original culvert capacity diminished by less than 15%.	85 % - 94 %
Poor	Original culvert capacity diminished by less than 25%.	75 % - 84 %
Below Minimum Tolerable	Original culvert capacity diminished by more than 25%.	0 % - 74 %

Culvert ID #	Culvert Type	Diameter Size / Height (m)	Diameter Size Meets Region's Standard (Minimum 375 mm)	Capacity Rating (CR)
1	entrance culvert	0.30	No	Below Minimum Tolerable
3	entrance culvert	0.35	No	Below Minimum Tolerable
4	entrance culvert	0.35	No	Below Minimum Tolerable
5	entrance culvert	0.30	No	Very Good
6	entrance culvert	0.30	No	Below Minimum Tolerable
7	entrance culvert	0.30	No	Good
8	entrance culvert	0.30	No	Below Minimum Tolerable
9	entrance culvert	0.30	No	Below Minimum Tolerable
11	entrance culvert	0.30	No	Below Minimum Tolerable
12	entrance culvert	0.30	No	Below Minimum Tolerable
13	entrance culvert	0.30	No	Below Minimum Tolerable
15	entrance culvert	0.30	No	Below Minimum Tolerable
18	entrance culvert	0.40	Yes	Below Minimum Tolerable
19	entrance culvert	0.40	Yes	Below Minimum Tolerable
20	entrance culvert	0.50	Yes	Below Minimum Tolerable
21	entrance culvert	0.40	Yes	Below Minimum Tolerable
22	entrance culvert	0.40	Yes	Good
23	entrance culvert	0.40	Yes	n/a
25	entrance culvert	0.40	Yes	Below Minimum Tolerable
26	entrance culvert	0.40	Yes	Below Minimum Tolerable
27	entrance culvert	0.30	No	Below Minimum Tolerable
28	entrance culvert	0.40	Yes	Fair
29	entrance culvert	0.40	Yes	Below Minimum Tolerable
30	entrance culvert	0.60	Yes	Good
31	entrance culvert	0.60	Yes	Below Minimum Tolerable
32	entrance culvert	0.60	Yes	Very Good
33	entrance culvert	0.40	Yes	Below Minimum Tolerable
35	entrance culvert	0.50	Yes	Below Minimum Tolerable
36	entrance culvert	0.60	Yes	Fair
38	entrance culvert	0.40	Yes	Below Minimum Tolerable
39	entrance culvert	0.50	Yes	Below Minimum Tolerable
40	entrance culvert	0.60	Yes	Good
41	entrance culvert	0.50	Yes	Below Minimum Tolerable
42	entrance culvert	0.50	Yes	Below Minimum Tolerable
45	entrance culvert	0.40	Yes	Below Minimum Tolerable
46	entrance culvert	0.30	No	Below Minimum Tolerable
49	entrance culvert	0.50	Yes	Good
50	entrance culvert	0.40	Yes	Below Minimum Tolerable
51	entrance culvert	0.40	Yes	Fair
52	entrance culvert	0.40	Yes	Fair
53	entrance culvert	0.30	No	Below Minimum Tolerable
54	entrance culvert	0.40	Yes	Poor
57	entrance culvert	0.20	No	Below Minimum Tolerable
58	entrance culvert	0.20	No	Below Minimum Tolerable

Appendix R.2
Drainage and Hydrology Assessment for
Winston Churchill Boulevard and
Olde Base Line Road

Region of Peel

Drainage and Hydrology Report

Olde Base Line Road and Winston Churchill Boulevard, Town of Caledon, Region of Peel

January 2014 (revised May 2014)

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1. INTRODUCTION

The Regional Municipality of Peel (the Region) is conducting a Schedule “C” Municipal Class Environmental Assessment (EA) to provide a comprehensive and environmentally sound Transportation and Road Infrastructure Improvement Plan using a Context Sensitive Solutions Approach for the following Regional Road corridors:

- Winston Churchill Boulevard (Peel Regional Road 19, Wellington County Road 25) – from Olde Base Line Road to Bush Street;
- Olde Base Line Road (Regional Road 12) – from Winston Churchill Boulevard to Mississauga Road;
- Mississauga Road and Old Main Street (Regional Road 1) – from Olde Base Line Road to Bush Street; and
- Bush Street (Regional Road 11) – from Mississauga Road / Old Main Street to Winston Churchill Boulevard;

The approximate limits of the Study Area are shown in **Exhibit 1-1**.

This Drainage and Hydrology Report was prepared to document the drainage and hydrologic assessments that were undertaken for Olde Base Line Road and Winston Churchill Boulevard.

The drainage assessments for the remaining roads are documented under separate cover in the *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft, June 2010* prepared by Dillon Consulting Limited.

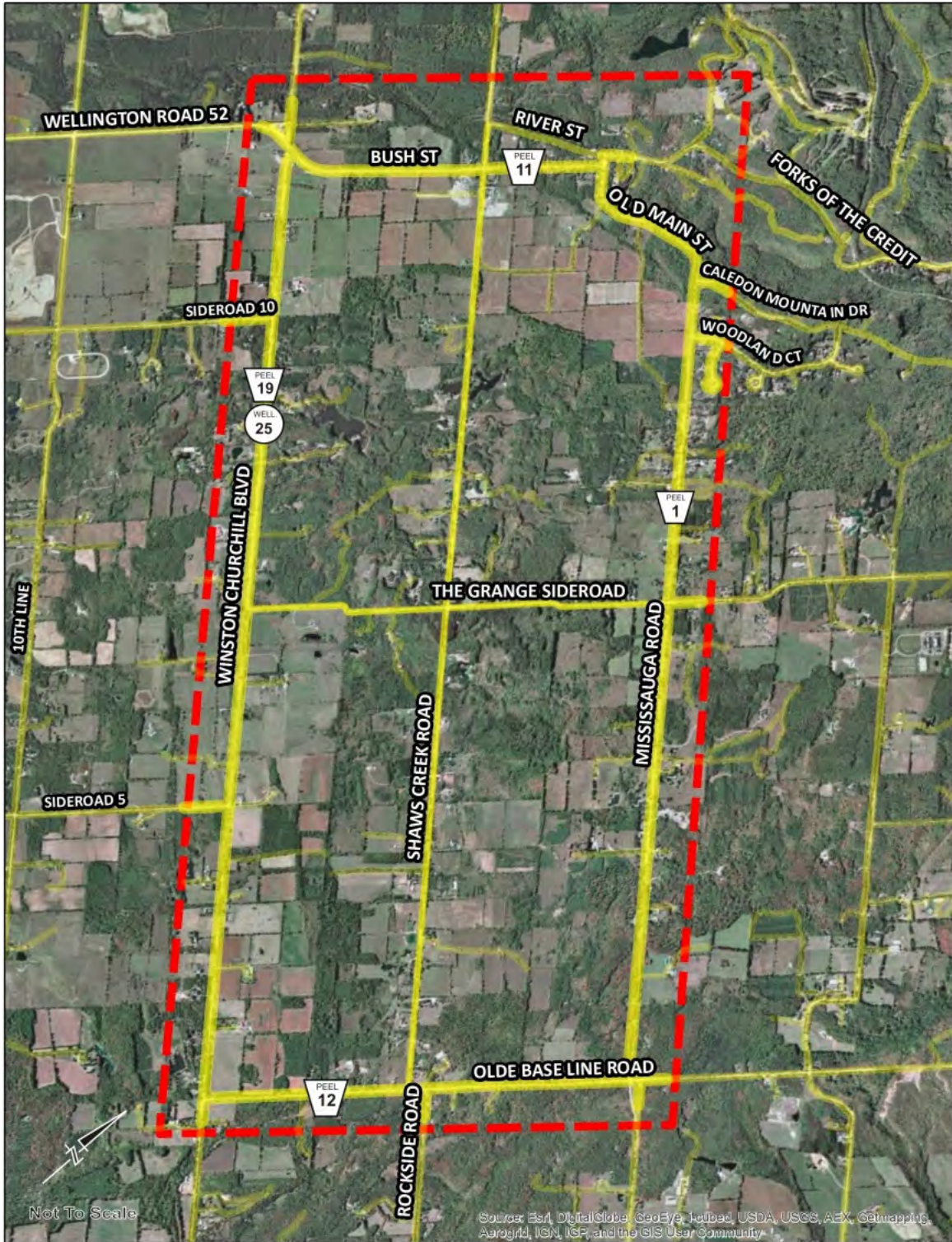
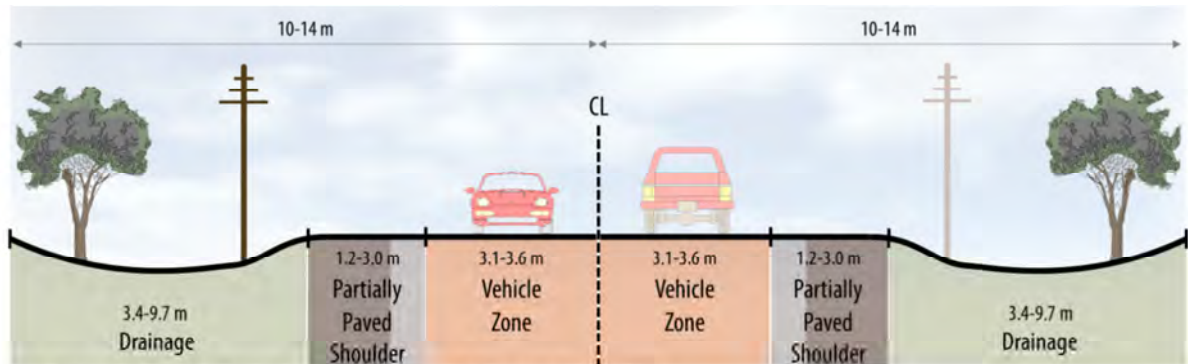


Exhibit 1-1: Study Area

1.1 Description of the Road Network

Winston Churchill Boulevard (Peel Regional Road 19, Wellington County Road 25) between Bush Street and Olde Base Line Road is a two-lane rural, north-south major road that is approximately 6.0 km in length. Adjacent land uses along the roadway include numerous private residences and farms, with driveways and accesses on Winston Churchill Boulevard. The vertical alignment of the road is a rolling profile with some moderate crests and sags. Winston Churchill Boulevard marks the boundary between Caledon (Peel Region) and the Town of Erin (Wellington County). Jurisdiction of the road is shared between Peel Region and Wellington County. The posted speed limit varies between 60 km/h and 70 km/h.

The existing cross-section of Winston Churchill Boulevard consists of two 3.1-3.6 m travel lanes with partially paved shoulders ranging between 1.2-3.0 m (of which 0-1.0 m is paved). The existing right-of-way is predominantly 20-23 m, but ranges between 20 m to 28 m. The range of dimensions for the different cross-sectional elements along the corridor is shown in **Exhibit 1-2**.

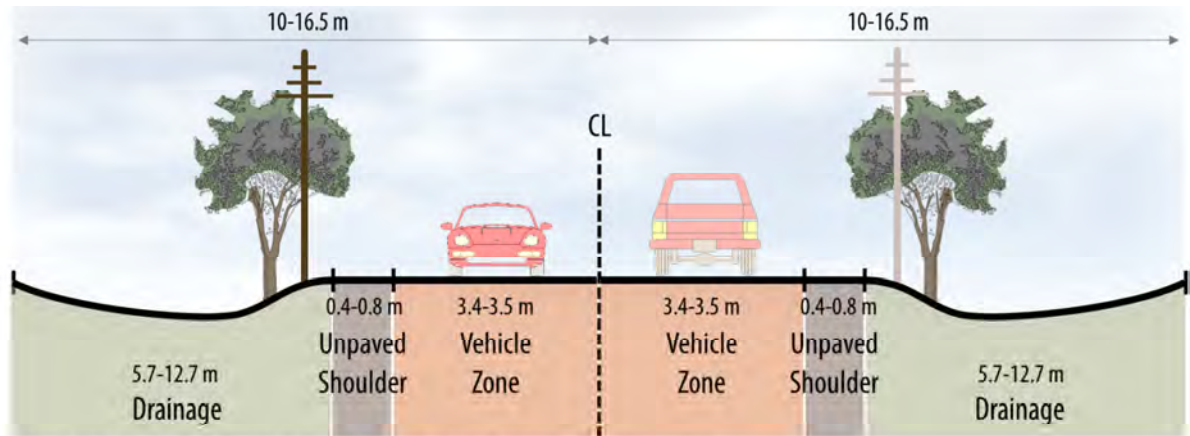


Note: Total right-of-way is predominantly 20-23 m; paved portion of shoulder ranges from 0-1.0 m; majority of above ground utilities run on east side of the road and crosses over between sides

Exhibit 1-2: Winston Churchill Boulevard Existing Cross Section

Olde Base Line Road (Regional Road 12) between Winston Churchill Boulevard and Mississauga Road is a two-lane rural, east-west major road, approximately 2.8 km in length. Adjacent land uses along the roadway consists mainly of undeveloped land, with some private residences and farms that have direct access to the road. The vertical alignment of the roadway consists of sharp crests and sag curves. The road is under the Region of Peel's jurisdiction and the posted speed limit is 60 km/h. Olde Base Line Road has offset intersections with Shaws Creek Road and Rockside Road.

The existing cross-section of Olde Base Line Road consists of two 3.4-3.5 m wide travel lanes with unpaved shoulders ranging between 0.4-0.8 m. The range of dimensions for the different cross-sectional elements along the corridor is shown in **Exhibit 1-3**.



Note: Total right-of-way is predominantly 20-25 m; no paved portion of shoulder exists;
majority of above ground utilities run on one side of the road and cross over between sides

Exhibit 1-3: Olde Base Line Road Existing Cross Section

Mississauga Road (Regional Road 1), between Olde Base Line Road and Caledon Mountain Drive is a two-lane rural north-south major road approximately 5.4 km in length. There are numerous vertical curves along the alignment of the roadway, resulting in a rolling vertical alignment. The adjacent land uses of this area include numerous private residences and farms with unpaved driveway accesses; the cemetery grounds of Melville White Church on the west side of the road, approximately 1.6 km north of Olde Base Line Road; and the Blair-Belfountain Community Cemetery, on the east side of the road, approximately 4.8 km north of Olde Base Line Road. The road is under the Region of Peel's jurisdiction and the posted speed limit varies between 60 km/h to 70 km/h.

The existing cross-section of Mississauga Road consists of two 3.3-3.5 m travel lanes with partially paved shoulders ranging between 0.5-2.3 m in width (of which 0-2.3 m is paved). The existing right-of-way varies between 20-28 m, and is predominantly 20 m throughout the corridor. The range of dimensions for the different cross-sectional elements along the corridor is shown in **Exhibit 1-4**.

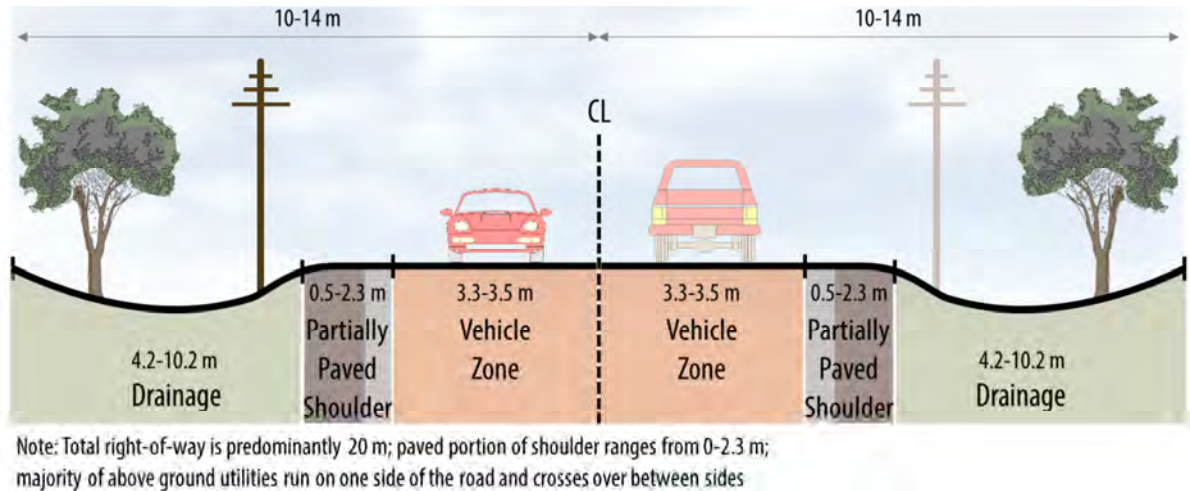
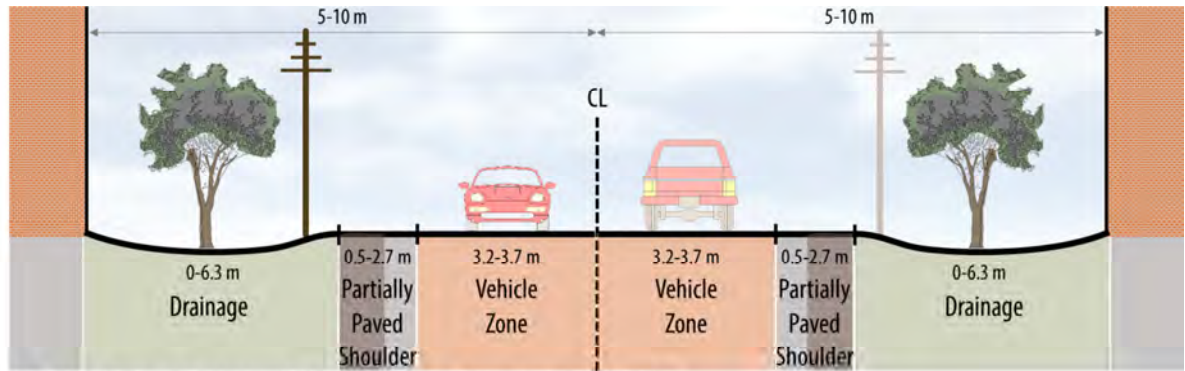


Exhibit 1-4: Mississauga Road Existing Cross Section

Old Main Street (Regional Road 1), a continuation of Mississauga Road north of Caledon Mountain Drive to Bush Street, is a major road approximately 1.1 km in length. It has a rural two-lane cross section south of Belfountain, and has urban characteristics in the village of Belfountain. The vertical alignment of the roadway generally descends towards the north, with a 5% downgrade towards Bush Street. The horizontal alignment has several relatively sharp horizontal curves. The adjacent land uses of this area include private residences and community buildings, with various driveways with direct access onto Old Main Street. On-street parking is permitted in the urban area directly south of Bush Street. The road is under the Region of Peel's jurisdiction and the posted speed limit varies between 40 km/h and 50 km/h.

In the village of Belfountain, which includes a portion of Bush Street (Regional Road 11), the existing cross-section consists of two 3.2-3.7 m travel lanes with partially paved shoulders ranging between 0.5-2.7 m (of which 0.2-2.0 m is paved). The existing right-of-way within the village (on both Old Main Street and Bush Street) varies between 10-20 m, and is predominantly 20 m. The range of dimensions for the different cross-sectional elements along the corridor is shown in **Exhibit 1-5**.



Note: Total right-of-way is predominantly 20 m; paved portion of shoulder ranges from 0.2-2.0 m; majority of above ground utilities run on one side of the road and cross over between sides

Exhibit 1-5: Belfountain Village Existing Cross Section (Old Main Street and Bush Street)

Bush Street (Regional Road 11) between Old Main Street and Winston Churchill Boulevard is a two-lane, east-west major road, approximately 2.1 km in length. In the village of Belfountain, it has urban characteristics at a 40 km/h speed limit, with numerous driveways for homes and businesses. West of the community, Bush Street has a rural cross-section. The vertical alignment of Bush Street rises with a 9-10% grade from the east as it approaches Shaws Creek Road, with a sharp vertical crest east of the Shaws Creek Road intersection. West of Shaws Creek Road, the vertical alignment is relatively flat with some moderate crests and sags. West of the community of Belfountain, the posted speed limit varies between 40 km/h and 80 km/h. Bush Street falls under the Region of Peel's jurisdiction.

The existing cross-section of Bush Street outside the community of Belfountain consists of two 3.2-3.8 m travel lanes with partially paved shoulders ranging between 1.3-3.5 m (of which 0.2-1.5 m is paved). The right-of-way along Bush Street, west of Belfountain Village to Shaws Creek Road is predominantly 20 m, but ranges between 20-25 m. In the section of Bush Street from Shaws Creek Road to Winston Churchill Boulevard, the right-of-way is predominantly 30 m, but ranges from 30-45 m. The range of dimensions for the different cross-sectional elements along the corridor is shown in **Exhibit 1-6**.

Bush Street intersects Winston Churchill Boulevard at two off-set intersections located on the reverse curve on Bush Street. The north leg of Winston Churchill Boulevard is offset approximately 80 m west of the south leg.

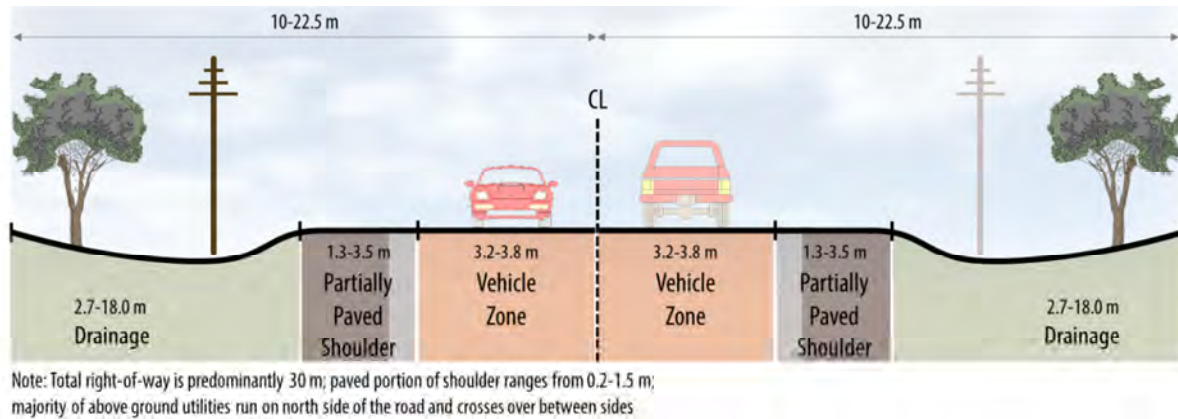


Exhibit 1-6: Bush Street Existing Cross Section

1.2 Study Objectives

To undertake the assessment and analysis for the two subject roads (Winston Churchill Boulevard and Olde Base Line Road), the following primary study objectives were addressed:

- Review existing drainage patterns and prepare a drainage mosaic for cross culverts and drainage system, and determine peak design flows;
- Carry out hydrology and hydraulic analysis for cross culverts for the design storm events;
- Review the existing capacity of culverts and identify inadequacies;
- Recommend sizing for culvert upgrades;

1.3 Data Collection and Review

The following information was also reviewed in the preparation of the report:

- *Summary of Findings (Draft) rev.1 Minor Culvert Condition Survey along Bush Street, Mississauga Road, Olde Baseline Road and Winston Churchill Boulevard, Belfountain ON*, dated September 4, 2013 prepared by Coffey Geotechnics Inc.;
- Survey (November 2012), Murray Layout Inc. (Auto CAD data file);
- Preferred Design Drawings (Plan as of PIC #2 - November 2013 and Profile as of January 2014);
- Region of Peel, Public Works Design, Specifications & Procedures Manuals for Linear Infrastructure
 - Storm Sewer Design Criteria (Revised July 2009)
 - Regional Roads and Traffic (Revised February 2010)
- Credit Valley Conservation Stormwater Management Guidelines (August 2012);
- Credit Valley Conservation Standard Parameters Document;
- Soil Map of Peel County, Soil Survey Report No. 18;
- Geography Network Canada Ontario Basic Mapping (OBM) topographic base map (GIS mapping, retrieved online September 5, 2012).
- *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft, June 2010* prepared by Dillon Consulting Limited.

2. SUMMARY OF CULVERT ASSESSMENT REPORT

An assessment of the road drainage system for Winston Churchill Boulevard and Olde Base Line Road, is included in the *Summary of Findings (Draft) rev.1 Minor Culvert Condition Survey along Bush Street, Mississauga Road, Olde Baseline Road and Winston Churchill Boulevard, Belfountain ON*, dated September 4, 2013 prepared by Coffey Geotechnics Inc. The centreline culvert recommendations, for Winston Churchill Boulevard and Olde Base Line Road, from this report and HDR's site visit (September 2013) are summarized in **Table 2-1**. Culvert locations and corresponding identification numbers are illustrated in **Appendix A**.

The results of the culvert condition survey indicated that five (5) culverts along Olde Base Line Road require repair and/or flushing and/or re-grading; zero (0) culverts require replacement. Along Winston Churchill Boulevard two (2) culverts require replacement due to poor condition, and fourteen (14) culverts require repair and/or flushing and/or re-grading.

Table 2-1: Existing Culvert Inspection Recommendations – Cross Culverts

Culvert ID	Coffey Report ID	Type / Material	Shape	Size (mm)	Length (m)	Flow Direction	Overall Condition	Recommendation
Olde Base Line Road								
OBL-01	N/A	CSP	Circular	450	12.50	N-S		Culvert was not picked up on survey or culvert inspection. Repair damage on north end, flush and cleanout, re-grade ditch.
OBL-02	CUL-012-140	CSP	Circular	600	14.30	N-S	Good	Do Nothing.
OBL-03	CUL-012-141	CSP	Circular	600	15.90	N-S	Good	Do Nothing.
OBL-04	CUL-012-150	RCB	Box	3300 x 1200	23.10	N-S	Good	Do Nothing.
OBL-05	CUL-012-152	CSP	Circular	450	12.50	N-S	Fair	Repair south end, flush and re-grade.
OBL-06	CUL-012-142	HDPE	Circular	450	20.50	N-S	Good	Do Nothing.
OBL-07	CUL-012-143	HDPE	Circular	450	12.00	N-S	Good	Do Nothing.
OBL-08	CUL-012-144	RCB	Box	3050 x 1400	26.60	N-S	Good	Do Nothing.
OBL-09	CUL-012-146	CSP	Circular	400	10.50	S-N	Poor	Flush culvert and re-grade
OBL-10	CUL-012-147	CSP	Circular	400	12.35	N-S	Poor to Fair	Repair north end.
OBL-11	CUL-012-148	CSP	Circular	400	12.30	N-S	Poor to Fair	Repair south end.
Winston Churchill Boulevard								
WCB-01	N/A	CSP	Circular	250 (Twin)	13.50	E-W		Re-ditch on east end, particularly north of the culvert.
WCB-02	CUL-019-351	CSP	Circular	400	12.20	E-W	Fair to Poor	Flush and repair west end.
WCB-03	CUL-019-350	CSP	Circular	400	12.10	E-W	Poor	Replace.
WCB-04	CUL-019-349	CSP	Circular	400	13.75	W-E	Fair to Good	Repair west end.
WCB-05	CUL-019-348	CSP	Circular	400	12.80	E-W	Fair	Repair west end.
WCB-06	CUL-019-347	CSP	Circular	600	11.00	E-W	Fair	Flush culvert.
WCB-07	CUL-019-346	CSP	Circular	400	12.35	E-W	Poor	Flush and repair.
WCB-08	CUL-019-345	HDPE	Circular	600	13.60	E-W	Good	Do Nothing.
WCB-09	CUL-019-344	CSP	Arch	1400 x 900	15.50	E-W	Fair	Flush culvert.

Culvert ID	Coffey Report ID	Type / Material	Shape	Size (mm)	Length (m)	Flow Direction	Overall Condition	Recommendation
WCB-10	CUL-019-343	CSP	Circular	400	12.70	E-W	Fair	Flush and repair east end.
WCB-11	CUL-019-397	CSP	Circular	400	15.50	W-E	Fair to Poor	Flush and repair east end.
WCB-12	CUL-019-396	CSP	Circular	600	18.20	W-E		Repair east end.
WCB-13	CUL-019-388	CSP	Circular	400	16.00	W-E	Poor	Flush and repair culvert.
WCB-14	CUL-019-394	CSP	Circular	450	22.20	E-W	Fair to Poor	Replace.
WCB-15	CUL-019-393	CSP	Circular	450	18.20	E-W	Fair to Good	Repair west end.
WCB-16	CUL-019-392	CSP	Circular	750	14.90	W-E	Fair	Flush and repair.
WCB-17	CUL-019-391	CSP	Circular	900	15.00	E-W	Good	Do Nothing.
WCB-18	CUL-019-390	CSP	Circular	900	23.00	E-W	Good	Flush and remove debris.
Notes: <ol style="list-style-type: none"> 1. CSP – Corrugated Steel 2. HDPE – High Density Polyethylene 3. RCB – Rigid Concrete Box 4. Only cross-culverts within the project limits are listed in Table 2-1. 								

3. CAPACITY ASSESSMENT

Based on the Study objectives a hydraulic capacity assessment of all cross culverts within the study area was undertaken for both the existing and proposed conditions. Culverts that transverse either Winston Churchill Boulevard or Olde Base Line Road are considered “cross culverts”. The results are summarized in **Sections 3.2** and **3.3** below. Driveway / entrance culverts are discussed in **Section 3.4**.

3.1 Design Criteria

The Region of Peel has, in practice, adopted the Ministry of Transportation Directive B-100 (MTO, October 16, 1980) and more recently the MTO Drainage Design Standards (2008) which requires that all hydraulic crossings be designed to allow the specified freeboard between the edge of travelled way and the upstream water surface elevation for specified storm events. Under the rural arterial classification, culverts with a total span up to 6m are designed for the 25 year design storm event (MTO Standard WC-1). The hydraulic freeboard requirements are as follows:

- The required freeboard for the assessment of crossings that are not classified as watercourses has been specified as 0.3 m (MTO Standard SD-13) which is a minor crossing and conveys runoff from a local external catchment area.
- The required freeboard for the assessment of crossings that are designated as watercourses, has been specified as 1.0 m for culvert crossings on arterial roads (MTO Standard WC-7).

Credit Valley Conservation has designated the following crossings as ‘watercourses’: On Olde Base Line Road, crossings OBL-02, OBL-04 and OBL-08; on Winston Churchill Boulevard, crossings WCB-06, WCB-09, WCB-14 and WCB-16. Crossings designated as watercourses are to be designed to be flood-free under the 100 year and Regional storm events, whichever is greater, as feasible. As directed by CVC, all watercourse crossings should be open-bottom with sizing based on hydraulic analysis and a fluvial geomorphologic considerations.

In addition to the above, the Region of Peel Design Guidelines stipulate that culverts crossing Regional Roads are to have a minimum 600 mm diameter and driveway culverts are to have a minimum 375mm diameter (inside diameter). Pipes are to be comprised of Corrugated Steel (CS), Polyethylene (PE) or an approved equivalent.

Storm Sewers

Storm sewers are to be designed using the local municipality’s intensity, duration and frequency rainfall curves for a 10 year storm with 15 minute inlet time for the roadway of way only. In the event the storm water catchment area includes areas beyond the right of way, the inlet time shall be calculated using the local municipality drainage calculation sheets

and appropriate rainfall intensity tables. Pipe sizing shall be for full flow with a minimum velocity of 0.75 m/s and a maximum velocity of 3.5 m/s.

3.2 Evaluation of Cross Culverts – Existing Conditions

3.2.1 Existing Condition Hydrologic Assessment

Hydrologic modelling, for the 25 year storm event, was undertaken for a total of 29 cross culverts (11 on Olde Base Line Road and 18 on Winston Churchill Boulevard). The hydrologic assessment was conducted to quantify the design peak flow to be conveyed by each culvert. A combination of spreadsheet calculations and hydrologic models (SWMHYMO) were utilized to establish the single event flow rates. Both models utilize Intensity-Duration Frequency (IDF) curves established by the CVC Stormwater Management Guidelines and CVC Standard Parameters documents.

3.2.1.1 Drainage Area Characterization

The drainage area tributary to each of the 29 cross culverts were established using a detailed Geographic Information System (GIS) analysis (consisting of topographic maps and contour data) and survey base mapping and aerial photography. **Appendix A** presents the culvert locations and catchment area plan for the 29 cross culvert locations.

Based on the Soil Map of Peel County (Soil Survey Report No. 18, November 1955), the majority of the lands within the study area consist of Dumfries loam, Caledon loam or Farmington loam (See **Appendix B**).

The Rational Method was used to calculate the peak design flows for all culvert watershed areas, with the exception of two culverts on Olde Base Line Road, OBL-04 and OBL-08, as it provides an accurate estimate of peak design flows for watershed areas less than 100 hectares in size. For watershed areas greater than 100 hectares (OBL-04 and OBL-08) the SWMHYMO model was utilized to compute the 2 to 100 year peak flows as well as the Regional event. In addition, the SWMHYMO model was used to calculate the Regional storm peak flows at all CVC designated ‘watercourse’ crossings.

As the composite runoff coefficient was less than 0.40 for all contributing catchments, the time of concentration was calculated using the Airport Formula. The rainfall intensity, duration, and frequency (IDF) values were obtained from the CVC guidelines. A 24 hour Chicago distribution was used in the model for the 25 year design storm. These IDF values are also consistent with those used in the *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft, June 2010* prepared by Dillon Consulting Limited.

The hydrologic analysis accounts for the irregular topography of the Belfountain area, which is dotted with numerous pocket wetlands as well as more extensive complex wetland

systems. These features have a pronounced effect in reducing runoff and peak flows within a given catchment, through natural retention and detention of stormwater runoff. When coupled with infiltration and evaporation, these systems provide significant benefits in reducing the overall rate and volume of runoff.

A summary of the peak flows determined at each of the cross culvert locations on Olde Base Line Road and Winston Churchill Boulevard is provided in **Table 3-1**.

Table 3-1: Summary of Peak Design Flows Draining to Cross Culvert

Drainage Area ID / Culvert ID	Approximate Station Location	Peak Design Flow Calculations			
		Time of Concentration (min)	Design Storm (years)	Rainfall Intensity (mm/hr)	Peak Design Flow (m ³ /s)
Olde Base Line Road					
OBL-01	30+030	60.25	25	48.69	0.48
OBL-02	30+540	86.25	2	19.14	0.92
			5	26.61	1.28
			10	31.15	1.50
			25	37.43	1.80
			50	42.25	2.03
			100	46.33	2.23
			Regional	n/a	5.23*
OBL-03	30+715	62.46	25	47.45	0.49
OBL-04	30+940	103.90	2	n/a	1.08*
			5	n/a	1.97*
			10	n/a	2.68*
			25	n/a	3.69*
			50	n/a	4.60*
			100	n/a	5.41*
			Regional	n/a	14.78*
OBL-05	31+280	59.32	25	49.24	0.22
OBL-06	31+300	82.51	25	38.69	0.11
OBL-07	31+380	41.99	25	62.66	0.05
OBL-08	31+410	171.04	2	n/a	2.54*
			5	n/a	4.61*
			10	n/a	6.30*
			25	n/a	8.65*
			50	n/a	10.81*
			100	n/a	12.73*
			Regional	n/a	46.80*
OBL-09	32+080	29.97	25	78.15	0.24
OBL-10	32+230	25.38	25	86.6	0.09

Drainage Area ID / Culvert ID	Approximate Station Location	Peak Design Flow Calculations			
		Time of Concentration (min)	Design Storm (years)	Rainfall Intensity (mm/hr)	Peak Design Flow (m ³ /s)
OBL-11	32+340	83.97	25	38.19	0.89
Winston Churchill Boulevard					
WCB-01	40+030	47.76	25	57.36	0.05
WCB-02	40+480	43.35	25	61.31	0.15
WCB-03	40+660	53.81	25	52.78	0.13
WCB-04	40+870	34.69	25	71.15	0.08
WCB-05	41+110	28.07	25	81.41	0.05
WCB-06	41+400	55.21	2	26.53	0.20
			5	36.76	0.28
			10	43.05	0.33
			25	51.83	0.40
			50	58.39	0.45
			100	64.10	0.49
			Regional	n/a	1.25*
WCB-07	41+710	30.02	25	65.71	0.63
WCB-08	41+890	26.4	25	84.55	0.56
WCB-09	42+195	56.12	2	20.84	1.14
			5	28.95	1.58
			10	33.90	1.85
			25	40.76	2.22
			50	46.00	2.51
			100	50.46	2.75
			Regional	n/a	7.50*
WCB-10	42+750	23.15	25	91.48	0.19
WCB-11	43+130	26.28	25	84.78	0.070
WCB-12	43+210	41.18	25	62.47	0.18
WCB-13 ⁺	44+140	-	25	-	0
WCB-14	44+310	18.87	2	54.32	0.023
			5	73.69	0.031
			10	86.04	0.036
			25	102.82	0.043
			50	114.47	0.048
			100	125.95	0.053
			Regional	n/a	0.063

Drainage Area ID / Culvert ID	Approximate Station Location	Peak Design Flow Calculations			
		Time of Concentration (min)	Design Storm (years)	Rainfall Intensity (mm/hr)	Peak Design Flow (m ³ /s)
WCB-15	44+615	30.82	25	76.77	0.25
WCB-16	44+945	57.82	2	25.66	0.53
			5	35.57	0.74
			10	41.66	0.86
			25	50.15	1.04
			50	56.51	1.17
			100	62.04	1.28
			Regional	n/a	3.33*
WCB-17	45+095	87.14	25	37.14	1.16
WCB-18	45+865	80.72	25	39.33	1.73
Notes: * Design Flow determined from SWMHYMO model +WCB-13 Equalization Culvert Peak Design Flow calculated using Rational Method: $Q = 0.0028 * C * I * A$ Rainfall Intensity calculated using a rainfall intensity: $I_{25} = A * (T_C + B)^{-C}$ Time of concentration (for $C < 0.40$) calculated using Airport Formula: $T_C = (3.26 * (1.1 - C) * L^{0.5}) / (S_w^{0.33})$ T_C and Peak Flow calculations presented in Tables B-3.1 to B-3.4 in Appendix B.3 – Hydrologic Calculations					

3.2.2 Fluvial Geomorphic Assessment

A fluvial geomorphic assessment was completed for all culvert crossing locations designated by CVC as ‘watercourses’. The results of this assessment show the minimum size span necessary to accommodate channel morphologic characteristics. The locations and span recommendations are summarized in **Table 3-2** below.

Table 3-2: Geomorphic Assessment Recommendations

Crossing Location	Existing Culvert Size (mm)	Recommended Span (m)
OBL-02	600 CSP	3.0
OBL-04	3300 x 1200 RCB	6.0
OBL-08	3050 x 1400 RCB	6.0
WCB-06	600 CSP	1.5
WCB-09	1400 x 900 Arch	6.0
WCB-14	450 CSP	1.5
WCB-16	750 CSP	3.0

Complete results of the fluvial geomorphic assessment are documented under separate cover (*Caledon Road Improvements EA – Geomorphic Assessment*, dated May 2014 prepared by Parish Geomorphic)

3.2.3 Existing Condition Hydraulic Assessment

The hydraulic assessment was undertaken using Bentley's CulvertMaster software. The assessment indicated that under existing conditions, in order to meet the hydraulic design criteria, meeting Peel Region's minimum size requirements, and accounting for fluvial geomorphic considerations, eleven (11) culverts along Olde Base Line Road and fourteen (14) culverts along Winston Churchill Boulevard will require upgrading. Of these, eighteen (18) culverts require upgrade solely to meet the Region's minimum size requirement. Since the results of the fluvial geomorphic assessment indicated that all watercourse crossings would need to be upgraded to meet the recommended span the 2 – 100 year and Regional storm event analysis was not completed for existing conditions. However, this analysis was completed for the proposed conditions (see Section 3.3).

A summary of the existing cross culvert hydraulic performance is presented in **Table 3-3**; recommendations from the culvert condition survey and geomorphic assessment are also included. A summary of the CulvertMaster input parameters is provided in **Appendix D** along with the CulvertMaster model output files.

Table 3-3: Summary of Existing Cross Culvert Hydraulic Performance for the 25 Year Peak Flow and Recommendations

Drainage Area ID / Culvert ID	Culvert Size (mm)	Peak Design Flow (m ³ /s)	U/S Invert (m)	D/S Invert (m)	Length (m)	Slope (%)	CulvertMaster Calculations					Recommendations and Notes
							Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)	
Olde Base Line Road												
OBL-01	450	0.479	372.40	372.25	12.50	1.200	372.90	374.63	-1.73	372.48	0.44	Upgrade based on hydraulic analysis and minimum size requirements. Repair damage on north end, flush and cleanout, re-grade ditch based on CIR.
OBL-02	600	1.800	372.71	372.70	14.30	0.070	372.55	380.84	-8.29	373.31	0.61	Upgrade based on hydraulic analysis with consideration of 100 Year and Regional storm events and to meet geomorphic recommended span.
OBL-03	600	0.490	369.16	369.09	15.90	0.440	369.62	370.23	-0.61	369.62	0.46	Upgrade based on hydraulic analysis.
OBL-04	3300 x 1200	3.69*	369.35	369.25	23.10	0.433	370.23	370.25	-0.02	370.09	0.47	Consider upgrading to meet 100 Year and/or Regional storm events and to meet geomorphic recommended span.
OBL-05	450	0.220	371.80	371.62	12.50	1.464	372.41	372.41	0.00	372.01	0.33	Upgrade to minimum size requirements. Repair south end, flush and re-grade ditches based on CIR.
OBL-06	450	0.111	371.91	371.56	20.50	1.712	372.18	372.26	-0.08	371.90	0.23	Upgrade based on hydraulic analysis and minimum size requirements.
OBL-07	450	0.049	370.92	370.73	12.00	1.558	371.35	371.14	0.21	371.03	0.15	Upgrade to minimum size requirements.
OBL-08	3050 x 1400	8.6*	370.22	370.19	26.60	0.102	371.15	371.90	-0.75	371.36	0.93	Consider upgrading based on hydraulic analysis to meet 100 Year and/or Regional storm events and to meet geomorphic recommended span..
OBL-09	400	0.244	372.54	372.48	10.50	0.533	373.16	373.72	-0.56	372.86	0.35	Upgrade based on hydraulic analysis and minimum size requirements. Flush culvert and re-grade ditched based on CIR.
OBL-10	400	0.094	373.56	373.42	12.35	1.190	373.79	373.94	-0.16	373.73	0.22	Upgrade based on hydraulic analysis and minimum size requirements. Repair north end based on CIR.
OBL-11	400	0.892	373.24	372.91	12.30	2.675	373.64	385.88	-12.25	373.11	0.40	Upgrade based on hydraulic analysis and minimum size requirements. Repair south end based on CIR.
Winston Churchill Boulevard												
WCB-01	250 (Twin)	0.045	372.44	372.15	13.5	2.148	372.58	373.25	-0.67	372.34	0.12	Upgrade based on hydraulic analysis and minimum size requirements. Re-ditch on east end, particularly north of the culvert based on CIR.

Drainage Area ID / Culvert ID	Culvert Size (mm)	Peak Design Flow (m ³ /s)	U/S Invert (m)	D/S Invert (m)	Length (m)	Slope (%)	CulvertMaster Calculations					Recommendations and Notes
							Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)	
WCB-02	400	0.154	381.34	381.15	12.2	1.541	381.65	381.87	-0.22	381.49	0.28	Upgrade based on hydraulic analysis and minimum size requirements. Flush and repair west end based on CIR.
WCB-03	400	0.134	382.82	382.79	12.1	0.207	383.34	383.42	-0.08	383.13	0.27	Upgrade based on hydraulic analysis, minimum size requirements and CIR.
WCB-04	400	0.084	385.21	384.85	13.75	2.582	385.22	385.57	-0.35	385.16	0.21	Upgrade based on hydraulic analysis and minimum size requirements. Repair west end based on CIR.
WCB-05	400	0.051	392.33	392.28	12.8	0.406	392.88	392.61	0.27	392.56	0.16	Upgrade to minimum size requirements. Repair west end based on CIR.
WCB-06	600	0.396	393.03	392.96	11	0.700	393.61	393.79	-0.18	393.46	0.41	Upgrade based on hydraulic analysis with consideration of 100 Year and Regional storm events and to meet geomorphic recommended span. Flush culvert based on CIR.
WCB-07	400	0.630	393.07	392.94	12.35	1.061	393.60	399.63	-6.03	393.34	0.4	Upgrade based on hydraulic analysis and minimum size requirements. Flush and repair based on CIR.
WCB-08	600	0.556	394.27	394.00	13.6	1.985	395.18	395.07	0.11	394.55	0.49	Do Nothing
WCB-09	1400 x 900	2.224	399.91	399.85	15.5	0.387	400.52	401.26	-0.74	400.63	0.66	Upgrade based on hydraulic analysis with consideration of 100 Year and Regional storm events and to meet geomorphic recommended span. Flush culvert based on CIR.
WCB-10	400	0.191	417.62	417.38	12.7	1.890	418.33	418.33	0.00	417.74	0.32	Upgrade to minimum size requirements. Flush and repair east end based on CIR.
WCB-11	400	0.069	425.25	425.17	15.5	0.516	425.95	425.57	0.38	425.47	0.19	Upgrade to minimum size requirements. Flush and repair east end based on CIR.
WCB-12	600	0.175	424.86	424.42	18.2	2.418	426.90	425.32	1.58	424.86	0.27	Repair east end based on CIR.
WCB-13	400	0	424.69	424.55	16	0.875	Equalization Culvert					Upgrade to minimum size requirements.
WCB-14	450	0.004	419.61	419.09	22.2	2.360	421.16	419.68	1.48	419.33	0.04	Upgrade to minimum size requirements and to meet geomorphic recommended span. Replace based on CIR.
WCB-15	450	0.249	416.82	416.60	18.2	1.221	418.30	417.65	0.65	417.00	0.35	Upgrade to minimum size requirements. Repair west end based on CIR.

Drainage Area ID / Culvert ID	Culvert Size (mm)	Peak Design Flow (m ³ /s)	U/S Invert (m)	D/S Invert (m)	Length (m)	Slope (%)	CulvertMaster Calculations					Recommendations and Notes
							Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)	
WCB-16	750	1.037	410.30	409.82	14.9	3.255	411.32	411.64	-0.32	410.51	0.63	Upgrade based on hydraulic analysis with consideration of 100 Year and Regional storm events and to meet geomorphic recommended span. Flush and repair based on CIR.
WCB-17	900	1.157	408.45	408.41	15	0.267	409.93	409.69	0.24	409.18	0.63	Do Nothing.
WCB-18	900	1.733	389.93	389.88	23	0.257	392.79	392.07	0.71	390.71	0.77	Flush and remove debris based on CIR.

*OBL-04 and OBL-08 - Peak Design Flow determined from SWMHYMO model.

3.3 Evaluation of Cross Culverts – Proposed Conditions

3.3.1 Proposed Condition Hydrologic Assessment

Similar to the Existing Conditions Assessment, a hydrologic analysis was completed for the current land use conditions to assess the hydraulic performance of the proposed drainage system. In addition, for all CVC designated watercourse crossings, additional hydrologic analysis was completed to identify peak flows for the 2, 5, 10, 25, 50, 100 and Regional storm events.

Under future conditions, the drainage area tributary to each of the 29 cross culverts would remain predominantly unchanged. A combination of spreadsheet calculations and hydrologic models (SWMHYMO) were utilized to establish the storm event peak flow rates. Both models utilize Intensity-Duration Frequency (IDF) curves established by the CVC Stormwater Management Guidelines and CVC Standard Parameters documents.

3.3.2 Proposed Condition Hydraulic Assessment

The hydraulic assessment was based on the preliminary proposed horizontal road design (as of PIC #2 - November 2013) and vertical profile design as of January 2014. Similar to the existing conditions assessment, hydraulic modelling was completed using Bentley's CulvertMaster software. A summary of the proposed cross culvert hydraulic performance is presented in **Table 3-4**. A listing of CulvertMaster input and output parameters are presented in **Appendix E**.

3.3.2.1 Cross-Culverts (Non-Watercourse)

Where possible, the roadway profile was adjusted to ensure that the minimum culvert diameter could be provided (i.e. 600mm). The assessment indicated that under the proposed conditions, for the 25 year storm event, most of the culverts will now meet the required freeboard (0.3 m) based on the proposed upgrades. Where the "Delta Headwater" column shows a negative value, this indicates that the required freeboard at the culvert crossing has not been met, in spite of any upgrades to the culvert. This is discussed more fully below:

Culvert OBL-06 – Due to roadway profile constraints, upgrading this culvert to the minimum 600mm diameter is not feasible. In order to achieve the required freeboard, a second 450mm culvert cell was added, which reduced the headwater elevation at the inlet sufficiently to meet the required design criteria.

Culvert OBL-11 – The proposed upgrade to a twin 600 mm diameter CSP is based on meeting the 0.3 metre freeboard requirement as well as meeting the culvert minimum size requirements. Based on the hydraulic analysis, the proposed upgrade will provide a major

improvement over existing conditions and eliminate potential overtopping of the roadway, despite not fully meeting the freeboard requirements.

3.3.2.2 Cross-Culverts (CVC Designated Watercourses)

As noted in **Section 3.1** (Design Criteria) crossings designated as a Watercourse by the CVC are to be designed to be flood free for the 100 year and Regional storm events, whichever is greater (as feasible). In addition, they should be open-bottom with sizing based on both hydraulic analysis and fluvial geomorphic assessment. The assessment indicated that under proposed conditions, for the 100 year and/or Regional storm events, all of the CVC designated watercourse crossings will not meet the required criteria for flood free (i.e. no overtopping) conditions. With respect to the 25 year storm event only two culverts, WCB-09 and WCB-16, will meet the required freeboard of 1.0 meter. This is shown where the “Delta Headwater” column shows a negative value, indicating that the required freeboard at the culvert crossing has not been met, in spite of any upgrades to the culvert. This is discussed more fully below:

Culvert OBL-02 – This culvert was upgraded from a 600mm pipe to an open bottom concrete box culvert of dimensions 3.0m x 1.2m which significantly increases the capacity of this crossing of the Rogers Creek tributary (Tributary ‘B’). Based on the hydraulic assessment, under existing conditions, overtopping of the roadway would occur during the 25 year storm event. Under proposed conditions for this event the culvert would not meet the requisite freeboard of 1.0 meter but the resulting headwater elevation would remain approximately 0.7 meters below the roadway edge of pavement. Similarly, under the 100 year and Regional storm events overtopping of the road will not occur as the resultant headwaters would remain at approximately 0.6 meters and 0.2 meters below the roadway edges of pavement respectively. The proposed culvert meets the 3.0m span recommended by the fluvial geomorphic assessment.

Culvert OBL-04 – This culvert conveys flow along Tributary ‘A’ of Rogers Creek. The existing culvert is 3.3m x 1.2m concrete box culvert and is in good condition. Under the 25 year storm flow conditions, the culvert would not meet the requisite freeboard, but the upstream headwater would remain approximately 0.9 metres below the roadway edge of pavement. Similarly, the 100 year event will not overtop the roadway, with a freeboard of 0.7 metres. Under Regional storm conditions however, overtopping of the road will occur. The fluvial geomorphic assessment recommends that this crossing have a minimum 6.0m span. However, it is not recommended to upgrade this culvert or raise the roadway profile further for the following reasons:

- The existing culvert is structurally stable and in good condition;
- There is no historical evidence that overtopping of the roadway has occurred at this crossing (through discussions with local property owners)
- Based on the hydraulic analysis, no overtopping is expected to occur under the 25 or 100 year storm events;
- Raising the roadway profile would potentially increase flooding upstream of the Culvert OBL-4 under the Regional storm event. Consequently, any increase in the

overtopping elevation would have a corresponding increase in the flood elevation upstream of the crossing.

Culvert OBL-08 – This culvert conveys flows along Tributary ‘A’ of Second Creek. The existing culvert is a 3.05m x 1.4m concrete box culvert and is in excellent condition. Under the 25 year storm event, the culvert would not meet the requisite freeboard, but the upstream headwater would remain approximately 0.2 metres below the roadway edge of pavement. Similarly, the 100 year event will not overtop the roadway, with a freeboard of 0.6 metres. Under Regional storm conditions however, overtopping of the road will occur. The fluvial geomorphic assessment recommends that this crossing have a minimum 6.0m span. However, due to the very shallow profile of Olde Base Line Road at this location, it is not recommended to upgrade this culvert nor raise the roadway profile due to the following:

- The existing culvert is structurally stable and in good condition;
- There is no historical evidence that overtopping of the roadway has occurred at this crossing (through discussions with local property owners)
- Based on the hydraulic analysis, no overtopping is expected to occur under the 25 or 100 year storm events;
- Raising the roadway profile would potentially increase flooding upstream of the Culvert OBL-08 under the Regional storm event. Consequently, any increase in the overtopping elevation would have a corresponding increase in the flood elevation upstream of the crossing.

Culvert WCB-06 – This culvert was upgraded from a 600mm pipe to an open bottom concrete box culvert of dimensions 1.8m x 0.6m which significantly increases the capacity of this unnamed watercourse. Under proposed conditions, for the 25 year, storm event, the culvert would not meet the requisite freeboard of 1.0 meter but the resulting headwater elevation would remain approximately 0.4 meters below the roadway edge of pavement. Similarly, under the 100 year and Regional storm events overtopping of the road will not occur as the resultant headwaters would remain at approximately 0.4 meters and 0.1 meters below the roadway edges of pavement respectively. The proposed culvert exceeds the minimum 1.5m span recommended by the fluvial geomorphic assessment.

Culvert WCB-09 – This culvert conveys flows along Tributary ‘C’ of Rogers Creek. An upgrade to the existing culvert (1.4m x 0.9m pipe arch) to an open bottom concrete box culvert of dimensions 6.0m x 1.5m is proposed which significantly increases the capacity of this watercourse. The proposed 6.0m span is a recommendation from the fluvial geomorphic assessment. Under proposed conditions, for the 25 year storm event, the resulting headwater elevation will meet the 1.0 metre freeboard requirement. Similarly, a resultant freeboard of 1.2 meters will be provided for the 100 year storm event. Under the Regional storm conditions the resultant freeboard will be 1.1 meters and overtopping of the roadway will not occur.

Culvert WCB-14 – This culvert was upgraded from a 450mm pipe to the minimum size open bottom concrete box culvert (1.8m x 0.9m). This significantly increases the capacity of this unnamed watercourse. Under proposed conditions, for the 25 year storm event, the

resulting headwater elevation will greatly exceed the 1.0 meter freeboard requirement. Similarly, a resultant freeboard of 6.8 meters will be provided for both the 100 year and Regional storm events. Overtopping of the roadway will not occur. The proposed culvert exceeds the minimum 1.5m span recommended by the fluvial geomorphic assessment.

Culvert WCB-16 – This culvert was upgraded from a 750mm pipe to an open bottom concrete box culvert of dimensions 3.0m x 1.2m which significantly increases the capacity of this unnamed watercourse. The proposed 3.0m span is a recommendation from the fluvial geomorphic assessment. Under proposed conditions, for the 25 year storm event, the culvert will meet the requisite freeboard of 1.0 meter. Under the 100 year and Regional storm events overtopping of the road will not occur as the resultant headwaters would remain at approximately 1.0 meters and 0.6 meters below the roadway edges of pavement respectively.

3.3.2.3 Equalization Culvert

An equalization culvert is a culvert that is used to balance the elevation of water on both sides of a roadway crossing location. Typically, there is no positive drainage outlet (e.g. to a receiving watercourse) on either side of the crossing. As such, drainage is confined and water levels will fluctuate as a result of surface runoff and or changes to groundwater levels. There is one culvert in the study area (WCB-13) that functions as an equalization culvert allowing wetland flow to move from one side of the road to the other. This culvert was upgraded from a 400mm pipe to the minimum 600mm diameter pipe as per Region of Peel standards.

Table 3-4: Summary of Proposed Conditions Cross Culvert Hydraulic Performance

Drainage Area ID / Culvert ID	Existing Culvert Size (mm)	Proposed Culvert Size (mm)	Recommendation and Notes	Design Storm (years)	CulvertMaster Calculations				
					Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)
Olde Base Line Road									
OBL-01	450 CSP	Twin 600 CSP	Upgrade to twin 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. The culvert location will also be shifted approximately 15m east in order to obtain adequate cover over the proposed pipe. Existing invert elevations will be maintained.	25	373.00	372.93	0.06	372.71	0.32
OBL-02	600 CSP	3000 x 1200 PRCONC	Tributary B of Rogers Creek. Upgrade to an open bottom 3000 mm x 1200 mm box culvert based on hydraulic analysis and fluvial geomorphic assessment. Upgrade will provide a major improvement over existing conditions.	25	373.19	373.53	-0.34	373.47	0.33
				100	374.19	373.57	0.62	373.49	0.38
				Regional	374.19	373.95	0.24	373.64	0.67
OBL-03	600 CSP	-	Maintain existing culvert. Hydraulic upgrade no longer required due to proposed vertical profile modifications.	25	372.58	370.23	2.35	369.62	0.46
OBL-04	3300 x 1200 PRCONC	-	Tributary A of Rogers Creek. Maintain existing concrete box culvert. Hydraulic / fluvial geomorphic upgrade not recommended due to good culvert condition and roadway vertical profile constraints.	25	370.23	370.30	-0.07	370.10	0.50
				100	371.23	370.52	0.71	370.18	0.65
				Regional	371.23	370.26	-1.03	370.45	1.20

Drainage Area ID / Culvert ID	Existing Culvert Size (mm)	Proposed Culvert Size (mm)	Recommendation and Notes	Design Storm (years)	CulvertMaster Calculations				
					Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)
OBL-05	450 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on minimum size requirements. Re-grade ditches.	25	372.41	372.31	0.10	372.07	0.30
OBL-06	450 PE	Twin 450 HDPE	Twin existing 450 mm Ø culvert based on hydraulic analysis. Existing HDPE pipe was recently replaced, therefore maintain existing pipe and add second cell. Due to roadway vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible.	25	372.13	372.14	-0.01	371.87	0.16
OBL-07	450 HDPE	-	Existing HDPE pipe was recently replaced, therefore maintain exiting pipe.	25	371.56	371.14	0.42	371.03	0.15
OBL-08	3050 x 1400 PRCONC	-	Maintain existing concrete box culvert. Tributary A of Second Creek. Hydraulic / fluvial geomorphic upgrade not recommended due to good culvert condition and roadway vertical profile constraints.	25	371.07	371.90	-0.83	371.36	0.94
				100	372.07	371.51	0.56	371.50	1.21
				Regional	372.07	385.56	-13.49	371.65	1.52
OBL-09	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. Re-grade ditches.	25	374.29	373.11	1.18	372.94	0.32
OBL-10	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements.	25	374.43	373.89	0.54	373.81	0.19

Drainage Area ID / Culvert ID	Existing Culvert Size (mm)	Proposed Culvert Size (mm)	Recommendation and Notes	Design Storm (years)	CulvertMaster Calculations				
					Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)
OBL-11	400 CSP	Twin 600 CSP	Upgrade to twin 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. Upgrade will provide a major improvement over existing conditions and eliminate potential overtopping of the roadway.	25	373.81	374.06	-0.25	373.43	0.44
Winston Churchill Boulevard									
WCB-01	Twin 250 CSP	N/A	Existing culverts to be removed, and replaced by DICB and sewer.	25	N/A				
WCB-02	400 CSP	Twin 400 CSP	Upgrade to twin 400 mm Ø culvert based on hydraulic analysis. Maintain existing pipe and add additional cell. Due to vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible. Flush and repair west end of existing culvert.	25	381.66	381.67	-0.01	381.49	0.28
WCB-03	400 CSP	Twin 400 CSP	Replace existing culvert with twin 400 mm Ø culverts based on hydraulic analysis and condition assessment. Due to vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible.	25	383.28	383.17	0.11	383.08	0.18
WCB-04	400 CSP	600 CSP	Upgrade to 600 mm Ø culvert based on hydraulic analysis and minimum size requirements.	25	385.75	385.52	0.23	385.24	0.18

Drainage Area ID / Culvert ID	Existing Culvert Size (mm)	Proposed Culvert Size (mm)	Recommendation and Notes	Design Storm (years)	CulvertMaster Calculations				
					Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)
WCB-05	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements.	25	393.45	392.67	0.79	392.65	0.14
WCB-06	600 CSP	1800 x 600 PRCONC	Upgrade to an 1800 mm x 600 mm open bottom box culvert based on hydraulic analysis (exceeds fluvial geomorphic recommended span). Upgrade will provide a major improvement over existing conditions and eliminate potential overtopping of the roadway.	25	392.81	393.39	-0.58	393.35	0.17
				100	393.81	393.43	0.38	393.36	0.19
				Regional	393.81	393.68	0.13	393.44	0.36
WCB-07	400 CSP	700 CSP	Upgrade to 700 mm Ø CSP based on hydraulic analysis and minimum size requirements.	25	394.12	394.00	0.12	393.54	0.50
WCB-08	600 PE	-	Maintain existing culvert. Hydraulic upgrade not required.	25	395.36	395.07	0.29	394.55	0.49
WCB-09	1400 x 900 CSP	6000 x 1500 PRCONC	Upgrade to 6000 mm x 1500 mm open bottom box culvert based on fluvial geomorphic assessment	25	401.08	400.75	0.32	400.73	0.24
				100	402.08	400.89	1.19	400.75	0.28
				Regional	402.08	400.94	1.13	400.88	0.54
WCB-10	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on minimum size requirements.	25	418.35	418.11	0.24	417.82	0.28
WCB-11	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on minimum size requirements.	25	427.26	425.59	1.67	425.56	0.17
WCB-12	600 CSP	-	Maintain existing culvert and repair east end.	25	426.88	425.32	1.56	424.86	0.27

Drainage Area ID / Culvert ID	Existing Culvert Size (mm)	Proposed Culvert Size (mm)	Recommendation and Notes	Design Storm (years)	CulvertMaster Calculations				
					Maximum Allowable Headwater Elevation (m)	Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical Tailwater Elevation (m)	Critical Depth (m)
WCB-13	400 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on minimum size requirements.	-	Equalization Culvert				
WCB-14	450 CSP	1800 x 900 PRCONC	Upgrade to minimum 1800 mm x 900 mm open bottom box culvert based on CVC watercourse classification, fluvial geomorphic assessment and condition assessment.	25	426.55	419.69	5.86	419.69	0.3
				100	426.55	419.74	6.81	419.74	0.4
				Regional	426.55	419.79	6.76	419.79	0.5
WCB-15	450 CSP	600 CSP	Upgrade to 600 mm Ø CSP based on minimum size requirements.	25	418.53	417.37	1.16	417.06	0.32
WCB-16	750 CSP	3000 x 1200 PRCONC	Upgrade to 300000 mm x 1200 mm open bottom box culvert based on fluvial geomorphic assessment and hydraulic analysis.	25	410.77	410.72	0.05	410.54	0.23
				100	411.77	410.79	0.98	410.56	0.26
				Regional	411.77	411.22	0.55	410.68	0.50
WCB-17	900 CSP	-	Maintain existing culvert.	25	410.15	409.69	0.46	409.18	0.63
WCB-18	900 CSP	-	Maintain existing culvert. Flush and remove debris based on condition assessment.	25	392.97	392.07	0.90	390.71	0.77

3.4 Driveway Culverts

Driveway / entrance culverts impacted by the proposed corridor improvements will be replaced by like sizes or upgraded as required to meet the minimum proposed sizing in compliance with Region of Peel Design Guidelines. The Region of Peel Design Guidelines stipulates that driveway / entrance culverts (i.e. ditch crossings) are to have a minimum 375mm diameter (inside diameter). Pipes are to be comprised of Corrugated Steel (CS), Polyethylene (PE) or an approved equivalent.

4. SUMMARY

The proposed improvements to Old Base Line Road and Winston Churchill Boulevard will result in the upgrading / modification / removal of seven (7) culverts on Olde Base Line Road and fourteen (14) culverts on Winston Churchill Boulevard. These recommendations will be confirmed during detailed design. A summary of the proposed culvert recommendations is presented in **Table 4-1**.

Table 4-1: Summary of Culvert Recommendations

Culvert ID	Recommendations
OBL-01	Upgrade to twin 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. The culvert location will also be shifted approximately 15m east in order to obtain adequate cover over the proposed pipe. Existing invert elevations will be maintained.
OBL-02	Tributary B of Rogers Creek. Upgrade to 3000 x 1200 mm open bottom concrete box culvert based on fluvial geomorphic assessment and hydraulic analysis. Upgrade will provide a major improvement over existing conditions.
OBL-03	Maintain existing culvert. Hydraulic upgrade no longer required due to proposed vertical profile modifications.
OBL-04	Tributary A of Rogers Creek. Maintain existing (3300 x 1200mm) concrete box culvert. Hydraulic upgrade not feasible due to roadway vertical profile constraints.
OBL-05	Upgrade to 600 mm Ø CSP based on minimum size requirements. Re-grade ditches.
OBL-06	Twin existing 450 mm Ø culvert based on hydraulic analysis. Existing HDPE pipe was recently replaced, therefore maintain existing pipe and add second cell. Due to vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible.
OBL-07	Existing HDPE pipe was recently replaced, therefore maintain existing pipe.
OBL-08	Maintain existing (3050 x 1400mm) concrete box culvert. Tributary A of Second Creek. Hydraulic upgrade not feasible due to roadway vertical profile constraints.
OBL-09	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. Re-grade ditches.
OBL-10	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements.
OBL-11	Upgrade to twin 600 mm Ø CSP based on hydraulic analysis and minimum size requirements. Upgrade will provide a major improvement over existing conditions and eliminate potential overtopping of the roadway.
WCB-01	Existing culverts to be removed, and replaced by DICB and sewer.
WCB-02	Upgrade to twin 400 mm Ø culvert based on hydraulic analysis. Maintain

Culvert ID	Recommendations
	existing pipe and add additional cell. Due to vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible. Flush and repair west end of existing culvert.
WCB-03	Replace existing culvert with twin 400 mm Ø culverts based on hydraulic analysis and condition assessment. Due to vertical profile constraints upgrade to minimum size requirements (600 mm Ø) is not feasible.
WCB-04	Upgrade to 600 mm Ø culvert based on hydraulic analysis and minimum size requirements.
WCB-05	Upgrade to 600 mm Ø CSP based on hydraulic analysis and minimum size requirements.
WCB-06	Unnamed watercourse. Upgrade to 1800 x 600 mm open bottom concrete box culvert based on hydraulic analysis. Upgrade will provide a major improvement over existing conditions and eliminate potential overtopping of the roadway.
WCB-07	Upgrade to 700 mm Ø CSP based on hydraulic analysis and minimum size requirements.
WCB-08	Maintain existing culvert. Hydraulic upgrade not required.
WCB-09	Tributary C of Rogers Creek. Upgrade to 6000 x 1500 mm open bottom concrete box culvert based on fluvial geomorphic assessment.
WCB-10	Upgrade to 600 mm Ø CSP based on minimum size requirements.
WCB-11	Upgrade to 600 mm Ø CSP based on minimum size requirements.
WCB-12	Maintain existing culvert and repair east end.
WCB-13	Upgrade to 600 mm Ø CSP based on minimum size requirements.
WCB-14	Unnamed watercourse. Upgrade to 1800 x 900 mm open bottom box culvert based on CVC watercourse classification, fluvial geomorphic assessment and culvert condition assessment.
WCB-15	Upgrade to 600 mm Ø CSP based on minimum size requirements.
WCB-16	Unnamed watercourse. Upgrade to 3000 x 1200 mm open bottom concrete box culvert based on fluvial geomorphic assessment and hydraulic analysis.
WCB-17	Maintain existing culvert.
WCB-18	Maintain existing culvert. Flush and remove debris based on condition assessment.

5. NEXT STEPS

The next steps include development and completion of a Stormwater Management Plan.

Stormwater Management Practices (SWMP's) for the management of roadway runoff generally fall into two categories; those that address water quantity and those that manage water quality of surface runoff. Water quantity management issues relate to properly sizing watercourse crossings of the roadway corridor, as well as the conveyance of roadway runoff along the roadway corridor for minor and major storm events. In addition, water quantity management strategies can include the need for facilities to address downstream flood and erosion potential from the development (expansion) of the roadway right-of-way.

In terms of water quality, the SWMP's relate to the treatment of new pavement and where possible, the treatment of existing pavement; however, current legislation solely relates to the former. Typically, the treatment level is related to the standards defined in the watershed or sub-watershed planning study, which are dependant on the quality and sensitivity of the receiving stream system.

Various Best management practices or Stormwater Management practices are available to address both the quantity and quality of runoff from roadways. Due to the linear nature of roadway corridors, however, the full spectrum of stormwater management practices is typically not appropriate.

There are a number of SWMP's which can be used to treat runoff and / or control peak flows from roadway surfaces. These include the following:

- Wet ponds / wetlands / hybrids (generally linear facilities);
- Grassed swales;
- Oil-grit separators;
- Off-site stormwater management facilities; and
- Cash-in-lieu of on-site treatment.

The applicability of these SWMP's will be reviewed and appropriate measures identified to minimize potential water quantity and quality impacts related to the proposed road corridor improvements.

6. REFERENCES

Coffey Geotechnics Inc., *Summary of Findings (Draft) rev.1 Minor Culvert Condition Survey along Bush Street, Mississauga Road, Olde Baseline Road and Winston Churchill Boulevard, Belfountain ON*, September 4, 2013.

Dillon Consulting Limited, *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft*, June 2010.

Parish Geomorphic, *Caledon Road Improvements EA – Geomorphic Assessment – Final Report*, May 2014.

Regional Municipality of Peel, *Public Works Design, Specifications and Procedures Manual – Storm Sewer Design*, July 2009.

Regional Municipality of Peel, *Public Works Design, Specifications and Procedures Manual – Regional Roads and Traffic*, February 2010.

Credit Valley Conservation (CVC), *Stormwater Management Guidelines*, August 2012.

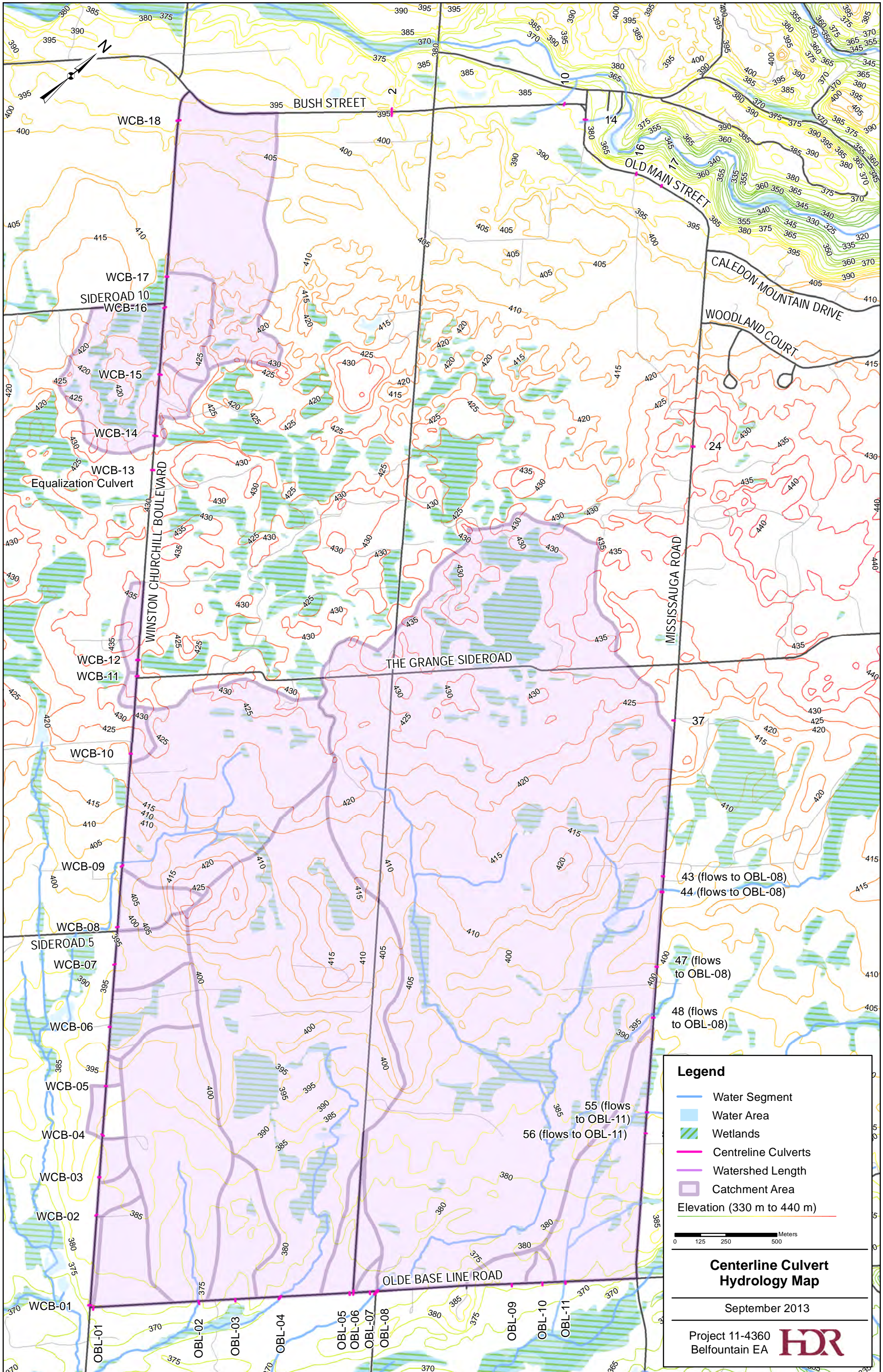
Credit Valley Conservation (CVC), *CVC Standard Parameters – Appendix B*.

Soil Survey of Peel County, Ontario 1953, Report No. 18 of the Ontario Soil Survey. Canada Department of Agriculture, Ottawa. Ontario Agricultural College, Guelph.

Experimental Farms Service, Dominion Department of Agriculture, Ottawa, *Soil Survey of Peel County, Ontario, Report No. 18*, 1953.

Appendix A

Hydrology Map



Legend


- Water Segment
- Water Area
- Wetlands
- Centreline Culverts
- Watershed Length
- Catchment Area
- Elevation (330 m to 440 m)

0 125 250 500 Meters

Centerline Culvert Hydrology Map

September 2013

Project 11-4360
Belfountain EA



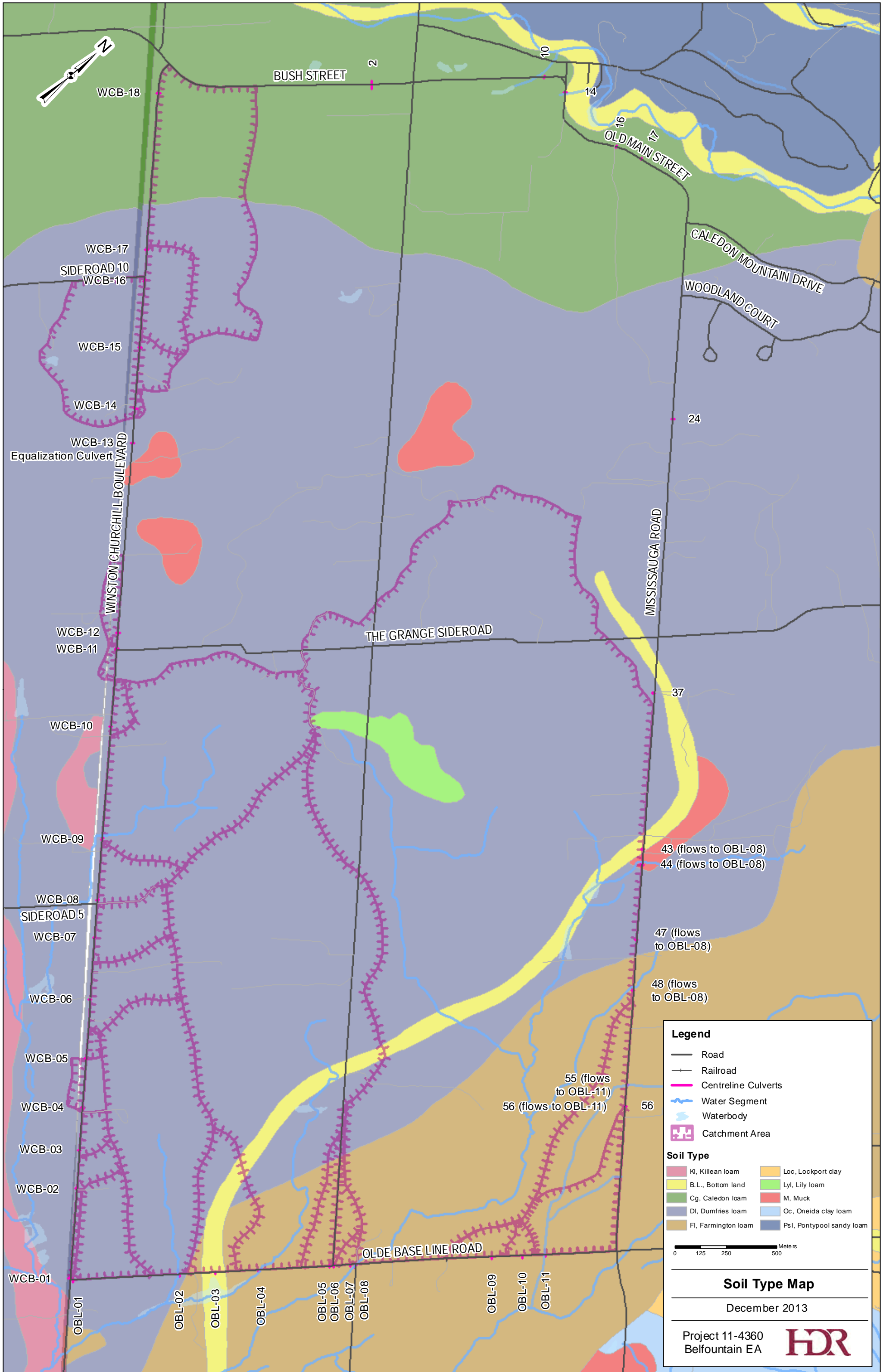
43 (flows to OBL-08)
44 (flows to OBL-08)

47 (flows to OBL-08)

48 (flows to OBL-08)

55 (flows to OBL-11)
56 (flows to OBL-11)

Appendix B
Soils Map



Legend

- Road
- +— Railroad
- Centreline Culverts
- Water Segment
- Waterbody
- Catchment Area

Soil Type

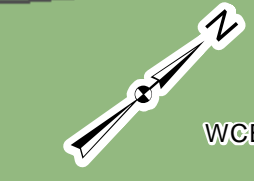
Ki, Killean loam	Loc, Lockport clay
B.L., Bottom land	Lyl, Lily loam
Cg, Caledon loam	M, Muck
Di, Dumfries loam	Oc, Oneida clay loam
Fi, Farmington loam	Psi, Pontypool sandy loam

0 125 250 500 Meters

Soil Type Map

December 2013

Project 11-4360
Belfountain EA



WCB-18
BUSH STREET
WCB-17
SIDEROAD 10
WCB-16
WCB-15
WCB-14
WCB-13
Equalization Culvert
WINSTON CHURCHILL BOULEVARD
WCB-12
WCB-11
WCB-10
WCB-09
WCB-08
SIDEROAD 5
WCB-07
WCB-06
WCB-05
WCB-04
WCB-03
WCB-02
WCB-01
OBL-01
OBL-02
OBL-03
OBL-04
OBL-05
OBL-06
OBL-07
OBL-08
OLDE BASE LINE ROAD
OBL-09
OBL-10
OBL-11
MISSISSAUGA ROAD
THE GRANGE SIDEROAD
OLD MAIN STREET
CALEDON MOUNTAIN DRIVE
WOODLAND COURT
2
10
14
16
24
37
43 (flows to OBL-08)
44 (flows to OBL-08)
47 (flows to OBL-08)
48 (flows to OBL-08)
55 (flows to OBL-11)
56 (flows to OBL-11)
56

Appendix C

Hydrologic Calculations

Appendix C.1.
Time of Concentration & Peak Design Flow
Calculations

OBL-01: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-01	OBL-01	12.65	715	1.678	12.0	0.22	0.475	1.004	0.256	0.084

Used

<<<input data in these squares only

OBL-01: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	12.65	3.54
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 12.65	3.54

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 60.25 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 48.69 mm/hr
 $I_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.28 co-efficient
- A= 12.65 ha
- i= 48.69 mm/hr

Compute design flow: Q= 0.479 m3/s

OBL-02: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-02	OBL-02	53.32	1650	1.697	28.0	0.23	0.948	1.437	0.446	0.159

Used

<<<input data in these squares only

OBL-02: Peak Flow Calculation (2 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 701.618 *A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency*
- B= 6.014 *Curves (CVC Standard Parameters - Appendix B)*
- C= 0.796
- tc= 86.25 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 19.14 mm/hr

$I_x = A^{tc+B} C^C$

Peak Flow Calculation - Rational Method

$Q=0.00278 \cdot C \cdot i \cdot A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 19.14 mm/hr

Compute design flow: Q= 0.921 m3/s

OBL-02: Peak Flow Calculation (5 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1025.002 *A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency*
- B= 7.559 *Curves (CVC Standard Parameters - Appendix B)*
- C= 0.804
- tc= 86.25 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 26.61 mm/hr

$I_x = A^{tc+B} \cdot C$

Peak Flow Calculation - Rational Method

$Q=0.00278 \cdot C \cdot i \cdot A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 26.61 mm/hr

Compute design flow: Q= 1.280 m3/s

OBL-02: Peak Flow Calculation (10 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1231.993 *A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency*
- B= 7.975 *Curves (CVC Standard Parameters - Appendix B)*
- C= 0.809
- tc= 86.25 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 31.15 mm/hr

$I_x = A^{tc+B} C^C$

Peak Flow Calculation - Rational Method

$Q=0.00278 \cdot C \cdot i \cdot A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 31.15 mm/hr

Compute design flow: Q= 1.499 m3/s

OBL-02: Peak Flow Calculation (25 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 86.25 mins (Airport Formula) Change cell based on method

Compute Intensity i= 37.43 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 37.43 mm/hr

Compute design flow: Q= 1.800 m3/s

OBL-02: Peak Flow Calculation (50 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1931.219 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 10.5 Curves (CVC Standard Parameters - Appendix B)
- C= 0.836
- tc= 86.25 mins (Airport Formula) Change cell based on method

Compute Intensity i= 42.25 mm/hr

$I_x = A^{tc+B} \cdot C^x$

Peak Flow Calculation - Rational Method

$Q=0.00278 \cdot C \cdot i \cdot A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 42.25 mm/hr

Compute design flow: Q= 2.032 m3/s

OBL-02: Peak Flow Calculation (100 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	37.32	13.06
2	15	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	8.00	2.24
3	15	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	8.00	2.00
Total	100.00			Total Area 53.32	17.30

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 2147.367 *A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency*
- B= 10.512 *Curves (CVC Standard Parameters - Appendix B)*
- C= 0.839
- tc= 86.25 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 46.33 mm/hr

$I_x = A^{tc+B} C^C$

Peak Flow Calculation - Rational Method

$Q=0.00278 \cdot C \cdot i \cdot A$

- C= 0.32 co-efficient
- A= 53.32 ha
- i= 46.33 mm/hr

Compute design flow: Q= 2.229 m3/s

OBL-03: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-03	OBL-03	15.10	770	1.905	14.7	0.28	0.490	1.041	0.258	0.088

Used

<<<input data in these squares only

OBL-03: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	98	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	14.80	3.70
2	2	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	0.30	0.02
				0.00	0.00
Total	100.00			Total Area 15.10	3.71

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 62.46 mins (Airport Formula) *Change cell based on method*

Compute Intensity i= 47.45 mm/hr
 $I_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.25 co-efficient
- A= 15.10 ha
- i= 47.45 mm/hr

Compute design flow: Q= 0.490 m3/s

OBL-05: Time of Concentration

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-05	OBL-05	5.73	635	1.470	9.3	0.17	0.469	0.989	0.200	0.076

Used

<<<input data in these squares only

OBL-05: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	5.73	1.60
2				0.00	0.00
3				0.00	0.00
Total	100.00			Total Area 5.73	1.60

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 59.32 mins (Airport Formula) Change cell based on method

Compute Intensity i= 49.24 mm/hr
 $I_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.28 co-efficient
- A= 5.73 ha
- i= 49.24 mm/hr

Compute design flow: Q= 0.220 m3/s

OBL-06: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-06	OBL-06	3.86	1070	1.246	13.3	0.10	0.850	1.375	0.185	0.114

Used

<<<input data in these squares only

OBL-06: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	40	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	1.54	0.39
2	60	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	2.32	0.65
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 3.86	1.03

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 38.69 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.27 co-efficient
- A= 3.86 ha
- i= 38.69 mm/hr

Compute design flow: Q= 0.111 m3/s

OBL-07: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-07	OBL-07	1.12	185	0.721	1.3	-0.14	0.186	0.700	0.147	0.030

Used

<<<input data in these squares only

OBL-07: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	1.12	0.28
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 1.12	0.28

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 *Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft*
- B= 9.457 *Chicago Storm, 25-year*
- C= 0.83
- tc=

Compute Intensity i= 62.66 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.25 co-efficient
- A= 1.12 ha
- i= 62.66 mm/hr

Compute design flow: Q= 0.049 m3/s

OBL-09: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-09	OBL-09	3.75	230	2.319	5.3	0.37	0.162	0.499	0.137	0.035

Used

<<<input data in these squares only

OBL-09: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	3.75	1.13
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 3.75	1.13

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 78.15 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.30 co-efficient
- A= 3.75 ha
- i= 78.15 mm/hr

Compute design flow: Q= 0.244 m3/s

OBL-10: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-10	OBL-10	1.56	175	3.048	5.3	0.48	0.127	0.423	0.086	0.028

Used

<<<input data in these squares only

OBL-10: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	1.56	0.39
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 1.56	0.39

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 86.60 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.25 co-efficient
- A= 1.56 ha
- i= 86.60 mm/hr

Compute design flow: Q= 0.094 m3/s

OBL-11: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
OBL-11	OBL-11	32.95	1355	1.771	24.0	0.25	0.810	1.399	0.362	0.137

Used

<<<input data in these squares only

OBL-11: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	50	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	16.48	4.94
2	40	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	13.18	3.30
3	10	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	3.30	0.16
				0.00	0.00
Total	100.00			Total Area 32.95	8.40

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 38.19 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.26 co-efficient
- A= 32.95 ha
- i= 38.19 mm/hr

Compute design flow: Q= 0.892 m3/s

WCB-01: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-01	WCB-01	1.00	460	1.739	8.0	0.24	0.391	0.796	0.094	0.059

Used

<<<input data in these squares only

WCB-01: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	1.00	0.28
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 1.00	0.28

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 57.36 mm/hr
 $i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.28 co-efficient
- A= 1.00 ha
- i= 57.36 mm/hr

Compute design flow: Q= 0.045 m3/s

WCB-02: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-02	WCB-02	3.08	270	0.988	2.7	-0.01	0.230	0.723	0.188	0.039

Used

<<<input data in these squares only

WCB-02: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	80	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	2.46	0.69
	20	Cultivated, flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	0.62	0.22
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 3.08	0.91

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 61.31 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.29 co-efficient
- A= 3.08 ha
- i= 61.31 mm/hr

Compute design flow: Q= 0.154 m3/s

WCB-03: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-03	WCB-03	2.60	290	0.460	1.3	-0.34	0.292	0.897	0.250	0.042

Used

<<<input data in these squares only

WCB-03: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Cultivated, flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	2.60	0.91
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 2.60	0.91

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 52.78 mm/hr
 $i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.35 co-efficient
- A= 2.60 ha
- i= 52.78 mm/hr

Compute design flow: Q= 0.134 m3/s

WCB-04: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-04	WCB-04	1.70	255	2.092	5.3	0.32	0.198	0.578	0.106	0.038

Used

<<<input data in these squares only

WCB-04: Peak Design Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	1.70	0.43
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 1.70	0.43

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 71.15 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.25 co-efficient
- A= 1.70 ha
- i= 71.15 mm/hr

Compute design flow: Q= 0.084 m3/s

WCB-05: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-05	WCB-05	0.90	150	1.778	2.7	0.25	0.128	0.468	0.089	0.025

Used

<<<input data in these squares only

WCB-05: Peak Design Flow

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	0.90	0.23
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.90	0.23

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 81.41 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.25 co-efficient
- A= 0.90 ha
- i= 81.41 mm/hr

Compute design flow: Q= 0.051 m3/s

WCB-06: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-06	WCB-06	11.96	510	1.569	8.0	0.20	0.345	0.920	0.258	0.064

Used

<<<input data in these squares only

WCB-06: Peak Flow Calculation (2 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 701.618 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 6.014 Curves (CVC Standard Parameters - Appendix B)
- C= 0.796
- tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 26.53 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.23 co-efficient
- A= 11.96 ha
- i= 26.53 mm/hr

Compute design flow: Q= 0.203 m3/s

WCB-06: Peak Flow Calculation (5 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1025.002 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 7.559 Curves (CVC Standard Parameters - Appendix B)
- C= 0.804
- tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 36.76 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.23 co-efficient
- A= 11.96 ha
- i= 36.76 mm/hr

Compute design flow: Q= 0.281 m3/s

WCB-06: Peak Flow Calculation (10 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1231.993 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 7.975 Curves (CVC Standard Parameters - Appendix B)
 C= 0.809
 tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 43.05 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 11.96 ha
 i= 43.05 mm/hr

Compute design flow: Q= 0.329 m3/s

WCB-06: Peak Flow Calculation (25 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1649.671 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 9.457 Curves (CVC Standard Parameters - Appendix B)
 C= 0.83
 tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 51.83 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 11.96 ha
 i= 51.83 mm/hr

Compute design flow: Q= 0.396 m3/s

WCB-06: Peak Flow Calculation (50 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1931.219 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.5 Curves (CVC Standard Parameters - Appendix B)
 C= 0.836
 tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 58.39 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 11.96 ha
 i= 58.39 mm/hr

Compute design flow: Q= 0.446 m3/s

WCB-06: Peak Flow Calculation (100 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	45	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	5.38	1.35
2	30	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.59	1.26
3	25	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	2.99	0.15
				0.00	0.00
Total	100.00			Total Area 11.96	2.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 2147.367 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.512 Curves (CVC Standard Parameters - Appendix B)
 C= 0.839
 tc= 55.21 mins (Airport Formula) Change cell based on method

Compute Intensity i= 64.10 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 11.96 ha
 i= 64.10 mm/hr

Compute design flow: Q= 0.490 m3/s

WCB-07: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 19-Dec-13
Modelled by: AR

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-07	WCB-07	9.86	650	4.103	26.7	0.61	0.370	0.652	0.154	0.078

Used

<<<input data in these squares only

WCB-07: Peak Design Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	19-Dec-13
Modelled by:	AR

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	40	Woodland hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.94	1.38
2	60	Cultivated flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	5.92	2.07
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 9.86	3.45

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 65.71 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.35 co-efficient
- A= 9.86 ha
- i= 65.71 mm/hr

Compute design flow: Q= 0.630 m3/s

WCB-08: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-08	WCB-08	7.22	440	8.182	36.0	0.91	0.225	0.440	0.099	0.057

Used

<<<input data in these squares only

WCB-08: Peak Design Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	1.81	0.72
2	25	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	1.81	0.63
3	50	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	3.61	1.01
				0.00	0.00
Total	100.00			Total Area 7.22	2.36

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 84.55 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.33 co-efficient
- A= 7.22 ha
- i= 84.55 mm/hr

Compute design flow: Q= 0.556 m3/s

WCB-09: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 19-Dec-13
Modelled by: AR

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-09	WCB-09	75.48	1200	1.889	22.7	0.28	0.651	1.282	0.486	0.124

Used

<<<input data in these squares only

WCB-09: Peak Flow Calculation (2 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 701.618 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 6.014 Curves (CVC Standard Parameters - Appendix B)
- C= 0.796
- tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 20.84 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.26 co-efficient
- A= 75.48 ha
- i= 20.84 mm/hr

Compute design flow: Q= 1.137 m3/s

WCB-09: Peak Flow Calculation (5 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1025.002 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 7.559 Curves (CVC Standard Parameters - Appendix B)
- C= 0.804
- tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 28.95 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.26 co-efficient
- A= 75.48 ha
- i= 28.95 mm/hr

Compute design flow: Q= 1.580 m3/s

WCB-09: Peak Flow Calculation (10 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1231.993 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 7.975 Curves (CVC Standard Parameters - Appendix B)
 C= 0.809
 tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 33.90 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.26 co-efficient
 A= 75.48 ha
 i= 33.90 mm/hr

Compute design flow: Q= 1.850 m3/s

WCB-09: Peak Flow Calculation (25 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 40.76 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.26 co-efficient
- A= 75.48 ha
- i= 40.76 mm/hr

Compute design flow: Q= 2.224 m3/s

WCB-09: Peak Flow Calculation (50 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1931.219 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.5 Curves (CVC Standard Parameters - Appendix B)
 C= 0.836
 tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 46.00 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.26 co-efficient
 A= 75.48 ha
 i= 46.00 mm/hr

Compute design flow: Q= 2.509 m3/s

WCB-09: Peak Flow Calculation (100 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	25	Woodland flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.25	18.87	4.72
2	20	Pasture hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.40	15.10	6.04
3	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	22.64	7.93
4	25	Lakes and wetlands (Ref: MTO Design Chart 1.07)	0.05	18.87	0.94
Total	100.00			Total Area 75.48	19.62

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 2147.367 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.512 Curves (CVC Standard Parameters - Appendix B)
 C= 0.839
 tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 50.46 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.26 co-efficient
 A= 75.48 ha
 i= 50.46 mm/hr

Compute design flow: Q= 2.753 m3/s

WCB-10: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
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Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-10	WCB-10	2.15	240	4.444	10.7	0.65	0.157	0.386	0.082	0.036

Used

<<<input data in these squares only

WCB-10: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	2.15	0.75
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 2.15	0.75

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 91.48 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.35 co-efficient
- A= 2.15 ha
- i= 91.48 mm/hr

Compute design flow: Q= 0.191 m3/s

WCB-11: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-11	WCB-11	1.05	170	2.353	4.0	0.37	0.135	0.438	0.083	0.028

Used

<<<input data in these squares only

WCB-11: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	1.05	0.29
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 1.05	0.29

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 84.78 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.28 co-efficient
- A= 1.05 ha
- i= 84.78 mm/hr

Compute design flow: Q= 0.069 m3/s

WCB-12: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-12	WCB-12	3.34	380	1.754	6.7	0.24	0.286	0.703	0.149	0.051

Used

<<<input data in these squares only

WCB-12: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	70	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	2.34	0.65
2	30	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	1.00	0.35
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 3.34	1.01

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 62.47 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.30 co-efficient
- A= 3.34 ha
- i= 62.47 mm/hr

Compute design flow: Q= 0.175 m3/s

WCB-14: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-14	WCB-14	0.50	100	2.667	2.7	0.43	0.084	0.314	0.059	0.018

Used

<<<input data in these squares only

WCB-14: Peak Flow Calculation (2 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-May-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 701.618 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 6.014 Curves (CVC Standard Parameters - Appendix B)
- C= 0.796
- tc= 18.87 mins (Airport Formula) Change cell based on method

Compute Intensity i= 54.32 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.30 co-efficient
- A= 0.50 ha
- i= 54.32 mm/hr

Compute design flow: Q= 0.023 m3/s

WCB-14: Peak Flow Calculation (5 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-May-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1025.002 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 7.559 Curves (CVC Standard Parameters - Appendix B)
- C= 0.804
- tc= 18.87 mins (Airport Formula) Change cell based on method

Compute Intensity i= 73.69 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.30 co-efficient
- A= 0.50 ha
- i= 73.69 mm/hr

Compute design flow: Q= 0.031 m3/s

WCB-14: Peak Flow Calculation (10 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-May-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1231.993 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 7.975 Curves (CVC Standard Parameters - Appendix B)
 C= 0.809
 tc= 18.87 mins (Airport Formula) Change cell based on method

Compute Intensity i= 86.04 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.30 co-efficient
 A= 0.50 ha
 i= 86.04 mm/hr

Compute design flow: Q= 0.036 m3/s

WCB-14: Peak Flow Calculation (25 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 102.82 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.30 co-efficient
- A= 0.50 ha
- i= 102.82 mm/hr

Compute design flow: Q= 0.043 m3/s

WCB-14: Peak Flow Calculation (50 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-May-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1931.219 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.5 Curves (CVC Standard Parameters - Appendix B)
 C= 0.836
 tc= 18.87 mins (Airport Formula) Change cell based on method

Compute Intensity i= 114.47 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.30 co-efficient
 A= 0.50 ha
 i= 114.47 mm/hr

Compute design flow: Q= 0.048 m3/s

WCB-14: Peak Flow Calculation (100 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-May-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	0.50	0.15
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 0.50	0.15

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 2147.367 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 10.512 Curves (CVC Standard Parameters - Appendix B)
- C= 0.839
- tc= 18.87 mins (Airport Formula) Change cell based on method

Compute Intensity i= 125.95 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.30 co-efficient
- A= 0.50 ha
- i= 125.95 mm/hr

Compute design flow: Q= 0.053 m3/s

WCB-15: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-15	WCB-15	3.89	260	2.564	6.7	0.41	0.179	0.514	0.133	0.038

Used

<<<input data in these squares only

WCB-15: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	100	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	3.89	1.17
				0.00	0.00
				0.00	0.00
				0.00	0.00
Total	100.00			Total Area 3.89	1.17

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 76.77 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.30 co-efficient
- A= 3.89 ha
- i= 76.77 mm/hr

Compute design flow: Q= 0.249 m3/s

WCB-16: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-16	WCB-16	32.33	920	3.333	30.7	0.52	0.485	0.964	0.269	0.101

Used

<<<input data in these squares only

WCB-16: Peak Flow Calculation (2 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 701.618 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 6.014 Curves (CVC Standard Parameters - Appendix B)
- C= 0.796
- tc= mins (Airport Formula) Change cell based on method

Compute Intensity i= 25.66 mm/hr

$I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.23 co-efficient
- A= 32.33 ha
- i= 25.66 mm/hr

Compute design flow: Q= 0.530 m3/s

WCB-16: Peak Flow Calculation (5 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1025.002 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 7.559 Curves (CVC Standard Parameters - Appendix B)
 C= 0.804
 tc= 57.82 mins (Airport Formula) Change cell based on method

Compute Intensity i= 35.57 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 32.33 ha
 i= 35.57 mm/hr

Compute design flow: Q= 0.735 m3/s

WCB-16: Peak Flow Calculation (10 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1231.993 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 7.975 Curves (CVC Standard Parameters - Appendix B)
 C= 0.809
 tc= 57.82 mins (Airport Formula) Change cell based on method

Compute Intensity i= 41.66 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 32.33 ha
 i= 41.66 mm/hr

Compute design flow: Q= 0.861 m3/s

WCB-16: Peak Flow Calculation (25 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 57.82 mins (Airport Formula) Change cell based on method

Compute Intensity i= 50.15 mm/hr

$I_x = A \cdot (tc + B)^C$

Peak Flow Calculation - Rational Method

$Q = 0.00278 \cdot C \cdot i \cdot A$

- C= 0.23 co-efficient
- A= 32.33 ha
- i= 50.15 mm/hr

Compute design flow: Q= 1.037 m3/s

WCB-16: Peak Flow Calculation (50 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

A= 1931.219 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
 B= 10.5 Curves (CVC Standard Parameters - Appendix B)
 C= 0.836
 tc= 57.82 mins (Airport Formula) Change cell based on method

Compute Intensity i= 56.51 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

C= 0.23 co-efficient
 A= 32.33 ha
 i= 56.51 mm/hr

Compute design flow: Q= 1.168 m3/s

WCB-16: Peak Flow Calculation (100 Year Storm Event)

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	3-Apr-14
Modelled by:	CH

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	60	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	19.40	5.82
2	10	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	3.23	1.13
3	30	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	9.70	0.48
				0.00	0.00
Total	100.00			Total Area 32.33	7.44

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 2147.367 A, B, & C parameters based on CVC Rainfall Intensity Duration Frequency
- B= 10.512 Curves (CVC Standard Parameters - Appendix B)
- C= 0.839
- tc= 57.82 mins (Airport Formula) Change cell based on method

Compute Intensity i= 62.04 mm/hr
 $I_x = A*(tc+B)^C$

Peak Flow Calculation - Rational Method

$Q=0.00278*C*i*A$

- C= 0.23 co-efficient
- A= 32.33 ha
- i= 62.04 mm/hr

Compute design flow: Q= 1.282 m3/s

WCB-17: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)	Airport (Use if C < 0.4)	Hyns	Kirpich
--------------------------------------	-----------------------------	------	---------

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-17	WCB-17	43.50	1030	1.036	10.7	0.02	0.666	1.452	0.517	0.111

Used

<<<input data in these squares only

WCB-17: Peak Flow Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	65	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	28.28	8.48
2	15	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	6.53	2.28
3	20	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	8.70	0.44
				0.00	0.00
Total	100.00			Total Area 43.50	11.20

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc=

Compute Intensity i= 37.14 mm/hr

$i_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.26 co-efficient
- A= 43.50 ha
- i= 37.14 mm/hr

Compute design flow: Q= 1.157 m3/s

WCB-18: Time of Concentration Calculation

Project: Belfountain EA
Project No.: 6776
Date: 9-Oct-13
Modelled by: CK

Enter runoff coefficient

Upland Method
 Other Equations

Bransby Williams (Use if C > 0.4)
 Airport (Use if C < 0.4)
 Hyns
 Kirpich

Culvert ID	Catchment ID	Area (ha)	Length (m)	Slope (%)	Height (m)	Log Slope (%)	Tc (hr)	Tc (hr)	Tc (hr)	Tc (hr)
WCB-18	WCB-18	52.77	1440	1.852	26.7	0.27	0.813	1.345	0.427	0.143

Used

<<<input data in these squares only

WCB-18: Peak Design Calculation

Composite Runoff Coefficient "C"

Project:	Belfountain EA
Project No.:	6776
Date:	9-Oct-13
Modelled by:	CK

Drainage Area ID	Area (%)	Land Use	Runoff Coefficient	Area (ha)	A x C
1	10	Woodland hilly slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	5.28	1.85
2	20	Woodland rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.30	10.55	3.17
3	20	Pasture rolling slopes - Loam (Ref: MTO Design Chart 1.07)	0.35	10.55	3.69
4	48	Pasture flat slopes - Loam (Ref: MTO Design Chart 1.07)	0.28	25.33	7.09
5	2	Lakes and Wetlands (Ref: MTO Design Chart 1.07)	0.05	1.06	0.05
Total	100.00			Total Area 52.77	15.85

Compute Composite C =>

<<<input data in these squares only

Rainfall Intensity (i)

- A= 1649.671 Using Dillon, June 2010, Bush Street & Mississauga Road Class EA Existing Conditions Drainage Report, Draft
- B= 9.457 Chicago Storm, 25-year
- C= 0.83
- tc= 80.72 mins (Airport Formula) Change cell based on method

Compute Intensity i= 39.33 mm/hr

$I_{25} = 1649.671 * (T_c + 9.457)^{-0.83}$

Peak Flow Calculation - Rational Method

$Q = 0.00278 * C * i * A$

- C= 0.30 co-efficient
- A= 52.77 ha
- i= 39.33 mm/hr

Compute design flow: Q= 1.733 m3/s

Appendix C.2. SWMHYMO Output

```

=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM 0 0 9 9 9 9
SSSSS W W W M M M H H H H Y M M M 0 0 ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M 0 0 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.com *****
*****

```

```

+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:27:53 RUN COUNTER: 000062 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\2yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\2yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\2yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001-----

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```


								2yr.out
4.50	.986	10.50	2.290	16.50	.846	22.50	.553	
4.67	1.026	10.67	2.170	16.67	.833	22.67	.548	
4.83	1.069	10.83	2.063	16.83	.820	22.83	.543	
5.00	1.118	11.00	1.968	17.00	.808	23.00	.538	
5.17	1.171	11.17	1.882	17.17	.796	23.17	.534	
5.33	1.231	11.33	1.804	17.33	.785	23.33	.529	
5.50	1.298	11.50	1.733	17.50	.774	23.50	.524	
5.67	1.374	11.67	1.668	17.67	.763	23.67	.520	
5.83	1.461	11.83	1.609	17.83	.753	23.83	.516	
6.00	1.562	12.00	1.554	18.00	.743	24.00	.511	

001:0003

*
* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437

PEAK FLOW (cms)= 1.083 (i)
 TIME TO PEAK (hrs)= 9.500
 RUNOFF VOLUME (mm)= 12.062
 TOTAL RAINFALL (mm)= 55.093
 RUNOFF COEFFICIENT = .219

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

*
* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020

PEAK FLOW (cms)= 2.545 (i)
 TIME TO PEAK (hrs)= 10.500
 RUNOFF VOLUME (mm)= 10.247
 TOTAL RAINFALL (mm)= 55.093
 RUNOFF COEFFICIENT = .186

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

2yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:27:53

=====
=

5yr.out

```

=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M O O 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
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***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****

```

```

+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:28:39 RUN COUNTER: 000063 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\5yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\5yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\5yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001-----

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```


5yr.out

*
*
* 5 YEAR, 24 HOUR CHICAGO STORM
*

* FILE NAME:
*

* PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
* Existing Conditions Drainage Report

*

| START | Project dir.: C:\C-Drive\PEELBE~1\SWMHYMO\
----- Rainfall dir.: C:\C-Drive\PEELBE~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=

-
001:0002-----
-

| CHICAGO STORM |
Ptotal= 70.76 mm

IDF curve parameters: A=1025.000
B= 7.560
C= .804
used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
Storm time step = 10.00 min
Time to peak ratio = .33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	.597	6.17	2.045	12.17	1.819	18.17	.860
.33	.608	6.33	2.225	12.33	1.759	18.33	.848
.50	.619	6.50	2.445	12.50	1.703	18.50	.837
.67	.631	6.67	2.720	12.67	1.651	18.67	.826
.83	.643	6.83	3.075	12.83	1.602	18.83	.816
1.00	.655	7.00	3.550	13.00	1.557	19.00	.805
1.17	.669	7.17	4.222	13.17	1.514	19.17	.795
1.33	.682	7.33	5.254	13.33	1.474	19.33	.786
1.50	.697	7.50	7.052	13.50	1.436	19.50	.776
1.67	.712	7.67	11.002	13.67	1.400	19.67	.767
1.83	.728	7.83	27.015	13.83	1.367	19.83	.758
2.00	.745	8.00	102.359	14.00	1.335	20.00	.750
2.17	.762	8.17	35.662	14.17	1.304	20.17	.741
2.33	.781	8.33	18.737	14.33	1.275	20.33	.733
2.50	.801	8.50	12.671	14.50	1.248	20.50	.725
2.67	.821	8.67	9.601	14.67	1.221	20.67	.717
2.83	.843	8.83	7.757	14.83	1.196	20.83	.709
3.00	.867	9.00	6.529	15.00	1.173	21.00	.702
3.17	.892	9.17	5.652	15.17	1.150	21.17	.694
3.33	.918	9.33	4.994	15.33	1.128	21.33	.687
3.50	.947	9.50	4.482	15.50	1.107	21.50	.680
3.67	.977	9.67	4.072	15.67	1.087	21.67	.674
3.83	1.010	9.83	3.736	15.83	1.067	21.83	.667
4.00	1.045	10.00	3.455	16.00	1.049	22.00	.660
4.17	1.083	10.17	3.217	16.17	1.031	22.17	.654
4.33	1.125	10.33	3.012	16.33	1.014	22.33	.648

			5yr.out				
4.50	1.170	10.50	2.834	16.50	.997	22.50	.642
4.67	1.219	10.67	2.677	16.67	.981	22.67	.636
4.83	1.274	10.83	2.539	16.83	.966	22.83	.630
5.00	1.334	11.00	2.415	17.00	.951	23.00	.624
5.17	1.401	11.17	2.304	17.17	.937	23.17	.618
5.33	1.475	11.33	2.204	17.33	.923	23.33	.613
5.50	1.560	11.50	2.113	17.50	.909	23.50	.607
5.67	1.656	11.67	2.030	17.67	.896	23.67	.602
5.83	1.766	11.83	1.953	17.83	.884	23.83	.597
6.00	1.894	12.00	1.883	18.00	.871	24.00	.592

001:0003

* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437
PEAK FLOW (cms)= 1.971 (i)
TIME TO PEAK (hrs)= 9.333
RUNOFF VOLUME (mm)= 19.740
TOTAL RAINFALL (mm)= 70.759
RUNOFF COEFFICIENT = .279

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020
PEAK FLOW (cms)= 4.613 (i)
TIME TO PEAK (hrs)= 10.333
RUNOFF VOLUME (mm)= 16.970
TOTAL RAINFALL (mm)= 70.759
RUNOFF COEFFICIENT = .240

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

5yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:28:39

=====
=

10yr.out

```

=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M O O 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.com *****
*****

```

```

+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:29:05 RUN COUNTER: 000064 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\10yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\10yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\10yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```

10yr.out

*
*
* 10 YEAR, 24 HOUR CHICAGO STORM

* FILE NAME:

* PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
* Existing Conditions Drainage Report

*

| START | Project dir.: C:\C-Drive\PEELBE~1\SWMHYMO\
----- Rainfall dir.: C:\C-Drive\PEELBE~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=

-
001:0002-----
-

| CHICAGO STORM |
Ptotal= 81.99 mm

IDF curve parameters: A=1232.000
B= 7.970
C= .809
used in: INTENSITY = A / (t + B)^C
Duration of storm = 24.00 hrs
Storm time step = 10.00 min
Time to peak ratio = .33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.17	.676	6.17	2.342	12.17	2.079	18.17	.975
.33	.688	6.33	2.551	12.33	2.010	18.33	.962
.50	.701	6.50	2.806	12.50	1.946	18.50	.950
.67	.714	6.67	3.126	12.67	1.886	18.67	.937
.83	.728	6.83	3.539	12.83	1.830	18.83	.925
1.00	.742	7.00	4.094	13.00	1.777	19.00	.913
1.17	.757	7.17	4.882	13.17	1.728	19.17	.902
1.33	.773	7.33	6.095	13.33	1.681	19.33	.891
1.50	.789	7.50	8.216	13.50	1.638	19.50	.880
1.67	.807	7.67	12.899	13.67	1.597	19.67	.870
1.83	.825	7.83	31.896	13.83	1.558	19.83	.860
2.00	.844	8.00	119.037	14.00	1.521	20.00	.850
2.17	.864	8.17	42.134	14.17	1.486	20.17	.840
2.33	.885	8.33	22.094	14.33	1.453	20.33	.831
2.50	.908	8.50	14.882	14.50	1.421	20.50	.821
2.67	.932	8.67	11.235	14.67	1.391	20.67	.812
2.83	.957	8.83	9.050	14.83	1.362	20.83	.804
3.00	.984	9.00	7.597	15.00	1.335	21.00	.795
3.17	1.012	9.17	6.563	15.17	1.308	21.17	.787
3.33	1.043	9.33	5.788	15.33	1.283	21.33	.779
3.50	1.075	9.50	5.187	15.50	1.259	21.50	.771
3.67	1.110	9.67	4.706	15.67	1.236	21.67	.763
3.83	1.148	9.83	4.312	15.83	1.214	21.83	.755
4.00	1.188	10.00	3.983	16.00	1.192	22.00	.748
4.17	1.232	10.17	3.705	16.17	1.172	22.17	.740
4.33	1.280	10.33	3.466	16.33	1.152	22.33	.733

				10yr.out				
4.50	1.331	10.50	3.258	16.50	1.133	22.50	.726	
4.67	1.388	10.67	3.076	16.67	1.115	22.67	.719	
4.83	1.451	10.83	2.915	16.83	1.097	22.83	.713	
5.00	1.520	11.00	2.771	17.00	1.080	23.00	.706	
5.17	1.597	11.17	2.642	17.17	1.064	23.17	.700	
5.33	1.683	11.33	2.526	17.33	1.048	23.33	.693	
5.50	1.781	11.50	2.420	17.50	1.032	23.50	.687	
5.67	1.891	11.67	2.324	17.67	1.017	23.67	.681	
5.83	2.019	11.83	2.235	17.83	1.003	23.83	.675	
6.00	2.167	12.00	2.154	18.00	.989	24.00	.670	

001:0003

* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437
PEAK FLOW (cms)= 2.689 (i)
TIME TO PEAK (hrs)= 9.333
RUNOFF VOLUME (mm)= 25.976
TOTAL RAINFALL (mm)= 81.991
RUNOFF COEFFICIENT = .317

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020
PEAK FLOW (cms)= 6.303 (i)
TIME TO PEAK (hrs)= 10.333
RUNOFF VOLUME (mm)= 22.500
TOTAL RAINFALL (mm)= 81.991
RUNOFF COEFFICIENT = .274

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

10yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:29:05

=====
=

25yr.out

```

=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M O O 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****

```

```

+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:29:30 RUN COUNTER: 000065 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\25yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\25yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\25yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```


25yr.out

*
*
* 25 YEAR, 24 HOUR CHICAGO STORM
*

* FILE NAME:
*

* PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
* Existing Conditions Drainage Report

*

| START | Project dir.: C:\C-Drive\PEELBE~1\SWMHYMO\
----- Rainfall dir.: C:\C-Drive\PEELBE~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=

-
001:0002-----
-

| CHICAGO STORM | IDF curve parameters: A=1649.700
| Ptotal= 94.15 mm | B= 9.457
C= .830
used in: INTENSITY = A / (t + B)^C
Duration of storm = 24.00 hrs
Storm time step = 10.00 min
Time to peak ratio = .33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	.697	6.17	2.542	12.17	2.244	18.17	1.019
.33	.710	6.33	2.781	12.33	2.166	18.33	1.005
.50	.723	6.50	3.076	12.50	2.093	18.50	.991
.67	.737	6.67	3.447	12.67	2.025	18.67	.978
.83	.752	6.83	3.929	12.83	1.962	18.83	.965
1.00	.768	7.00	4.584	13.00	1.904	19.00	.952
1.17	.784	7.17	5.525	13.17	1.848	19.17	.940
1.33	.801	7.33	6.992	13.33	1.797	19.33	.928
1.50	.818	7.50	9.600	13.50	1.748	19.50	.916
1.67	.837	7.67	15.464	13.67	1.702	19.67	.905
1.83	.856	7.83	39.330	13.83	1.659	19.83	.894
2.00	.877	8.00	140.434	14.00	1.618	20.00	.883
2.17	.899	8.17	52.114	14.17	1.579	20.17	.873
2.33	.922	8.33	27.094	14.33	1.542	20.33	.862
2.50	.946	8.50	17.964	14.50	1.507	20.50	.853
2.67	.972	8.67	13.367	14.67	1.474	20.67	.843
2.83	.999	8.83	10.634	14.83	1.442	20.83	.834
3.00	1.028	9.00	8.834	15.00	1.412	21.00	.824
3.17	1.059	9.17	7.563	15.17	1.383	21.17	.815
3.33	1.092	9.33	6.619	15.33	1.355	21.33	.807
3.50	1.127	9.50	5.891	15.50	1.328	21.50	.798
3.67	1.165	9.67	5.313	15.67	1.303	21.67	.790
3.83	1.206	9.83	4.843	15.83	1.279	21.83	.781
4.00	1.251	10.00	4.453	16.00	1.255	22.00	.774
4.17	1.299	10.17	4.124	16.17	1.233	22.17	.766
4.33	1.351	10.33	3.843	16.33	1.211	22.33	.758

				25yr.out				
4.50	1.408	10.50	3.600	16.50	1.191	22.50	.751	
4.67	1.471	10.67	3.388	16.67	1.171	22.67	.743	
4.83	1.540	10.83	3.201	16.83	1.151	22.83	.736	
5.00	1.617	11.00	3.035	17.00	1.133	23.00	.729	
5.17	1.702	11.17	2.886	17.17	1.115	23.17	.722	
5.33	1.799	11.33	2.753	17.33	1.097	23.33	.716	
5.50	1.907	11.50	2.632	17.50	1.081	23.50	.709	
5.67	2.032	11.67	2.522	17.67	1.065	23.67	.703	
5.83	2.176	11.83	2.421	17.83	1.049	23.83	.696	
6.00	2.343	12.00	2.329	18.00	1.034	24.00	.690	

001:0003

* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437
PEAK FLOW (cms)= 3.694 (i)
TIME TO PEAK (hrs)= 9.333
RUNOFF VOLUME (mm)= 33.293
TOTAL RAINFALL (mm)= 94.149
RUNOFF COEFFICIENT = .354

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020
PEAK FLOW (cms)= 8.646 (i)
TIME TO PEAK (hrs)= 10.333
RUNOFF VOLUME (mm)= 29.050
TOTAL RAINFALL (mm)= 94.149
RUNOFF COEFFICIENT = .309

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

25yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:29:30

=====
=

50yr.out

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=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM 0 0 9 9 9 9
SSSSS W W W M M M H H H H Y M M M 0 0 ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M 0 0 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****

```

```

+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:29:52 RUN COUNTER: 000066 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\50yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\50yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\50yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```

50yr.out

*
*
* 50 YEAR, 24 HOUR CHICAGO STORM
*
* FILE NAME:

* PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
* Existing Conditions Drainage Report

| START | Project dir.: C:\C-Drive\PEELBE~1\SWMHYMO\
----- Rainfall dir.: C:\C-Drive\PEELBE~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=

001:0002-----

| CHICAGO STORM |
Ptotal=105.44 mm

IDF curve parameters: A=1931.200
B= 10.500
C= .836
used in: INTENSITY = A / (t + B)^C
Duration of storm = 24.00 hrs
Storm time step = 10.00 min
Time to peak ratio = .33

Table with 8 columns: TIME (hrs), RAIN (mm/hr), TIME (hrs), RAIN (mm/hr), TIME (hrs), RAIN (mm/hr), TIME (hrs), RAIN (mm/hr). It contains a detailed hourly rainfall schedule for a 24-hour storm event.

				50yr.out				
4.50	1.544	10.50	4.019	16.50	1.302	22.50	.816	
4.67	1.614	10.67	3.777	16.67	1.280	22.67	.808	
4.83	1.691	10.83	3.564	16.83	1.258	22.83	.800	
5.00	1.777	11.00	3.375	17.00	1.238	23.00	.792	
5.17	1.872	11.17	3.207	17.17	1.218	23.17	.785	
5.33	1.980	11.33	3.055	17.33	1.199	23.33	.777	
5.50	2.102	11.50	2.918	17.50	1.180	23.50	.770	
5.67	2.242	11.67	2.794	17.67	1.162	23.67	.763	
5.83	2.403	11.83	2.680	17.83	1.145	23.83	.756	
6.00	2.593	12.00	2.576	18.00	1.128	24.00	.749	

001:0003

* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437

PEAK FLOW (cms)= 4.603 (i)
 TIME TO PEAK (hrs)= 9.333
 RUNOFF VOLUME (mm)= 40.539
 TOTAL RAINFALL (mm)= 105.441
 RUNOFF COEFFICIENT = .384

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020

PEAK FLOW (cms)= 10.817 (i)
 TIME TO PEAK (hrs)= 10.333
 RUNOFF VOLUME (mm)= 35.591
 TOTAL RAINFALL (mm)= 105.441
 RUNOFF COEFFICIENT = .338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

50yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:29:52

=====
=

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=====
SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M O O 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9
9 9 9 9 # 1432652
=====
StormWater Management Hydrologic Model 999 999

```

```

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****

```

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+++++
+++++ Licensed user: HDR inc. +++++
+++++ richmond hill SERIAL#:1432652 +++++
+++++

```

```

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

```

```

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2014-04-03 TIME: 14:30:02 RUN COUNTER: 000067 *
*****
* Input filename: C:\C-Drive\PEELBE~1\SWMHYMO\100yr.DAT *
* Output filename: C:\C-Drive\PEELBE~1\SWMHYMO\100yr.out *
* Summary filename: C:\C-Drive\PEELBE~1\SWMHYMO\100yr.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

001:0001-----

```

*
* PROJECT NUMBER:
* Belfountain Class Environmental Assessment
* Region of Peel
*
* EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
*
*
* DATE: October 2013
*
*

```


100yr.out

*
*
* 100 YEAR, 24 HOUR CHICAGO STORM

* FILE NAME:

* PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
* Existing Conditions Drainage Report

*

| START | Project dir.: C:\C-Drive\PEELBE~1\SWMHYMO\
----- Rainfall dir.: C:\C-Drive\PEELBE~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=

-
001:0002-----
-

| CHICAGO STORM |
Ptotal=114.71 mm

IDF curve parameters: A=2147.400
B= 10.500
C= .839
used in: INTENSITY = A / (t + B)^C

Duration of storm = 24.00 hrs
Storm time step = 10.00 min
Time to peak ratio = .33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.17	.809	6.17	3.031	12.17	2.667	18.17	1.191
.33	.824	6.33	3.324	12.33	2.572	18.33	1.174
.50	.840	6.50	3.686	12.50	2.483	18.50	1.157
.67	.857	6.67	4.144	12.67	2.401	18.67	1.141
.83	.874	6.83	4.742	12.83	2.325	18.83	1.126
1.00	.892	7.00	5.557	13.00	2.253	19.00	1.111
1.17	.911	7.17	6.735	13.17	2.187	19.17	1.096
1.33	.931	7.33	8.585	13.33	2.124	19.33	1.082
1.50	.952	7.50	11.894	13.50	2.065	19.50	1.068
1.67	.974	7.67	19.382	13.67	2.010	19.67	1.055
1.83	.998	7.83	49.592	13.83	1.957	19.83	1.042
2.00	1.022	8.00	170.354	14.00	1.908	20.00	1.029
2.17	1.048	8.17	65.649	14.17	1.861	20.17	1.017
2.33	1.075	8.33	34.228	14.33	1.817	20.33	1.005
2.50	1.104	8.50	22.579	14.50	1.774	20.50	.993
2.67	1.134	8.67	16.700	14.67	1.734	20.67	.982
2.83	1.167	8.83	13.210	14.83	1.696	20.83	.970
3.00	1.201	9.00	10.918	15.00	1.660	21.00	.959
3.17	1.238	9.17	9.306	15.17	1.625	21.17	.949
3.33	1.277	9.33	8.112	15.33	1.592	21.33	.938
3.50	1.320	9.50	7.195	15.50	1.560	21.50	.928
3.67	1.365	9.67	6.469	15.67	1.530	21.67	.918
3.83	1.414	9.83	5.880	15.83	1.501	21.83	.909
4.00	1.467	10.00	5.393	16.00	1.473	22.00	.899
4.17	1.525	10.17	4.984	16.17	1.446	22.17	.890
4.33	1.587	10.33	4.635	16.33	1.420	22.33	.881

								100yr.out
4.50	1.656	10.50	4.334	16.50	1.395	22.50	.872	
4.67	1.731	10.67	4.071	16.67	1.371	22.67	.864	
4.83	1.814	10.83	3.840	16.83	1.348	22.83	.855	
5.00	1.907	11.00	3.636	17.00	1.326	23.00	.847	
5.17	2.010	11.17	3.453	17.17	1.305	23.17	.839	
5.33	2.126	11.33	3.289	17.33	1.284	23.33	.831	
5.50	2.258	11.50	3.140	17.50	1.264	23.50	.823	
5.67	2.409	11.67	3.006	17.67	1.245	23.67	.816	
5.83	2.584	11.83	2.883	17.83	1.226	23.83	.808	
6.00	2.788	12.00	2.771	18.00	1.208	24.00	.801	

001:0003

* Determine runoff from Catchment OBL-04
*
*

CALIB NASHYD	Area (ha)=	163.70	Curve Number (CN)=	65.00
01:001000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.150		

Unit Hyd Qpeak (cms)= 5.437

PEAK FLOW (cms)= 5.407 (i)
 TIME TO PEAK (hrs)= 9.333
 RUNOFF VOLUME (mm)= 46.770
 TOTAL RAINFALL (mm)= 114.712
 RUNOFF COEFFICIENT = .408

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004

* Determine runoff from Catchment OBL-08
*
*

CALIB NASHYD	Area (ha)=	647.70	Curve Number (CN)=	60.00
02:002000 DT=10.00	Ia (mm)=	8.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	1.900		

Unit Hyd Qpeak (cms)= 13.020

PEAK FLOW (cms)= 12.726 (i)
 TIME TO PEAK (hrs)= 10.333
 RUNOFF VOLUME (mm)= 41.252
 TOTAL RAINFALL (mm)= 114.712
 RUNOFF COEFFICIENT = .360

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005

*
*

100yr.out

*
*
*

*PRINT HYD ID=[1], # OF PCYCLES=[6]
FINISH

-

*

WARNINGS / ERRORS / NOTES

Simulation ended on 2014-04-03 at 14:30:02

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00001> -----
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999 -----
00004> S W W W M M M H H Y Y M M M O O 9 9 9 9
00005> SSSSS W W M M M H H H H Y Y M M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M M H H Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y M M O O 9 9 9 # 1432652
00008>
00009> StormWater Management Hydrologic Model 999 999 -----
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTTHYMO-83 and OTTHYMO-89. *****
00016> *****
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhymo@jfsa.Com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: HDR inc. *****
00025> ***** richmond hill SERIAL#:1432652 *****
00026> *****
00027> *****
00028> *****
00029> ***** PROGRAM ARRAY DIMENSIONS *****
00030> ***** Maximum value for ID numbers : 10 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034>
00035>
00036> ***** D E T A I L E D O U T P U T *****
00037> *****
00038> ***** DATE: 2014-05-12 TIME: 10:12:29 RUN COUNTER: 000074 *****
00039> *****
00040> * Input filename: C:\C-Drive\PEELBE-1\SWMHYMO\HAZ.DAT *
00041> * Output filename: C:\C-Drive\PEELBE-1\SWMHYMO\HAZ.out *
00042> * Summary filename: C:\C-Drive\PEELBE-1\SWMHYMO\HAZ.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048>
00049>
00050> 001:0001-----
00051> *
00052> * PROJECT NUMBER:
00053> * Belfourin Class Environmental Assessment
00054> * Region of Peel
00055> *
00056> * EXISTING CONDITIONS - Cross-Culvert Hydrologic Analysis
00057> *
00058> *
00059> * DATE: October 2013
00060> *
00061> * Regional Storm - Hurricane Hazel
00062> *
00063> * FILE NAME:
00064> *
00065> *****
00066> * PRECIPITATION: From Dillon, June 2010, Bush St. and Mississauga Road EA
00067> * Existing Conditions Drainage Report
00068> *****
00069> *
00070> -----
00071> | START | Project dir.: C:\C-Drive\PEELBE-1\SWMHYMO\
00072> | RZERO = 0 | Rainfall dir.: C:\C-Drive\PEELBE-1\SWMHYMO\
00073> | METOUT= 2 (output = METRIC)
00074> | NRUN = 001
00075> | NSTORM= 1
00076> | # 1=HAZEL-HR.STM
00077>
00078>
00079> 001:0002-----
00080>
00081> | READ STORM | Filename: Hurricane Hazel for the last 12 hrs of t
00082> | Ptotal= 212.00 mm | Comments: Hurricane Hazel for the last 12 hrs of t
00083>
00084> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00085> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00086> 1.00 6.000 | 4.00 13.000 | 7.00 23.000 | 10.00 53.000
00087> 2.00 4.000 | 5.00 17.000 | 8.00 13.000 | 11.00 38.000
00088> 3.00 6.000 | 6.00 13.000 | 9.00 13.000 | 12.00 13.000
00089>
00090>
00091> 001:0003-----
00092> *
00093> * Determine runoff from Catchment OBL-02
00094> *
00095>
00096> | CALIB NASHYD | Area (ha)= 53.30 Curve Number (CN)=80.00
00097> | 01:001000 DT=10.00 | Ia (mm)= 12.700 # of Linear Res. (N)= 3.00
00098> | U.H. Tp(hrs)= .960
00099>
00100> Ia as 0.2xS (mm)= 12.700
00101> Unit Hyd Qpeak (cms)= 2.121
00102>
00103> PEAK FLOW (cms)= 5.233 (i)
00104> TIME TO PEAK (hrs)= 11.167
00105> RUNOFF VOLUME (mm)= 151.143
00106> TOTAL RAINFALL (mm)= 212.000
00107> RUNOFF COEFFICIENT = .713
00108>
00109> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00110>
00111> -----
00112> 001:0004-----
00113> *
00114> *
00115> * Determine runoff from Catchment OBL-04
00116> *
00117> *
00118> -----
00119> | CALIB NASHYD | Area (ha)= 163.70 Curve Number (CN)=78.00
00120> | 02:001001 DT=10.00 | Ia (mm)= 14.328 # of Linear Res. (N)= 3.00
00121> | U.H. Tp(hrs)= 1.150
00122>
00123> Ia as 0.2xS (mm)= 14.328
00124> Unit Hyd Qpeak (cms)= 5.437
00125>
00126> PEAK FLOW (cms)= 14.785 (i)
00127> TIME TO PEAK (hrs)= 11.333
00128> RUNOFF VOLUME (mm)= 145.088
00129> TOTAL RAINFALL (mm)= 212.000
00130> RUNOFF COEFFICIENT = .684
00131>
00132> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00133>
00134> -----
00135> 001:0005-----

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```

00136> *
00137> *
00138> * Determine runoff from Catchment OBL-08
00139> *
00140> *
00141> -----
00142> | CALIB NASHYD | Area (ha)= 647.70 Curve Number (CN)=78.00
00143> | 03:001002 DT=10.00 | Ia (mm)= 14.328 # of Linear Res. (N)= 3.00
00144> | U.H. Tp(hrs)= 1.900
00145>
00146> Ia as 0.2xS (mm)= 14.328
00147> Unit Hyd Qpeak (cms)= 13.020
00148>
00149> PEAK FLOW (cms)= 46.822 (i)
00150> TIME TO PEAK (hrs)= 12.000
00151> RUNOFF VOLUME (mm)= 145.088
00152> TOTAL RAINFALL (mm)= 212.000
00153> RUNOFF COEFFICIENT = .684
00154>
00155> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00156>
00157> -----
00158> 001:0006-----
00159> *
00160> *
00161> * Determine runoff from Catchment WCB-06
00162> *
00163> *
00164> -----
00165> | CALIB NASHYD | Area (ha)= 11.96 Curve Number (CN)=76.00
00166> | 04:001003 DT=10.00 | Ia (mm)= 16.042 # of Linear Res. (N)= 3.00
00167> | U.H. Tp(hrs)= .610
00168>
00169> Ia as 0.2xS (mm)= 16.042
00170> Unit Hyd Qpeak (cms)= .749
00171>
00172> PEAK FLOW (cms)= 1.248 (i)
00173> TIME TO PEAK (hrs)= 10.500
00174> RUNOFF VOLUME (mm)= 139.044
00175> TOTAL RAINFALL (mm)= 212.000
00176> RUNOFF COEFFICIENT = .656
00177>
00178> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00179>
00180> -----
00181> 001:0007-----
00182> *
00183> *
00184> * Determine runoff from Catchment WCB-09
00185> *
00186> *
00187> -----
00188> | CALIB NASHYD | Area (ha)= 75.50 Curve Number (CN)=78.00
00189> | 05:001004 DT=10.00 | Ia (mm)= 14.328 # of Linear Res. (N)= 3.00
00190> | U.H. Tp(hrs)= .850
00191>
00192> Ia as 0.2xS (mm)= 14.328
00193> Unit Hyd Qpeak (cms)= 3.393
00194>
00195> PEAK FLOW (cms)= 7.504 (i)
00196> TIME TO PEAK (hrs)= 11.000
00197> RUNOFF VOLUME (mm)= 145.088
00198> TOTAL RAINFALL (mm)= 212.000
00199> RUNOFF COEFFICIENT = .684
00200>
00201> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00202>
00203> -----
00204> 001:0008-----
00205> *
00206> *
00207> * Determine runoff from Catchment WCB-16
00208> *
00209> *
00210> -----
00211> | CALIB NASHYD | Area (ha)= 32.30 Curve Number (CN)=76.00
00212> | 06:001005 DT=10.00 | Ia (mm)= 16.042 # of Linear Res. (N)= 3.00
00213> | U.H. Tp(hrs)= .640
00214>
00215> Ia as 0.2xS (mm)= 16.042
00216> Unit Hyd Qpeak (cms)= 1.928
00217>
00218> PEAK FLOW (cms)= 3.331 (i)
00219> TIME TO PEAK (hrs)= 10.500
00220> RUNOFF VOLUME (mm)= 139.044
00221> TOTAL RAINFALL (mm)= 212.000
00222> RUNOFF COEFFICIENT = .656
00223>
00224> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00225>
00226> -----
00227> 001:0009-----
00228> *
00229> *
00230> * Determine runoff from Catchment WCB-14
00231> *
00232> *
00233> -----
00234> | CALIB NASHYD | Area (ha)= .50 Curve Number (CN)=76.00
00235> | 07:001006 DT= 5.00 | Ia (mm)= 16.042 # of Linear Res. (N)= 3.00
00236> | U.H. Tp(hrs)= .210
00237>
00238> Ia as 0.2xS (mm)= 16.042
00239> Unit Hyd Qpeak (cms)= .091
00240>
00241> PEAK FLOW (cms)= .063 (i)
00242> TIME TO PEAK (hrs)= 10.000
00243> RUNOFF VOLUME (mm)= 139.043
00244> TOTAL RAINFALL (mm)= 212.000
00245> RUNOFF COEFFICIENT = .656
00246>
00247> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00248>
00249> -----
00250> 001:0010-----
00251> *
00252> *
00253> *
00254> * FINISH
00255> *
00256> -----
00257> * WARNINGS / ERRORS / NOTES
00258> *
00259> * Simulation ended on 2014-05-12 at 10:12:29
00260> -----
00261>
00262>

```

Appendix C.3.
Hydrologic Summary Table

Culvert No.	Station	Watershed Area		Watershed Slope, Using the 85/10 Method					Peak Design Flow Calculations						
		Total Watershed Area (A, m ²)	Total Watershed Area (A, ha)	Watershed Length (L, m)	Elevation at 85% (h ₈₅ , m)	Elevation at 85% (h ₁₀ , m)	Difference in Elevation (Δh, m)	Watershed Slope (S _w , %)	Runoff Coefficient (C)	Time of Concentration Method	Time of Concentration (T _c , min)	Return Period (x)	Rainfall Intensity for x Year Return Period (i, mm/hr) $i_x = 1649.671 * (T_c + 9.457)^{-0.83}$	Design Peak Flow for x Year Return Period (Q, m ³ /s) $Q_x = 0.0028 * C * i * A$	Unit Flow Rate (Q/A, m/s)
Olde Base Line Road															
OBL-01	30+030	126500	12.65	715	385	376	9	1.678	0.28	Airport Formula	60.25	25	48.69	0.479	0.038
OBL-02 (Tributary B of Rogers Creek)	30+540	533200	53.32	1650	394	373	21	1.697	0.32	Airport Formula	86.25	2	19.14	0.921	0.017
												5	26.61	1.28	0.024
												10	31.15	1.499	0.028
												25	37.43	1.8	0.034
												50	42.25	2.032	0.038
												100	46.33	2.229	0.042
												Regional	N/A	5.233 (See Note 1)	0.098
OBL-03	30+715	151000	15.1	770	385	374	11	1.905	0.25	Airport Formula	62.46	25	47.45	0.49	0.032
OBL-04 (Tributary A of Rogers Creek)	30+940	1636600	163.66	2400	417	376	41	2.278	0.25	Airport Formula	103.9	2	N/A	1.08 (See Note 1)	0.007
												5	N/A	1.97 (See Note 1)	0.012
												10	N/A	2.68 (See Note 1)	0.016
												25	N/A	3.69 (See Note 1)	0.023
												50	N/A	4.6 (See Note 1)	0.028
												100	N/A	5.41 (See Note 1)	0.033
												Regional	N/A	14.78 (See Note 1)	0.090
OBL-05	31+280	57300	5.73	635	382	375	7	1.470	0.28	Airport Formula	59.32	25	49.24	0.22	0.038
OBL-06	31+300	38600	3.86	785	385	375	10	1.699	0.27	Airport Formula	82.51	25	38.69	0.111	0.029
OBL-07	31+380	11200	1.12	185	376	375	1	0.721	0.25	Airport Formula	41.99	25	62.66	0.049	0.044
OBL-08 (Tributary A of Second Creek)	31+410	6476850	647.685	4500	421	376	45	1.333	0.25	Airport Formula	171.04	2	N/A	2.54 (See Note 1)	0.004
												5	N/A	4.61 (See Note 1)	0.007
												10	N/A	6.3 (See Note 1)	0.010
												25	N/A	8.65 (See Note 1)	0.013
												50	N/A	10.81 (See Note 1)	0.017
												100	N/A	12.73 (See Note 1)	0.020
												Regional	N/A	46.8 (See Note 1)	0.072
OBL-09	32+080	37500	3.75	230	380	376	4	2.319	0.3	Airport Formula	29.97	25	78.15	0.244	0.065
OBL-10	32+230	15600	1.56	175	380	376	4	3.048	0.25	Airport Formula	25.38	25	86.6	0.094	0.060
OBL-11	32+340	406600	40.66	1355	394	376	18	1.771	0.28	Airport Formula	83.97	25	38.19	0.892	0.022

Note 1: Peak Flow determined from SYMHYMO Model

		Watershed Area		Watershed Slope, Using the 85/10 Method					Peak Design Flow Calculations						
Culvert No.	Station	Total Watershed Area (A, m ²)	Total Watershed Area (A, ha)	Watershed Length (L, m)	Elevation at 85% (h ₈₅ , m)	Elevation at 85% (h ₁₀ , m)	Difference in Elevation (Δh, m)	Watershed Slope (S _w , %)	Runoff Coefficient (C)	Time of Concentration Method	Time of Concentration (T _c , min)	Return Period (x)	Rainfall Intensity for x Year Return Period (i, mm/hr) $i_x = 1649.671 * (T_c + 9.457)^{-0.83}$	Design Peak Flow for x Year Return Period (Q, m ³ /s) $Q_x = 0.0028 * C * i * A$	Unit Flow Rate (Q/A, m/s)
Winston Churchill Boulevard															
WCB-01	40+030	10000	1	460	383	377	6	1.739	0.28	Airport Formula	47.76	25	57.36	0.045	0.045
WCB-02	40+480	30800	3.08	270	385	383	2	0.988	0.29	Airport Formula	43.35	25	61.31	0.154	0.050
WCB-03	40+660	26000	2.6	290	385	384	1	0.460	0.35	Airport Formula	53.81	25	52.78	0.134	0.052
WCB-04	40+870	17000	1.7	255	394	390	4	2.092	0.25	Airport Formula	34.69	25	71.15	0.084	0.049
WCB-05	41+110	9000	0.9	150	395	393	2	1.778	0.25	Airport Formula	28.07	25	81.41	0.051	0.057
WCB-06 (Watercourse)	41+400	119600	11.96	510	399	393	6	1.569	0.23	Airport Formula	55.21	2	26.53	0.203	0.017
												5	36.76	0.281	0.023
												10	43.05	0.329	0.028
												25	51.83	0.396	0.033
												50	58.39	0.446	0.037
												100	64.1	0.49	0.041
												Regional	N/A	1.248 (See Note 1)	0.104
WCB-07	41+710	98600	9.86	650	418	398	20	4.103	0.35	Airport Formula	39.12		65.71	0.63	0.064
WCB-08	41+890	72200	7.22	440	425	398	27	8.182	0.33	Airport Formula	26.4		84.55	0.556	0.077
WCB-09 (Tributary C of Rogers Creek)	42+195	754800	75.48	1200	420	403	17	1.889	0.26	Airport Formula	76.9	2	20.84	1.137	0.015
												5	28.95	1.58	0.021
												10	33.90	1.85	0.025
												25	40.76	2.224	0.029
												50	46.00	2.509	0.033
												100	50.46	2.753	0.036
Regional	N/A	7.504 (See Note 1)	0.099												
WCB-10	42+750	21500	2.15	240	430	422	8	4.444	0.35	Airport Formula	23.15	25	91.48	0.191	0.089
WCB-11	43+130	10500	1.05	170	430	427	3	2.353	0.28	Airport Formula	26.28	25	84.78	0.069	0.066
WCB-12	43+210	33400	3.34	380	435	430	5	1.754	0.3	Airport Formula	41.18	25	62.47	0.175	0.052
WCB-13	44+140	Equalization Culvert	-	0			0	-						Equalization Culvert	-
WCB-14 (Watercourse)	44+310	500	0.05	100	425	423	2	2.667	0.3	Airport Formula	18.87	2	54.32	0.023	0.460
												5	73.69	0.031	0.620
												10	86.04	0.036	0.720
												25	102.82	0.043	0.860
												50	114.47	0.048	0.960
												100	125.95	0.053	1.060
Regional	N/A	0.063 (See Note 1)	1.260												
WCB-15	44+615	38900	3.89	260	425	420	5	2.564	0.3	Airport Formula	30.82	25	76.77	0.249	0.064
WCB-16 (Watercourse)	44+945	323300	32.33	920	435	412	23	3.333	0.23	Airport Formula	57.82	2	25.66	0.53	0.016
												5	35.57	0.735	0.023
												10	41.66	0.861	0.027
												25	50.15	1.037	0.032
												50	56.51	1.168	0.036
												100	62.04	1.282	0.040
Regional	N/A	3.331 (See Note 1)	0.103												
WCB-17	45+095	435000	43.5	1030	420	412	8	1.036	0.26	Airport Formula	87.14	25	37.14	1.157	0.027
WCB-18	45+865	527700	52.77	1440	420	400	20	1.852	0.3	Airport Formula	80.72	25	39.33	1.733	0.033

Note 1: Peak Flow determined from SYMHYMO Model

Appendix D
CulvertMaster Assessment
(Existing Conditions)

**Appendix D.1.
CulvertMaster Output
(Existing Conditions)**

Culvert Calculator Report

OBL-01 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.90 m	Headwater Depth/Height	4.88
Computed Headwater Elev:	374.63 m	Discharge	0.4790 m ³ /s
Inlet Control HW Elev.	374.19 m	Tailwater Elevation	372.70 m
Outlet Control HW Elev.	374.63 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.40 m	Downstream Invert	372.25 m
Length	12.50 m	Constructed Slope	0.012000 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.45 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.44 m
Velocity Downstream	2.93 m/s	Critical Slope	0.076944 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	374.63 m	Upstream Velocity Head	0.43 m
Ke	0.90	Entrance Loss	0.39 m

Inlet Control Properties			
Inlet Control HW Elev.	374.19 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-02 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.55 m	Headwater Depth/Height	13.34
Computed Headwater Elev:	380.84 m	Discharge	1.8000 m ³ /s
Inlet Control HW Elev.	379.94 m	Tailwater Elevation	373.31 m
Outlet Control HW Elev.	380.84 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.71 m	Downstream Invert	372.70 m
Length	14.30 m	Constructed Slope	0.000699 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.61 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.61 m
Velocity Downstream	6.17 m/s	Critical Slope	0.255430 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	380.84 m	Upstream Velocity Head	1.94 m
Ke	0.90	Entrance Loss	1.75 m

Inlet Control Properties			
Inlet Control HW Elev.	379.94 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-03 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	369.62 m	Headwater Depth/Height	1.75
Computed Headwater Elev:	370.23 m	Discharge	0.4900 m ³ /s
Inlet Control HW Elev.	370.01 m	Tailwater Elevation	369.62 m
Outlet Control HW Elev.	370.23 m	Control Type	Outlet Control

Grades			
Upstream Invert	369.16 m	Downstream Invert	369.09 m
Length	15.90 m	Constructed Slope	0.004403 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.53 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.46 m
Velocity Downstream	1.82 m/s	Critical Slope	0.024000 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	370.23 m	Upstream Velocity Head	0.14 m
Ke	0.90	Entrance Loss	0.13 m

Inlet Control Properties			
Inlet Control HW Elev.	370.01 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-04 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	370.23 m	Headwater Depth/Height	0.73
Computed Headwater Elev:	370.25 m	Discharge	3.6900 m ³ /s
Inlet Control HW Elev.	370.15 m	Tailwater Elevation	370.09 m
Outlet Control HW Elev.	370.25 m	Control Type	Outlet Control

Grades			
Upstream Invert	369.35 m	Downstream Invert	369.25 m
Length	23.10 m	Constructed Slope	0.004329 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.84 m
Slope Type	Steep	Normal Depth	0.41 m
Flow Regime	Subcritical	Critical Depth	0.47 m
Velocity Downstream	1.20 m/s	Critical Slope	0.002892 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.66 m
Section Size	3660 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	370.25 m	Upstream Velocity Head	0.10 m
Ke	0.70	Entrance Loss	0.07 m

Inlet Control Properties			
Inlet Control HW Elev.	370.15 m	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	4.5 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-05 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.41 m	Headwater Depth/Height	1.34
Computed Headwater Elev:	372.41 m	Discharge	0.2200 m ³ /s
Inlet Control HW Elev.	372.39 m	Tailwater Elevation	372.01 m
Outlet Control HW Elev.	372.41 m	Control Type	Outlet Control

Grades			
Upstream Invert	371.80 m	Downstream Invert	371.62 m
Length	12.50 m	Constructed Slope	0.014640 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.39 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.33 m
Velocity Downstream	1.47 m/s	Critical Slope	0.024754 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	372.41 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	372.39 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-06 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.18 m	Headwater Depth/Height	0.74
Computed Headwater Elev:	372.25 m	Discharge	0.1110 m ³ /s
Inlet Control HW Elev.	372.23 m	Tailwater Elevation	371.90 m
Outlet Control HW Elev.	372.25 m	Control Type	Entrance Control

Grades			
Upstream Invert	371.91 m	Downstream Invert	371.56 m
Length	20.50 m	Constructed Slope	0.016927 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.34 m
Slope Type	Steep	Normal Depth	0.16 m
Flow Regime	N/A	Critical Depth	0.23 m
Velocity Downstream	0.86 m/s	Critical Slope	0.004590 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	372.25 m	Upstream Velocity Head	0.09 m
Ke	0.20	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	372.23 m	Flow Control	Unsubmerged
Inlet Type	Groove end projecting	Area Full	0.2 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

OBL-07 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.35 m	Headwater Depth/Height	0.47
Computed Headwater Elev:	371.14 m	Discharge	0.0490 m ³ /s
Inlet Control HW Elev.	371.12 m	Tailwater Elevation	371.03 m
Outlet Control HW Elev.	371.14 m	Control Type	Entrance Control

Grades			
Upstream Invert	370.92 m	Downstream Invert	370.73 m
Length	12.00 m	Constructed Slope	0.015583 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.30 m
Slope Type	Steep	Normal Depth	0.11 m
Flow Regime	N/A	Critical Depth	0.15 m
Velocity Downstream	0.43 m/s	Critical Slope	0.004190 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	371.14 m	Upstream Velocity Head	0.05 m
Ke	0.20	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	371.12 m	Flow Control	N/A
Inlet Type	Groove end projecting	Area Full	0.2 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

OBL-08 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.15 m	Headwater Depth/Height	1.10
Computed Headwater Elev:	371.90 m	Discharge	8.6000 m ³ /s
Inlet Control HW Elev.	371.82 m	Tailwater Elevation	371.36 m
Outlet Control HW Elev.	371.90 m	Control Type	Outlet Control

Grades			
Upstream Invert	370.22 m	Downstream Invert	370.19 m
Length	26.60 m	Constructed Slope	0.001128 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	1.17 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.93 m
Velocity Downstream	2.41 m/s	Critical Slope	0.003206 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	371.90 m	Upstream Velocity Head	0.28 m
Ke	0.70	Entrance Loss	0.20 m

Inlet Control Properties			
Inlet Control HW Elev.	371.82 m	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	4.6 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-09 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.16 m	Headwater Depth/Height	2.96
Computed Headwater Elev:	373.72 m	Discharge	0.2440 m ³ /s
Inlet Control HW Elev.	373.44 m	Tailwater Elevation	372.86 m
Outlet Control HW Elev.	373.72 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.54 m	Downstream Invert	372.48 m
Length	10.50 m	Constructed Slope	0.005333 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.38 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.35 m
Velocity Downstream	1.99 m/s	Critical Slope	0.042266 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.72 m	Upstream Velocity Head	0.19 m
Ke	0.90	Entrance Loss	0.17 m

Inlet Control Properties			
Inlet Control HW Elev.	373.44 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-10 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.79 m	Headwater Depth/Height	0.94
Computed Headwater Elev:	373.94 m	Discharge	0.0940 m ³ /s
Inlet Control HW Elev.	373.91 m	Tailwater Elevation	373.73 m
Outlet Control HW Elev.	373.94 m	Control Type	Outlet Control

Grades			
Upstream Invert	373.56 m	Downstream Invert	373.42 m
Length	12.35 m	Constructed Slope	0.011336 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.31 m
Slope Type	Mild	Normal Depth	0.27 m
Flow Regime	Subcritical	Critical Depth	0.22 m
Velocity Downstream	0.90 m/s	Critical Slope	0.020082 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.94 m	Upstream Velocity Head	0.05 m
Ke	0.90	Entrance Loss	0.05 m

Inlet Control Properties			
Inlet Control HW Elev.	373.91 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-11 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.64 m	Headwater Depth/Height	31.60
Computed Headwater Elev:	385.88 m	Discharge	0.8920 m ³ /s
Inlet Control HW Elev.	382.59 m	Tailwater Elevation	373.31 m
Outlet Control HW Elev.	385.88 m	Control Type	Outlet Control

Grades			
Upstream Invert	373.24 m	Downstream Invert	372.91 m
Length	12.30 m	Constructed Slope	0.026829 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.40 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.40 m
Velocity Downstream	7.10 m/s	Critical Slope	0.609186 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	385.88 m	Upstream Velocity Head	2.57 m
Ke	0.90	Entrance Loss	2.31 m

Inlet Control Properties			
Inlet Control HW Elev.	382.59 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-01 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.58 m	Headwater Depth/Height	0.82
Computed Headwater Elev:	372.65 m	Discharge	0.0450 m ³ /s
Inlet Control HW Elev.	372.62 m	Tailwater Elevation	372.34 m
Outlet Control HW Elev.	372.65 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.44 m	Downstream Invert	372.15 m
Length	13.50 m	Constructed Slope	0.021481 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.19 m
Slope Type	Mild	Normal Depth	0.12 m
Flow Regime	Subcritical	Critical Depth	0.12 m
Velocity Downstream	0.55 m/s	Critical Slope	0.021759 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.25 m
Section Size	250 mm	Rise	0.25 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	372.65 m	Upstream Velocity Head	0.05 m
Ke	0.90	Entrance Loss	0.04 m

Inlet Control Properties			
Inlet Control HW Elev.	372.62 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-02 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	381.65 m	Headwater Depth/Height	1.33
Computed Headwater Elev:	381.87 m	Discharge	0.1540 m ³ /s
Inlet Control HW Elev.	381.84 m	Tailwater Elevation	381.49 m
Outlet Control HW Elev.	381.87 m	Control Type	Outlet Control

Grades			
Upstream Invert	381.34 m	Downstream Invert	381.15 m
Length	12.20 m	Constructed Slope	0.014074 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.34 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.28 m
Velocity Downstream	1.35 m/s	Critical Slope	0.025457 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	381.87 m	Upstream Velocity Head	0.08 m
Ke	0.90	Entrance Loss	0.07 m

Inlet Control Properties			
Inlet Control HW Elev.	381.84 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-03 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	383.34 m	Headwater Depth/Height	1.49
Computed Headwater Elev:	383.42 m	Discharge	0.1340 m ³ /s
Inlet Control HW Elev.	383.27 m	Tailwater Elevation	383.13 m
Outlet Control HW Elev.	383.42 m	Control Type	Outlet Control

Grades			
Upstream Invert	382.82 m	Downstream Invert	382.79 m
Length	12.10 m	Constructed Slope	0.002479 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.34 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.27 m
Velocity Downstream	1.18 m/s	Critical Slope	0.023318 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	383.42 m	Upstream Velocity Head	0.06 m
Ke	0.90	Entrance Loss	0.05 m

Inlet Control Properties			
Inlet Control HW Elev.	383.27 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-04 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	385.22 m	Headwater Depth/Height	0.91
Computed Headwater Elev:	385.57 m	Discharge	0.0840 m ³ /s
Inlet Control HW Elev.	385.53 m	Tailwater Elevation	385.16 m
Outlet Control HW Elev.	385.57 m	Control Type	Entrance Control

Grades			
Upstream Invert	385.21 m	Downstream Invert	384.85 m
Length	13.75 m	Constructed Slope	0.026182 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.19 m
Slope Type	Steep	Normal Depth	0.19 m
Flow Regime	N/A	Critical Depth	0.21 m
Velocity Downstream	1.42 m/s	Critical Slope	0.019458 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	385.57 m	Upstream Velocity Head	0.08 m
Ke	0.90	Entrance Loss	0.07 m

Inlet Control Properties			
Inlet Control HW Elev.	385.53 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-05 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	392.88 m	Headwater Depth/Height	0.70
Computed Headwater Elev:	392.61 m	Discharge	0.0510 m ³ /s
Inlet Control HW Elev.	392.57 m	Tailwater Elevation	392.56 m
Outlet Control HW Elev.	392.61 m	Control Type	Outlet Control

Grades			
Upstream Invert	392.33 m	Downstream Invert	392.28 m
Length	12.80 m	Constructed Slope	0.003906 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.20 m
Slope Type	Mild	Normal Depth	0.25 m
Flow Regime	Subcritical	Critical Depth	0.16 m
Velocity Downstream	0.81 m/s	Critical Slope	0.017912 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	392.61 m	Upstream Velocity Head	0.02 m
Ke	0.90	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	392.57 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-06 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	393.61 m	Headwater Depth/Height	1.26
Computed Headwater Elev:	393.80 m	Discharge	0.3960 m ³ /s
Inlet Control HW Elev.	393.74 m	Tailwater Elevation	393.46 m
Outlet Control HW Elev.	393.80 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.03 m	Downstream Invert	392.96 m
Length	11.00 m	Constructed Slope	0.006364 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.50 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.41 m
Velocity Downstream	1.55 m/s	Critical Slope	0.020617 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	393.80 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	393.74 m	Flow Control	Unsubmerged
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-07 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	393.60 m	Headwater Depth/Height	16.39
Computed Headwater Elev:	399.63 m	Discharge	0.6300 m ³ /s
Inlet Control HW Elev.	397.84 m	Tailwater Elevation	393.34 m
Outlet Control HW Elev.	399.63 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.07 m	Downstream Invert	392.94 m
Length	12.35 m	Constructed Slope	0.010526 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	0.40 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	0.40 m
Velocity Downstream	5.01 m/s	Critical Slope	0.296130 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	399.63 m	Upstream Velocity Head	1.28 m
Ke	0.90	Entrance Loss	1.15 m

Inlet Control Properties			
Inlet Control HW Elev.	397.84 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-08 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	395.18 m	Headwater Depth/Height	1.31
Computed Headwater Elev:	395.07 m	Discharge	0.5600 m ³ /s
Inlet Control HW Elev.	395.07 m	Tailwater Elevation	394.55 m
Outlet Control HW Elev.	395.06 m	Control Type	Inlet Control

Grades			
Upstream Invert	394.27 m	Downstream Invert	394.00 m
Length	13.60 m	Constructed Slope	0.019853 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.36 m
Slope Type	Steep	Normal Depth	0.33 m
Flow Regime	N/A	Critical Depth	0.49 m
Velocity Downstream	3.10 m/s	Critical Slope	0.006833 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	395.06 m	Upstream Velocity Head	0.26 m
Ke	0.20	Entrance Loss	0.05 m

Inlet Control Properties			
Inlet Control HW Elev.	395.07 m	Flow Control	N/A
Inlet Type	Groove end projecting	Area Full	0.3 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

WCB-09 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	400.52 m	Headwater Depth/Height	1.39
Computed Headwater Elev:	401.26 m	Discharge	2.2240 m ³ /s
Inlet Control HW Elev.	401.17 m	Tailwater Elevation	400.63 m
Outlet Control HW Elev.	401.26 m	Control Type	Outlet Control

Grades			
Upstream Invert	399.91 m	Downstream Invert	399.85 m
Length	15.50 m	Constructed Slope	0.003871 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.78 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.66 m
Velocity Downstream	2.28 m/s	Critical Slope	0.016868 m/m

Section			
Section Shape	Arch	Mannings Coefficient	0.024
Section Material	Steel and Aluminum Var CR	Span	1.45 m
Section Size	1390 x 970 mm	Rise	0.97 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	401.26 m	Upstream Velocity Head	0.21 m
Ke	0.90	Entrance Loss	0.19 m

Inlet Control Properties			
Inlet Control HW Elev.	401.17 m	Flow Control	N/A
Inlet Type	Thin wall projecting	Area Full	1.1 m ²
K	0.03400	HDS 5 Chart	34
M	1.50000	HDS 5 Scale	3
C	0.04960	Equation Form	1
Y	0.57000		

Culvert Calculator Report

WCB-10 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	418.33 m	Headwater Depth/Height	1.77
Computed Headwater Elev:	418.33 m	Discharge	0.1910 m ³ /s
Inlet Control HW Elev.	418.25 m	Tailwater Elevation	417.74 m
Outlet Control HW Elev.	418.33 m	Control Type	Outlet Control

Grades			
Upstream Invert	417.62 m	Downstream Invert	417.38 m
Length	12.70 m	Constructed Slope	0.018898 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.36 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.32 m
Velocity Downstream	1.60 m/s	Critical Slope	0.030710 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	418.33 m	Upstream Velocity Head	0.12 m
Ke	0.90	Entrance Loss	0.11 m

Inlet Control Properties			
Inlet Control HW Elev.	418.25 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-11 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	425.95 m	Headwater Depth/Height	0.85
Computed Headwater Elev:	425.59 m	Discharge	0.0690 m ³ /s
Inlet Control HW Elev.	425.54 m	Tailwater Elevation	425.47 m
Outlet Control HW Elev.	425.59 m	Control Type	Outlet Control

Grades			
Upstream Invert	425.25 m	Downstream Invert	425.17 m
Length	15.50 m	Constructed Slope	0.005161 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.30 m
Slope Type	Mild	Normal Depth	0.28 m
Flow Regime	Subcritical	Critical Depth	0.19 m
Velocity Downstream	0.68 m/s	Critical Slope	0.018650 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	425.59 m	Upstream Velocity Head	0.03 m
Ke	0.90	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	425.54 m	Flow Control	Unsubmerged
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-12 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	426.90 m	Headwater Depth/Height	0.76
Computed Headwater Elev:	425.32 m	Discharge	0.1750 m ³ /s
Inlet Control HW Elev.	425.26 m	Tailwater Elevation	424.86 m
Outlet Control HW Elev.	425.32 m	Control Type	Entrance Control

Grades			
Upstream Invert	424.86 m	Downstream Invert	424.42 m
Length	18.20 m	Constructed Slope	0.024176 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.44 m
Slope Type	Steep	Normal Depth	0.24 m
Flow Regime	N/A	Critical Depth	0.27 m
Velocity Downstream	0.78 m/s	Critical Slope	0.015910 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	425.32 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	425.26 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-14 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	421.16 m	Headwater Depth/Height	0.15
Computed Headwater Elev:	419.68 m	Discharge	0.0040 m ³ /s
Inlet Control HW Elev.	419.66 m	Tailwater Elevation	419.33 m
Outlet Control HW Elev.	419.68 m	Control Type	Entrance Control

Grades			
Upstream Invert	419.61 m	Downstream Invert	419.09 m
Length	22.20 m	Constructed Slope	0.023423 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.24 m
Slope Type	Steep	Normal Depth	0.04 m
Flow Regime	N/A	Critical Depth	0.04 m
Velocity Downstream	0.05 m/s	Critical Slope	0.020017 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	419.68 m	Upstream Velocity Head	0.01 m
Ke	0.90	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	419.66 m	Flow Control	Unsubmerged
Inlet Type	Projecting	Area Full	0.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-15 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	418.30 m	Headwater Depth/Height	1.82
Computed Headwater Elev:	417.65 m	Discharge	0.2490 m ³ /s
Inlet Control HW Elev.	417.48 m	Tailwater Elevation	417.00 m
Outlet Control HW Elev.	417.65 m	Control Type	Outlet Control

Grades			
Upstream Invert	416.82 m	Downstream Invert	416.60 m
Length	18.20 m	Constructed Slope	0.012088 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.35 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.35 m
Velocity Downstream	1.85 m/s	Critical Slope	0.027438 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	417.65 m	Upstream Velocity Head	0.12 m
Ke	0.90	Entrance Loss	0.11 m

Inlet Control Properties			
Inlet Control HW Elev.	417.48 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.2 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-16 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	411.32 m	Headwater Depth/Height	1.76
Computed Headwater Elev:	411.64 m	Discharge	1.0370 m ³ /s
Inlet Control HW Elev.	411.64 m	Tailwater Elevation	410.51 m
Outlet Control HW Elev.	411.58 m	Control Type	Inlet Control

Grades			
Upstream Invert	410.30 m	Downstream Invert	409.82 m
Length	14.90 m	Constructed Slope	0.032215 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.58 m
Slope Type	Steep	Normal Depth	0.58 m
Flow Regime	N/A	Critical Depth	0.63 m
Velocity Downstream	2.81 m/s	Critical Slope	0.027132 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.76 m
Section Size	750 mm	Rise	0.76 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	411.58 m	Upstream Velocity Head	0.34 m
Ke	0.90	Entrance Loss	0.31 m

Inlet Control Properties			
Inlet Control HW Elev.	411.64 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.5 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-17 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	409.93 m	Headwater Depth/Height	1.36
Computed Headwater Elev:	409.69 m	Discharge	1.1570 m ³ /s
Inlet Control HW Elev.	409.56 m	Tailwater Elevation	409.18 m
Outlet Control HW Elev.	409.69 m	Control Type	Outlet Control

Grades			
Upstream Invert	408.45 m	Downstream Invert	408.41 m
Length	15.00 m	Constructed Slope	0.002667 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.77 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.63 m
Velocity Downstream	1.96 m/s	Critical Slope	0.018669 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	409.69 m	Upstream Velocity Head	0.16 m
Ke	0.90	Entrance Loss	0.14 m

Inlet Control Properties			
Inlet Control HW Elev.	409.56 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-18 Existing Conditions

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	392.79 m	Headwater Depth/Height	2.34
Computed Headwater Elev:	392.07 m	Discharge	1.7330 m ³ /s
Inlet Control HW Elev.	391.69 m	Tailwater Elevation	390.71 m
Outlet Control HW Elev.	392.07 m	Control Type	Outlet Control

Grades			
Upstream Invert	389.93 m	Downstream Invert	389.88 m
Length	23.00 m	Constructed Slope	0.002174 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.83 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.77 m
Velocity Downstream	2.77 m/s	Critical Slope	0.027475 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	392.07 m	Upstream Velocity Head	0.36 m
Ke	0.90	Entrance Loss	0.32 m

Inlet Control Properties			
Inlet Control HW Elev.	391.69 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Appendix D.2.
CulvertMaster Summary Table
(Existing Conditions)

Culvert No.	Road	Station	Peak Design Flow Calculations					CulvertMaster Calculations																
			Watershed Time of Concentration	Design Storm	Rainfall Intensity	Peak Design Flow	Material	Shape	Size / Diameter		Length	Depth of Fill	Flow Direction	U/S Invert	D/S Invert	Slope	Edge of Pavement Elevation	Minimum Freeboard	Minimum Clearance	Maximum Allowable Headwater Elevation	Calculated Headwater Elevation	Delta Headwater	Theoretical /Calculated Tailwater Elevation	Critical Depth
			Tc (min)	(years)	I (mm/hr)	Q (m ³ /s)			Span (mm)	Rise (mm)	(m)	(m)		(m)	(m)	(%)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)
OBL-01	Olde Base Line Road	30+030	60.25	25	48.69	0.479	CSP	Circular		450	12.5	0.35	N-S	372.4	372.25	1.200	373.200	0.3	0	372.90	374.63	-1.73	372.70	0.44
OBL-02	Olde Base Line Road	30+540	86.25	25	37.43	1.8	CSP	Circular		600	14.3	0.24	N-S	372.71	372.70	0.070	373.545	1.0	0.3	372.55	380.84	-8.29	373.31	0.61
OBL-03	Olde Base Line Road	30+715	62.46	25	47.45	0.49	CSP	Circular		600	15.9	0.16	N-S	369.16	369.09	0.440	369.920	0.3	0	369.62	370.23	-0.61	369.62	0.46
OBL-04	Olde Base Line Road	30+940	103.9	25	n/a	3.69 (See Note 1)	RCB	Box	3300	1200	23.1	0.68	N-S	369.35	369.25	0.433	371.229	1.0	0.3	370.23	370.25	-0.02	370.09	0.47
OBL-05	Olde Base Line Road	31+280	59.32	25	49.24	0.22	CSP	Circular		450	12.5	0.46	N-S	371.80	371.62	1.464	372.713	0.3	0	372.41	372.41	0.00	372.01	0.33
OBL-06	Olde Base Line Road	31+300	82.51	25	38.69	0.111	HDPE	Circular		450	20.5	0.12	N-S	371.91	371.56	1.712	372.480	0.3	0	372.18	372.25	-0.07	371.90	0.23
OBL-07	Olde Base Line Road	31+380	41.99	25	62.66	0.049	HDPE	Circular		450	12	0.28	N-S	370.92	370.73	1.558	371.650	0.3	0	371.35	371.14	0.21	371.03	0.15
OBL-08	Olde Base Line Road	31+410	171.04	25	n/a	8.6 (See Note 1)	RCB	Box	3050	1400	26.6	0.53	N-S	370.22	370.19	0.102	372.148	1.0	0.3	371.15	371.9	-0.75	371.36	0.93
OBL-09	Olde Base Line Road	32+080	29.97	25	78.15	0.244	CSP	Circular		400	10.5	0.52	S-N	372.54	372.48	0.533	373.464	0.3	0	373.16	373.72	-0.56	372.86	0.35
OBL-10	Olde Base Line Road	32+230	25.38	25	86.6	0.094	CSP	Circular		400	12.35	0.12	N-S	373.56	373.42	1.190	374.085	0.3	0	373.79	373.94	-0.16	373.73	0.22
OBL-11	Olde Base Line Road	32+340	83.97	25	38.19	0.892	CSP	Circular		400	12.3	0.29	N-S	373.24	372.91	2.675	373.935	0.3	0	373.64	385.88	-12.25	373.31	0.4
WCB-01	Winston Churchill Boulevard	40+030	47.76	25	57.36	0.045	CSP	Twin Circular		250	13.5	0.19	E-W	372.44	372.15	2.148	372.878	0.3	0	372.58	372.65	-0.07	372.34	0.12
WCB-02	Winston Churchill Boulevard	40+480	43.35	25	61.31	0.154	CSP	Circular		400	12.2	0.21	E-W	381.34	381.15	1.541	381.950	0.3	0	381.65	381.87	-0.22	381.49	0.28
WCB-03	Winston Churchill Boulevard	40+660	53.81	25	52.78	0.134	CSP	Circular		400	12.1	0.42	E-W	382.82	382.79	0.207	383.638	0.3	0	383.34	383.42	-0.08	383.13	0.27
WCB-04	Winston Churchill Boulevard	40+870	34.69	25	71.15	0.084	CSP	Circular		400	13.75	0.20	W-E	385.21	384.85	2.582	385.520	0.3	0	385.22	385.57	-0.35	385.16	0.21
WCB-05	Winston Churchill Boulevard	41+110	28.07	25	81.41	0.051	CSP	Circular		400	12.8	0.46	E-W	392.33	392.28	0.406	393.183	0.3	0	392.88	392.61	0.27	392.56	0.16
WCB-06	Winston Churchill Boulevard	41+400	55.21	25	51.83	0.396	CSP	Circular		600	11	0.28	E-W	393.03	392.96	0.700	393.910	0.3	0	393.61	393.8	-0.19	393.46	0.41
WCB-07	Winston Churchill Boulevard	41+710	39.12	25	65.71	0.63	CSP	Circular		400	12.35	0.43	E-W	393.07	392.94	1.061	393.900	0.3	0	393.60	399.63	-6.03	393.34	0.4
WCB-08	Winston Churchill Boulevard	41+890	26.4	25	84.55	0.556	HDPE	Circular		600	13.6	0.61	E-W	394.27	394.00	1.985	395.480	0.3	0	395.18	395.07	0.11	394.55	0.49
WCB-09	Winston Churchill Boulevard	42+195	76.9	25	40.76	2.224	CSPA	Arch	1400	900	15.5	0.71	E-W	399.91	399.85	0.387	401.520	1.0	0.3	400.52	401.26	-0.74	400.63	0.66
WCB-10	Winston Churchill Boulevard	42+750	23.15	25	91.48	0.191	CSP	Circular		400	12.7	0.61	E-W	417.62	417.38	1.890	418.630	0.3	0	418.33	418.33	0.00	417.74	0.32
WCB-11	Winston Churchill Boulevard	43+130	26.28	25	84.78	0.069	CSP	Circular		400	15.5	0.60	W-E	425.25	425.17	0.516	426.250	0.3	0	425.95	425.59	0.36	425.47	0.19
WCB-12	Winston Churchill Boulevard	43+210	41.18	25	62.47	0.175	CSP	Circular		600	18.2	1.74	W-E	424.86	424.42	2.418	427.200	0.3	0	426.90	425.32	1.58	424.86	0.27
WCB-13	Winston Churchill Boulevard	44+140	0	25	0	0	CSP	Circular		400	16	1.34	W-E	424.69	424.55	0.875	426.425	0.3	0	426.13	Equalization Culvert		424.75	
WCB-14	Winston Churchill Boulevard	44+310	18.87	25	102.82	0.004	CSP	Circular		450	22.2	1.40	E-W	419.61	419.09	2.360	421.458	0.3	0	421.16	419.68	1.48	419.33	0.04
WCB-15	Winston Churchill Boulevard	44+615	30.82	25	76.77	0.249	CSP	Circular		450	18.2	1.33	E-W	416.82	416.60	1.221	418.600	0.3	0	418.30	417.65	0.65	417.00	0.35
WCB-16	Winston Churchill Boulevard	44+945	57.82	25	50.15	1.037	CSP	Circular		750	14.9	0.57	W-E	410.30	409.82	3.255	411.622	0.3	0	411.32	411.64	-0.32	410.51	0.63
WCB-17	Winston Churchill Boulevard	45+095	87.14	25	37.14	1.157	CSP	Circular		900	15	0.88	E-W	408.45	408.41	0.267	410.234	0.3	0	409.93	409.69	0.24	409.18	0.63
WCB-18	Winston Churchill Boulevard	45+865	80.72	25	39.33	1.733	CSP	Circular		900	23	2.25	E-W	389.93	389.88	0.257	393.085	0.3	0	392.79	392.07	0.71	390.71	0.77

Note 1: 25 year peak flow determined from SWMHYMO Model

Appendix E
CulvertMaster Assessment
(Future Conditions)

Appendix E.1.
CulvertMaster Output
(Future Conditions)

Culvert Calculator Report

OBL-01 - Future Conditions - Upgrade 2x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.00 m	Headwater Depth/Height	0.87
Computed Headwater Elev:	372.93 m	Discharge	0.4790 m ³ /s
Inlet Control HW Elev.	372.89 m	Tailwater Elevation	372.71 m
Outlet Control HW Elev.	372.93 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.40 m	Downstream Invert	372.25 m
Length	12.50 m	Constructed Slope	0.012000 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.46 m
Slope Type	Mild	Normal Depth	0.35 m
Flow Regime	Subcritical	Critical Depth	0.32 m
Velocity Downstream	1.01 m/s	Critical Slope	0.016883 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	372.93 m	Upstream Velocity Head	0.08 m
Ke	0.90	Entrance Loss	0.07 m

Inlet Control Properties			
Inlet Control HW Elev.	372.89 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.6 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-02 - Future Conditions - Upgrade 3000 x1200 Box (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.19 m	Headwater Depth/Height	0.67
Computed Headwater Elev:	373.53 m	Discharge	1.8000 m ³ /s
Inlet Control HW Elev.	373.47 m	Tailwater Elevation	373.47 m
Outlet Control HW Elev.	373.53 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.71 m	Downstream Invert	372.70 m
Length	14.30 m	Constructed Slope	0.000699 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.77 m
Slope Type	Mild	Normal Depth	0.64 m
Flow Regime	Subcritical	Critical Depth	0.33 m
Velocity Downstream	0.77 m/s	Critical Slope	0.005328 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.53 m	Upstream Velocity Head	0.03 m
Ke	0.70	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	373.47 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-02 - Future Conditions - Upgrade 3000 x1200 Box (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	374.19 m	Headwater Depth/Height	0.71
Computed Headwater Elev:	373.57 m	Discharge	2.2290 m ³ /s
Inlet Control HW Elev.	373.49 m	Tailwater Elevation	373.49 m
Outlet Control HW Elev.	373.57 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.71 m	Downstream Invert	372.70 m
Length	14.30 m	Constructed Slope	0.000699 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.79 m
Slope Type	Mild	Normal Depth	0.75 m
Flow Regime	Subcritical	Critical Depth	0.38 m
Velocity Downstream	0.93 m/s	Critical Slope	0.005266 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.57 m	Upstream Velocity Head	0.04 m
Ke	0.70	Entrance Loss	0.03 m

Inlet Control Properties			
Inlet Control HW Elev.	373.49 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-02 - Future Conditions - Upgrade 3000 x1200 Box (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	374.19 m	Headwater Depth/Height	1.02
Computed Headwater Elev:	373.95 m	Discharge	5.2330 m ³ /s
Inlet Control HW Elev.	373.85 m	Tailwater Elevation	373.64 m
Outlet Control HW Elev.	373.95 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.71 m	Downstream Invert	372.70 m
Length	14.30 m	Constructed Slope	0.000699 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.94 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.67 m
Velocity Downstream	1.83 m/s	Critical Slope	0.005265 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.95 m	Upstream Velocity Head	0.16 m
Ke	0.70	Entrance Loss	0.11 m

Inlet Control Properties			
Inlet Control HW Elev.	373.85 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-03 - Future Conditions - Maintian Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.58 m	Headwater Depth/Height	1.75
Computed Headwater Elev:	370.23 m	Discharge	0.4900 m ³ /s
Inlet Control HW Elev.	370.01 m	Tailwater Elevation	369.62 m
Outlet Control HW Elev.	370.23 m	Control Type	Outlet Control

Grades			
Upstream Invert	369.16 m	Downstream Invert	369.09 m
Length	15.90 m	Constructed Slope	0.004403 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.53 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.46 m
Velocity Downstream	1.82 m/s	Critical Slope	0.024000 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	370.23 m	Upstream Velocity Head	0.14 m
Ke	0.90	Entrance Loss	0.13 m

Inlet Control Properties			
Inlet Control HW Elev.	370.01 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-04 - Future Conditions - Maintain Existing (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	370.23 m	Headwater Depth/Height	0.79
Computed Headwater Elev:	370.30 m	Discharge	3.6900 m ³ /s
Inlet Control HW Elev.	370.20 m	Tailwater Elevation	370.10 m
Outlet Control HW Elev.	370.30 m	Control Type	Outlet Control

Grades			
Upstream Invert	369.35 m	Downstream Invert	369.25 m
Length	23.10 m	Constructed Slope	0.004329 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.85 m
Slope Type	Mild	Normal Depth	0.53 m
Flow Regime	Subcritical	Critical Depth	0.50 m
Velocity Downstream	1.32 m/s	Critical Slope	0.005081 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.30 m
Section Size	3300 x 1200 mm	Rise	1.20 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	370.30 m	Upstream Velocity Head	0.11 m
Ke	0.70	Entrance Loss	0.08 m

Inlet Control Properties			
Inlet Control HW Elev.	370.20 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.0 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-04 - Future Conditions - Maintain Existing (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.23 m	Headwater Depth/Height	0.98
Computed Headwater Elev:	370.52 m	Discharge	5.4100 m ³ /s
Inlet Control HW Elev.	370.46 m	Tailwater Elevation	370.18 m
Outlet Control HW Elev.	370.52 m	Control Type	Outlet Control

Grades			
Upstream Invert	369.35 m	Downstream Invert	369.25 m
Length	23.10 m	Constructed Slope	0.004329 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.93 m
Slope Type	Mild	Normal Depth	0.69 m
Flow Regime	Subcritical	Critical Depth	0.65 m
Velocity Downstream	1.76 m/s	Critical Slope	0.005094 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.30 m
Section Size	3300 x 1200 mm	Rise	1.20 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	370.52 m	Upstream Velocity Head	0.19 m
Ke	0.70	Entrance Loss	0.13 m

Inlet Control Properties			
Inlet Control HW Elev.	370.46 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.0 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-04 - Future Conditions - Maintain Existing (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.23 m	Headwater Depth/Height	2.43
Computed Headwater Elev:	372.26 m	Discharge	14.7800 m ³ /s
Inlet Control HW Elev.	372.26 m	Tailwater Elevation	370.45 m
Outlet Control HW Elev.	371.94 m	Control Type	Inlet Control

Grades			
Upstream Invert	369.35 m	Downstream Invert	369.25 m
Length	23.10 m	Constructed Slope	0.004329 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	1.20 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	1.20 m
Velocity Downstream	3.73 m/s	Critical Slope	0.012030 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.30 m
Section Size	3300 x 1200 mm	Rise	1.20 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	371.94 m	Upstream Velocity Head	0.71 m
Ke	0.70	Entrance Loss	0.50 m

Inlet Control Properties			
Inlet Control HW Elev.	372.26 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.0 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-05 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.41 m	Headwater Depth/Height	0.84
Computed Headwater Elev:	372.31 m	Discharge	0.2200 m ³ /s
Inlet Control HW Elev.	372.26 m	Tailwater Elevation	372.07 m
Outlet Control HW Elev.	372.31 m	Control Type	Outlet Control

Grades			
Upstream Invert	371.80 m	Downstream Invert	371.62 m
Length	12.50 m	Constructed Slope	0.014640 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.45 m
Slope Type	Mild	Normal Depth	0.31 m
Flow Regime	Subcritical	Critical Depth	0.30 m
Velocity Downstream	0.95 m/s	Critical Slope	0.016557 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	372.31 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	372.26 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-06 - Future Conditions - Upgrade 2x450

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.13 m	Headwater Depth/Height	0.51
Computed Headwater Elev:	372.14 m	Discharge	0.1110 m ³ /s
Inlet Control HW Elev.	372.13 m	Tailwater Elevation	371.87 m
Outlet Control HW Elev.	372.14 m	Control Type	Entrance Control

Grades			
Upstream Invert	371.91 m	Downstream Invert	371.56 m
Length	20.50 m	Constructed Slope	0.016927 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.31 m
Slope Type	Steep	Normal Depth	0.11 m
Flow Regime	N/A	Critical Depth	0.16 m
Velocity Downstream	0.47 m/s	Critical Slope	0.004207 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	372.14 m	Upstream Velocity Head	0.06 m
Ke	0.20	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	372.13 m	Flow Control	N/A
Inlet Type	Groove end projecting	Area Full	0.3 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

OBL-07 - Future Conditions Maintain Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.56 m	Headwater Depth/Height	0.47
Computed Headwater Elev:	371.14 m	Discharge	0.0490 m ³ /s
Inlet Control HW Elev.	371.12 m	Tailwater Elevation	371.03 m
Outlet Control HW Elev.	371.14 m	Control Type	Entrance Control

Grades			
Upstream Invert	370.92 m	Downstream Invert	370.73 m
Length	12.00 m	Constructed Slope	0.015583 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.30 m
Slope Type	Steep	Normal Depth	0.11 m
Flow Regime	N/A	Critical Depth	0.15 m
Velocity Downstream	0.43 m/s	Critical Slope	0.004190 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.46 m
Section Size	450 mm	Rise	0.46 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	371.14 m	Upstream Velocity Head	0.05 m
Ke	0.20	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	371.12 m	Flow Control	N/A
Inlet Type	Groove end projecting	Area Full	0.2 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

OBL-08 - Future Conditions - Maintain Existing (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	371.07 m	Headwater Depth/Height	1.10
Computed Headwater Elev:	371.90 m	Discharge	8.6500 m ³ /s
Inlet Control HW Elev.	371.82 m	Tailwater Elevation	371.36 m
Outlet Control HW Elev.	371.90 m	Control Type	Outlet Control

Grades			
Upstream Invert	370.22 m	Downstream Invert	370.19 m
Length	26.60 m	Constructed Slope	0.001128 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	1.17 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.94 m
Velocity Downstream	2.43 m/s	Critical Slope	0.003208 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	371.90 m	Upstream Velocity Head	0.28 m
Ke	0.70	Entrance Loss	0.20 m

Inlet Control Properties			
Inlet Control HW Elev.	371.82 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.6 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-08 - Future Conditions - Maintain Existing (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.07 m	Headwater Depth/Height	1.50
Computed Headwater Elev:	372.51 m	Discharge	12.7300 m ³ /s
Inlet Control HW Elev.	372.51 m	Tailwater Elevation	371.50 m
Outlet Control HW Elev.	372.39 m	Control Type	Inlet Control

Grades			
Upstream Invert	370.22 m	Downstream Invert	370.19 m
Length	26.60 m	Constructed Slope	0.001128 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	1.31 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	1.21 m
Velocity Downstream	3.19 m/s	Critical Slope	0.003391 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	372.39 m	Upstream Velocity Head	0.44 m
Ke	0.70	Entrance Loss	0.31 m

Inlet Control Properties			
Inlet Control HW Elev.	372.51 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.6 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-08 - Future Conditions - Maintain Existing (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	372.07 m	Headwater Depth/Height	10.06
Computed Headwater Elev:	385.56 m	Discharge	46.8000 m ³ /s
Inlet Control HW Elev.	385.56 m	Tailwater Elevation	371.65 m
Outlet Control HW Elev.	381.64 m	Control Type	Inlet Control

Grades			
Upstream Invert	370.22 m	Downstream Invert	370.19 m
Length	26.60 m	Constructed Slope	0.001128 m/m

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	1.52 m
Slope Type	N/A	Normal Depth	N/A m
Flow Regime	N/A	Critical Depth	1.52 m
Velocity Downstream	10.08 m/s	Critical Slope	0.042321 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	381.64 m	Upstream Velocity Head	5.18 m
Ke	0.70	Entrance Loss	3.62 m

Inlet Control Properties			
Inlet Control HW Elev.	385.56 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	4.6 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

OBL-09 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	374.29 m	Headwater Depth/Height	0.93
Computed Headwater Elev:	373.11 m	Discharge	0.2440 m ³ /s
Inlet Control HW Elev.	373.04 m	Tailwater Elevation	372.94 m
Outlet Control HW Elev.	373.11 m	Control Type	Outlet Control

Grades			
Upstream Invert	372.54 m	Downstream Invert	372.48 m
Length	10.50 m	Constructed Slope	0.005333 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.46 m
Slope Type	Mild	Normal Depth	0.48 m
Flow Regime	Subcritical	Critical Depth	0.32 m
Velocity Downstream	1.04 m/s	Critical Slope	0.016965 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.11 m	Upstream Velocity Head	0.05 m
Ke	0.90	Entrance Loss	0.05 m

Inlet Control Properties			
Inlet Control HW Elev.	373.04 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-10 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	374.43 m	Headwater Depth/Height	0.54
Computed Headwater Elev:	373.89 m	Discharge	0.0940 m ³ /s
Inlet Control HW Elev.	373.83 m	Tailwater Elevation	373.81 m
Outlet Control HW Elev.	373.89 m	Control Type	Outlet Control

Grades			
Upstream Invert	373.56 m	Downstream Invert	373.42 m
Length	12.35 m	Constructed Slope	0.011336 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.41 m
Slope Type	Mild	Normal Depth	0.21 m
Flow Regime	Subcritical	Critical Depth	0.19 m
Velocity Downstream	0.45 m/s	Critical Slope	0.015204 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	373.89 m	Upstream Velocity Head	0.03 m
Ke	0.90	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	373.83 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

OBL-11 - Future Conditions - Upgrade 2x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	373.81 m	Headwater Depth/Height	1.35
Computed Headwater Elev:	374.06 m	Discharge	0.8920 m ³ /s
Inlet Control HW Elev.	374.01 m	Tailwater Elevation	373.43 m
Outlet Control HW Elev.	374.06 m	Control Type	Entrance Control

Grades			
Upstream Invert	373.24 m	Downstream Invert	372.91 m
Length	12.30 m	Constructed Slope	0.026829 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.52 m
Slope Type	Steep	Normal Depth	0.41 m
Flow Regime	N/A	Critical Depth	0.44 m
Velocity Downstream	1.68 m/s	Critical Slope	0.022282 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	374.06 m	Upstream Velocity Head	0.20 m
Ke	0.90	Entrance Loss	0.18 m

Inlet Control Properties			
Inlet Control HW Elev.	374.01 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.6 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-02 - Future Conditions - Upgrade 2x400

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	381.66 m	Headwater Depth/Height	0.84
Computed Headwater Elev:	381.68 m	Discharge	0.1540 m ³ /s
Inlet Control HW Elev.	381.65 m	Tailwater Elevation	381.45 m
Outlet Control HW Elev.	381.68 m	Control Type	Outlet Control

Grades			
Upstream Invert	381.34 m	Downstream Invert	381.15 m
Length	12.20 m	Constructed Slope	0.014074 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.30 m
Slope Type	Mild	Normal Depth	0.22 m
Flow Regime	Subcritical	Critical Depth	0.20 m
Velocity Downstream	0.76 m/s	Critical Slope	0.019040 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	381.68 m	Upstream Velocity Head	0.06 m
Ke	0.90	Entrance Loss	0.06 m

Inlet Control Properties			
Inlet Control HW Elev.	381.65 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-03 - Future Conditions - Upgrade 2x400

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	383.28 m	Headwater Depth/Height	0.88
Computed Headwater Elev:	383.17 m	Discharge	0.1340 m ³ /s
Inlet Control HW Elev.	383.10 m	Tailwater Elevation	383.08 m
Outlet Control HW Elev.	383.17 m	Control Type	Outlet Control

Grades			
Upstream Invert	382.82 m	Downstream Invert	382.79 m
Length	12.10 m	Constructed Slope	0.002479 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.29 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.18 m
Velocity Downstream	0.69 m/s	Critical Slope	0.018570 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.40 m
Section Size	400 mm	Rise	0.40 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	383.17 m	Upstream Velocity Head	0.02 m
Ke	0.90	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	383.10 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-04 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	385.75 m	Headwater Depth/Height	0.51
Computed Headwater Elev:	385.52 m	Discharge	0.0840 m ³ /s
Inlet Control HW Elev.	385.46 m	Tailwater Elevation	385.24 m
Outlet Control HW Elev.	385.52 m	Control Type	Entrance Control

Grades			
Upstream Invert	385.21 m	Downstream Invert	384.85 m
Length	13.75 m	Constructed Slope	0.026182 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.39 m
Slope Type	Steep	Normal Depth	0.16 m
Flow Regime	N/A	Critical Depth	0.18 m
Velocity Downstream	0.43 m/s	Critical Slope	0.015189 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	385.52 m	Upstream Velocity Head	0.07 m
Ke	0.90	Entrance Loss	0.06 m

Inlet Control Properties			
Inlet Control HW Elev.	385.46 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-05 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	393.45 m	Headwater Depth/Height	0.55
Computed Headwater Elev:	392.67 m	Discharge	0.0510 m ³ /s
Inlet Control HW Elev.	392.65 m	Tailwater Elevation	392.65 m
Outlet Control HW Elev.	392.67 m	Control Type	Outlet Control

Grades			
Upstream Invert	392.33 m	Downstream Invert	392.28 m
Length	12.80 m	Constructed Slope	0.003906 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.37 m
Slope Type	Mild	Normal Depth	0.20 m
Flow Regime	Subcritical	Critical Depth	0.14 m
Velocity Downstream	0.28 m/s	Critical Slope	0.015367 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	392.67 m	Upstream Velocity Head	0.01 m
Ke	0.90	Entrance Loss	0.00 m

Inlet Control Properties			
Inlet Control HW Elev.	392.65 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-06 - Future Conditions - Upgrade 1829 x 610 Box (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	392.81 m	Headwater Depth/Height	0.59
Computed Headwater Elev:	393.39 m	Discharge	0.3960 m ³ /s
Inlet Control HW Elev.	393.35 m	Tailwater Elevation	393.35 m
Outlet Control HW Elev.	393.39 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.03 m	Downstream Invert	392.96 m
Length	11.00 m	Constructed Slope	0.006364 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.39 m
Slope Type	Mild	Normal Depth	0.17 m
Flow Regime	Subcritical	Critical Depth	0.17 m
Velocity Downstream	0.56 m/s	Critical Slope	0.006429 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1829 x 610 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	393.39 m	Upstream Velocity Head	0.02 m
Ke	0.70	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	393.35 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	1.1 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-06 - Future Conditions - Upgrade 1829 x 610 Box (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	393.81 m	Headwater Depth/Height	0.63
Computed Headwater Elev:	393.42 m	Discharge	0.4900 m ³ /s
Inlet Control HW Elev.	393.36 m	Tailwater Elevation	393.36 m
Outlet Control HW Elev.	393.42 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.03 m	Downstream Invert	392.96 m
Length	11.00 m	Constructed Slope	0.006364 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.40 m
Slope Type	Steep	Normal Depth	0.19 m
Flow Regime	Subcritical	Critical Depth	0.19 m
Velocity Downstream	0.67 m/s	Critical Slope	0.006327 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1829 x 610 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	393.42 m	Upstream Velocity Head	0.03 m
Ke	0.70	Entrance Loss	0.02 m

Inlet Control Properties			
Inlet Control HW Elev.	393.36 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	1.1 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-06 - Future Conditions - Upgrade 1829 x 610 Box (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	393.51 m	Headwater Depth/Height	1.07
Computed Headwater Elev:	393.68 m	Discharge	1.2480 m ³ /s
Inlet Control HW Elev.	393.65 m	Tailwater Elevation	393.44 m
Outlet Control HW Elev.	393.68 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.03 m	Downstream Invert	392.96 m
Length	11.00 m	Constructed Slope	0.006364 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.48 m
Slope Type	Steep	Normal Depth	0.36 m
Flow Regime	Subcritical	Critical Depth	0.36 m
Velocity Downstream	1.42 m/s	Critical Slope	0.006204 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1829 x 610 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	393.68 m	Upstream Velocity Head	0.14 m
Ke	0.70	Entrance Loss	0.10 m

Inlet Control Properties			
Inlet Control HW Elev.	393.65 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	1.1 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-07 - Future Conditions - Upgrade 1x700

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	394.12 m	Headwater Depth/Height	1.33
Computed Headwater Elev:	394.00 m	Discharge	0.6300 m ³ /s
Inlet Control HW Elev.	393.96 m	Tailwater Elevation	393.54 m
Outlet Control HW Elev.	394.00 m	Control Type	Outlet Control

Grades			
Upstream Invert	393.07 m	Downstream Invert	392.94 m
Length	12.35 m	Constructed Slope	0.010526 m/m

Hydraulic Profile			
Profile	M2	Depth, Downstream	0.60 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.50 m
Velocity Downstream	1.79 m/s	Critical Slope	0.021273 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.70 m
Section Size	700 mm	Rise	0.70 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	394.00 m	Upstream Velocity Head	0.14 m
Ke	0.90	Entrance Loss	0.13 m

Inlet Control Properties			
Inlet Control HW Elev.	393.96 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.4 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-08 - Future Conditions - Maintain Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	395.36 m	Headwater Depth/Height	1.31
Computed Headwater Elev:	395.07 m	Discharge	0.5600 m ³ /s
Inlet Control HW Elev.	395.07 m	Tailwater Elevation	394.55 m
Outlet Control HW Elev.	395.06 m	Control Type	Inlet Control

Grades			
Upstream Invert	394.27 m	Downstream Invert	394.00 m
Length	13.60 m	Constructed Slope	0.019853 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.36 m
Slope Type	Steep	Normal Depth	0.33 m
Flow Regime	N/A	Critical Depth	0.49 m
Velocity Downstream	3.10 m/s	Critical Slope	0.006833 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.012
Section Material	HDPE (Smooth Interior)	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	395.06 m	Upstream Velocity Head	0.26 m
Ke	0.20	Entrance Loss	0.05 m

Inlet Control Properties			
Inlet Control HW Elev.	395.07 m	Flow Control	N/A
Inlet Type	Groove end projecting	Area Full	0.3 m ²
K	0.00450	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	3
C	0.03170	Equation Form	1
Y	0.69000		

Culvert Calculator Report

WCB-09 - Future Conditions - Upgrade 6000 x 1524 Box (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	401.08 m	Headwater Depth/Height	0.55
Computed Headwater Elev:	400.75 m	Discharge	2.2240 m ³ /s
Inlet Control HW Elev.	400.73 m	Tailwater Elevation	400.73 m
Outlet Control HW Elev.	400.75 m	Control Type	Outlet Control

Grades			
Upstream Invert	399.91 m	Downstream Invert	399.85 m
Length	15.50 m	Constructed Slope	0.003871 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.88 m
Slope Type	Mild	Normal Depth	0.27 m
Flow Regime	Subcritical	Critical Depth	0.24 m
Velocity Downstream	0.41 m/s	Critical Slope	0.005548 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	400.75 m	Upstream Velocity Head	0.01 m
Ke	0.70	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	400.73 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	9.3 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-09 - Future Conditions - Upgrade 6000 x1524 Box (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	402.08 m	Headwater Depth/Height	0.64
Computed Headwater Elev:	400.89 m	Discharge	2.7530 m ³ /s
Inlet Control HW Elev.	400.87 m	Tailwater Elevation	400.75 m
Outlet Control HW Elev.	400.89 m	Control Type	Outlet Control

Grades			
Upstream Invert	399.91 m	Downstream Invert	399.85 m
Length	15.50 m	Constructed Slope	0.003871 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	1.02 m
Slope Type	Mild	Normal Depth	0.31 m
Flow Regime	Subcritical	Critical Depth	0.28 m
Velocity Downstream	0.44 m/s	Critical Slope	0.005437 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	400.89 m	Upstream Velocity Head	0.01 m
Ke	0.70	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	400.87 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	9.3 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-09 - Future Conditions - Upgrade 6000 x1524 Box (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	402.08 m	Headwater Depth/Height	0.68
Computed Headwater Elev:	400.94 m	Discharge	7.5040 m ³ /s
Inlet Control HW Elev.	400.82 m	Tailwater Elevation	400.88 m
Outlet Control HW Elev.	400.94 m	Control Type	Outlet Control

Grades			
Upstream Invert	399.91 m	Downstream Invert	399.85 m
Length	15.50 m	Constructed Slope	0.003871 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.90 m
Slope Type	Mild	Normal Depth	0.59 m
Flow Regime	Subcritical	Critical Depth	0.54 m
Velocity Downstream	1.37 m/s	Critical Slope	0.005214 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1520 mm	Rise	1.52 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	400.94 m	Upstream Velocity Head	0.11 m
Ke	0.70	Entrance Loss	0.08 m

Inlet Control Properties			
Inlet Control HW Elev.	400.82 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	9.3 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-10 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	418.35 m	Headwater Depth/Height	0.80
Computed Headwater Elev:	418.11 m	Discharge	0.1910 m ³ /s
Inlet Control HW Elev.	418.04 m	Tailwater Elevation	417.82 m
Outlet Control HW Elev.	418.11 m	Control Type	Entrance Control

Grades			
Upstream Invert	417.62 m	Downstream Invert	417.38 m
Length	12.70 m	Constructed Slope	0.018898 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.44 m
Slope Type	Steep	Normal Depth	0.27 m
Flow Regime	N/A	Critical Depth	0.28 m
Velocity Downstream	0.85 m/s	Critical Slope	0.016105 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	418.11 m	Upstream Velocity Head	0.11 m
Ke	0.90	Entrance Loss	0.10 m

Inlet Control Properties			
Inlet Control HW Elev.	418.04 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-11 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	427.26 m	Headwater Depth/Height	0.56
Computed Headwater Elev:	425.59 m	Discharge	0.0690 m ³ /s
Inlet Control HW Elev.	425.56 m	Tailwater Elevation	425.56 m
Outlet Control HW Elev.	425.59 m	Control Type	Outlet Control

Grades			
Upstream Invert	425.25 m	Downstream Invert	425.17 m
Length	15.50 m	Constructed Slope	0.005161 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.39 m
Slope Type	Mild	Normal Depth	0.22 m
Flow Regime	Subcritical	Critical Depth	0.17 m
Velocity Downstream	0.35 m/s	Critical Slope	0.015220 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	425.59 m	Upstream Velocity Head	0.01 m
Ke	0.90	Entrance Loss	0.01 m

Inlet Control Properties			
Inlet Control HW Elev.	425.56 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-12 - Future Conditions - Maintain Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	426.88 m	Headwater Depth/Height	0.76
Computed Headwater Elev:	425.32 m	Discharge	0.1750 m ³ /s
Inlet Control HW Elev.	425.26 m	Tailwater Elevation	424.86 m
Outlet Control HW Elev.	425.32 m	Control Type	Entrance Control

Grades			
Upstream Invert	424.86 m	Downstream Invert	424.42 m
Length	18.20 m	Constructed Slope	0.024176 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.44 m
Slope Type	Steep	Normal Depth	0.24 m
Flow Regime	N/A	Critical Depth	0.27 m
Velocity Downstream	0.78 m/s	Critical Slope	0.015910 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	425.32 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	425.26 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-14 - Future Conditions - Upgrade 1800 x 900 Box (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	425.55 m	Headwater Depth/Height	0.09
Computed Headwater Elev:	419.69 m	Discharge	0.0230 m ³ /s
Inlet Control HW Elev.	419.69 m	Tailwater Elevation	419.69 m
Outlet Control HW Elev.	419.69 m	Control Type	Outlet Control

Grades			
Upstream Invert	419.61 m	Downstream Invert	419.09 m
Length	22.20 m	Constructed Slope	0.023423 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.60 m
Slope Type	Steep	Normal Depth	0.02 m
Flow Regime	Subcritical	Critical Depth	0.03 m
Velocity Downstream	0.02 m/s	Critical Slope	0.010016 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1830 x 910 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	419.69 m	Upstream Velocity Head	0.00 m
Ke	0.70	Entrance Loss	0.00 m

Inlet Control Properties			
Inlet Control HW Elev.	419.69 m	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	1.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-14 - Future Conditions - Upgrade 1800 x 900 Box (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	426.55 m	Headwater Depth/Height	0.15
Computed Headwater Elev:	419.74 m	Discharge	0.0530 m ³ /s
Inlet Control HW Elev.	419.74 m	Tailwater Elevation	419.74 m
Outlet Control HW Elev.	419.74 m	Control Type	Outlet Control

Grades			
Upstream Invert	419.61 m	Downstream Invert	419.09 m
Length	22.20 m	Constructed Slope	0.023423 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.65 m
Slope Type	Steep	Normal Depth	0.03 m
Flow Regime	Subcritical	Critical Depth	0.04 m
Velocity Downstream	0.04 m/s	Critical Slope	0.008543 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1830 x 910 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	419.74 m	Upstream Velocity Head	0.00 m
Ke	0.70	Entrance Loss	0.00 m

Inlet Control Properties			
Inlet Control HW Elev.	419.74 m	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	1.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-14 - Future Conditions - Upgrade 1800 x 900 Box (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	426.25 m	Headwater Depth/Height	0.20
Computed Headwater Elev:	419.79 m	Discharge	0.0630 m ³ /s
Inlet Control HW Elev.	419.79 m	Tailwater Elevation	419.79 m
Outlet Control HW Elev.	419.79 m	Control Type	Outlet Control

Grades			
Upstream Invert	419.61 m	Downstream Invert	419.09 m
Length	22.20 m	Constructed Slope	0.023423 m/m

Hydraulic Profile			
Profile	S1	Depth, Downstream	0.70 m
Slope Type	Steep	Normal Depth	0.04 m
Flow Regime	Subcritical	Critical Depth	0.05 m
Velocity Downstream	0.05 m/s	Critical Slope	0.008283 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	1.83 m
Section Size	1830 x 910 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	419.79 m	Upstream Velocity Head	0.00 m
Ke	0.70	Entrance Loss	0.00 m

Inlet Control Properties			
Inlet Control HW Elev.	419.79 m	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	1.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-15 - Future Conditions - Upgrade 1x600

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	418.53 m	Headwater Depth/Height	0.90
Computed Headwater Elev:	417.37 m	Discharge	0.2490 m ³ /s
Inlet Control HW Elev.	417.33 m	Tailwater Elevation	417.06 m
Outlet Control HW Elev.	417.37 m	Control Type	Outlet Control

Grades			
Upstream Invert	416.82 m	Downstream Invert	416.60 m
Length	18.20 m	Constructed Slope	0.012088 m/m

Hydraulic Profile			
Profile	M1	Depth, Downstream	0.46 m
Slope Type	Mild	Normal Depth	0.36 m
Flow Regime	Subcritical	Critical Depth	0.32 m
Velocity Downstream	1.05 m/s	Critical Slope	0.017056 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.61 m
Section Size	600 mm	Rise	0.61 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	417.37 m	Upstream Velocity Head	0.10 m
Ke	0.90	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	417.33 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.3 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-16 - Future Conditions - Upgrade 3000 x 1219 Box (025 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	410.77 m	Headwater Depth/Height	0.35
Computed Headwater Elev:	410.72 m	Discharge	1.0370 m ³ /s
Inlet Control HW Elev.	410.66 m	Tailwater Elevation	410.54 m
Outlet Control HW Elev.	410.72 m	Control Type	Entrance Control

Grades			
Upstream Invert	410.30 m	Downstream Invert	409.82 m
Length	14.90 m	Constructed Slope	0.032215 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.72 m
Slope Type	Steep	Normal Depth	0.13 m
Flow Regime	N/A	Critical Depth	0.23 m
Velocity Downstream	0.47 m/s	Critical Slope	0.005588 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	410.72 m	Upstream Velocity Head	0.11 m
Ke	0.70	Entrance Loss	0.08 m

Inlet Control Properties			
Inlet Control HW Elev.	410.66 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-16 - Future Conditions - Upgrade 3000 x1219 Box (100 yr)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	411.47 m	Headwater Depth/Height	0.40
Computed Headwater Elev:	410.79 m	Discharge	1.2820 m ³ /s
Inlet Control HW Elev.	410.72 m	Tailwater Elevation	410.56 m
Outlet Control HW Elev.	410.79 m	Control Type	Entrance Control

Grades			
Upstream Invert	410.30 m	Downstream Invert	409.82 m
Length	14.90 m	Constructed Slope	0.032215 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.76 m
Slope Type	Steep	Normal Depth	0.15 m
Flow Regime	N/A	Critical Depth	0.26 m
Velocity Downstream	0.55 m/s	Critical Slope	0.005472 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	410.79 m	Upstream Velocity Head	0.13 m
Ke	0.70	Entrance Loss	0.09 m

Inlet Control Properties			
Inlet Control HW Elev.	410.72 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-16 - Future Conditions - Upgrade 3000 x1219 Box (Regional)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	411.47 m	Headwater Depth/Height	0.75
Computed Headwater Elev:	411.22 m	Discharge	3.3310 m ³ /s
Inlet Control HW Elev.	411.12 m	Tailwater Elevation	410.68 m
Outlet Control HW Elev.	411.22 m	Control Type	Entrance Control

Grades			
Upstream Invert	410.30 m	Downstream Invert	409.82 m
Length	14.90 m	Constructed Slope	0.032215 m/m

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	0.86 m
Slope Type	Steep	Normal Depth	0.27 m
Flow Regime	N/A	Critical Depth	0.50 m
Velocity Downstream	1.27 m/s	Critical Slope	0.005213 m/m

Section			
Section Shape	Box	Mannings Coefficient	0.017
Section Material	Concrete	Span	3.05 m
Section Size	3050 x 1220 mm	Rise	1.22 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	411.22 m	Upstream Velocity Head	0.25 m
Ke	0.70	Entrance Loss	0.17 m

Inlet Control Properties			
Inlet Control HW Elev.	411.12 m	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	3.7 m ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

WCB-17 - Future Conditions - Maintain Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	410.15 m	Headwater Depth/Height	1.36
Computed Headwater Elev:	409.69 m	Discharge	1.1570 m ³ /s
Inlet Control HW Elev.	409.56 m	Tailwater Elevation	409.18 m
Outlet Control HW Elev.	409.69 m	Control Type	Outlet Control

Grades			
Upstream Invert	408.45 m	Downstream Invert	408.41 m
Length	15.00 m	Constructed Slope	0.002667 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.77 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.63 m
Velocity Downstream	1.96 m/s	Critical Slope	0.018669 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	409.69 m	Upstream Velocity Head	0.16 m
Ke	0.90	Entrance Loss	0.14 m

Inlet Control Properties			
Inlet Control HW Elev.	409.56 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Culvert Calculator Report

WCB-18 - Future Conditions - Maintain Existing

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	392.97 m	Headwater Depth/Height	2.34
Computed Headwater Elev:	392.07 m	Discharge	1.7330 m ³ /s
Inlet Control HW Elev.	391.69 m	Tailwater Elevation	390.71 m
Outlet Control HW Elev.	392.07 m	Control Type	Outlet Control

Grades			
Upstream Invert	389.93 m	Downstream Invert	389.88 m
Length	23.00 m	Constructed Slope	0.002174 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.83 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.77 m
Velocity Downstream	2.77 m/s	Critical Slope	0.027475 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.91 m
Section Size	900 mm	Rise	0.91 m
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	392.07 m	Upstream Velocity Head	0.36 m
Ke	0.90	Entrance Loss	0.32 m

Inlet Control Properties			
Inlet Control HW Elev.	391.69 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.7 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Appendix E.2.
CulvertMaster Summary Table
(Future Conditions)

Culvert No.	Road	Station	Peak Design Flow Calculations			CulvertMaster Calculations															Recommendations				
			Watershed Time of Concentration	Design Storm	Rainfall Intensity	Peak Design Flow	Material	Shape	Size / Diameter		Length	Depth of Fill	Flow Direction	U/S Invert	D/S Invert	Slope	Proposed Edge of Pavement Elevation	Minimum Freeboard	Minimum Clearance	Maximum Allowable Headwater Elevation		Calculated Headwater Elevation	Delta Headwater	Theoretical/Calculated Tailwater Elevation	Critical Depth
			Tc (min)	(years)	I (mm/hr)	Q (m ³ /s)			Span (mm)	Rise (mm)	(m)	(m)		(m)	(m)	(%)	(m)	(m)	(m)	(m)		(m)	(m)	(m)	(m)
OBL-01	Olde Base Line Road	30+030	60.25	25	48.69	0.479	CSP	Circular		600	12.5	0.29	N-S	372.4	372.25	1.200	373.295	0.3	0	373.00	372.93	0.06	372.71	0.32	Upgrade to Twin 600 (existing 1 x 450)
OBL-02	Olde Base Line Road	30+540	86.25	25	37.43	1.8	RCB	Box	3000	1200	14.3	0.28	N-S	372.71	372.70	0.070	374.190	1.0	0.3	373.19	373.53	-0.34	373.47	0.33	Upgrade to 3000 x 1200 Box Open Bottom / watercourse (existing 600 CSP)
				100	46.33	2.229	RCB	Box	3000	1200	14.3	0.28		372.71	372.70	0.070	374.190	0.0	0.3	374.19	373.57	0.62	373.49	0.38	
				Regional	N/A	5.233 (See Note 1)	RCB	Box	3000	1200	14.3	0.28		372.71	372.70	0.070	374.190	0.0	0.3	374.19	373.95	0.24	373.64	0.67	
OBL-03	Olde Base Line Road	30+715	62.46	25	47.45	0.49	CSP	Circular		600	15.9	3.12	N-S	369.16	369.09	0.440	372.877	0.3	0	372.58	370.23	2.35	369.62	0.46	Maintain existing culvert
OBL-04	Olde Base Line Road	30+940	103.9	25	N/A	3.69 (See Note 1)	RCB	Box	3300	1200	23.1	0.68	N-S	369.35	369.25	0.433	371.230	1.0	0.3	370.23	370.3	-0.07	370.10	0.5	Maintain existing culvert (3300 x 1200) (Watercourse)
				100	N/A	5.41 (See Note 1)	RCB	Box	3300	1200	23.1			369.35	369.25	0.433	371.230	0.0	0.3	371.23	370.52	0.71	370.18	0.65	
				Regional	N/A	14.78 (See Note 1)	RCB	Box	3300	1200	23.1			369.35	369.25	0.433	371.230	0.0	0.3	371.23	372.26	-1.03	370.45	1.2	
OBL-05	Olde Base Line Road	31+280	59.32	25	49.24	0.22	CSP	Circular		600	12.5	0.31	N-S	371.80	371.62	1.464	372.707	0.3	0	372.41	372.31	0.10	372.07	0.3	Upgrade to 600 (existing 450)
OBL-06	Olde Base Line Road	31+300	82.51	25	38.69	0.111	HDPE	Circular		450	20.5	0.06	N-S	371.91	371.56	1.712	372.426	0.3	0	372.13	372.14	-0.01	371.87	0.16	Upgrade to Twin 450 (existing 450)
OBL-07	Olde Base Line Road	31+380	41.99	25	62.66	0.049	HDPE	Circular		450	12	0.49	N-S	370.92	370.73	1.558	371.864	0.3	0	371.56	371.14	0.42	371.03	0.15	Maintain exiting culvert
OBL-08	Olde Base Line Road	31+410	171.04	25	N/A	8.65 (See Note 1)	RCB	Box	3050	1400	26.6	0.45	N-S	370.22	370.19	0.102	372.070	1.0	0.3	371.07	371.9	-0.83	371.36	0.94	Maintain existing culvert (3050 x 1400) (Watercourse)
				100	N/A	12.73 (See Note 1)	RCB	Box	3050	1400	26.6	0.45		370.22	370.19	0.102	372.070	0.0	0.3	372.07	371.51	0.56	371.50	1.21	
				Regional	N/A	46.8 (See Note 1)	RCB	Box	3050	1400	26.6	0.45		370.22	370.19	0.102	372.070	0.0	0.3	372.07	385.56	-13.49	371.65	1.52	
OBL-09	Olde Base Line Road	32+080	29.97	25	78.15	0.244	CSP	Circular		600	10.5	1.45	S-N	372.54	372.48	0.533	374.593	0.3	0	374.29	373.11	1.18	372.94	0.32	Upgrade to 600 (existing 400)
OBL-10	Olde Base Line Road	32+230	25.38	25	86.60	0.094	CSP	Circular		600	12.35	0.57	N-S	373.56	373.42	1.190	374.731	0.3	0	374.43	373.89	0.54	373.81	0.19	Upgrade to 600 (existing 400)
OBL-11	Olde Base Line Road	32+340	83.97	25	38.19	0.892	CSP	Circular		600	12.3	0.27	N-S	373.24	372.91	2.675	374.113	0.3	0	373.81	374.06	-0.25	373.43	0.44	Upgrade to Twin 600 (existing 400)

Note 1: Peak flow determined from SWMHYMO Model

Culvert No.	Road	Station	Peak Design Flow Calculations			Peak Design Flow Q (m ³ /s)	Material	Shape	Size / Diameter		Length (m)	Depth of Fill (m)	Flow Direction	U/S Invert (m)	D/S Invert (m)	Slope (%)	Proposed Edge of Pavement Elevation (m)	Minimum Freeboard (m)	Minimum Clearance (m)	Maximum Allowable Headwater Elevation (m)	CulvertMaster Calculations				Recommendations
			Watershed Time of Concentration Tc (min)	Design Storm (years)	Rainfall Intensity I (mm/hr)				Span (mm)	Rise (mm)											Calculated Headwater Elevation (m)	Delta Headwater (m)	Theoretical/Calculated Tailwater Elevation (m)	Critical Depth (m)	
WCB-01	Winston Churchill Boulevard	40+030	47.76	25	57.36	0.045	CSP	Circular		0.25	13.5	0.30	E-W	372.44	372.15	2.148	372.741	0.3	0	372.44	372.65	-0.21	372.21	0.12	Remove existing culverts and replace with DICB and sewer.
WCB-02	Winston Churchill Boulevard	40+480	43.35	25	61.31	0.154	CSP	Circular		400	12.2	0.22	E-W	381.34	381.15	1.541	381.961	0.3	0	381.66	381.68	-0.02	381.45	0.2	Upgrade to Twin 400 (existing 400)
WCB-03	Winston Churchill Boulevard	40+660	53.81	25	52.78	0.134	CSP	Circular		400	12.1	0.36	E-W	382.82	382.79	0.207	383.582	0.3	0	383.28	383.17	0.11	383.08	0.18	Upgrade to Twin 400 (existing 400)
WCB-04	Winston Churchill Boulevard	40+870	34.69	25	71.15	0.084	CSP	Circular		600	13.75	0.24	W-E	385.21	384.85	2.582	386.049	0.3	0	385.75	385.52	0.23	385.24	0.18	Upgrade to 600 (existing 400)
WCB-05	Winston Churchill Boulevard	41+110	28.07	25	81.41	0.051	CSP	Circular		600	12.8	0.82	E-W	392.33	392.28	0.406	393.748	0.3	0	393.45	392.67	0.78	392.65	0.14	Upgrade to 600 (existing 400)
WCB-06	Winston Churchill Boulevard	41+400	55.21	25	51.83	0.396	RCB	Box	1829	610	11	0.17	E-W	393.03	392.96	0.700	393.814	1.0	0.3	392.81	393.39	-0.58	393.35	0.17	Upgrade to 1800 x 610 Box Open Bottom (existing 600 CSP)
				100	64.10	0.49	RCB	Box	1829	610	11	0.17	E-W	393.03	392.96	0.700	393.814	0.0	0.3	393.81	393.43	0.38	393.36	0.19	
				Regional	N/A	1.248 (See Note 1)	RCB	Box	1829	610	11	0.17	E-W	393.03	392.96	0.700	393.814	0.0	0.3	393.81	393.68	0.13	393.44	0.36	
WCB-07	Winston Churchill Boulevard	41+710	39.12	25	65.71	0.63	CSP	Circular		700	12.35	0.65	E-W	393.07	392.94	1.061	394.418	0.3	0	394.12	394.00	0.12	393.54	0.5	Upgrade to 700 (existing 400)
WCB-08	Winston Churchill Boulevard	41+890	26.4	25	84.55	0.556	HDPE	Circular		600	13.6	0.79	E-W	394.27	394.00	1.985	395.662	0.3	0	395.36	395.07	0.29	394.55	0.49	Maintain Existing
WCB-09	Winston Churchill Boulevard	42+195	76.9	25	40.76	2.224	RCB	Box	6000	1524	15.5	0.64	E-W	399.91	399.85	0.387	402.075	1.0	0.3	401.08	400.75	0.32	400.73	0.24	Upgrade to 6000 x 1500 Box Open Bottom (existing 1400x900 arch)
				100	50.46	2.753	RCB	Box	6000	1524	15.5	0.64	E-W	399.91	399.85	0.387	402.075	0.0	0.3	402.08	400.89	1.19	400.75	0.28	
				Regional	N/A	7.504 (See Note 1)	RCB	Box	6000	1524	15.5	0.64	E-W	399.91	399.85	0.387	402.075	0.0	0.3	402.08	400.94	1.13	400.88	0.54	
WCB-10	Winston Churchill Boulevard	42+750	23.15	25	91.48	0.191	CSP	Circular		600	12.7	0.43	E-W	417.62	417.38	1.890	418.649	0.3	0	418.35	418.11	0.24	417.82	0.28	Upgrade to 600 (existing 400)
WCB-11	Winston Churchill Boulevard	43+130	26.28	25	84.78	0.069	CSP	Circular		600	15.5	1.71	W-E	425.25	425.17	0.516	427.557	0.3	0	427.26	425.59	1.67	425.56	0.17	Upgrade to 600 (existing 400)
WCB-12	Winston Churchill Boulevard	43+210	41.18	25	62.47	0.175	CSP	Circular		600	18.2	1.72	W-E	424.86	424.42	2.418	427.182	0.3	0	426.88	425.32	1.56	424.86	0.27	Maintain Existing
WCB-13	Winston Churchill Boulevard	44+140	0	25	-	Equalization Culvert	CSP	Circular		600	16	1.18	W-E	424.69	424.55	0.875	426.474	0.3	0	426.17	Equalization Culvert		424.85		Upgrade to 600 (existing 400)
WCB-14	Winston Churchill Boulevard	44+310	18.87	25	54.32	0.023	CSP	Circular	1800	900	22.2	6.04	E-W	419.61	419.09	2.360	426.549	1	0	425.55	419.69	5.86	419.69	0.3	Upgrade to 1800 x 900 Box Open Bottom (existing 450)
				100	125.95	0.053	RCB	Circular	1800	900	22.2	6.04	E-W	419.61	419.09	2.360	426.549	0	0	426.55	419.74	6.81	419.74	0.4	
				Regional	N/A	0.063 (See Note 1)	RCB	Circular	1800	900	22.2	6.04	E-W	419.61	419.09	2.360	426.549	0	0	426.55	419.79	6.76	419.79	0.5	
WCB-15	Winston Churchill Boulevard	44+615	30.82	25	76.77	0.249	CSP	Circular		600	18.2	1.41	E-W	416.82	416.60	1.221	418.829	0.3	0	418.53	417.37	1.16	417.06	0.32	Upgrade to 600 (existing 450)
WCB-16			57.82	25	50.15	1.037	RCB	Box	3000	1219	14.9	0.25	W-E	410.30	409.82	3.255	411.773	1	0	410.77	410.72	0.05	410.54	0.23	Upgrade to 1800 x 1200 Box Open Bottom (existing 750 CSP)
				100	62.04	1.282	RCB	Box	3000	1219	14.9	0.25	W-E	410.30	409.82	3.255	411.773	0	0	411.77	410.79	0.98	410.56	0.26	
				Regional	N/A	3.331 (See Note 1)	RCB	Box	3000	1219	14.9	0.25	W-E	410.30	409.82	3.255	411.773	0	0	411.77	411.22	0.55	410.68	0.50	
WCB-17	Winston Churchill Boulevard	45+095	87.14	25	37.14	1.157	CSP	Circular		900	15	1.10	E-W	408.45	408.41	0.267	410.449	0.3	0	410.15	409.69	0.46	409.18	0.63	Maintain Existing
WCB-18	Winston Churchill Boulevard	45+865	80.72	25	39.33	1.733	CSP	Circular		900	23	2.43	E-W	389.93	389.88	0.257	393.268	0.3	0	392.97	392.07	0.90	390.71	0.77	Maintian Existing

Note 1: Peak flow determined from SWMHYMO Model



HDR

Appendix R.3
Stormwater Management Report



Region of Peel

Stormwater Management Report

Mississauga Road / Old Main Street, Bush Street, Olde Base Line Road and
Winston Churchill Boulevard, Town of Caledon, Region of Peel

Submitted by:
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May 2014



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1. INTRODUCTION

The Regional Municipality of Peel (the Region) is conducting a Schedule “C” Municipal Class Environmental Assessment (EA) to provide a comprehensive and environmentally sound Transportation and Road Infrastructure Improvement Plan using a Context Sensitive Solutions Approach for the following Regional Road corridors:

- Winston Churchill Boulevard (Peel Regional Road 19, Wellington County Road 25) – from Olde Base Line Road to Bush Street;
- Olde Base Line Road (Regional Road 12) – from Winston Churchill Boulevard to Mississauga Road;
- Mississauga Road and Old Main Street (Regional Road 1) – from Olde Base Line Road to Bush Street; and
- Bush Street (Regional Road 11) – from Mississauga Road / Old Main Street to Winston Churchill Boulevard;

The approximate limits of the Study Area are shown in **Exhibit 1-1**.

Subsequent to the *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft, June 2010* prepared by Dillon Consulting Limited and the *Drainage and Hydrology Report, Olde Baseline Road and Winston Churchill Boulevard, Town of Caledon, Region of Peel, Draft January 2014* prepared by HDR Corporation, this report was prepared to document the Stormwater Management strategy proposed for the improvements to the four corridors noted above.

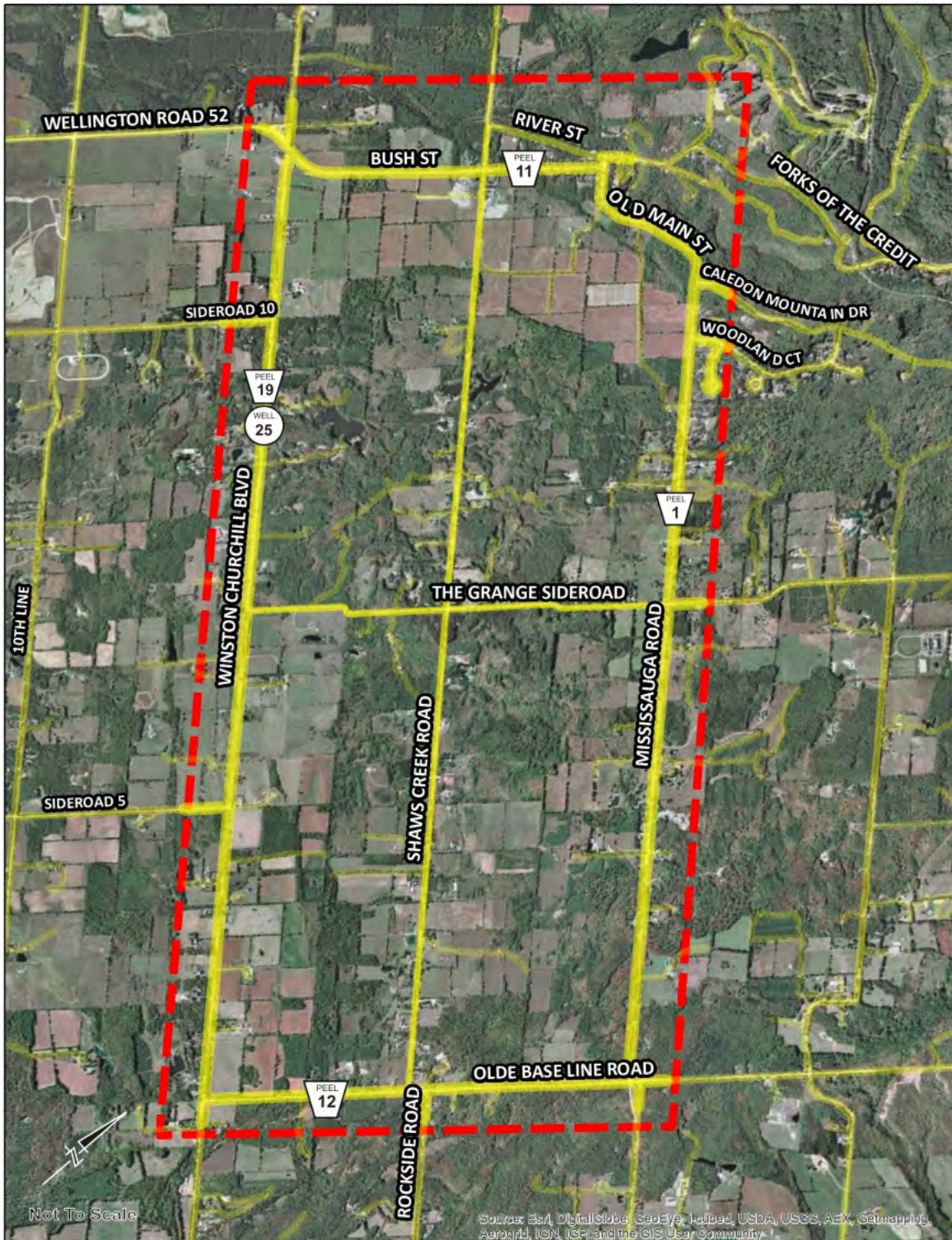


Exhibit 1-1: Study Area

and 0.5 m rounding on each side of the road (illustrated in **Exhibit 1-3**). Drainage is addressed through ditches with 2:1 slopes on either side. This cross-section connects to a rural cross-section at Bush Street.

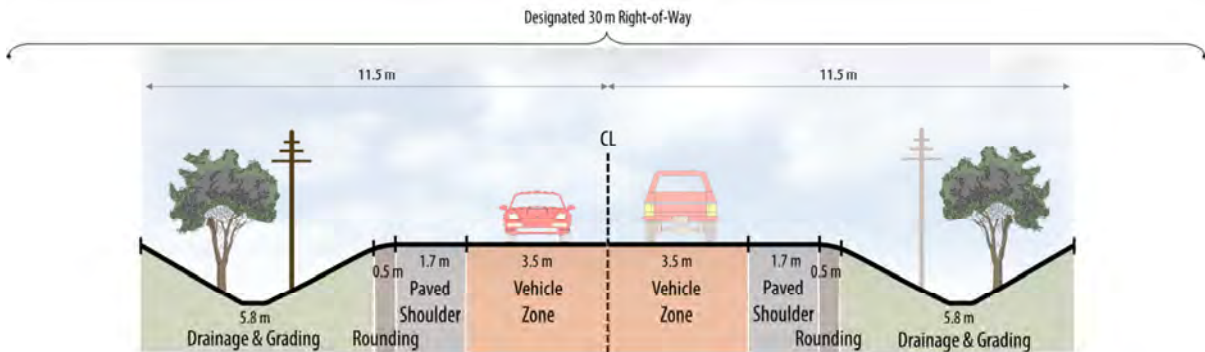


Exhibit 1-3: 11.4 m Platform Rural Cross-Section for Winston Churchill Boulevard

The proposed vertical alignment accommodates a 70 km/h design speed. This vertical alignment was chosen to match the existing road profile wherever possible, while at the same time improving any existing substandard grades and vertical curves to meet the geometric standards required for the class of the road. The vertical profile also aims to minimize impacts to existing entrances and driveways, and to reduce grading impacts to adjacent properties and features.

1.1.2 Olde Base Line Road

Due to the existing topography and constraints along the right-of-way, and to minimize grading impacts to adjacent properties and features, a semi-rural cross-section is proposed for the majority of the corridor, between Stations 30+000 (Winston Churchill Boulevard) and 30+945, and between 31+380 and 32+760 (Mississauga Road). This cross-section consists of one 3.5 m wide travel lane in each direction, with a 1.7 m wide paved shoulder to accommodate active transportation and a 0.5 m mountable curb on each side of the road (illustrated in **Exhibit 1-4**) 0.3 m rounding and a 2:1 slope then match to existing ground on either side of the road. Drainage is addressed through underground infrastructure. This cross-section connects to a semi-rural cross-section at Winston Churchill Boulevard and Mississauga Road.

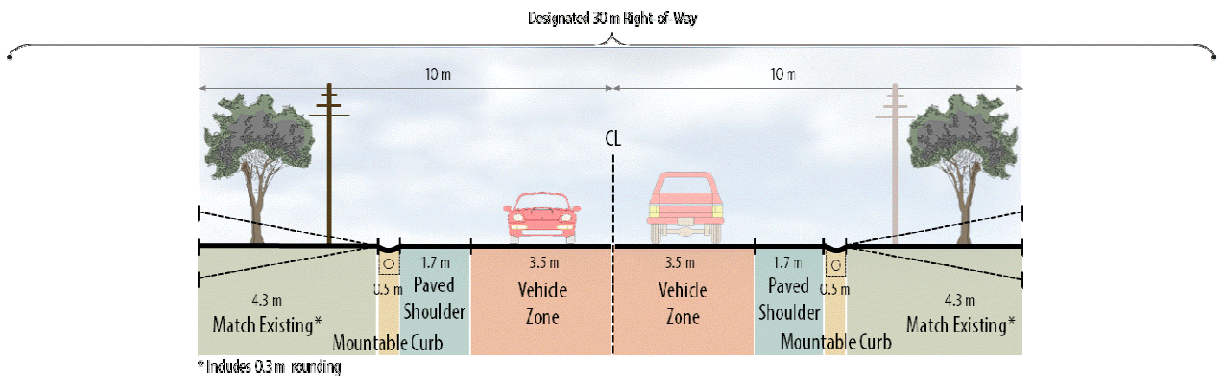


Exhibit 1-4: 11.4 m Platform Semi-Rural Cross-Section for Olde Base Line Road

Between Stations 30+945 and 31+380, a semi-rural cross-section was also considered for continuity, but due to the sensitive watercourse at this location where the design has the potential to address storm water management quality and improve flow conveyance, and where the wider right-of-way can accommodate more extensive grading, a rural cross-section is proposed. This cross-section consists of one 3.5 m wide travel lane in each direction, with a 1.7 m wide paved shoulder and 0.5 m rounding on each side of the road (illustrated in **Exhibit 1-5**). Drainage is addressed through ditches with 2:1 slopes on either side.

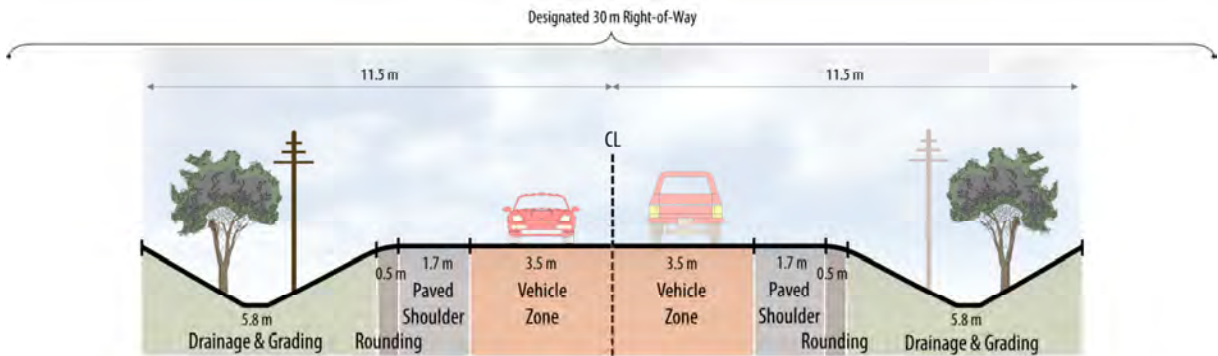


Exhibit 1-5: 11.4 m Platform Rural Cross-Section for Olde Base Line Road

The proposed vertical alignment accommodates a 60 km/h design speed. This vertical alignment was chosen to match the existing road profile wherever possible, while at the same time improving any existing substandard grades and vertical curves to meet the geometric standards required for the class of the road. The vertical profile also aims to minimize impacts to existing entrances and driveways, and to reduce grading impacts to adjacent properties and features.

1.1.3 Mississauga Road / Old Main Street

Due to the existing topography and constraints along the narrow right-of-way, and to minimize grading impacts to adjacent properties and features, a semi-rural cross-section is proposed for the entire length of the corridor, between Olde Base Line Road and approximately 580 m north/west of Caledon Mountain Drive. This cross-section consists of one 3.5 m wide travel lane in each direction, with a 1.7 m wide paved shoulder to accommodate active transportation and a 0.5 m mountable curb on each side of the road (illustrated in **Exhibit 1-6**). 0.3 m rounding and a 2:1 slope then match to existing ground on either side of the road. Drainage is addressed through underground infrastructure. This cross-section connects to a semi-rural cross-section at Olde Base Line Road, and transitions into a semi-rural cross-section through the Belfountain Village.

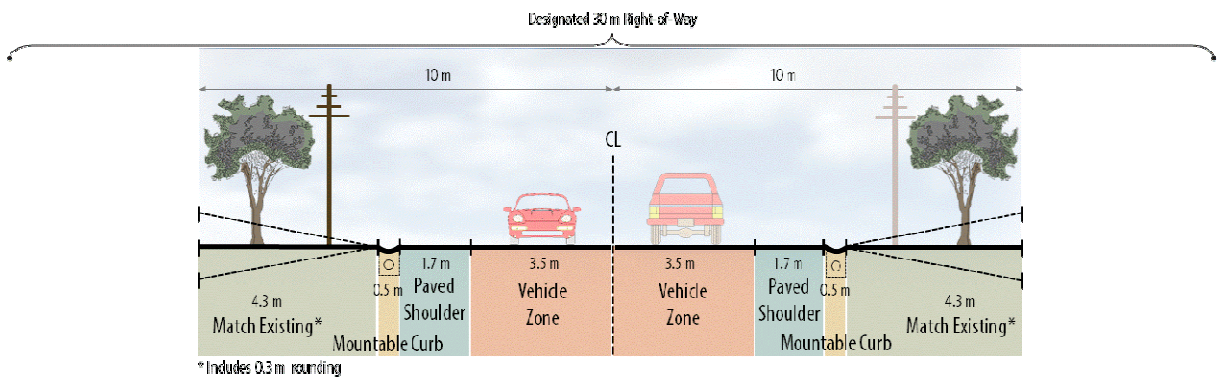


Exhibit 1-6: 11.4 m Platform Semi-Rural Cross-Section for Mississauga Rd. / Old Main St.

The proposed vertical alignment accommodates a 60-70 km/h design speed. Between Olde Base Line Road and approximately 250 m north of Caledon Mountain Drive, the proposed design follows a 70 km/h design speed. North/west of this location, towards the village, the design follows a 60 km/h design speed to accommodate the existing 50 km/h posted speed limit. This vertical alignment was chosen to match the existing road profile wherever possible, while at the same time improving any existing substandard grades and vertical curves to meet the geometric standards required for the class of the road. The vertical profile also aims to minimize impacts to existing entrances and driveways, and to reduce grading impacts to adjacent properties and features.

1.1.4 Belfountain Village

Due to a narrow and highly constrained right-of-way, and to minimize grading impacts to adjacent properties and features, a semi-rural cross-section is proposed through the Belfountain Village, with different cross-section variations for different segments.

On Bush Street, the proposed cross-section consists of one 3.3 m wide travel lane in each direction, with a 0.5 m mountable curb on each side of the road and a 1.7 m wide sidewalk on

the south side to connect to the Belfountain Elementary School on Shaws Creek Road south of Bush. This cross-section is illustrated in **Exhibit 1-7**. A 0.3 m rounding and a 2:1 slope then match to existing ground on either side of the road, although extensive grading is not required. Drainage is addressed through underground infrastructure. For consistency, this cross-section will start at Shaws Creek Road (just west of the Belfountain Village study limits) and end at Mississauga Road / Old Main Street, where it connects to another semi-rural cross-section.

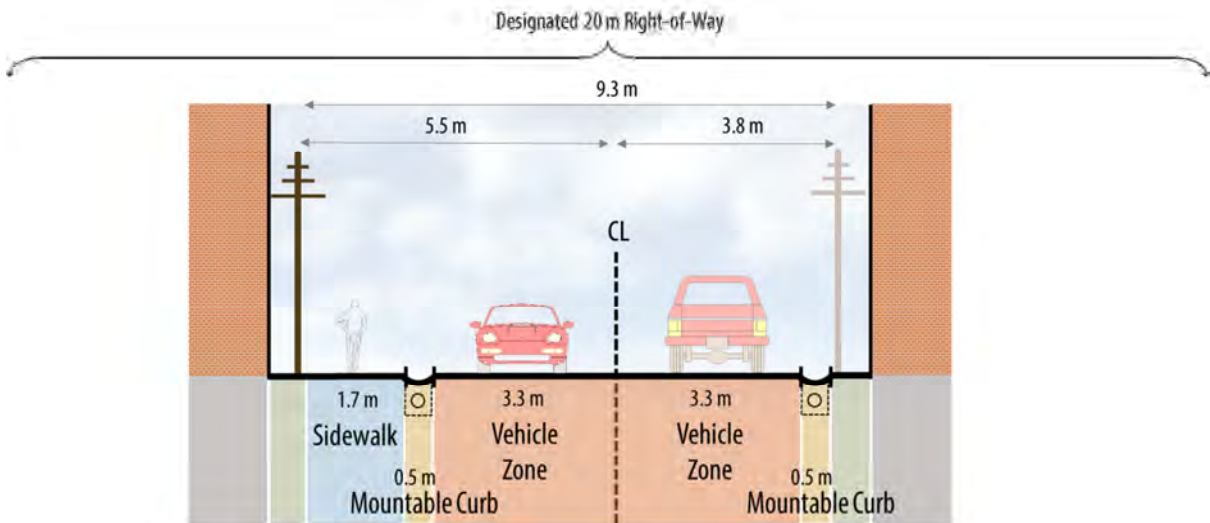


Exhibit 1-7: 9.3 m Platform Semi-Rural Cross-Section with Sidewalk for Belfountain Village (Shaws Creek Rd. to Mississauga Rd. / Old Main St.)

Between Bush Street and the Belfountain Community Centre, the proposed cross-section consists of one 3.3 m wide travel lane in each direction, with 2.4 m wide on-street parking on the east side and a 0.5 m mountable curb on each side of the road. A 1.7 m wide sidewalk on the west side connects to the sidewalk on the south side of Bush Street. This cross-section is illustrated in **Exhibit 1-8**. A 0.3 m rounding and a 2:1 slope then match to existing ground on either side of the road, although extensive grading is not required. Drainage is addressed through underground infrastructure. This cross-section connects to another semi-rural cross-section east of the Community Centre.

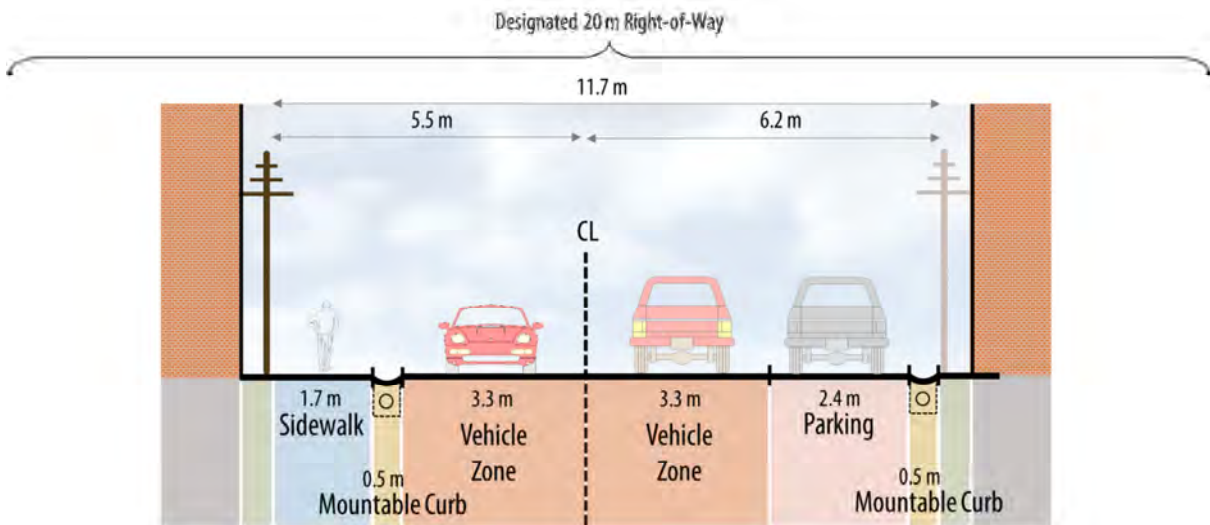


Exhibit 1-8: 11.7 m Platform Semi-Rural Cross-Section with Sidewalk and Parking for Belfountain Village (Bush St. to Community Centre)

Between the Belfountain Community Centre and north/west of Caledon Mountain Drive, the proposed cross-section consists of one 3.3 m wide travel lane in each direction, with a 1.7 m wide paved shoulder on the south side and a 0.5 m mountable curb on each side of the road. This cross-section is illustrated in **Exhibit 1-9**. A 0.3 m rounding and a 2:1 slope then match to existing ground on either side of the road, although extensive grading is not required. Drainage is addressed through underground infrastructure.

At the pinch point just east of the Community Centre, where the right-of-way is highly constrained by a retaining wall / guiderail on the north side, and buildings, fences and other features on the south side, the paved shoulder width is proposed to be reduced as required to minimize impacts. East of the pinch point, where the right-of-way is less constrained, it is proposed to introduce a paved shoulder on the north side as well and widen the travel lanes to 3.5 m to transition to a cross-section consistent to that proposed south of Caledon Mountain Drive.

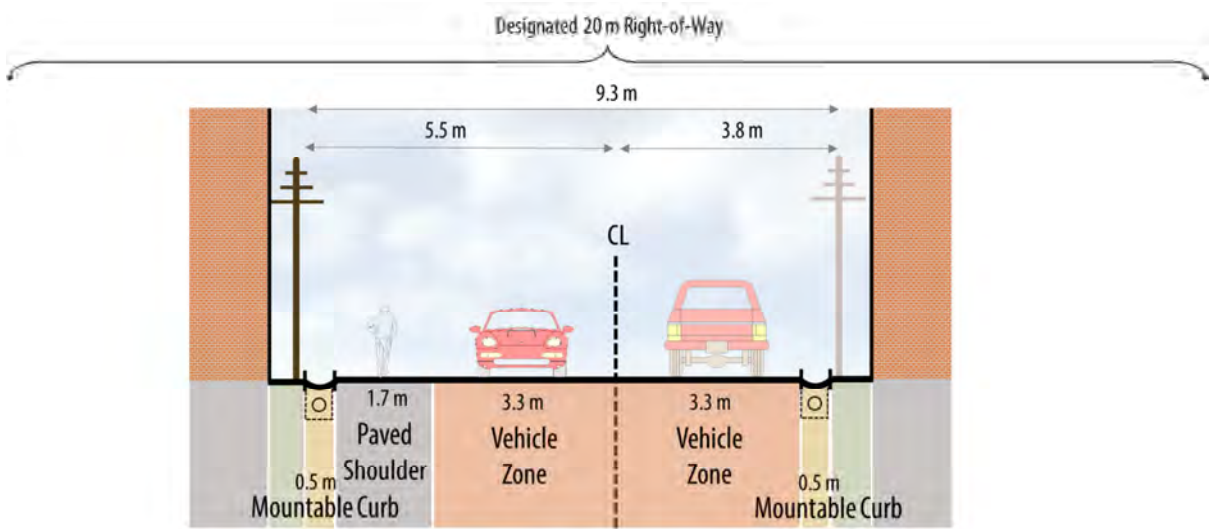


Exhibit 1-9: 9.3 m Platform Semi-Rural Cross-Section with Paved Shoulder for Belfountain Village (Community Centre to north/west of Caledon Mountain Drive)

The proposed horizontal alignment generally follows the existing road centreline with the exception of a slight realignment to the north between Stations 11+975 and 12+100 to minimize impacts and avoid property acquisition on the south side.

Due to the narrow and highly constrained right-of-way through Belfountain Village and the low proposed posted speed limit, the proposed design generally follows the existing road profile and accommodates a 50km/h design speed. The proposed vertical profile aims to minimize impacts to existing entrances and driveways, and to reduce grading impacts to adjacent properties and features. This vertical alignment was chosen to match the existing road profile wherever possible, while at the same time improving any existing substandard grades and vertical curves to meet the geometric standards required for the class of the road to the extent possible.

1.1.5 Bush Street

Due to a wider available right-of-way along Bush Street, a rural cross-section can be accommodated and is therefore proposed for the majority of the corridor, between Stations 10+000 (Winston Churchill Boulevard) and 11+125, and between Stations 11+220 and 11+365 (Shaws Creek Road). This cross-section consists of one 3.5 m wide travel lane in each direction, with a 1.7 m wide paved shoulder to accommodate active transportation and 0.5 m rounding on each side of the road (refer to **Exhibit 1-10**). Drainage is addressed through ditches with 2:1 slopes on either side. This cross-section connects to a rural cross-section at Winston Churchill Boulevard.

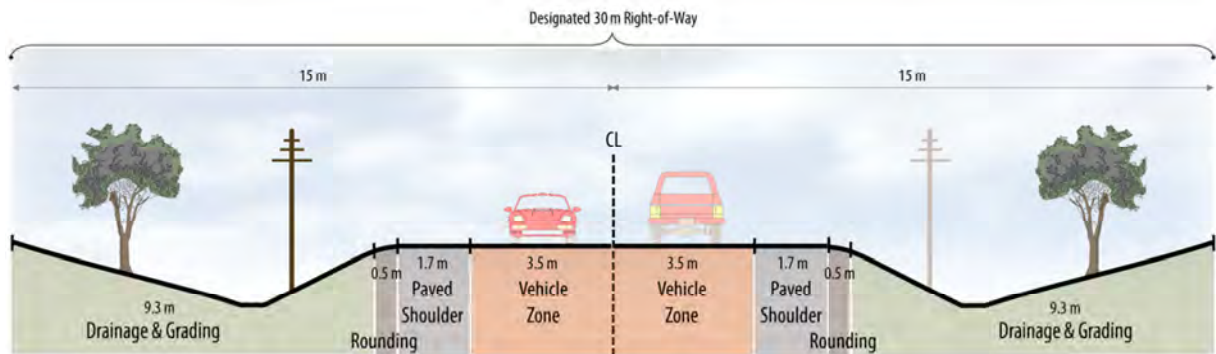


Exhibit 1-10: 11.4 m Platform Rural Cross-Section for Bush Street

Between Stations 11+125 and 11+220, where there is a steep slope and an existing guiderail on either side of the road, the proposed design will match to existing conditions. The road platform (including one 3.5 m travel lane in each direction and 1.7 m paved shoulder on each side of the road) will fit between the existing guiderails, and drainage will follow existing conditions, with water flowing down the steep slopes on either side of the road. No mountable curb is proposed through this segment.

East of Shaws Creek, a transition to a semi-rural cross-section is proposed for continuity with the cross-section through the Belfountain Village.

The proposed vertical alignment accommodates a 60-80 km/h design speed. Between Winston Churchill Boulevard and Shaws Creek Road, the proposed design follows an 80 km/h design speed. East of Shaws Creek Road, towards the village, the design follows a 60 km/h design speed to accommodate the existing 50 km/h posted speed limit. This vertical alignment was chosen to match the existing road profile wherever possible, while at the same time improving any existing substandard grades and vertical curves to meet the geometric standards required for the class of the road. The vertical profile also aims to minimize impacts to existing entrances and driveways, and to reduce grading impacts to adjacent properties and features.

1.2 Objectives of Drainage and Stormwater Management Study

The purpose of this Stormwater Management Report was to develop a stormwater management plan for the Mississauga Road, Old Main Street, Bush Street, Olde Base Line Road, and Winston Churchill Boulevard Class EA project that will address both water quantity and quality issues. In essence, the Stormwater Management Report was carried out with the view of minimizing the potential impacts of the proposed road widening on the natural environment, while ensuring an adequate roadway drainage system is incorporated as part of the overall improvements.

The objectives of the Drainage and Stormwater Management Report are to develop a strategy for the project that will:

- Identify potential stormwater runoff quality and quantity impacts to the receiving watercourses from the increased pavement area in comparison with the existing condition;
- Address concerns from the review agencies including the Credit Valley Conservation Authority (CVC), Ministry of Natural Resources (MNR), as well as the development community, and any public interest groups; and
- Propose an appropriate pavement drainage system for roadway operation and safety.

2. BACKGROUND INFORMATION

The following information was also reviewed in the preparation of the report:

1. *Belfountain Transportation Corridor Class Environmental Assessment Study, Peel Region - Natural Heritage Report – Existing Conditions and Natural Feature Constraints, August 2013* prepared by Natural Resource Solutions Inc.
2. *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft, June 2010* prepared by Dillon Consulting Limited.
3. *Drainage and Hydrology Report, Olde Baseline Road and Winston Churchill Boulevard, Town of Caledon, Region of Peel, Draft January 2014* prepared by HDR Corporation.
4. Preferred Design Drawings (Plan and Profile) dated February 21, 2014;

2.1 Land Use

The study area is part of the Greenbelt Plan Area and includes part of the Niagara Escarpment Plan Area. The existing land use in the vicinity of the study area is primarily agricultural and rural residential.

2.2 Soils

Based on the Soil Map of Peel County (Soil Survey Report No. 18, November 1955), the majority of the lands within the study area consist of Dumfries loam, Caledon loam or Farmington loam.

2.3 Watershed Descriptions

The study area is located in the Credit River watershed and specifically within the West Credit River subwatershed and the Cheltenham to Glen Williams subwatershed.

2.3.1 West Credit Subwatershed

Two unnamed tributaries, identified as A and B in this report are found within the study area which are part of the West Credit subwatershed. The two unnamed tributaries drain into the west branch of the Credit River, near Belfountain, upstream of the Forks of the Credit. Tributary A is a headwater tributary which flows north under Bush Street and connects to the west branch of the Credit River less than 150 m to the west of the study area. The origin of flow for this feature is located outside of the study area and is formed through groundwater seepages and runoff. Tributary B is located within Belfountain and drains under Old Main

Street into the Credit River to the north of the study area. This feature has a steep gradient and carries surface runoff from the neighbouring areas to the west branch of the Credit River.

2.3.2 Cheltenham to Glen Williams Subwatershed

Three tributaries to the Credit River fall within the study area. These tributaries are Rogers Creek, Second Creek, and an Unnamed Tributary.

Second Creek

Second Creek and its unnamed tributaries cross the study area three times, twice along Mississauga Road (Tributaries A and B) and once along Olde Baseline Road (Tributary A). All of the unnamed tributaries, along with Second Creek itself, flow in a southwesterly direction through wetlands and numerous online ponds. The unnamed tributaries that cross the study area originate within wetlands to the north of Mississauga Road. Second Creek connects with the main branch of the Credit River approximately 6 km downstream of the culvert crossing along Olde Baseline Road.

Unnamed Tributary

The two tributaries to an unnamed watercourse cross under Mississauga Road near Olde Baseline Road. These tributaries flow in a southeasterly direction and converge upstream of a crossing of Olde Baseline Road, and subsequently drain into the unnamed watercourse approximately 120 m east of the study area. The crossings along Mississauga Road are all located within low lying wetland features. The culvert crossing along Olde Baseline Road appears to be a constructed drainage feature to carry surface runoff to the unnamed tributary. The unnamed tributary eventually drains into the main branch of the Credit River to the south of the study area.

Rogers Creek

Rogers Creek and its unnamed tributaries cross the study area three times. Tributary A to Rogers Creek crosses under Olde Baseline Road and flows in a southeasterly direction. This tributary originates upstream of the crossing location and is formed through agricultural runoff, online ponds, and potentially groundwater seepages. Tributary B to Rogers Creek also crosses under Olde Baseline Road and flows in a southeasterly direction. The tributary is a headwater feature and originates through agricultural runoff as well as groundwater features. The third tributary to Rogers Creek (Tributary C) crosses under Winston Churchill Boulevard and flows in a southeasterly direction. This feature flows through numerous wetland features before its confluence with Rogers Creek.

2.4 Designated Natural Areas

2.4.1 Provincially Significant Wetlands

Portions of two Provincially Significant Wetlands (PSW) complexes occur within the study area: the Eramosa River-Blue Spring Creek PSW Complex and the Caledon Mountain PSW Complex.

The Eramosa River-Blue Spring Creek PSW is located in the extreme south-western portion of the study area, adjacent to Winston Churchill Boulevard and west of The Grange Side Road.

The Caledon Mountain PSW is comprised of seven smaller wetlands, being predominantly swamp (95%), and a lesser extent marsh (5%). The PSW is important for whitetailed deer (*Odocoileus virginianus*) as well as for fish spawning and rearing, particularly for brook trout (*Salvelinus fontinalis*). The PSW lies within the east end of the study, along Winston Churchill Boulevard and Mississauga Road.

2.4.2 Life Science Areas of Natural and Scientific Interest

Two Life Science Areas of Natural and Scientific Interest (ANSIs) occur within the study area: the Caledon Mountain Slope Forest ANSI and the Credit Forks ANSI.

Caledon Mountain Slope Forest ANSI is a large tract of primarily deciduous forest, harbouring locally significant lands for mammals, predominantly white-tailed deer. The ANSI offers habitat for sizeable populations of amphibians, predominantly salamanders. The Caledon Mountain Slope Forest ANSI is located within the Caledon Mountain ESA (described below), and within the eastern end of the study area, adjacent to Olde Baseline Road.

The Credit Forks ANSI is comprised of 46 individual wetlands, and supports locally significant habitat for white-tailed deer, herpetofauna (specifically snapping turtle (*Chelydra serpentina*)), and supports potential waterfowl breeding and staging habitats. The ANSI is located in the northwestern portion of the study area, along Mississauga Road and Bush Street.

2.4.3 Environmentally Significant or Sensitive Areas

Three Environmentally Significant Areas (ESAs) occur within the study area: the Grange Woods ESA, Caledon Mountain ESA, and the Credit Forks – Devil's Pulpit ESA.

The Caledon Mountain ESA is within the Niagara Escarpment Plan Area and is also part of the Region of Peel Core Greenlands System (Region of Peel 2008). The Caledon Mountain ESA abuts the eastern end of the study area, along Olde Baseline Road.

The Credit Forks – Devil’s Pulpit ESA, located on the Niagara Escarpment, provides some of the most extensive and complimentary views of the escarpment. The Credit Forks – Devil’s Pulpit ESA is a major outlier valley feature, displaying rugged talus slopes. It is one of the most important regions for fish spawning and nursery habitat in the region, and supports a wide diversity of fish species. The Credit Forks – Devil’s Pulpit ESA is located peripherally on the extreme northwestern portion of the study area, along Mississauga Road and the Credit River.

The Grange Woods ESA is comprised of seven individual wetlands, largely comprised of swamp (96%), and to a lesser extent marsh (4%) habitat. Hydrologically, the Grange Woods ESA is connected by surface water to adjacent wetlands, up to 0.5 km away. The ESA provides valuable habitat to the flora and fauna of the region, and is locally significant as winter cover for wildlife, specifically white-tailed deer. The Grange Woods ESA is located along the northern section of the study area, specifically along Mississauga Road, west of The Grange Sideroad.

2.4.4 Credit Valley Conservation Natural Area Inventory Regions

Three sites identified within the Credit Valley Conservation’s (CVC’s) Natural Areas Inventory (NAI) fall within the study area: Tenth Line – 5 Sideroad South, Winston Churchill – Ballinafad, and Mississauga Road-Grange Central.

The Tenth Line – 5 Sideroad South NAI site consists of 140 ha of rolling topography, mixed with open grassland and interior forest habitats. The property is currently entirely private. This property has a diverse set of vegetation communities and is similarly diverse in regards to the flora and fauna found within the property. Several SAR and species of conservation concern have been confirmed to be present throughout this site, including butternut (*Juglans cinerea*), barn swallow (*Hirundo rustica*), Canada warbler (*Cardellina canadensis*), hooded warbler (*Setophaga citrina*), bobolink (*Dolichonyx oryzivorus*), eastern meadowlark (*Sturnella magna*), and western chorus frog (*Pseudacris triseriata*).

The Winston Churchill – Ballinafad NAI site consists of 717 ha and is regarded as an exceptional property with high quality natural areas. Ownership is primarily private (83%), versus public (17%). This property is regarded as particularly ecologically diverse, due to its size, location and distinct elevational properties (being along the Niagara Escarpment. A total of seven SAR and species of conservation concern have been confirmed present on this site: American hart’s-tongue fern (*Asplenium scolopendrium* var. *americanum*), butternut, barn swallow, Canada warbler, bobolink, eastern meadowlark, and western chorus frog. Numerous regionally rare plant and bird species have also been observed throughout the property.

The Mississauga Road-Grange Central NAI site is the second largest of the three NAI regions in the study area vicinity at 263 ha. This natural area is predominantly swamp and

deciduous forest, with scattered mixed and coniferous forest. SAR and species of conservation concern found on-site include: butternut, Canada warbler, hooded warbler, and monarch (*Danaus plexippus*).

2.5 Fisheries

2.5.1 West Credit River Subwatershed

The west branch of the Credit River within the area of Belfountain is considered to be a coldwater fishery. The documented fish community within the west branch of the river includes a variety of species that exhibit varied life history requirements and trophic statuses. Sensitive cool/coldwater species have also been identified within the west branch of the Credit River.

Redside dace (*Clinostomus elongatus*), which is listed as Endangered under the ESA, has also been observed as occurring within 1 km of the study area within the west branch of the Credit River; however, this species is not known to occur in the portion of the watercourses in the study area. No other SAR fish or mussels were identified as occurring within the study area.

Brook trout are also found within the unnamed Tributary A to the West Credit River. Additional species information was not available for this tributary and no information was provided for Tributary B.

2.5.2 Cheltenham to Glen Williams Subwatershed

Both Rogers Creek and Second Creek are considered coldwater fisheries. The fish community is better documented within Rogers Creek than Second Creek but both have sensitive cool/coldwater species, including brook trout and rainbow trout. No significant species are known from these watercourses.

3. SURFACE WATER MANAGEMENT

The following sections discuss the proposed drainage system, outline the applicable stormwater management guidelines, review and select appropriate stormwater management strategies, and summarize the proposed stormwater management plan.

3.1 Description of the Proposed Subsurface Drainage System

The majority of the roadway corridor improvements recommend the provision of a semi-rural roadway cross-section. As such a sub-surface drainage system is recommended for inclusion into the roadway cross-section. The subsurface drainage system will consist of a series of catchbasins, storm sewers and subdrains which will collect and convey both the granular base material and surface runoff and discharge to existing drainage outlets. The storm sewers shall be sized to accommodate a 10 year return period event, using a minimum inlet time of 15 minutes as per Region of Peel design standards. The design of the sewers will need to take into account any drainage from roadway boulevard areas as well as drainage external to the roadway right-of-way. In addition, where the roadway is adjacent to wetlands or in areas of a high groundwater table, storm sewer trenches shall include trench-plug units to ensure groundwater resources are not affected.

Effort has been made to ensure that existing drainage patterns and locations are maintained throughout the various roadway corridors. A conceptual storm system layout is illustrated on the preliminary design plates.

3.2 Drainage and Stormwater Management Criteria

In accordance with the Region of Peel guidelines, the stormwater management plan should conform to the following documents / guidelines:

1. MOEE Stormwater Management Practices Planning and Design Manual, March 2003.
2. Credit Valley Conservation Authority Valley Policies for water management.

3.2.1 Pavement Drainage Criteria

Minor System

The storm sewer system draining the pavement for the ultimate roadway configuration is to be designed to the 10 year design storm standard.

Major System

The major drainage system for the roadway is to be designed to convey overland flow to the adjacent watercourse in a safe manner.

3.2.2 Water Quality Control Criteria

Credit Valley Conservation requires water quality controls commensurate with the maximum downstream habitat type. In this case, all watercourses within the study limits require “Enhanced” protection (Level 1). Level 1 protection is to be provided, as a minimum for a pavement area equivalent to the new pavement area.

The MOEE Stormwater Management Practices and Planning Manual, March 2003, provides guidance for the selection of appropriate levels of stormwater quality protection for enhanced habitats, based on removal of total suspended solids (TSS).

3.3 Pavement Area Analysis

A pavement area analysis was undertaken to determine whether or not the proposed improvements to Mississauga Road, Old Main Street, Bush Street, Olde Base Line Road and Winston Churchill Boulevard corridors will result in an increase in impervious coverage when compared to existing conditions. The existing and proposed pavement areas, based on the preferred design, are summarized in **Table 3-1**.

Table 3-1: Existing and Proposed Pavement Areas

Location	Existing Pavement Area (m ²)	Proposed Pavement Area (m ²)	Increase in Pavement Area (m ²)	Increase in paved area (%)
Mississauga Road	50,000	65,190	15,190	30%
Bush Street / Old Main Street	18,250	20,420	2,170	12%
Olde Base Line Road	20,650	28,580	7,930	38%
Winston Churchill Boulevard	44,420	63,750	19,330	44%
TOTAL	133,320	177,940	44,620	33%

The pavement analysis determined that the proposed improvements will result in a 33% (4.46 ha) increase in impervious area over existing conditions. Therefore, stormwater management measures will be required in order to offset the impacts associated with the increase in pavement.

3.4 Stormwater Management Options

Stormwater Management Practices (SWMP's) for the management of roadway runoff generally fall into two categories; those that address water quantity and those that manage water quality of surface runoff. Water quantity management issues relate to properly sizing

watercourse crossings of the roadway corridor, as well as the conveyance of roadway runoff along the roadway corridor for minor and major storm events. In addition, water quantity management strategies can include the need for facilities to address downstream flood and erosion potential from the development (expansion) of the roadway right-of-way.

In terms of water quality, the SWMP's relate to the treatment of new pavement and where possible, the treatment of existing pavement; however, current legislation solely relates to the former. Typically, the treatment level is related to the standards defined in the watershed or sub-watershed planning study, which are dependant on the quality and sensitivity of the receiving stream system.

Various Best management practices or Stormwater Management practices are available to address both the quantity and quality of runoff from roadways. Due to the linear nature of roadway corridors, however, the full spectrum of stormwater management practices is typically not appropriate.

There are a number of SWMP's which can be used to treat runoff and / or control peak flows from roadway surfaces. These include the following:

1. Water Quality Inlets
2. Vegetative Facilities
 - Filter strips
 - Enhanced grassed swales
3. Infiltration Facilities
 - Infiltration basins
 - Infiltration trenches
 - Soak-away pits
4. Detention Facilities
 - Extended detention wet ponds
 - Extended detention dry ponds
 - Extended detention wetlands

The applicability of these SWMP's are reviewed below and appropriate measures identified to minimize potential water quantity and quality impacts related to the proposed road corridor improvements.

3.4.1 Water Quality Inlets

Water quality inlets, also known as oil / grit separators, combine storage chambers for sediment trapping and oil separation with drainage inlets or inflow sewers for intercepting or receiving roadway stormwater runoff. Oil / grit separators (OGS) are capable of removing up

to 80% of the annual sediment load when properly designed as a source control for small areas. This type of SWMP was considered feasible for this study.

3.4.2 Vegetative Facilities

Vegetative facilities treat runoff through filtration and sedimentation. With appropriate site condition, they can provide effective treatment of sediment. They have limited effectiveness for controlling peak flows and downstream erosion.

Filter Strips

Filter Strips operate through a combination of sedimentation and infiltration. Shallow flows are routed over grassed filter strips, which slow down runoff to enhance both the retention of the particulate matter and the infiltration of the runoff with its dissolved constituents. Filter strips are applicable to a rural road cross section where there are at least several meters of grassed shoulder on the side of the roadway in addition to the standard shoulder and ditch. They may also be applicable where there are high vegetated embankments at deep valley crossings. Vegetated filter strips were not considered to be a water quality treatment option for any of the corridors in our study area due to limited land availability.

Grassed Swales

Grassed swales are formed by widening the roadway ditches and in some instances, installing small, porous check dams to retard the flow. The check dams slow down and detain the flow which increase the degree of sedimentation and infiltration that occurs. The enlarged ditches provide additional storage capacity for flow retention and sediment accumulation. Due to the limited storage capacities in ditches, the degree of flow control may be small. However, they are relatively more effective at controlling runoff from smaller, more frequent events which results in some erosion control benefit. The sediment storage capacity is also relatively small and may require more frequent clean out than a detention pond. For the grassed swales to be effective at providing the desired treatment for runoff, they should be designed with a maximum flow of 0.15 m³/s for the 25 mm Chicago type storm distribution and a maximum flow velocity of 0.5 m/s. Grassed swales can be created by relatively minor modifications to the standard ditches in a rural roadway section. Grassed swales were considered to be a feasible water quality treatment option for segments of Old Base Line Road and Bush Street, where a rural road cross-section is proposed.

However, should the design parameters not meet the above MOE's criteria, check dam installation may be necessary to "Enhance" the quality of treatment. In such cases, grassed swales with check dams would need to be included to treat the roadway storm runoff.

3.4.3 Infiltration Facilities

Infiltration facilities capture runoff for infiltration to groundwater. This reduces the rates of runoff to the streams and provides a high level of treatment through the capture of both particulate and dissolved constituents. These types of facilities reduce water temperature impacts and enhance stream base flows through groundwater recharge. Since the volume of runoff to the receiving streams is reduced, these facilities also contribute to controlling downstream erosion and peak flow increases.

The disadvantage of these types of facilities is that they tend to become clogged by sediment wash-off from the roadway. As a result, the maintenance of an infiltration facility may be more frequent and more costly than other types of stormwater management. A second disadvantage is the need to protect the groundwater from contamination from chlorides and other constituents of road runoff. For these reasons, infiltration facilities were not considered further.

3.4.4 Stormwater Management Detention Facilities

Detention facilities operate on the basis of temporary storage of runoff to promote the removal of pollutants through sedimentation. They are generally effective at removing particulate constituents such as sediments and metals but ineffective at removing dissolved constituents such as salt. Extended detention wet ponds and constructed wetlands are considered to be effective at achieving an enhanced level of treatment for roadway runoff. Extended detention dry ponds generally do not provide this level of treatment. Detention facilities are also effective for erosion and peak flow (flood) control.

The disadvantage of these facilities is their large land requirement. For this project, there is a space constraint within the right-of-way that would not accommodate the construction of detention facilities.

3.4.5 Feasible Stormwater Management Options

Based on the screening of stormwater management options documented in **Sections 3.4.1 to 3.4.4**, oil grit separators and grassed swales are considered to be feasible for the study corridors.

3.5 Proposed Stormwater Management Plan

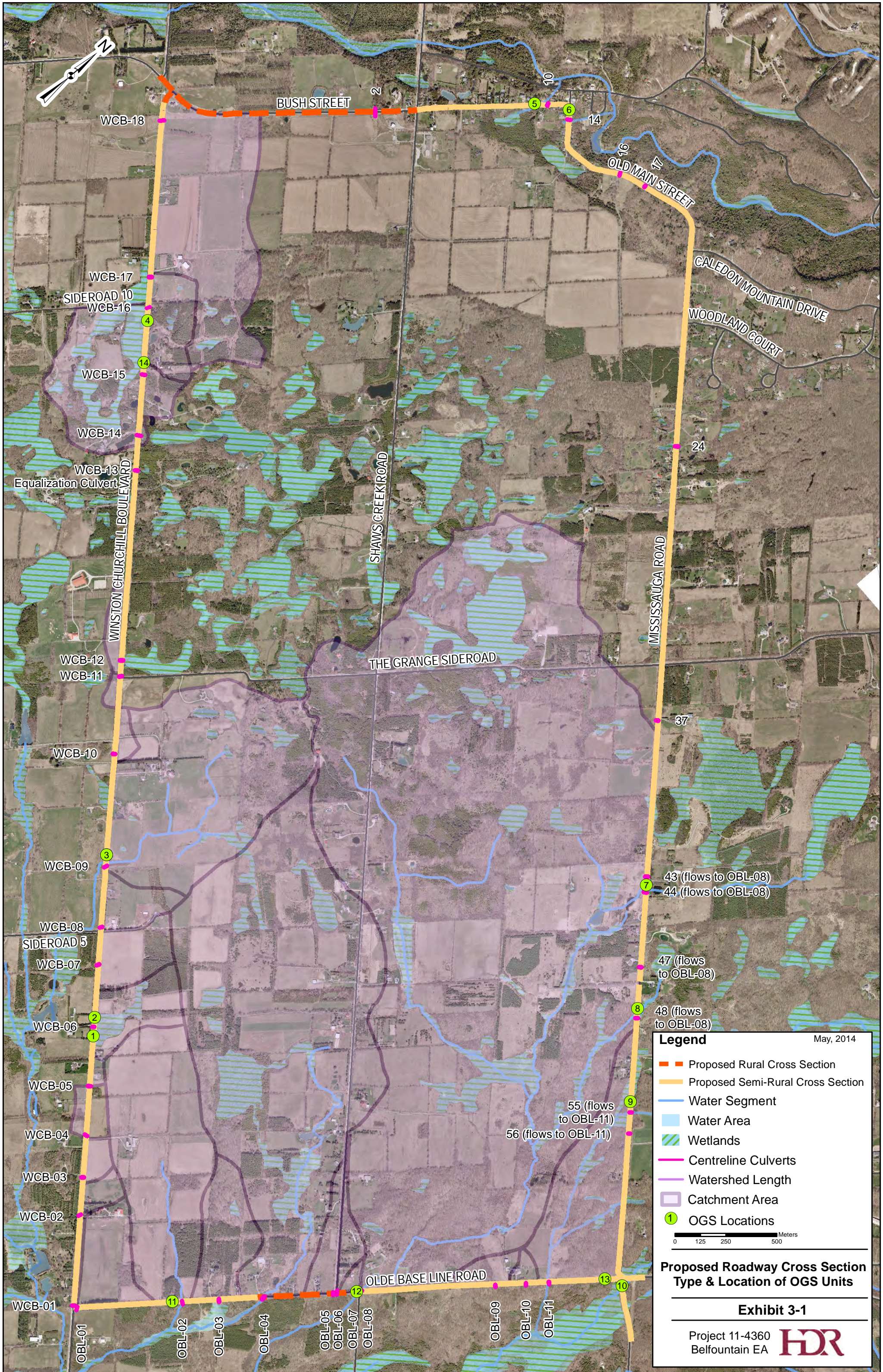
The proposed stormwater management plan for the project has been developed by examining the opportunities and constraints within the entire project area. The proposed plan consists of rural and semi-rural roadway sections. Runoff from the paved roadway area will be conveyed by existing roadside ditches, proposed grassed swales, new subsurface drainage system and existing and proposed culverts. The proposed locations of all rural and semi-rural roadway sections are illustrated in **Exhibit 3-1**.

The majority of the existing rural cross-sections will be converted into semi-rural cross-sections with a subsurface drainage system. The subsurface drainage system will consist of a series of catchbasins, storm sewers and subdrains which will collect and convey both the granular base material and surface runoff and discharge to existing drainage outlets.

Where the existing rural ditch system is to remain, ditches will be re-graded to flat-bottom swale systems (grassed swales), where possible, to provide additional water quality benefits within the project limits. They will continue to collect and convey drainage from external lands along the roadway corridors to the respective culvert crossing locations.

As previously indicated in **Table 3-1**, under the proposed condition, the total roadway pavement area will be increased by 44,620m² (4.46 ha). This increase forms the basis for the level of water quality treatment to be provided.

Oil grit separator and grassed swales were selected for stormwater management quality control to treat the roadway runoff corresponding to the additional pavement area resulting from the roadway improvements. These stormwater management practices are described in more detail below.



May, 2014

Legend

- Proposed Rural Cross Section
- Proposed Semi-Rural Cross Section
- Water Segment
- Water Area
- Wetlands
- Centreline Culverts
- Watershed Length
- Catchment Area
- 1 OGS Locations

0 125 250 500 Meters

Proposed Roadway Cross Section Type & Location of OGS Units

Exhibit 3-1

3.5.1 Oil / Grit Separator Option

Due to limited land availability, the principal features of the proposed stormwater management system are the provision of oil-grit separator (OGS) units to provide water quality control. The recommended placement of the OGS units was focused on locations with fisheries sensitivity (i.e. watercourse crossing that support direct fish habitat) and locations of Provincially Significant Wetlands. These locations are listed in **Table 3-2** as identified in the *Belfountain Transportation Corridor Class Environmental Assessment Study, Peel Region - Natural Heritage Report – Existing Conditions and Natural Feature Constraints, August 2013* prepared by Natural Resource Solutions Inc. Report.

Table 3-2: OGS Locations

Location (Culvert ID)	Station	OGS Unit I.D No.	Paved Treatment Area (ha)	Notes
Winston Churchill Blvd. (WCB-06)	41+400	1 and 2	0.373	Provincially Significant Wetland Fisheries Habitat
Winston Churchill Blvd. (WCB-09)	43+010	3	0.632	Tributary C of Rogers Creek Fisheries Habitat
Winston Churchill Blvd (WCB-15)	44+610	14	0.274	Unnamed Watercourse
Winston Churchill Blvd. (WCB-16)	44+950	4	0.374	Provincially Significant Wetland
Bush Street (10)	12+010	5	0.198	Tributary A of Credit River Fish Habitat
Old Main Street (14)	26+375	6	0.396	Tributary B of Credit River
Mississauga Road (44)	22+210	7	0.828	Tributary A of Second Creek Fish Habitat
Mississauga Road (48)	21+595	8	0.2130	Tributary B of Second Creek Wetland Contribution
Mississauga Road (55)	21+130	9	0.535	Provincially Significant Wetland
Mississauga Road	20+220	10	0.472	Unnamed watercourse
Olde Base Line Road (OBL-02)	30+540	11	0.368	Tributary B of Rogers Creek
Olde Base Line Road (OBL-08)	30+400	12	0.513	Discharges downstream to Tributary A of Second Creek
Olde Base Line Road	32+650	13	0.593	Wetland / Jefferson Salamander Regulated Habitat
Total		14	5.56	

A total of fourteen (14) OGS units are proposed (see **Exhibit 3-1**) providing a total collective area for stormwater treatment of 5.56 ha. Water quality criteria will be met at each OGS location based on Enhanced (Level 1) protection as outlined in the MOE Stormwater Management Practices Manual. For further illustration please refer to Appendix A to Appendix K.

3.5.2 Grassed Swale Option

To augment the impacts associated with the increased pavement, wide bottom (1.0m) grassed swales are proposed at the locations listed in **Table 3-3**.

Table 3-3: Grassed Swale Locations

Location	Station		Length (m)
	From	To	
Olde Base Line Road (North Side)	30+940	31+280	340
Olde Base Line Road (South Side)	30+940	31+240	300
Bush Street (North Side)	10+000	11+140	1,140
	11+200	11+350	150
Bush Street (South Side)	10+000	10+200	200
	10+300	10+580	280
	10+820	11+120	300
	11+200	11+350	150
Winston Churchill Blvd. (West Side)	45+940	46+010	70
Winston Churchill Blvd. (East Side)	45+950	46+010	60
Total			2,990

Based on a typical pavement width of 11.5 metres, the potential collective area of treatment that can be provided by the grassed swales noted in **Table 3-3** above is approximately 3.4 ha. During detailed design, the location and performance characteristics of the swales will need to be confirmed to ensure that all swale criteria can be met.

3.5.3 Summary of Water Quality Recommendations

The stormwater management strategy recommended for this project will provide water quality treatment to 5.56 ha of pavement area through the use of OGS units and approximately 3.4 ha of pavement area through the incorporation of grassed swales along the roadway corridors. Therefore the treated pavement area would significantly exceed the additional pavement area of 4.46 ha resulting from the roadway improvements. This represents a 101% increase in treated pavement area over additional pavement area.

4. EROSION AND SEDIMENT CONTROL DURING CONSTRUCTIONS

Erosion and sediment control measures should be implemented and monitored through the construction period. Construction activity should be conducted during periods that are least likely to result in in-stream impacts to fish habitat.

Detailed erosion and sediment control plans will be required as part of the detailed design component for all phases of the construction. The erosion and sediment control plans will be subject to review and approval by the various external agencies involved in the project. These would include the Credit Valley Conservation Authority.

During construction, disturbances to watercourse riparian vegetation should be minimized. If riparian vegetation is removed or disturbed, erosion and sediment control measures such as silt fences, rock flow check dams and sedimentation ponds should be utilized to provide a maximum protection of local and downstream aquatic resources. These measures should be maintained during construction and until disturbed areas have been stabilized with seed and mulch. Additionally, topsoil should not be stockpiled close to the watercourses and water should not be withdrawn from these sensitive streams for construction purposes.

The site engineer and contractor will be responsible for delineating work areas, and ensuring that erosion and sediment control measures are functional. In addition, the engineer will ensure that provisions related to fisheries and watercourse protection is met and that fish habitat compensation measures are implemented in accordance with the terms and conditions of the Fisheries Act Authorization.

5. SUMMARY AND CONCLUSIONS

The preliminary stormwater management plan is designed to prevent impacts from the future roadway configuration by using available technologies and opportunities to achieve the highest degree of control possible given the constraints of the study corridor. The following design elements are recommended as part of the proposed roadway improvements;

1. Where the roadway improvements recommend the provision of a semi-rural roadway cross-section, a sub-surface drainage system is recommended for inclusion into the roadway cross-section. The subsurface drainage system will consist of a series of catchbasins, storm sewers and subdrains which will collect and convey both the granular base material and surface runoff and discharge to existing drainage outlets. The storm sewers shall be sized to accommodate a 10 year return period event, using a minimum inlet time of 15 minutes as per Region of Peel design standards. The design of the sewers will need to take into account any drainage from roadway boulevard areas as well as drainage external to the roadway right-of-way. Effort has been made to ensure that existing drainage patterns and locations are maintained throughout the various roadway corridors. A conceptual storm system layout is illustrated on the preliminary design plates.
2. The principal features of the project's stormwater management system are the provision of oil-grit separator units to provide water quality control. A total of twelve (12) OGS units are proposed providing a total collective area for stormwater treatment of 4.68 ha. Water quality criteria will be met at each OGS location based on Enhanced (Level 1) protection as outlined in the MOE Stormwater Management Practices Manual.
3. Existing roadside ditches will be re-graded to flat-bottom swale systems (grassed swales), where possible, to provide additional water quality benefits within the project limits. There is a potential to treat up to 3.4 hectares of pavement area through the incorporation of grassed swale systems. It is recommended that during detail design, the proposed grassed swale areas are reviewed for their effectiveness in meeting the MOE criteria for flowrate, velocity and contributing area.
4. Erosion and sediment control measures should be implemented and monitored through the construction period. Construction activity should be conducted during periods that are least likely to result in in-stream impacts to fish habitat.

6. REFERENCES

HDR Corporation, Preferred Design Drawings (Plan and Profile), Draft February 21, 2014;

HDR Corporation, *Drainage and Hydrology Report, Olde Baseline Road and Winston Churchill Boulevard, Town of Caledon, Region of Peel*, Draft January 2014

Natural Resource Solutions Inc., *Belfountain Transportation Corridor Class Environmental Assessment Study, Peel Region - Natural Heritage Report – Existing Conditions and Natural Feature Constraints*, August 2013

Dillon Consulting Limited, *Bush Street and Mississauga Road Class EA Existing Conditions Drainage Report - Draft*, June 2010.

Regional Municipality of Peel, *Public Works Design, Specifications and Procedures Manual – Functional Servicing and Storm Water Management Report*, July 2009.

Regional Municipality of Peel, *Public Works Design, Specifications and Procedures Manual – Storm Sewer Design*, July 2009.

Regional Municipality of Peel, *Public Works Design, Specifications and Procedures Manual – Regional Roads and Traffic*, February 2010.

Credit Valley Conservation (CVC), *Stormwater Management Guidelines*, August 2012.

Appendix A
Proposed OGS System Treatment Area
OGS 1 & 2 (WCB-06)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HP • HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by: _____ Chkd. _____ Approved by: _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBREOPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

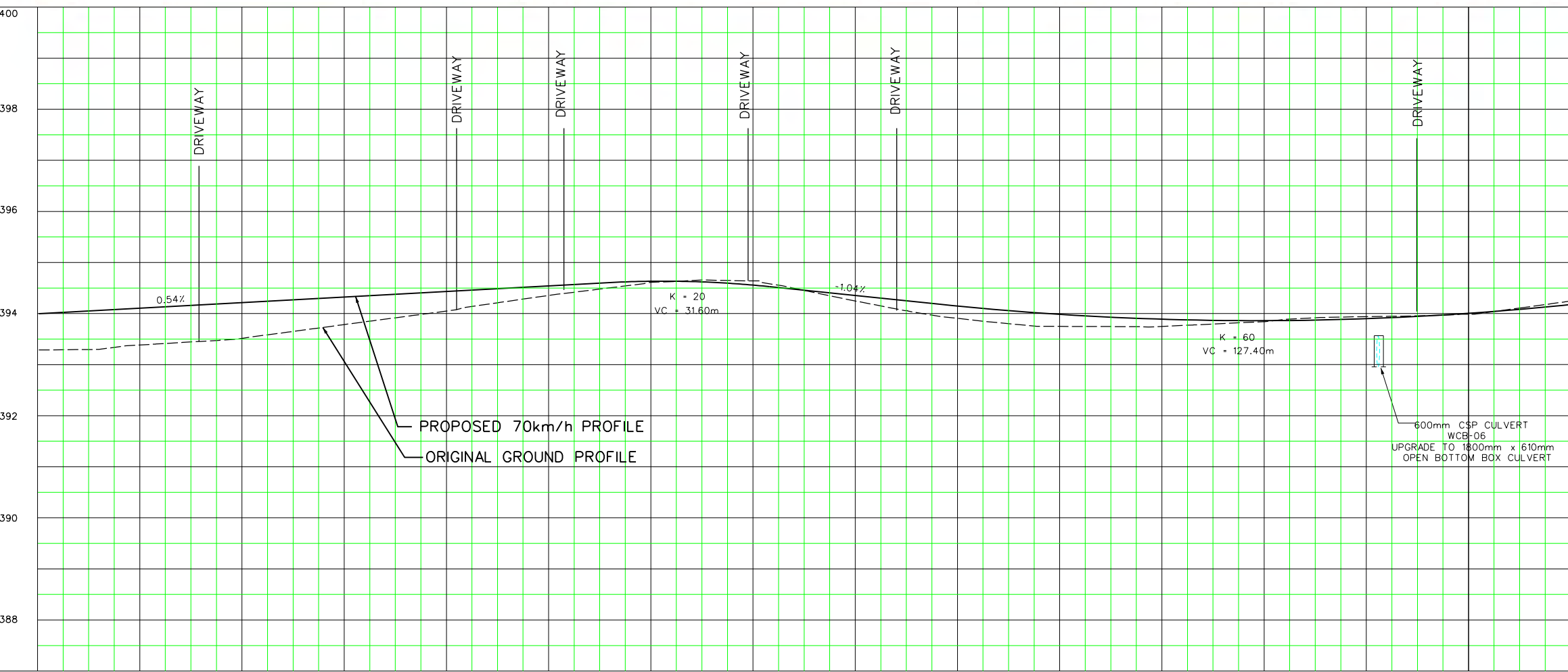
10m 0 10 20 30m HORIZONTAL SCALE

1m 0 1 2 3m VERTICAL SCALE

Region of Peel
Working for you

WINSTON CHURCHILL BOULEVARD
(FROM STA 41+140 to STA 41+440)

PROPOSED OGS SYSTEM TREATMENT AREAS			
BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet WCB1	Plan No. -D



41+200	41+300	41+400
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CATCHMENT AREA TO OGS-2
2180m²

WINSTON CHURCHILL BOULEVARD

PROPOSED ROAD CENTRELINE
EXISTING ROAD CENTRELINE

POTENTIAL PROPERTY ACQUISITION OR OTHER MITIGATION MEASURES TO BE REVIEWED

POTENTIAL IMPACT TO HERITAGE CEDAR FENCE MITIGATION MEASURES TO BE REVIEWED

EXISTING RIGHT-OF-WAY CEDAR RAIL FENCE

POTENTIAL PROPERTY ACQUISITION OR OTHER MITIGATION MEASURES TO BE REVIEWED

3.5m TRAVEL LANE
1.7m PAVED SHOULDER
0.5m MOUNTABLE CURB

CEDAR RAIL FENCE

3.5m TRAVEL LANE
1.7m PAVED SHOULDER
0.5m MOUNTABLE CURB

EXISTING RIGHT-OF-WAY

REMNANTS OF DECIDUOUS TREE LINED ROAD

REPLACE WITH 700mm CULVERT

41+500

41+600

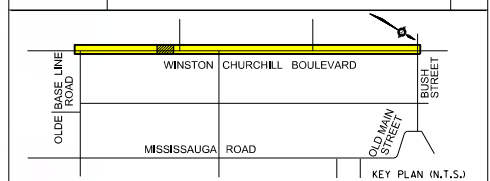
41+700

MATCH LINE STA. 41+440

MATCH LINE STA. 41+740

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
DNT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
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B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

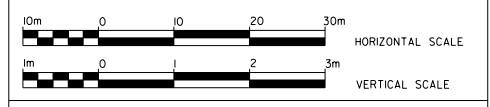
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

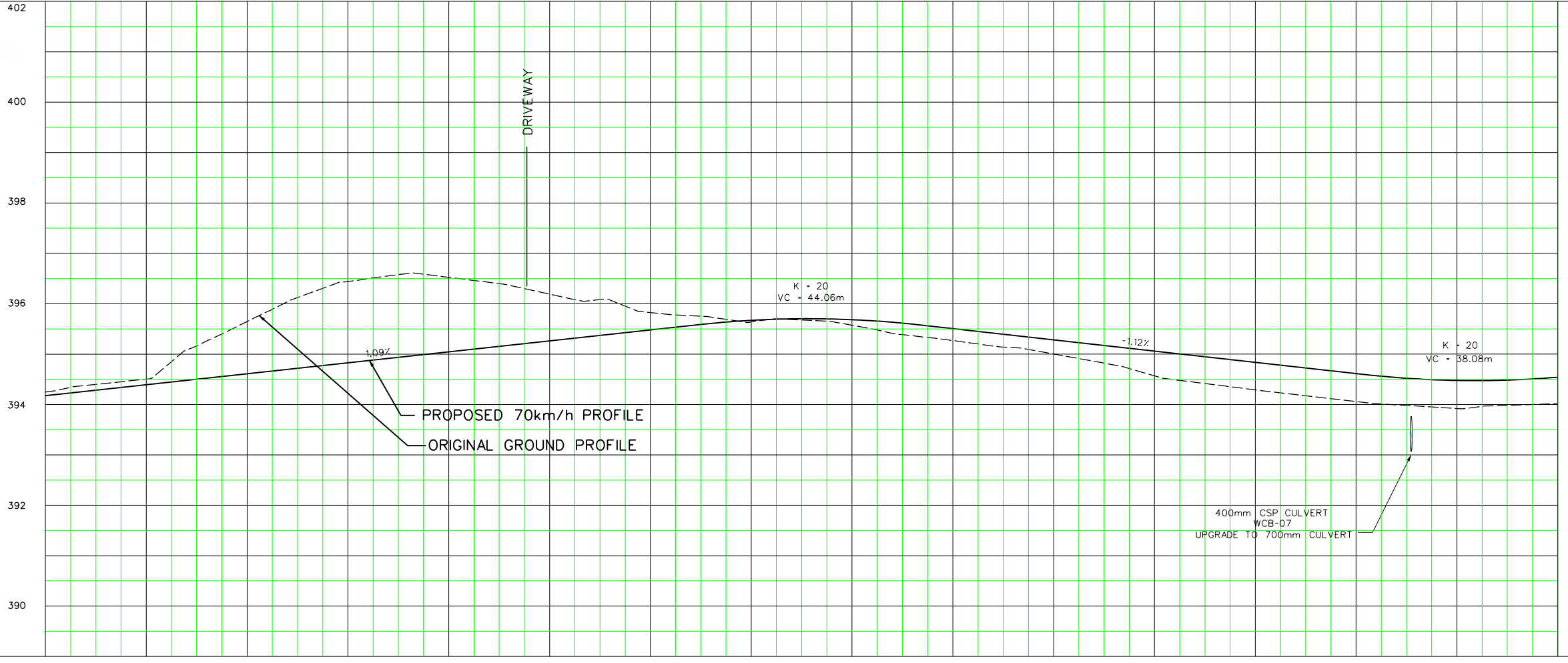
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF BRAMPTON WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FIBROBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



WINSTON CHURCHILL BOULEVARD
(FROM STA 41+440 to STA 41+740)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet WCB2	



41-500	41-600	41-700
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Appendix B
Proposed OGS System Treatment Area
OGS 3 (WCB-09)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
DNT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HP • HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

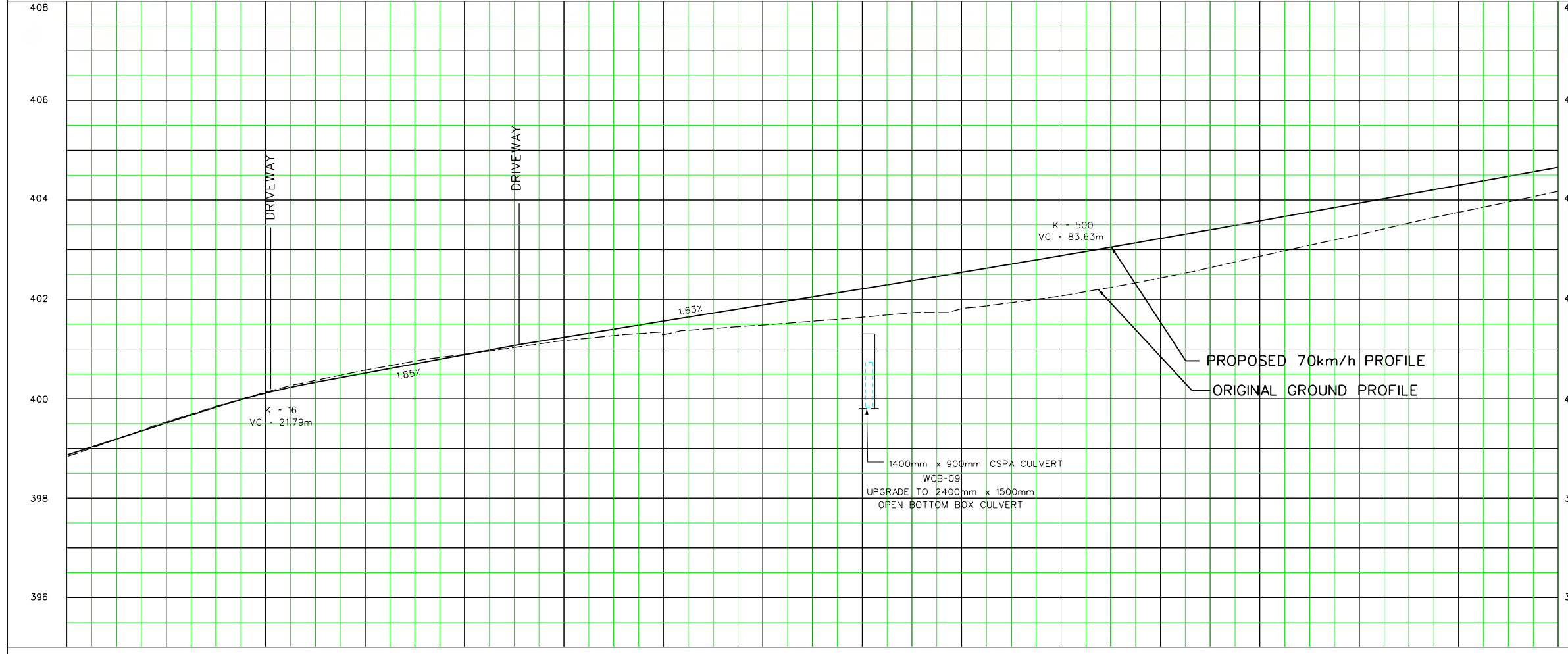
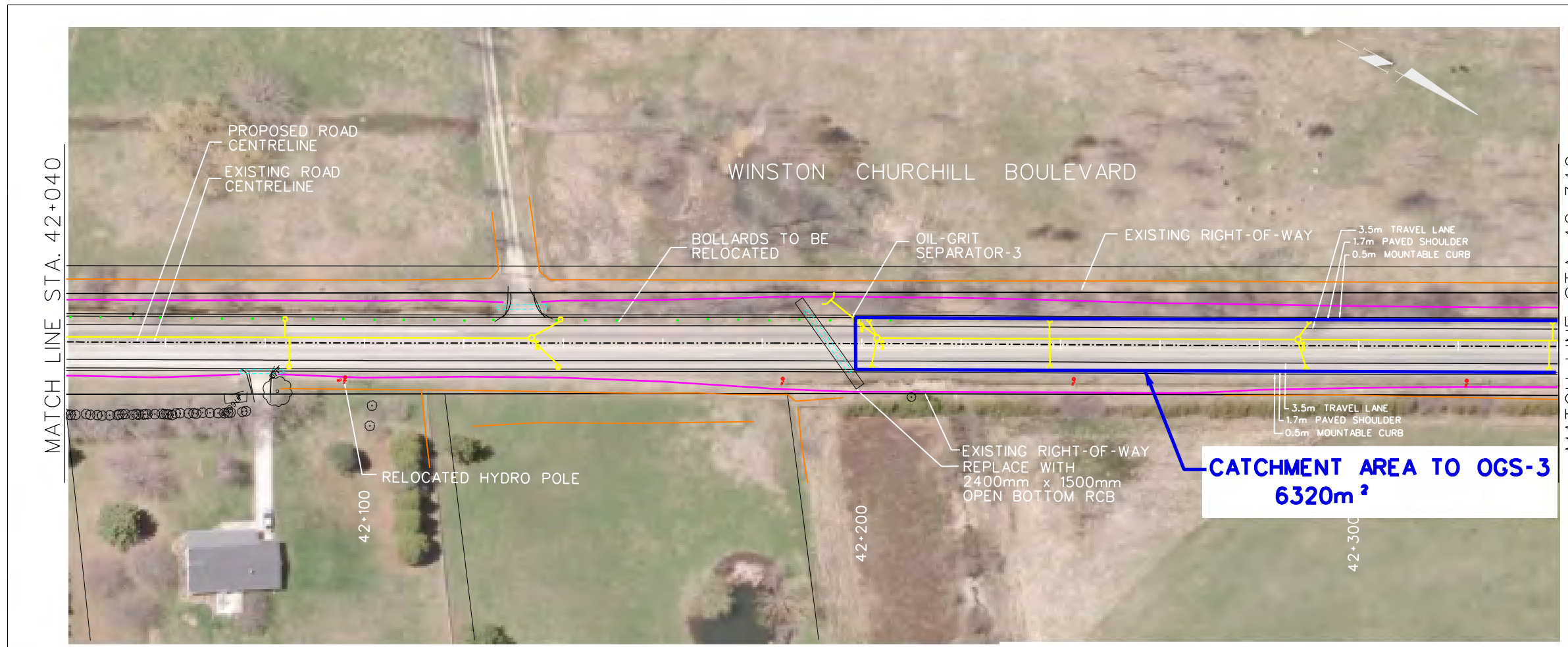
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING:

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



WINSTON CHURCHILL BOULEVARD
(FROM STA 42+040 to STA 42+340)

PROPOSED OGS SYSTEM TREATMENT AREAS



BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet WCB3	-D

42+100

42+200

42+300

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HP HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- ⊞ Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor Is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location Of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

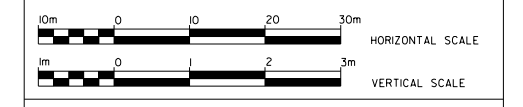
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

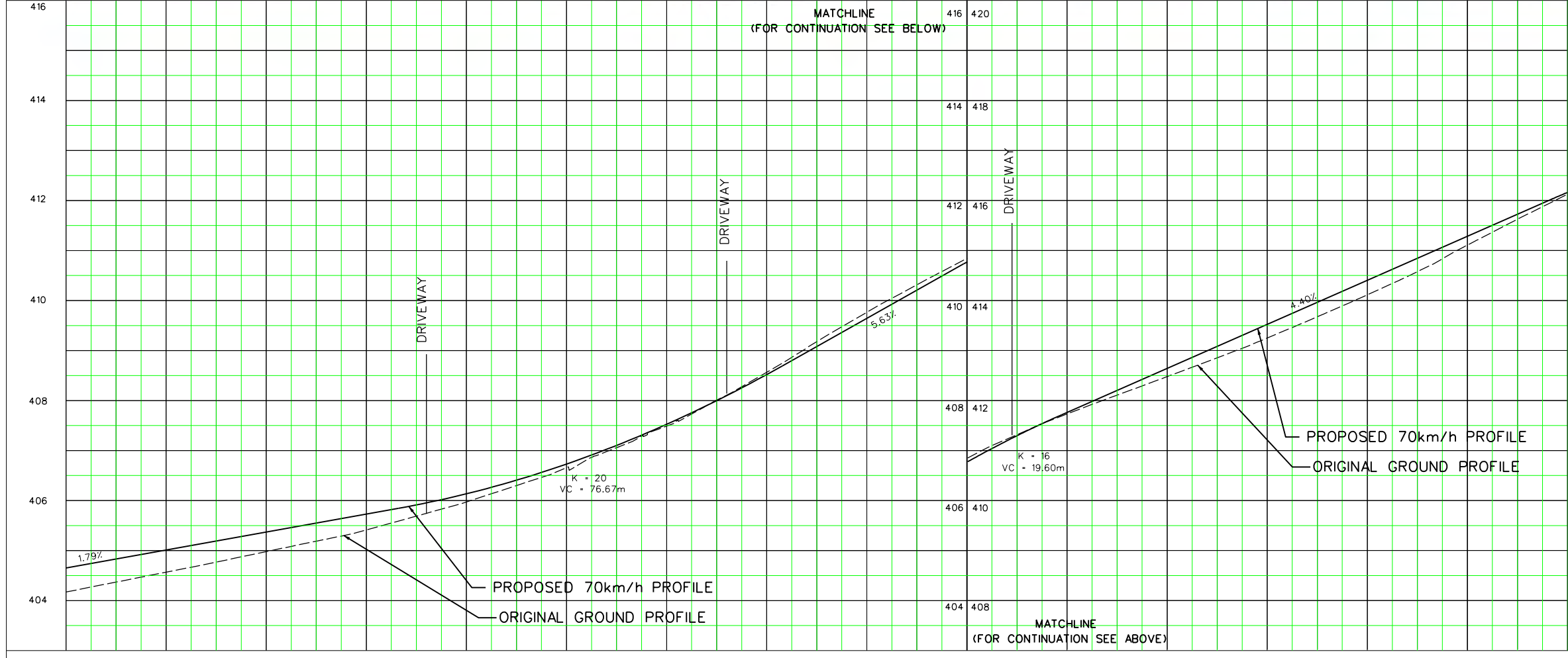
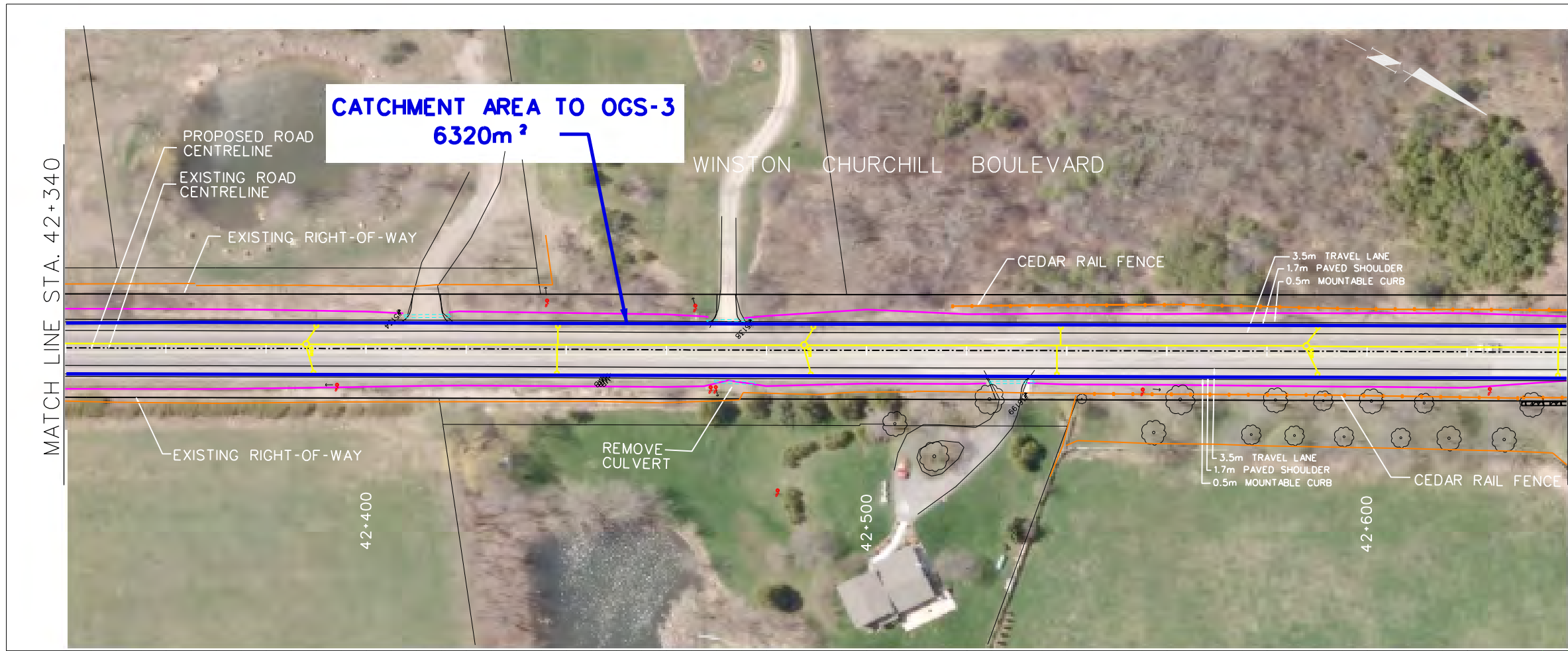
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



WINSTON CHURCHILL BOULEVARD
(FROM STA 42+340 to STA 42+640)

PROPOSED OGS SYSTEM TREATMENT AREAS		
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet WCB4	

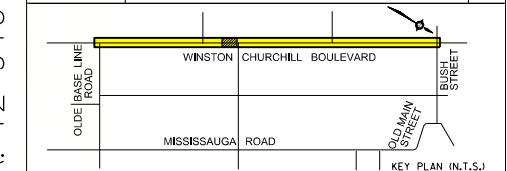


BOT.EL. OF WM.		CAD Area		Area X-X		Project No. XX-XXX	
42+400	42+500	42+400	42+500	42+400	42+500	42+400	42+500
EX. ROAD ELEV.		Checked by		Drawn by JM		Plan No.	
ROAD CHAINAGE		Date MAY, 2014		Sheet WCB4		-D	

**CATCHMENT AREA TO OGS-3
6320m²**

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
INT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

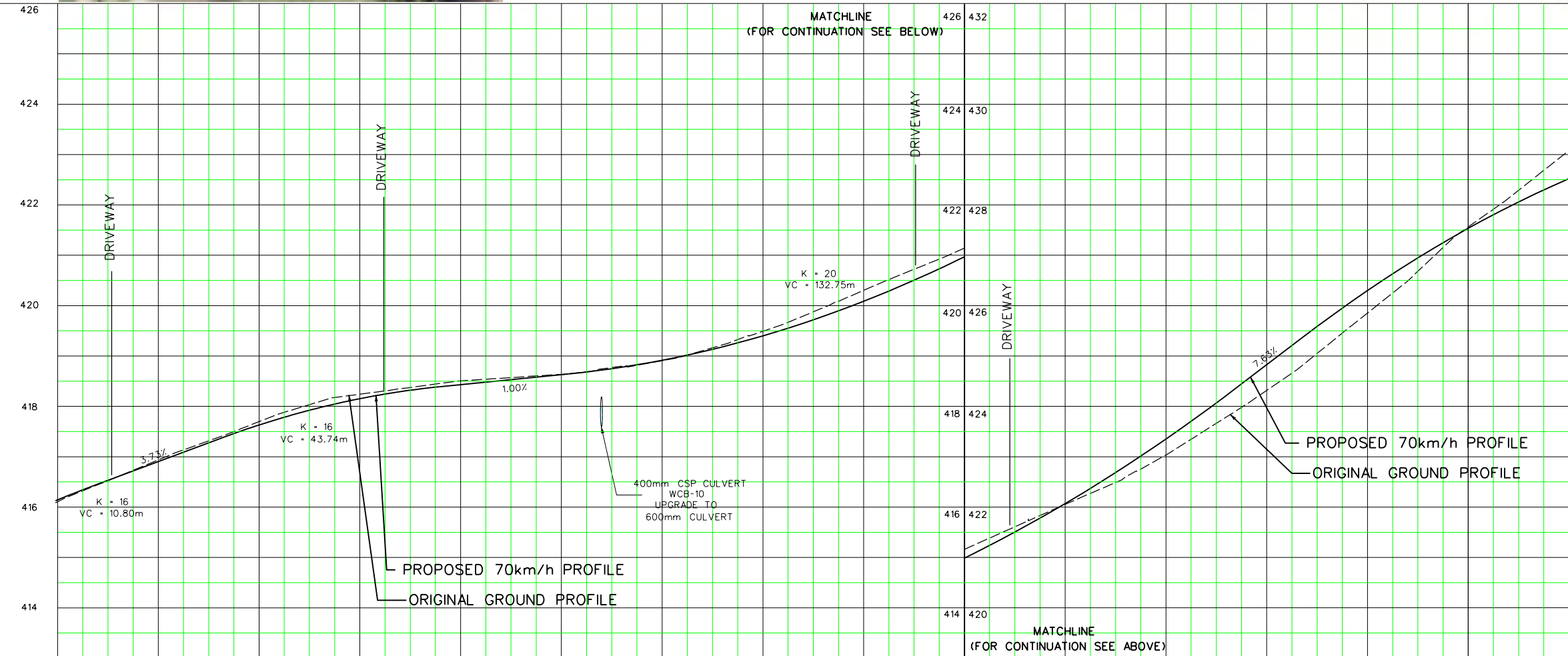
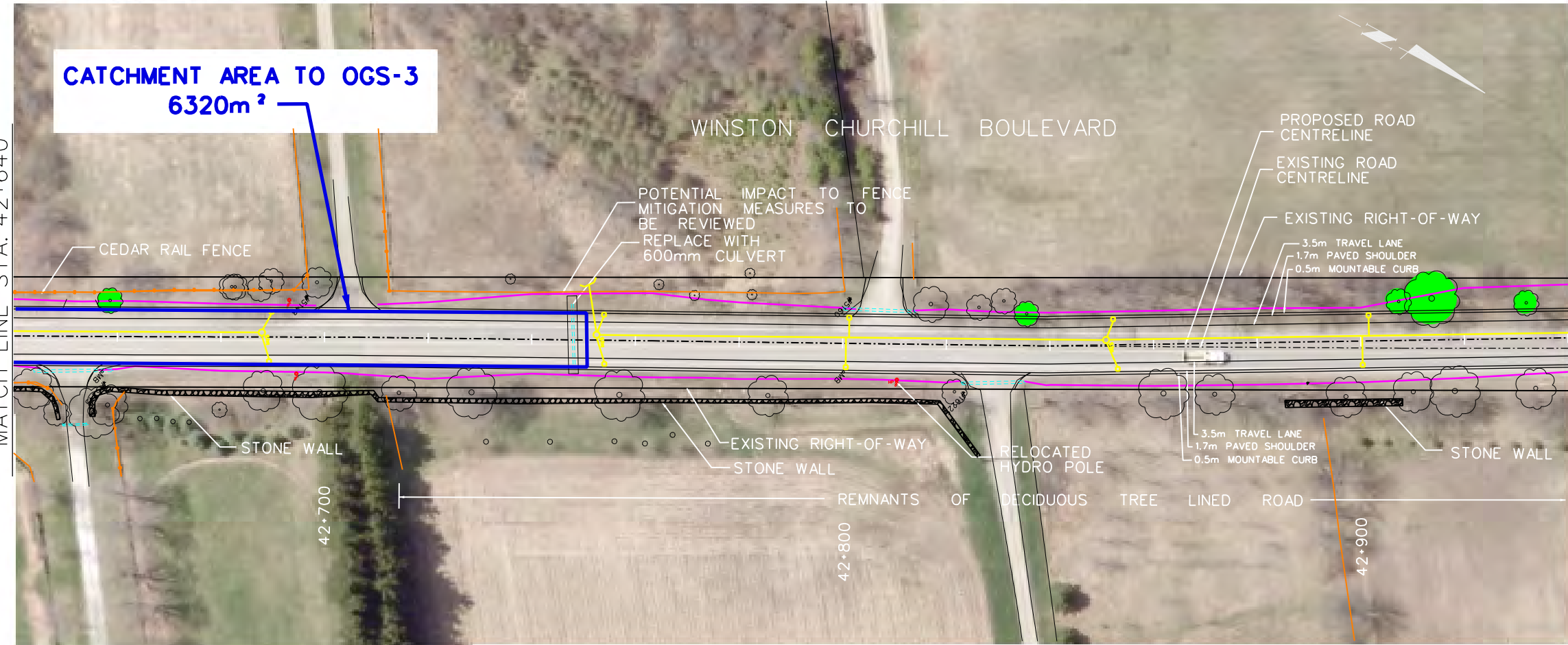


- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

MATCH LINE STA. 42+640

MATCH LINE STA. 42+940



General Notes

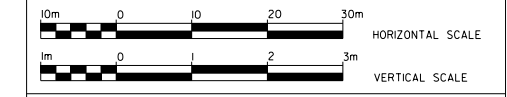
- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
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- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.
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Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

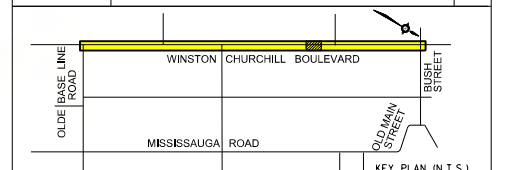
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



WINSTON CHURCHILL BOULEVARD
(FROM STA 42+640 to STA 42+940)
PROPOSED OGS SYSTEM TREATMENT AREAS

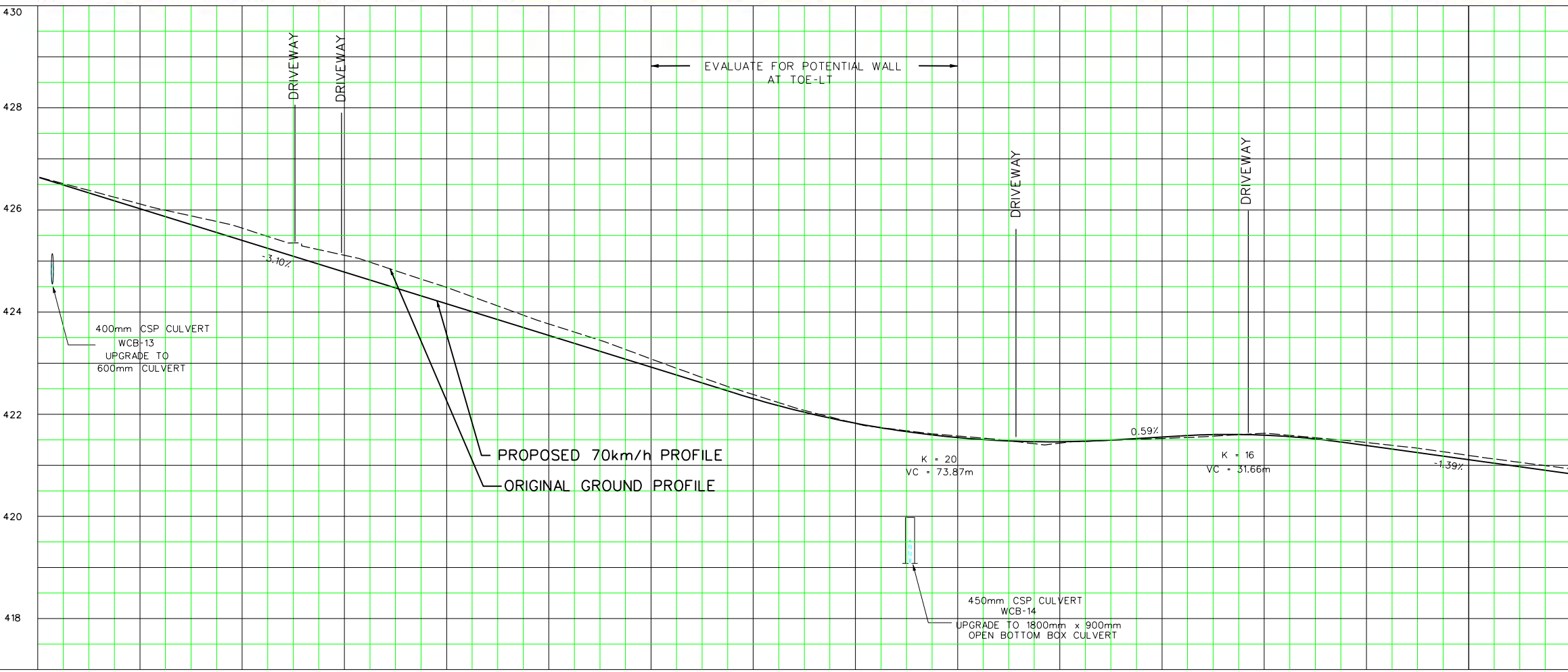
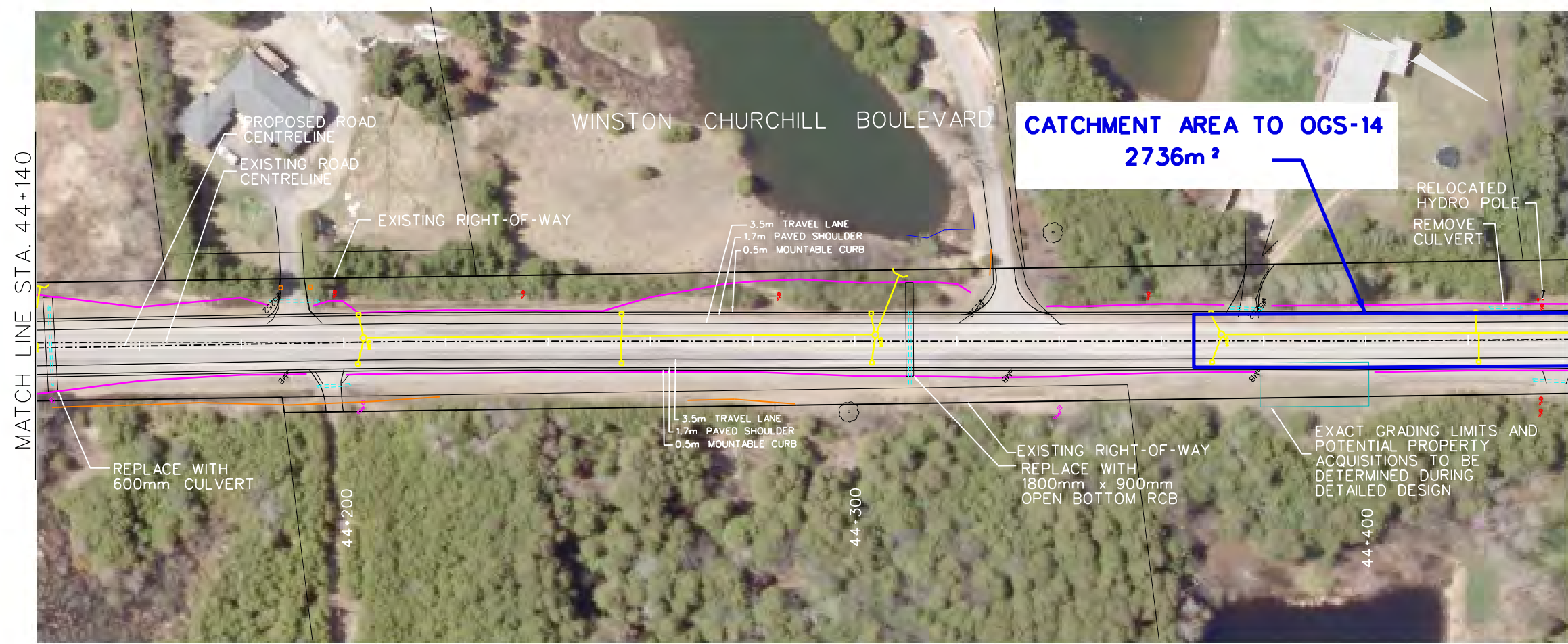
Appendix C
Proposed OGS System Treatment Area
OGS 14 (WCB-15)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

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- ⊞ Denotes Building Located
- ▭ Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

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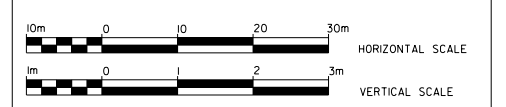
Designed by _____ Chkd. _____

Approved by _____

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CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FIBROBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



Region of Peel
Working for you

WINSTON CHURCHILL BOULEVARD
(FROM STA 44+140 TO STA 44+440)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet WCB6	-D

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

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- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.
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Designed by: _____ Chkd. _____
Approved by: _____

NOTICE TO CONTRACTOR
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

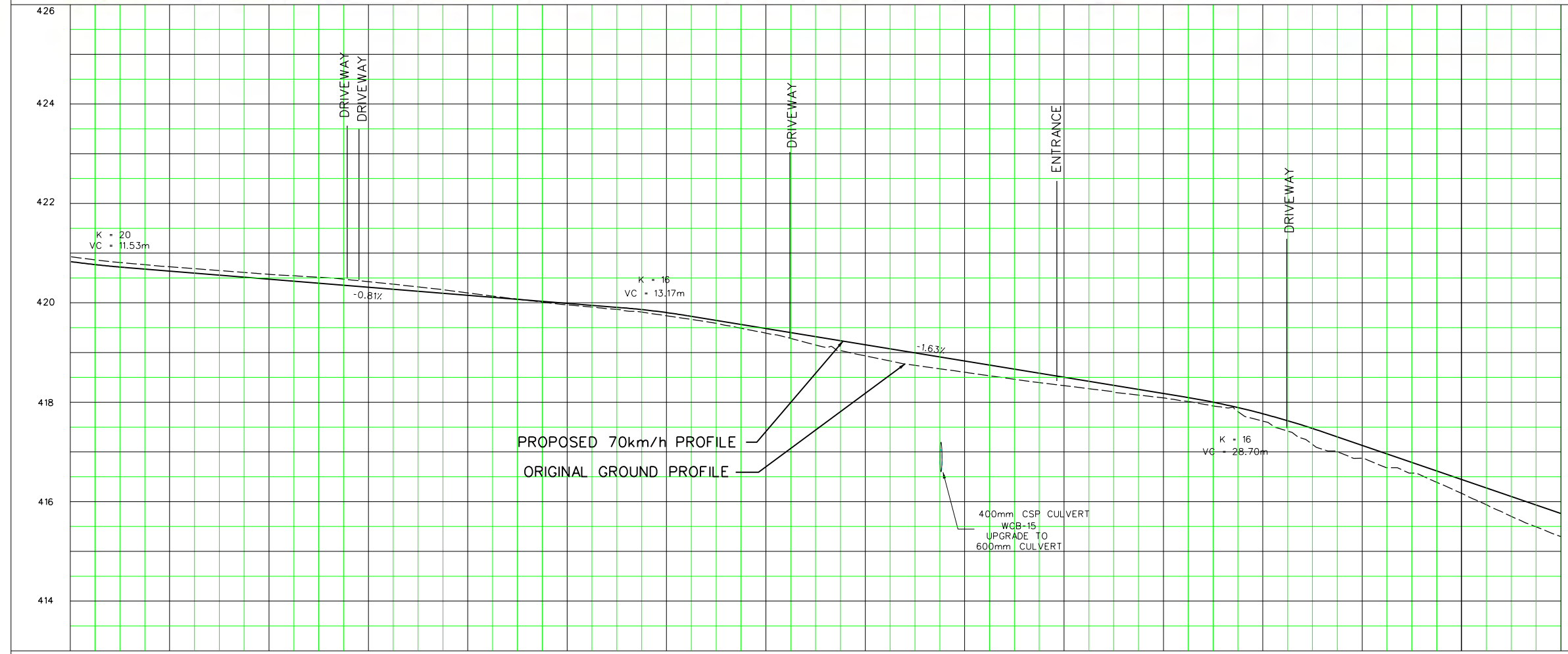
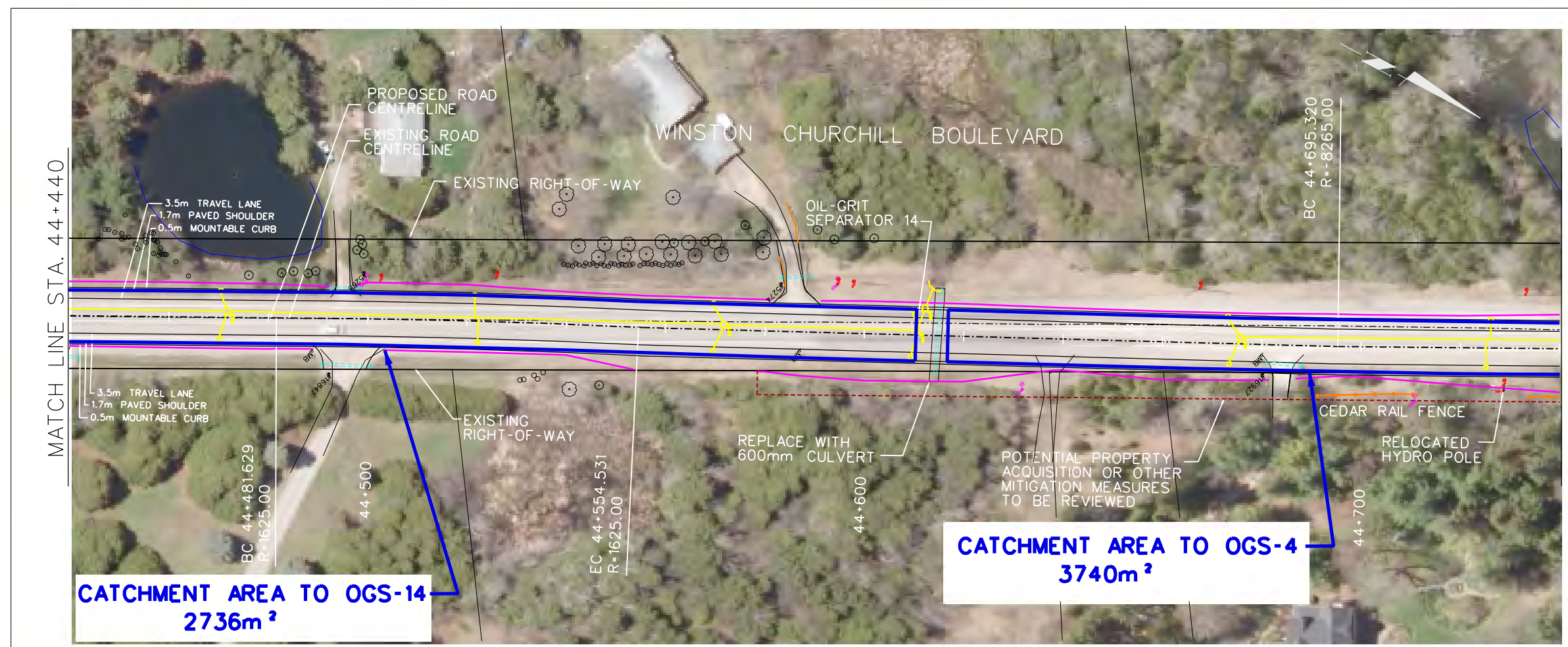
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	RODGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



WINSTON CHURCHILL BOULEVARD
(FROM STA 44+440 TO STA 44+740)

PROPOSED OGS SYSTEM TREATMENT AREAS

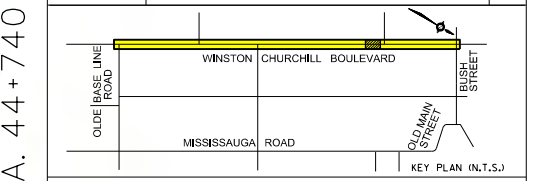
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet WCB7	-D



44+500	44+600	44+700	BOT. EL. OF WM. EX. ROAD ELEV.
ROAD CHAINAGE			

Appendix D
Proposed OGS System Treatment Area
OGS 4 (WCB-16)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
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- ⊙ Denotes Building - Not Located
- ⊙ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

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Designed by: _____ Chkd. _____
 Approved by: _____

NOTICE TO CONTRACTOR
 48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

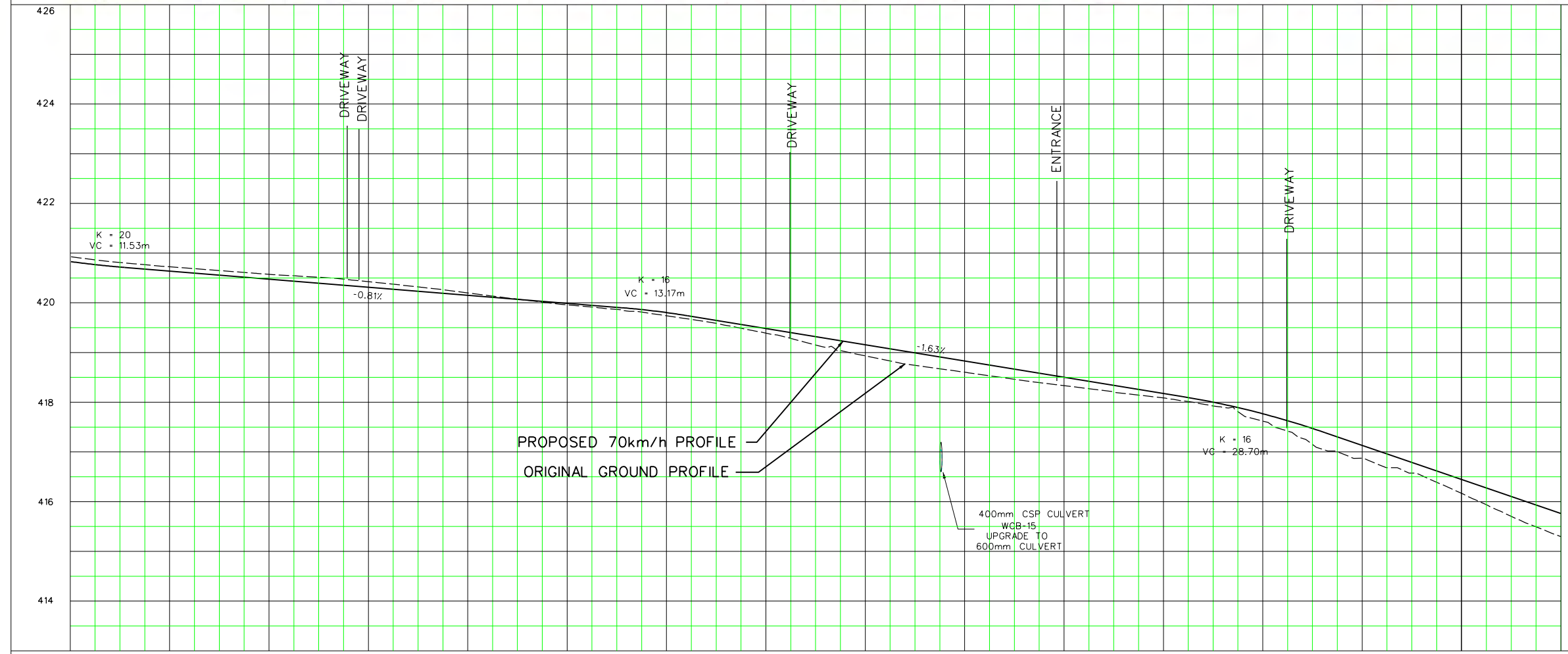
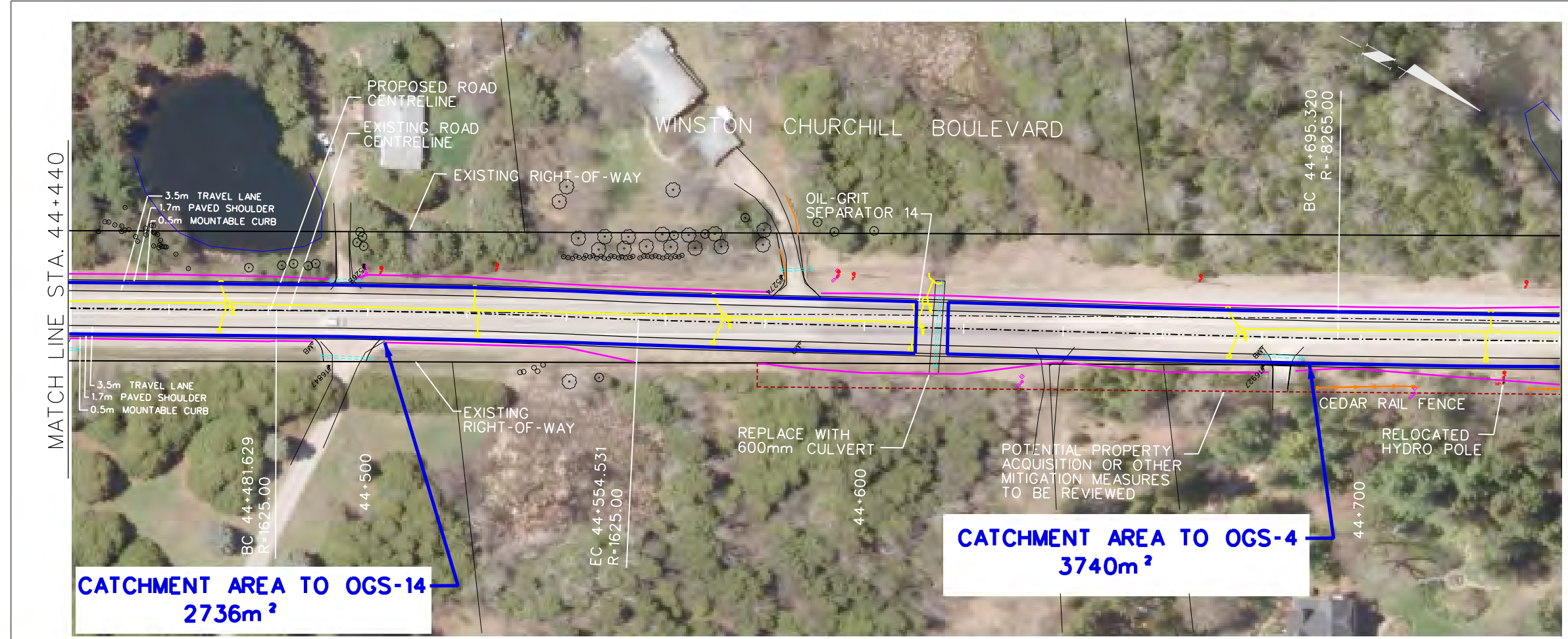
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



Region of Peel
 Working for you

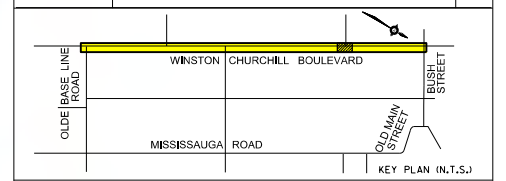
WINSTON CHURCHILL BOULEVARD
 (FROM STA 44+440 TO STA 44+740)

PROPOSED OGS SYSTEM TREATMENT AREAS		
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet WCB7	-D



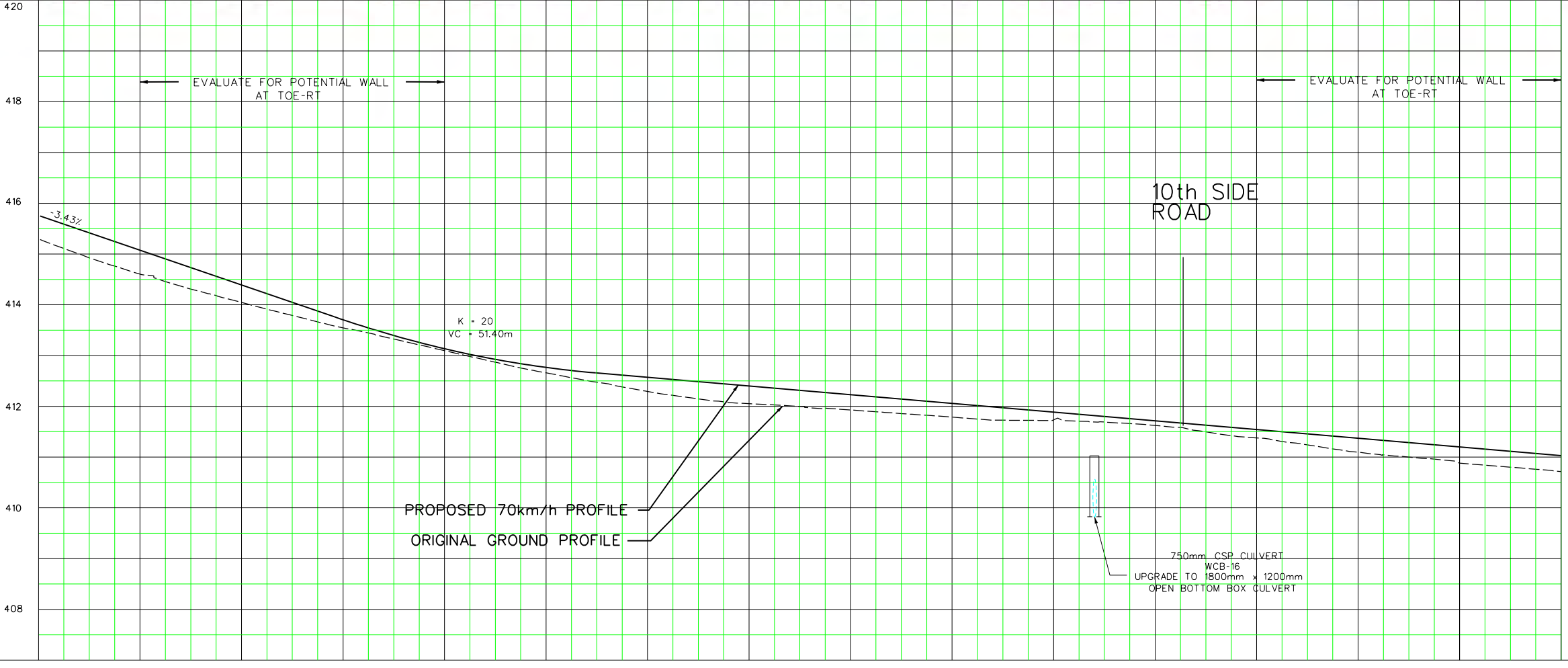
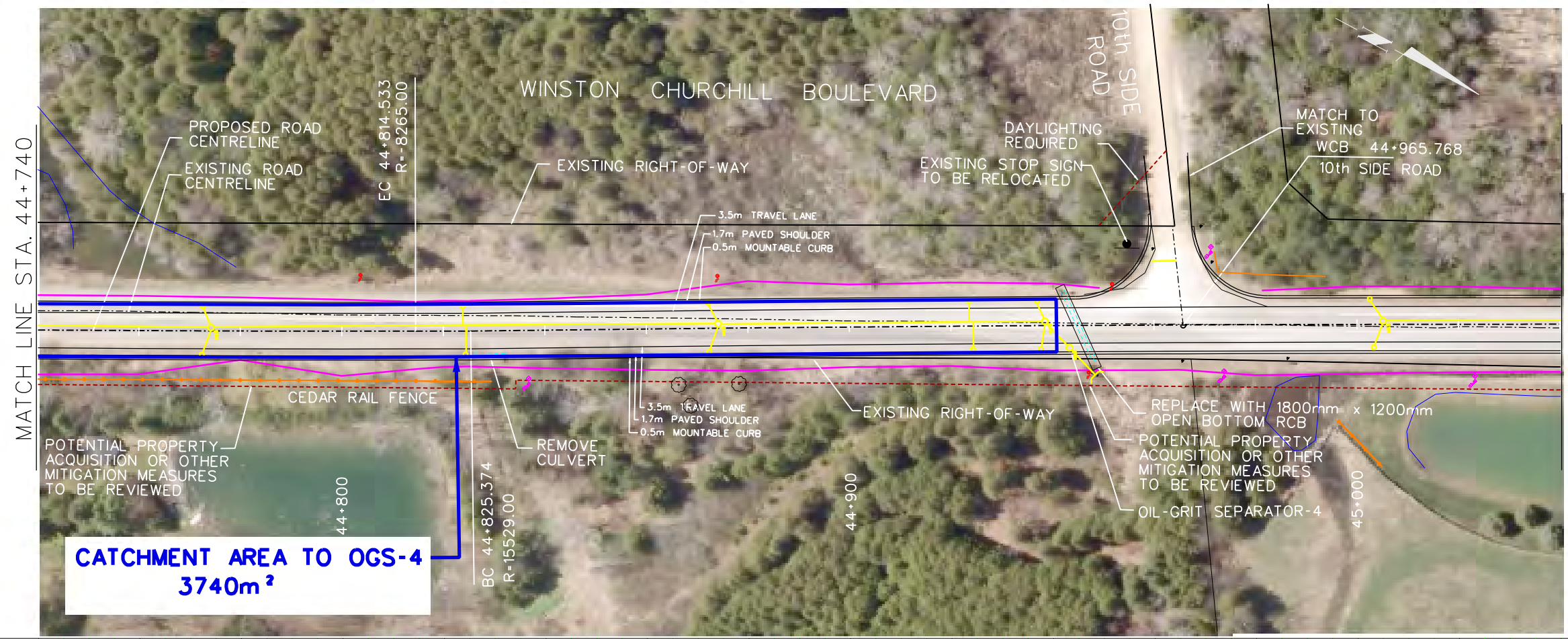
44+500	44+600	44+700	BOT. EL. OF WM. EX. ROAD ELEV.
ROAD CHAINAGE			

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

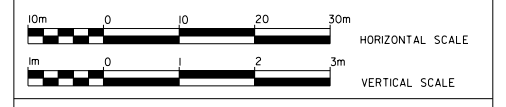
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



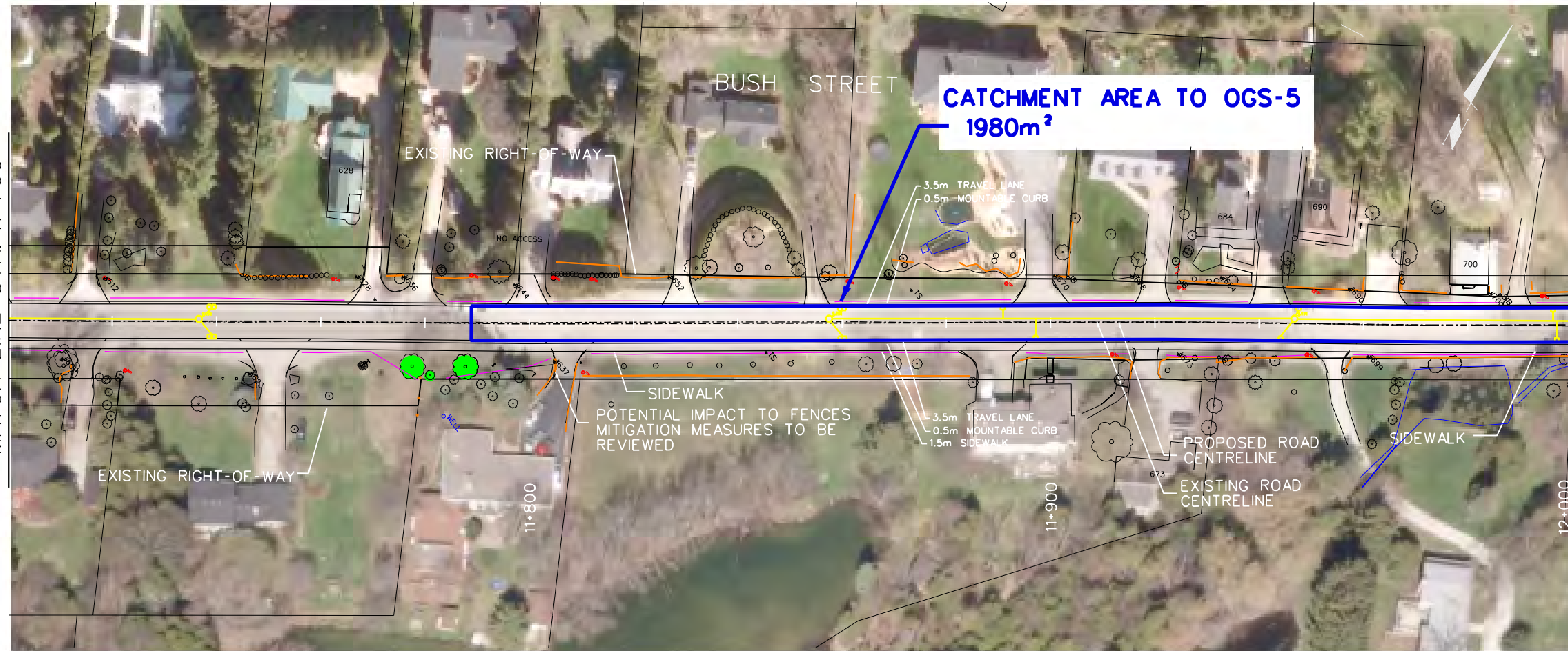
Region of Peel
Working for you

WINSTON CHURCHILL BOULEVARD
(FROM STA 44+740 TO STA 45+040)

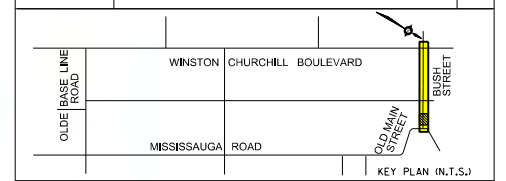
PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
ROAD CHAINAGE	Date MAY, 2014	Sheet WCB8	Plan No. -D

Appendix E
Proposed OGS System Treatment Area
OGS 5 (Bush Street 10)



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

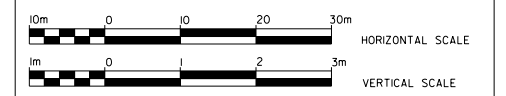
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

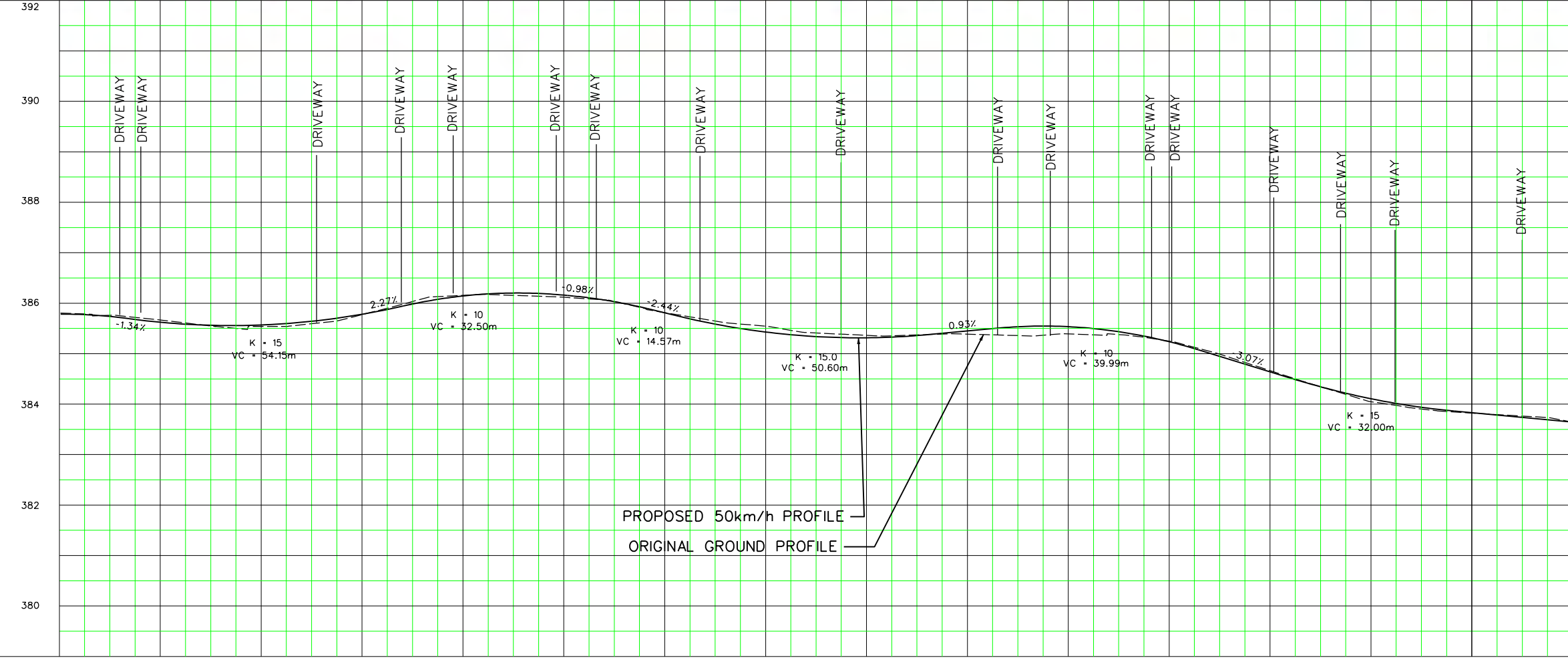
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



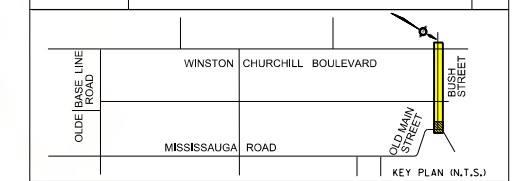
BUSH STREET
(FROM STA 11+700 TO STA 12+000)

PROPOSED OGS SYSTEM TREATMENT AREAS

CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY , 2014	Sheet BI	

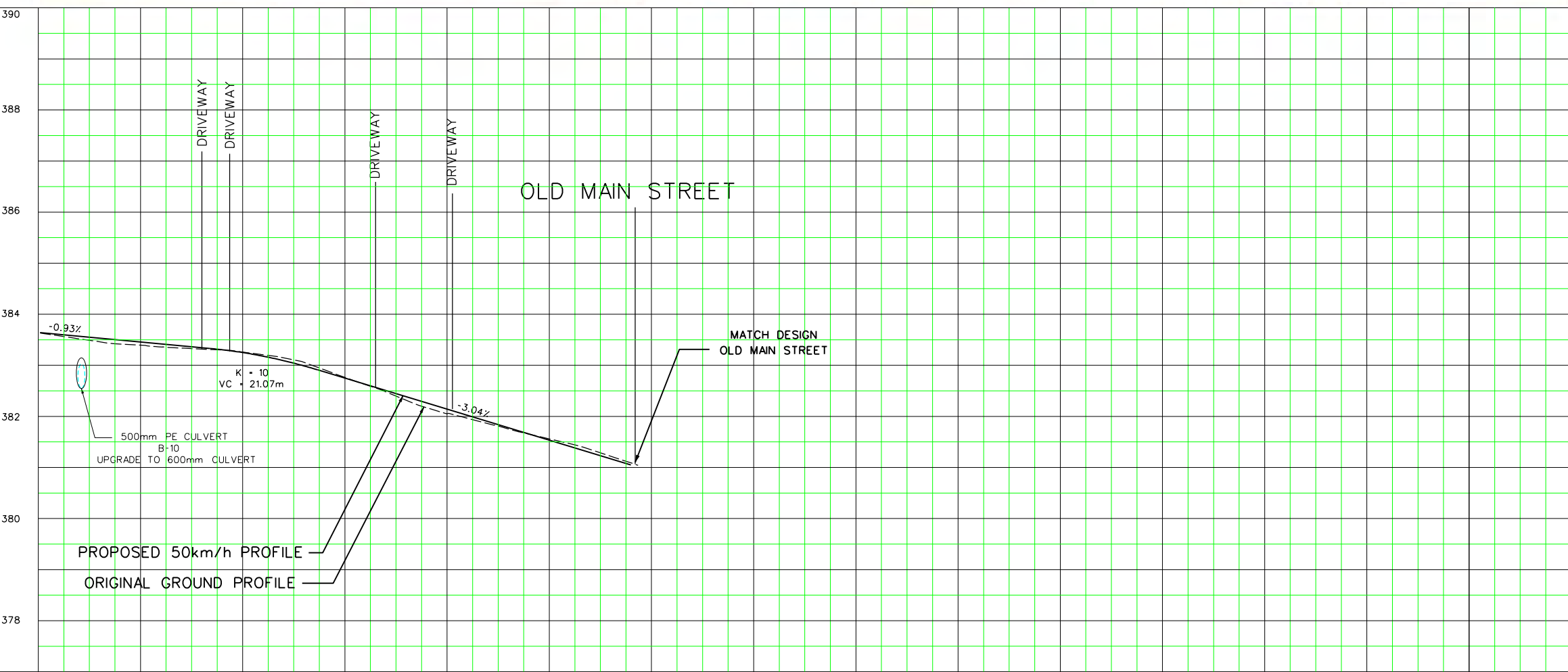
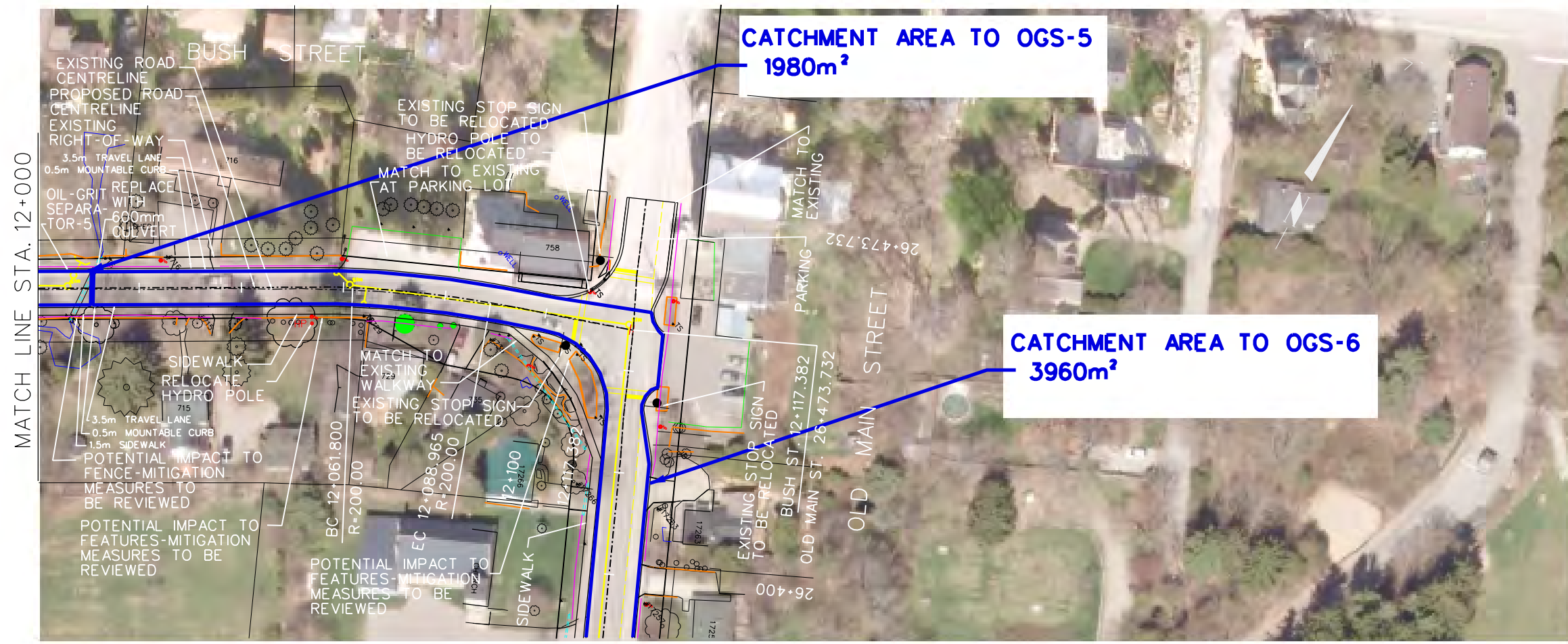


SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

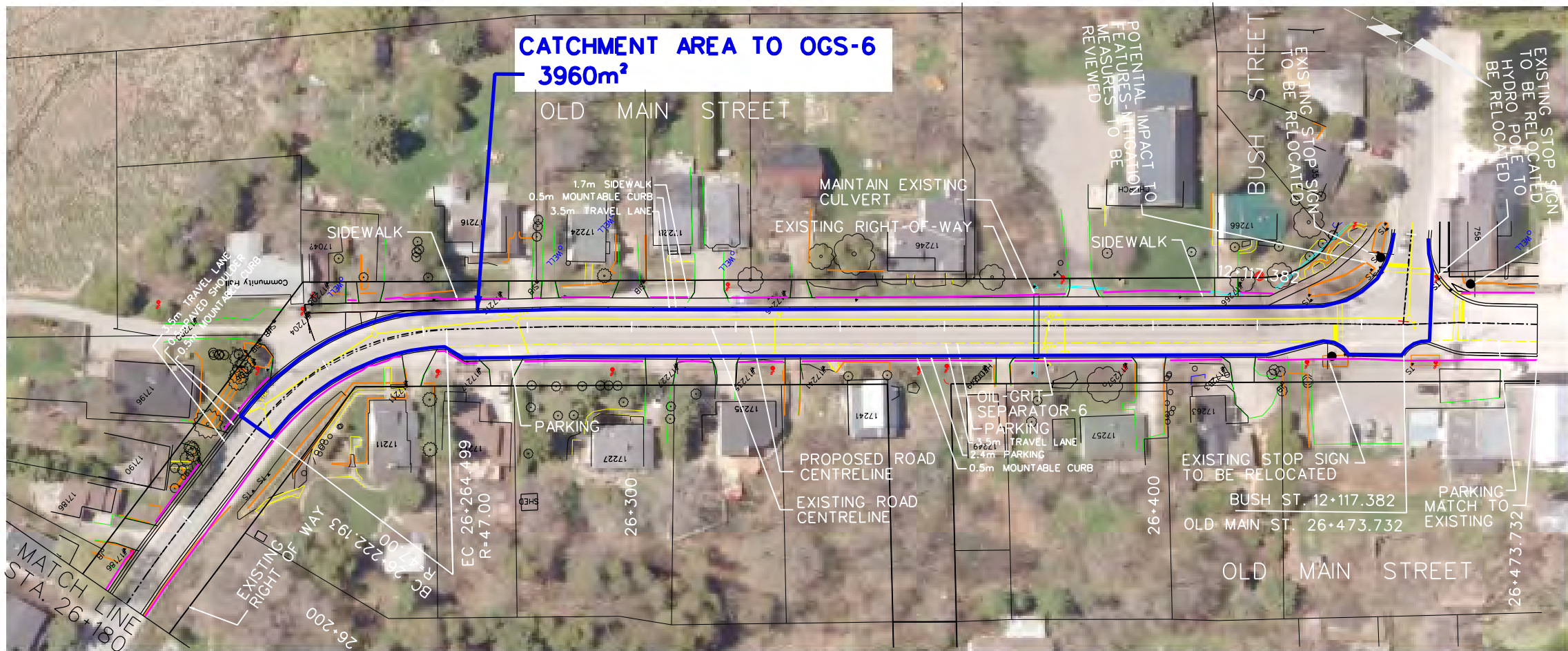
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



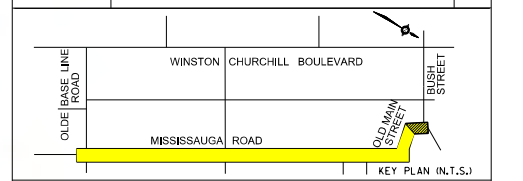
BUSH STREET
(FROM STA 12+000 TO STA 12+117)

PROPOSED OGS SYSTEM TREATMENT AREAS

Appendix F
Proposed OGS System Treatment Area
OGS 6 (Olde Main Street 14)

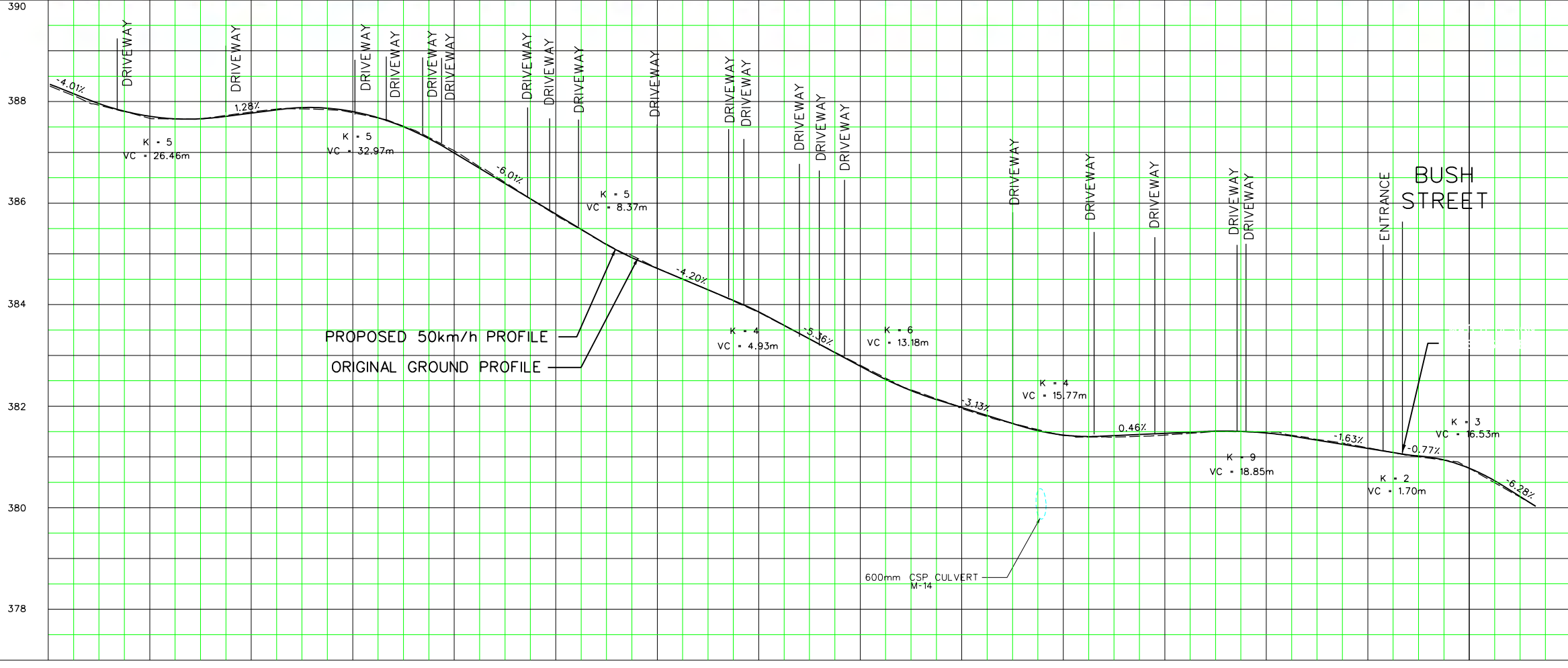


SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE CITY		
PARKS & REC.			COMMUNIC. CABLES		
ONT. CLEAN WATER					



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

- - All Driveways ASPHALT Unless Otherwise Noted.
- - All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊠ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



Region of Peel
Working for you

**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 26+180 TO STA 26+480)

PROPOSED OGS SYSTEM TREATMENT AREAS

26+200	26+300	26+400	26+480
BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
ROAD CHAINAGE	Date MAY, 2014	Sheet M10	Plan No. -D

Appendix G
Proposed OGS System Treatment Area
OGS 7 (Mississauga Rd. 44)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
INT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

NOTES

- DRIVEWAYS TO BE REGRADED AS REQUIRED
- HYDRO POLE RELOCATIONS ARE PRELIMINARY
- REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by: _____ Chkd. _____ Approved by: _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FIBROBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

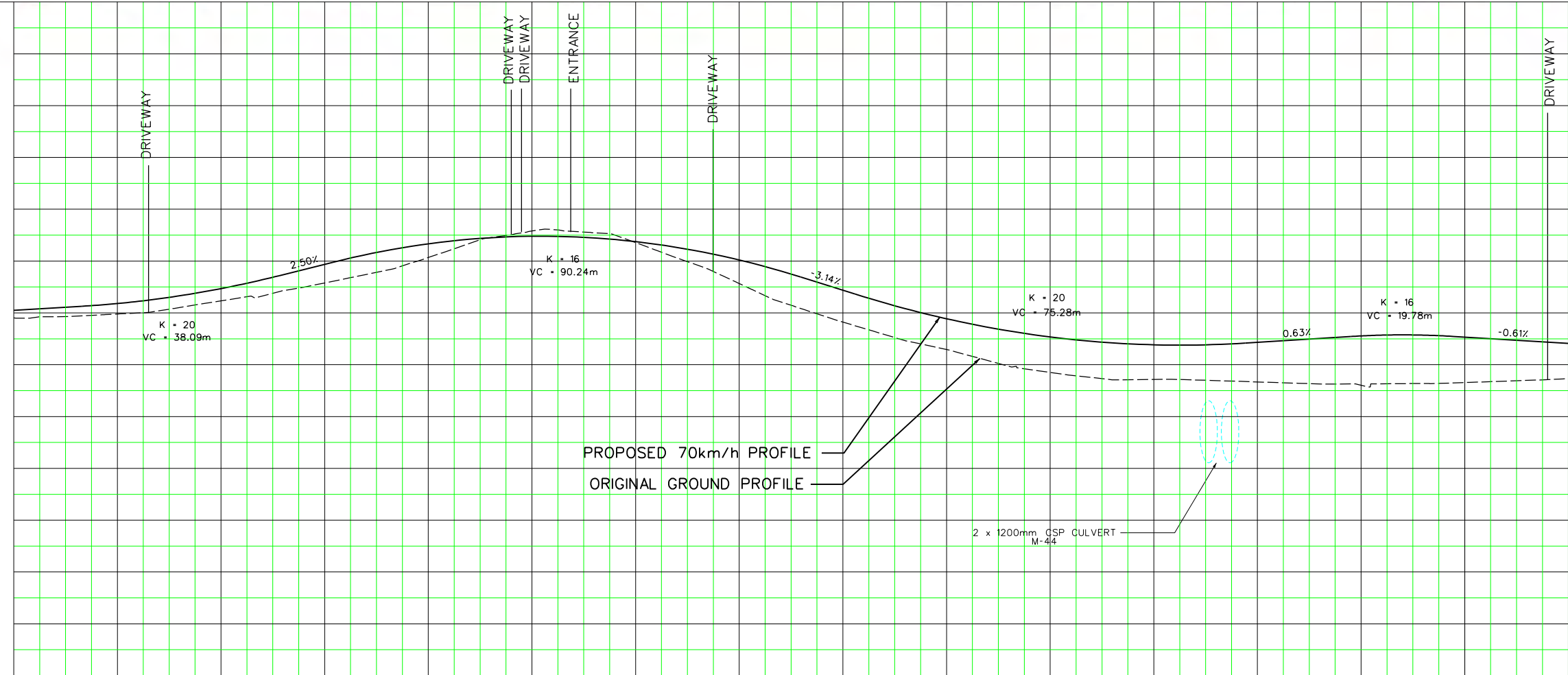
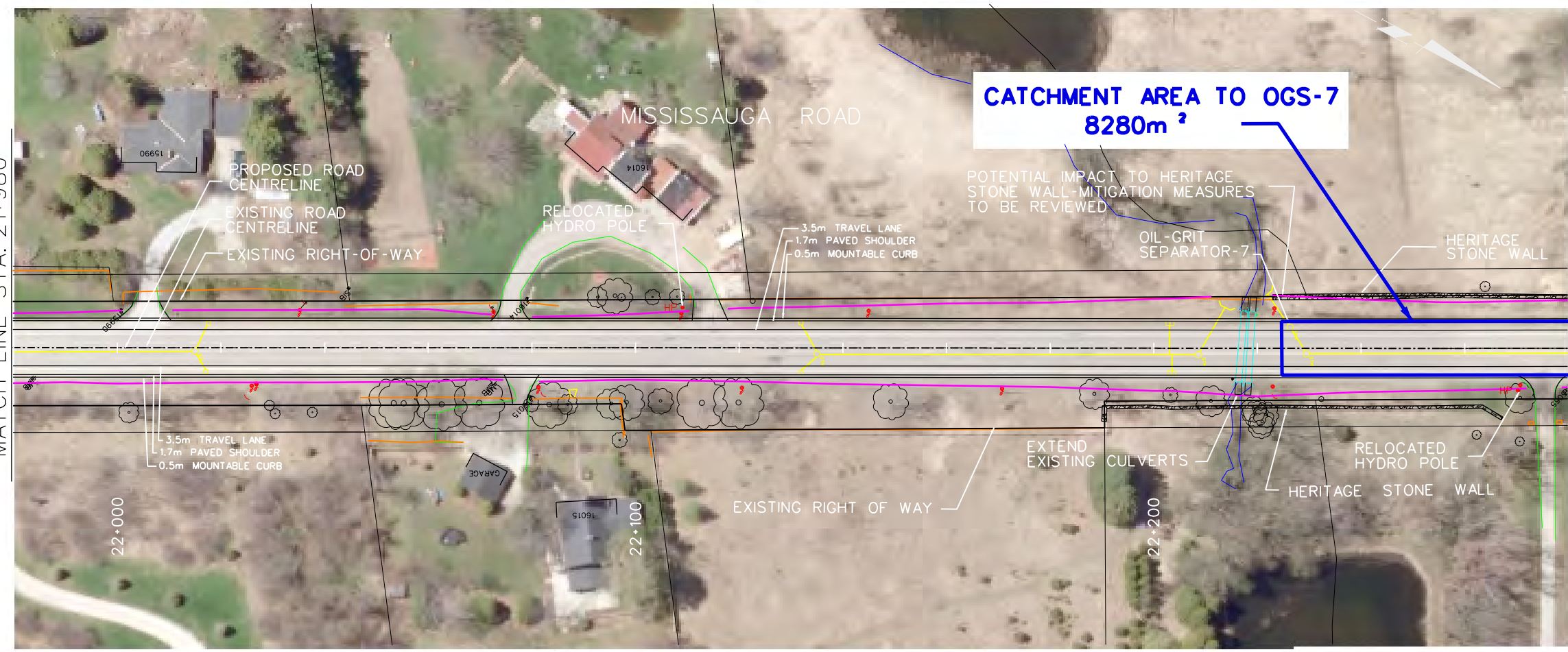
10m 0 10 20 30m HORIZONTAL SCALE
1m 0 1 2 3m VERTICAL SCALE

Region of Peel
Working for you

MISSISSAUGA ROAD/
OLD MAIN STREET
(FROM STA 21+980 to STA 22+280)

PROPOSED OGS SYSTEM TREATMENT AREAS

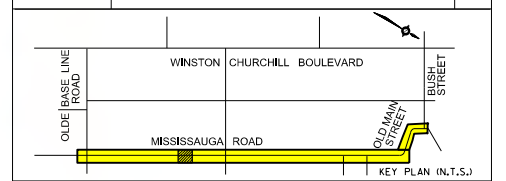
BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
ROAD CHAINAGE	Date MAY, 2014	Sheet M6	Plan No. -D



22+000	22+100	22+200
--------	--------	--------

CATCHMENT AREA TO OGS-7
8280m²

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

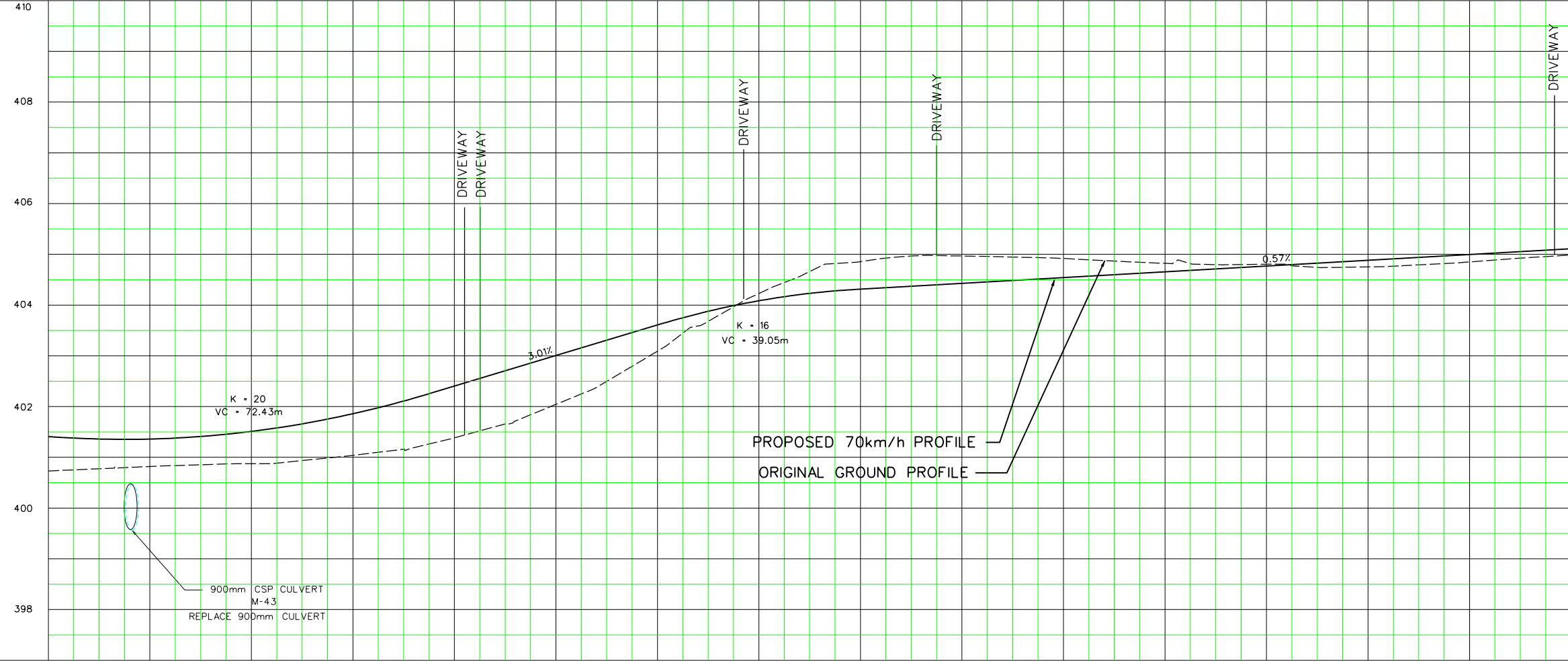
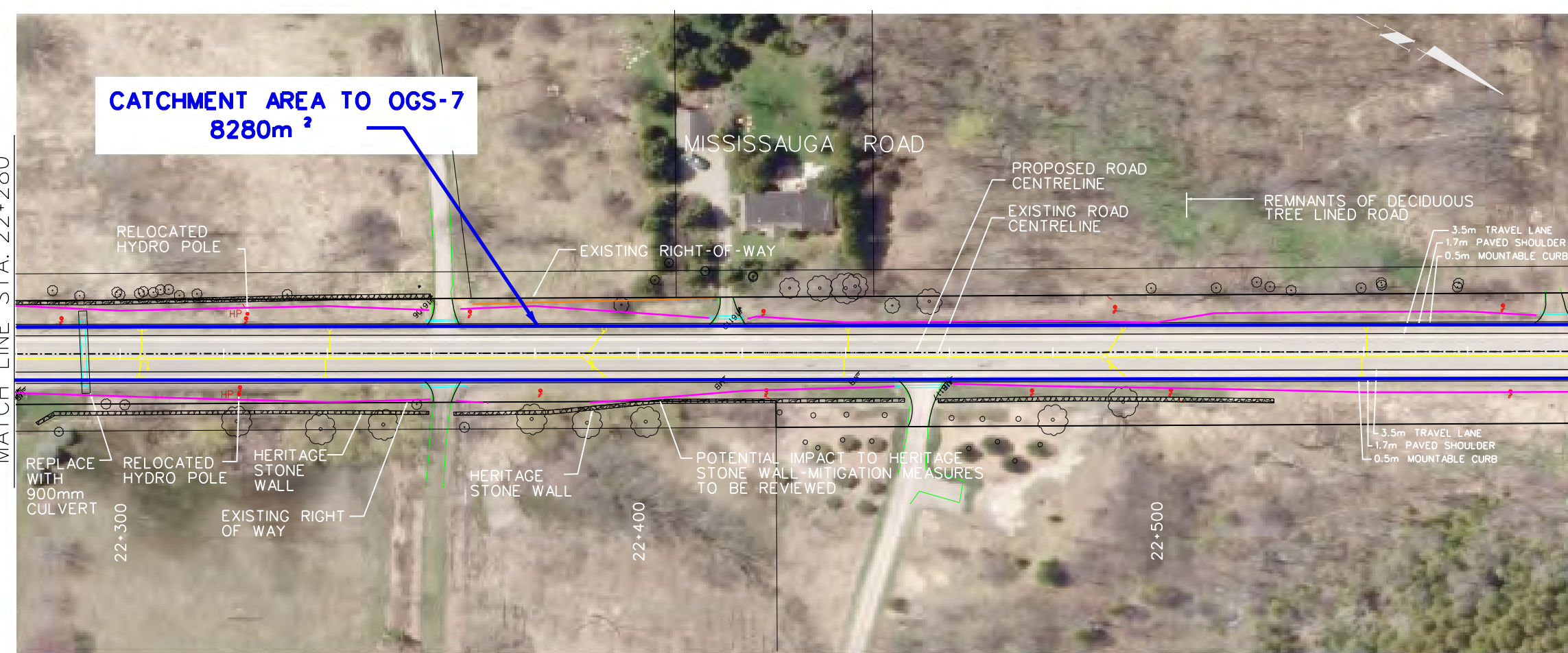


- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

MATCH LINE STA. 22+280

MATCH LINE STA. 22+580



General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
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- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SANI)

B.M. No. Elev.

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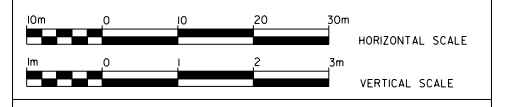
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



MISSISSAUGA ROAD/ OLD MAIN STREET
(FROM STA 22+280 TO STA 22+580)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
ROAD CHAINAGE	Date MAY, 2014	Sheet M7	Plan No. -D

22+300

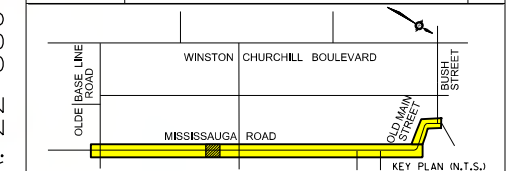
22+400

22+500

**CATCHMENT AREA TO OGS-7
8280m²**

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CITY		
INT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

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B.M. No. Elev.

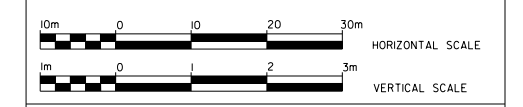
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Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR

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CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



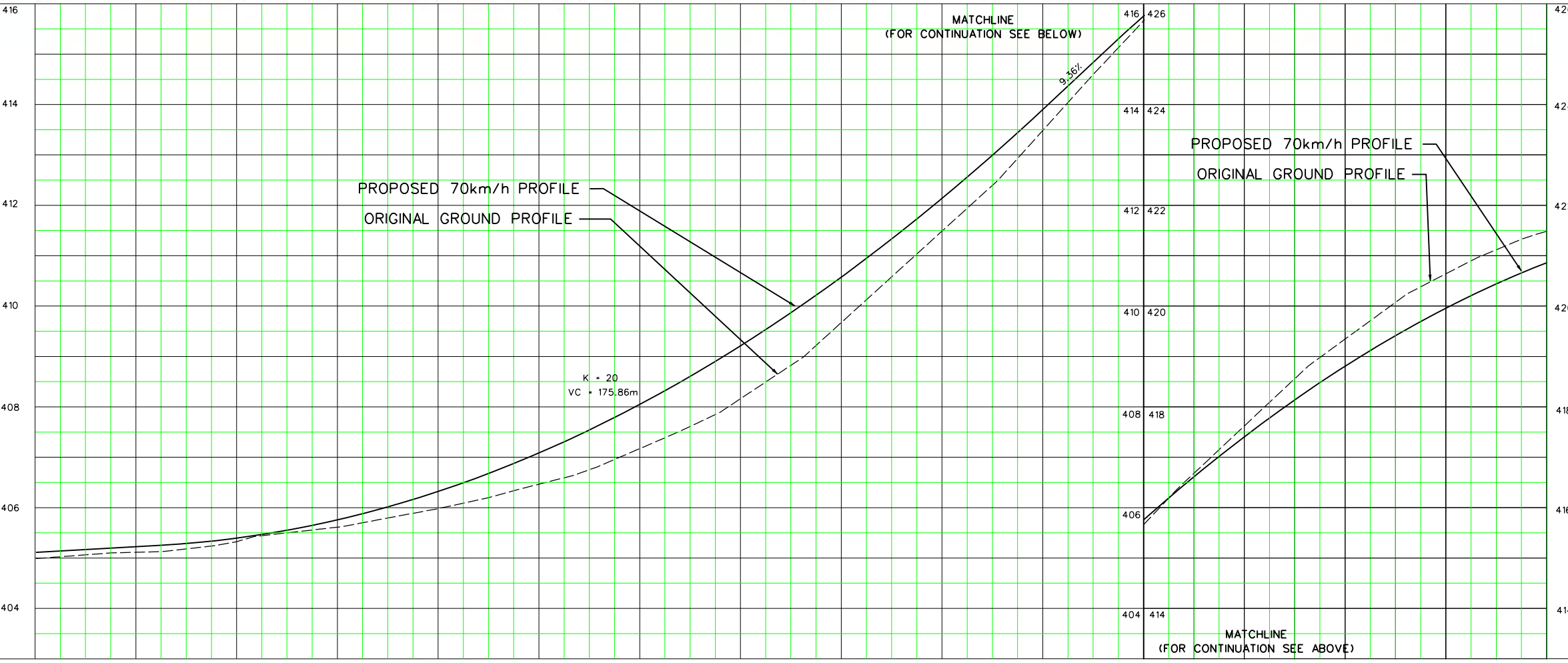
Region of Peel
Working for you

**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 22+580 to STA 22+880)

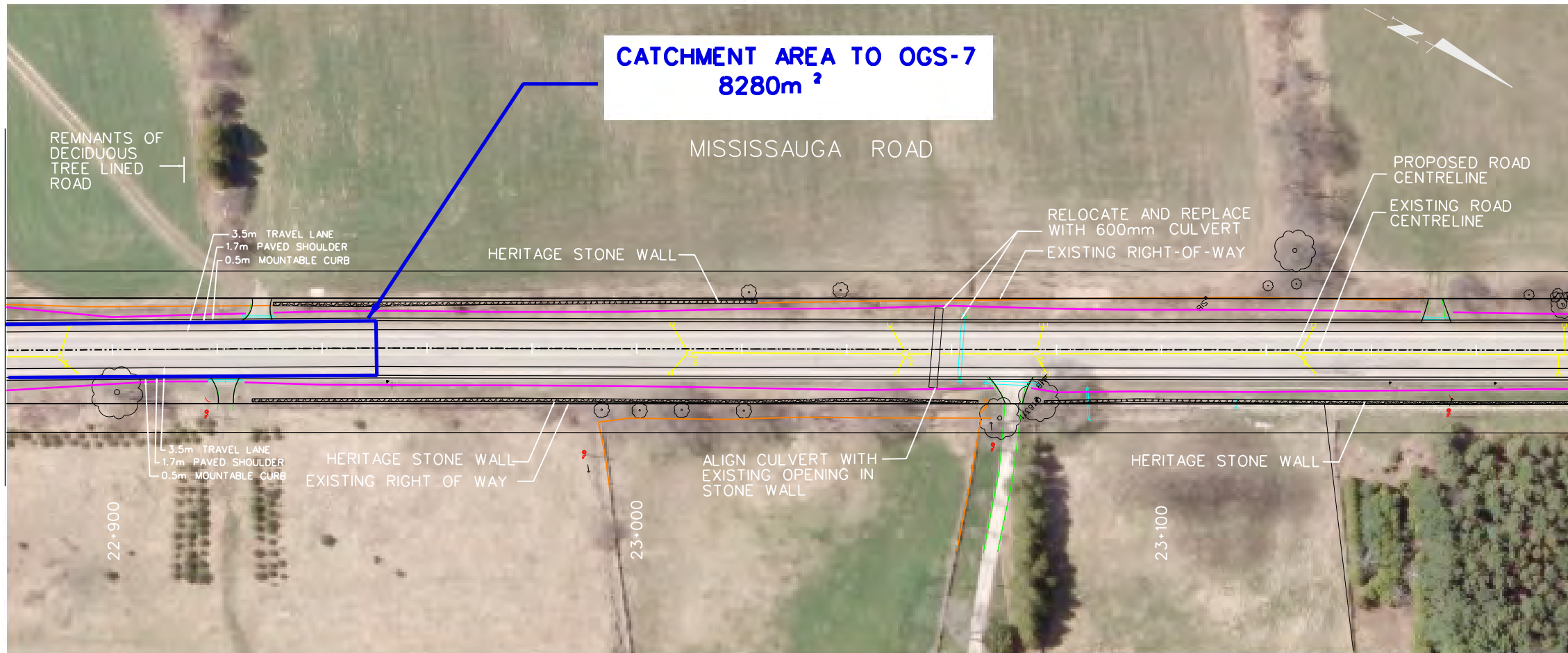
PROPOSED OGS SYSTEM TREATMENT AREAS			
BOT. EL. OF WM.	CAD Area	Area x-x	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet M8	-D

MATCH LINE STA. 22+580

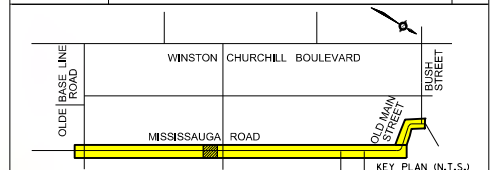
MATCH LINE STA. 22+880



22+600	22+700	22+800
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SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- Denotes Building - Not Located
- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

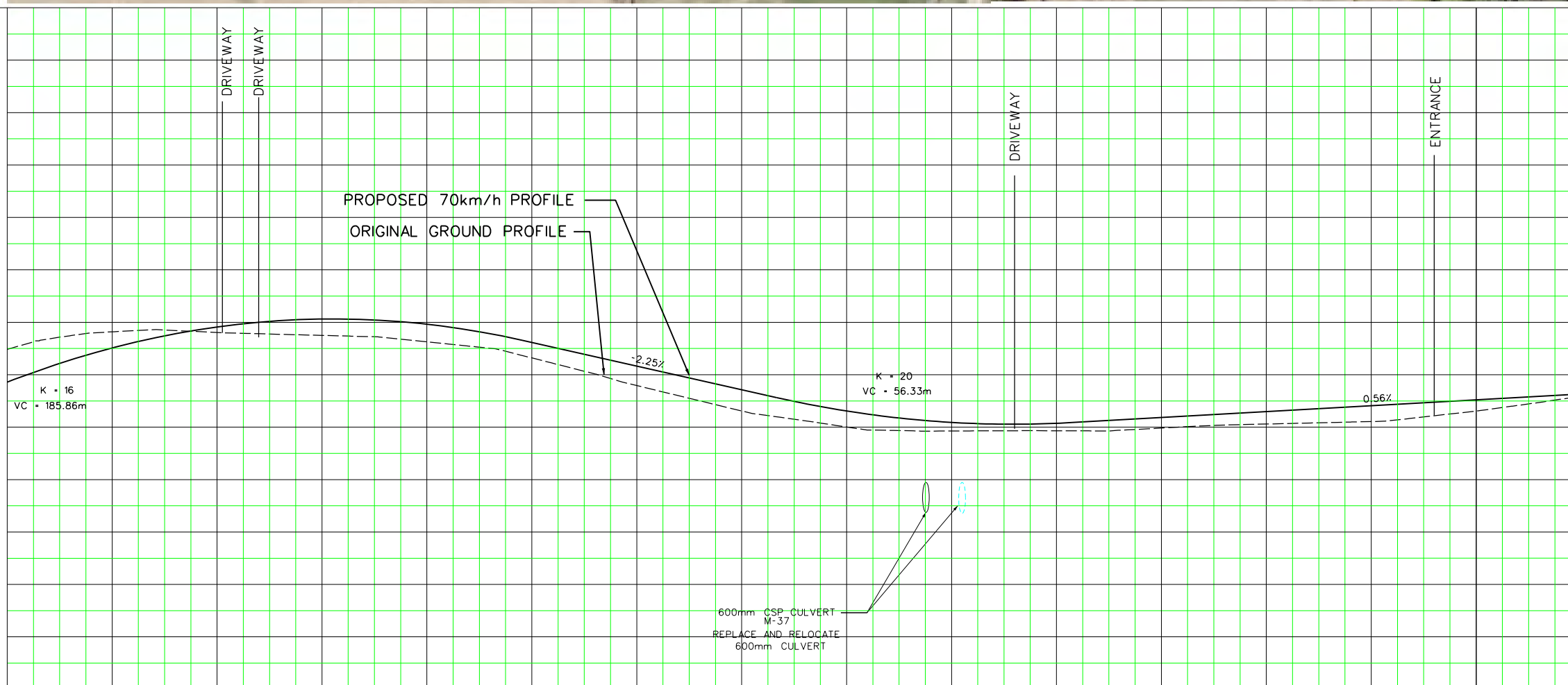


Region of Peel
Working for you

**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 22+880 to STA 23+180)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area x-x	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
ROAD CHAINAGE	Date MAY, 2014	Sheet M9	Plan No. -D

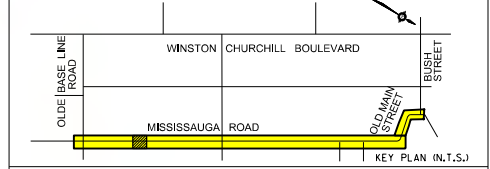


22+900	23+000	23+100
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Appendix H
Proposed OGS System Treatment Area
OGS 8 (Mississauga Rd. 48)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMAINS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

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- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by: Cnkd. Approved by: _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

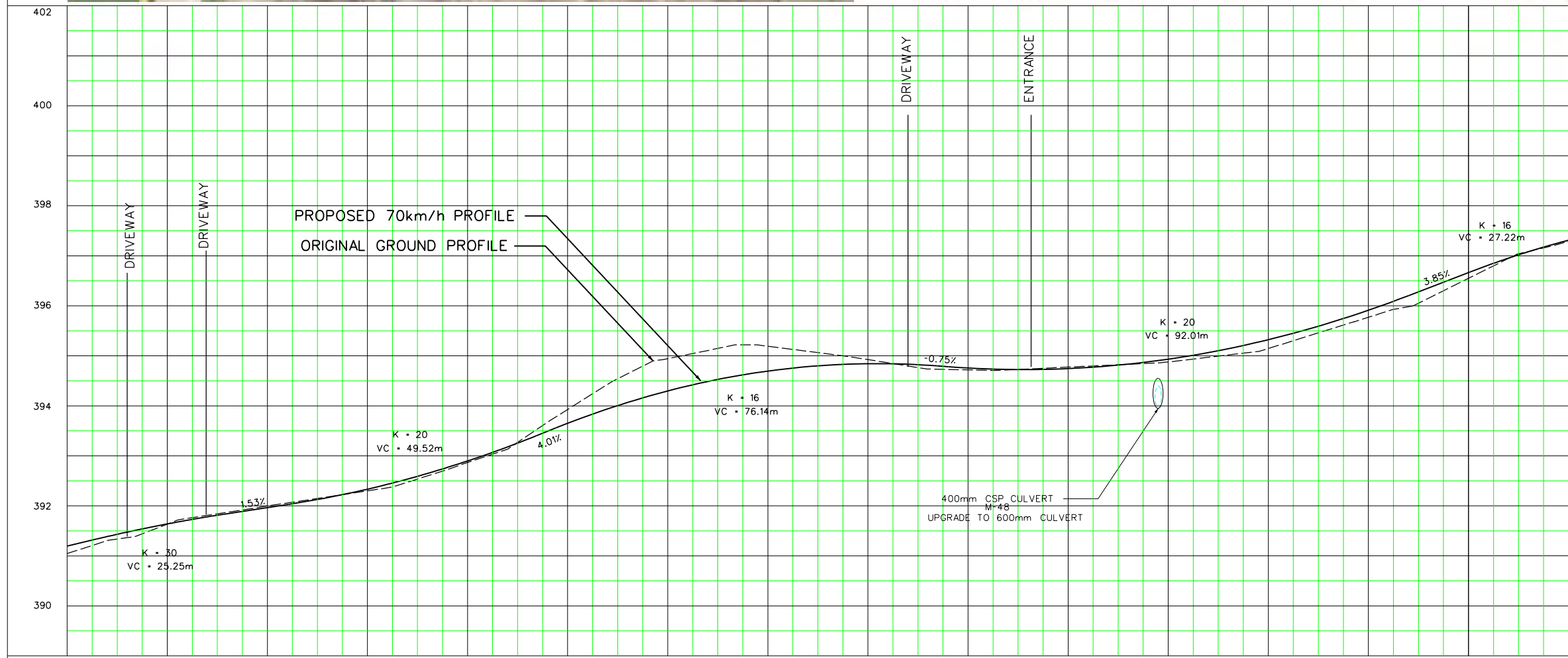
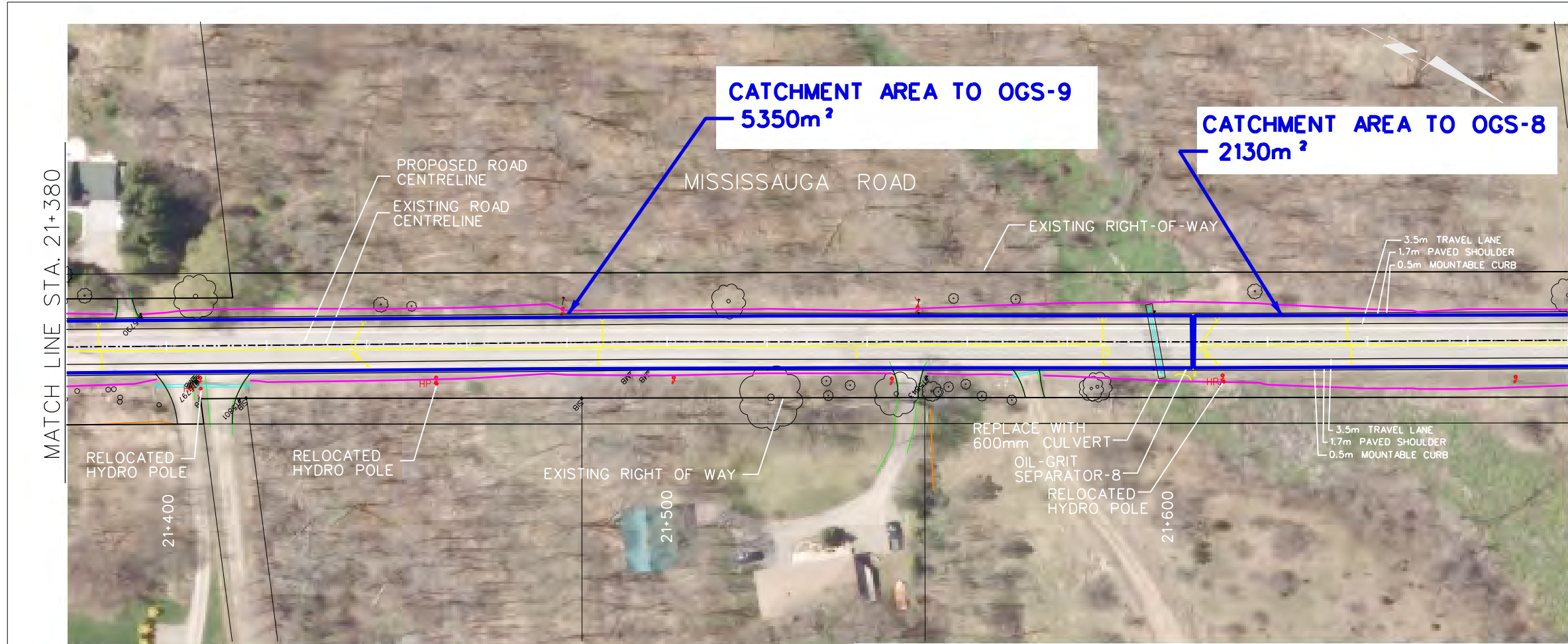


Region of Peel
Working for you

MISSISSAUGA ROAD/
OLD MAIN STREET
(FROM STA 21+380 to STA 21+680)

PROPOSED OGS SYSTEM TREATMENT AREAS

CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet M4	



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
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- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

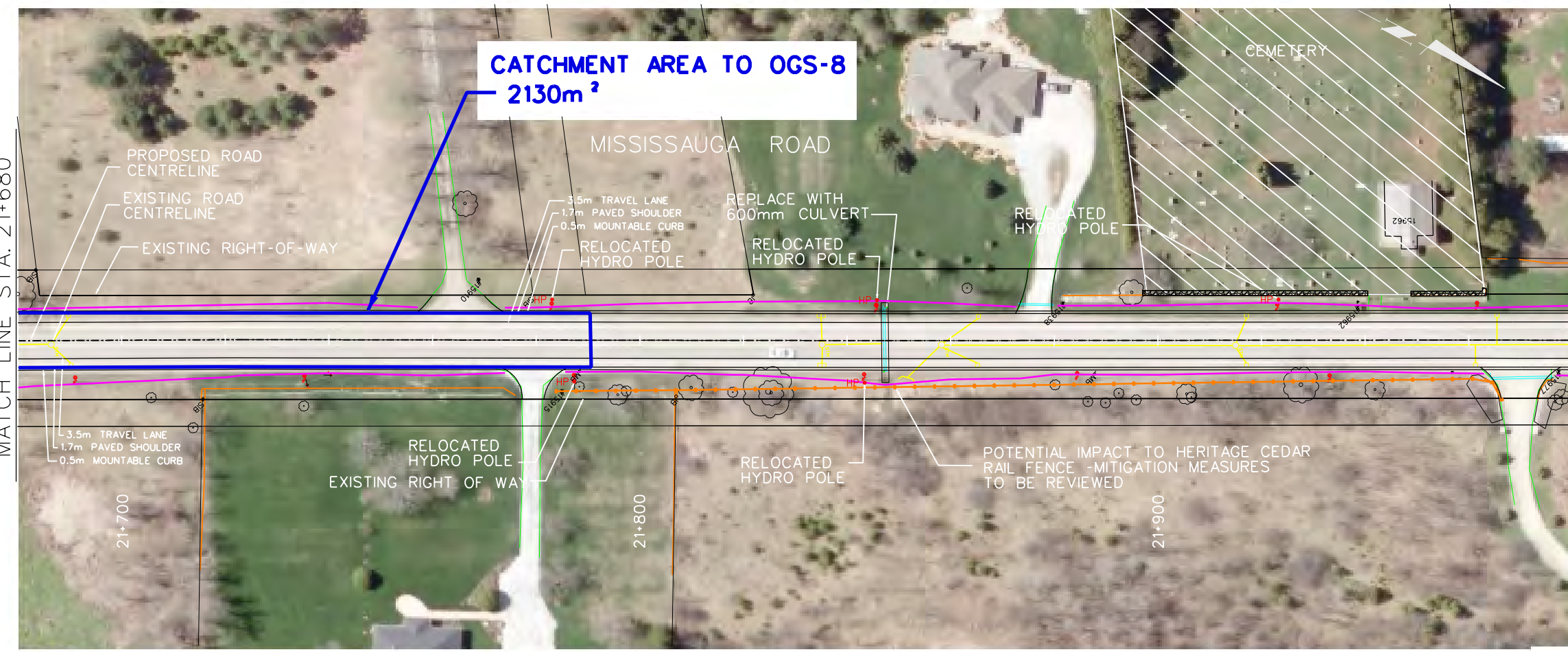
10m 0 10 20 30m HORIZONTAL SCALE
1m 0 1 2 3m VERTICAL SCALE

Region of Peel
Working for you

**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 21+680 TO STA 21+980)

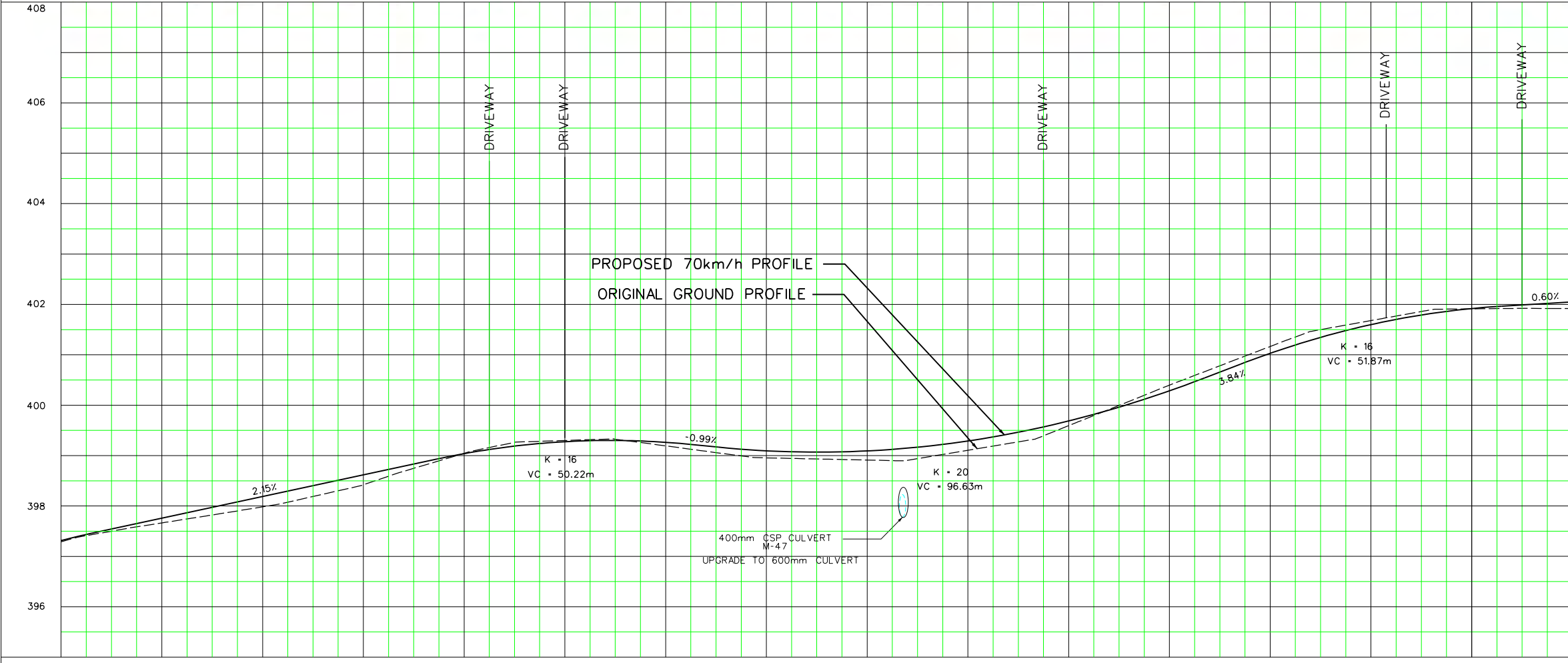
PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	Plan No.
ROAD CHAINAGE	Date MAY, 2014	Sheet M5	Page No. -D



MATCH LINE STA. 21+680

MATCH LINE STA. 21+980

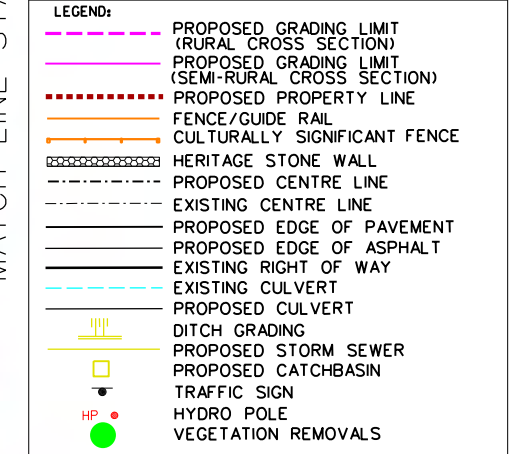


21+700	21+800	21+900
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Appendix I
Proposed OGS System Treatment Area
OGS 9 (Mississauga Rd. 55)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CITY		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
1. DRIVEWAYS TO BE REGRADED AS REQUIRED
 2. HYDRO POLE RELOCATIONS ARE PRELIMINARY
 3. REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SANI)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by: _____ Chkd. _____

Approved by: _____

NOTICE TO CONTRACTOR

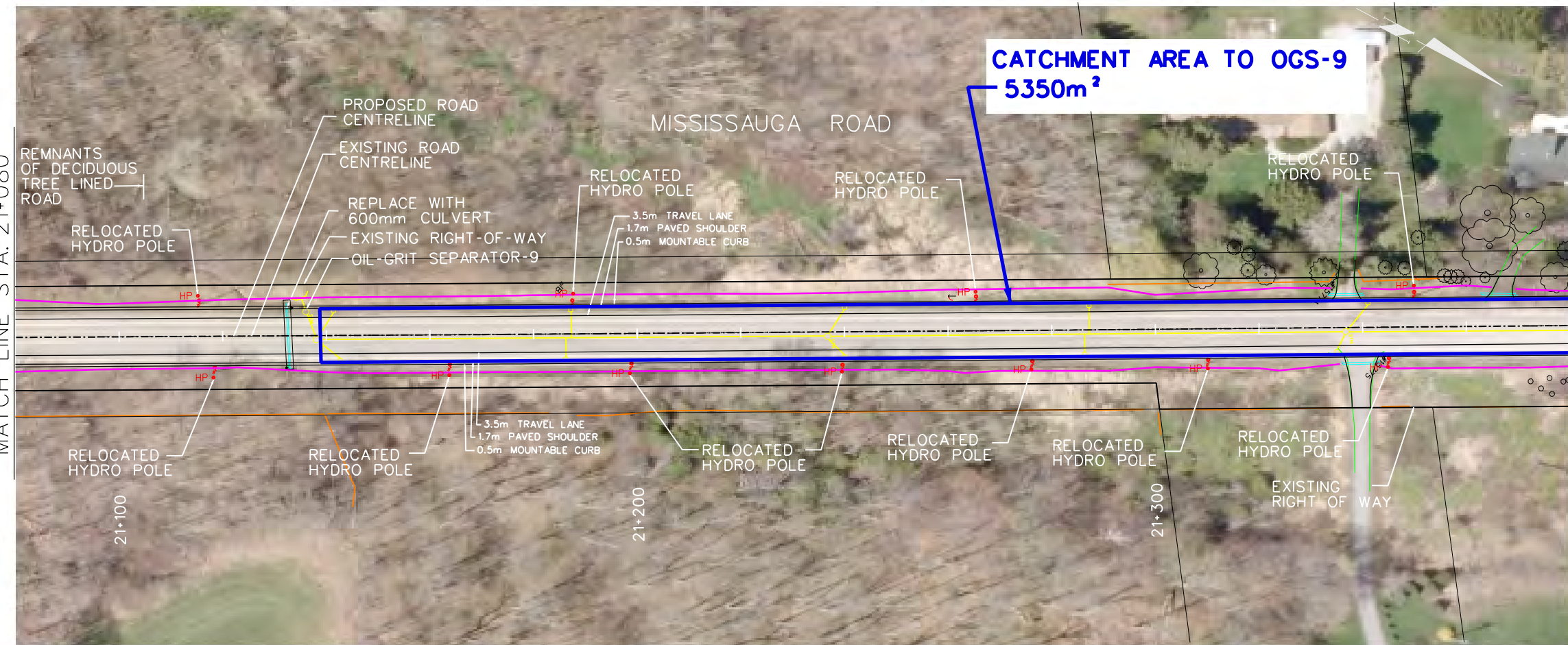
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



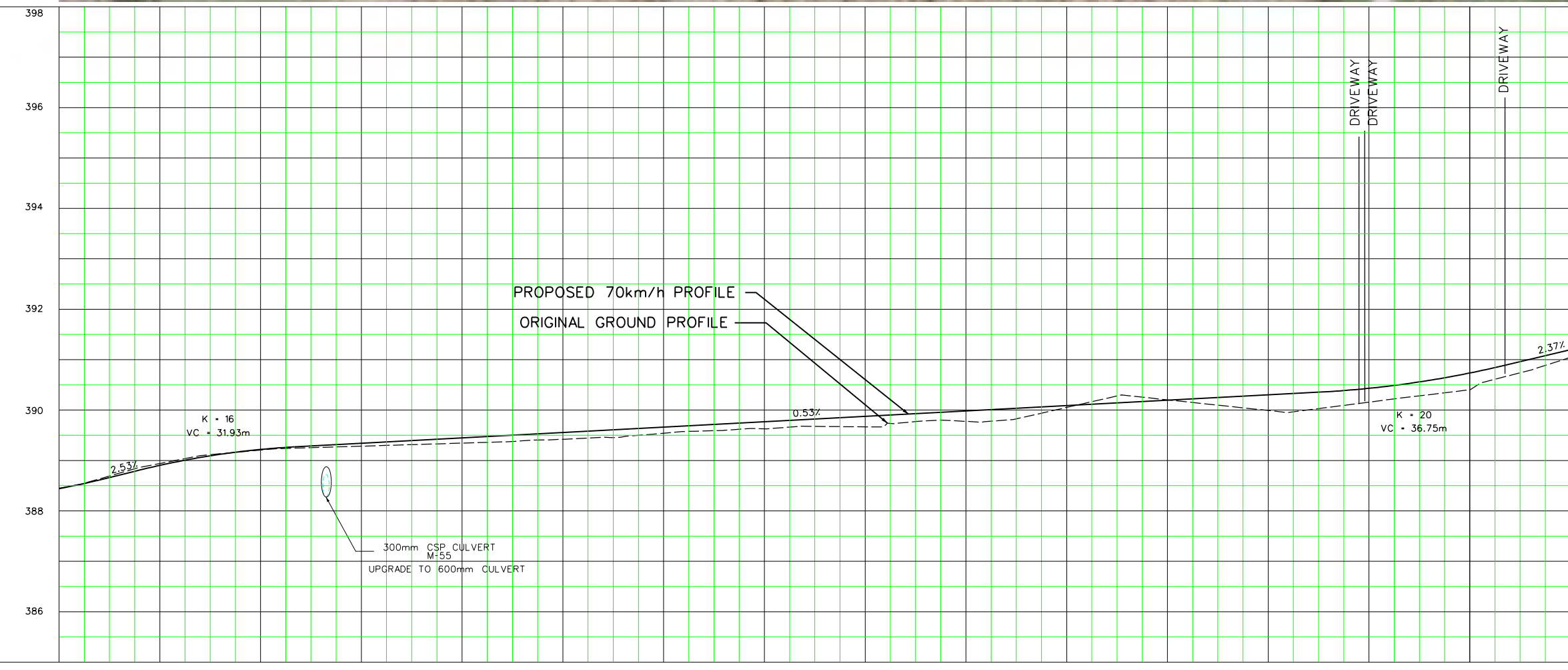
**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 21+080 TO STA 21+380)

PROPOSED OGS SYSTEM TREATMENT AREAS		
BOT. EL. OF WM.	CAD Area	Area X-X
EX. ROAD ELEV.	Checked by	Drawn by JM
ROAD CHAINAGE	Date MAY, 2014	Sheet M3
		Project No. XX-XXX
		Plan No. -D



MATCH LINE STA. 21+080

MATCH LINE STA. 21+380



21+100	21+200	21+300
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SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HP • HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

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- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

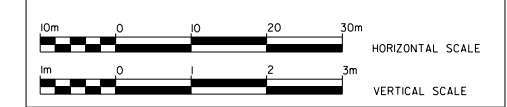
The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by: Cnk. Approved by:

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

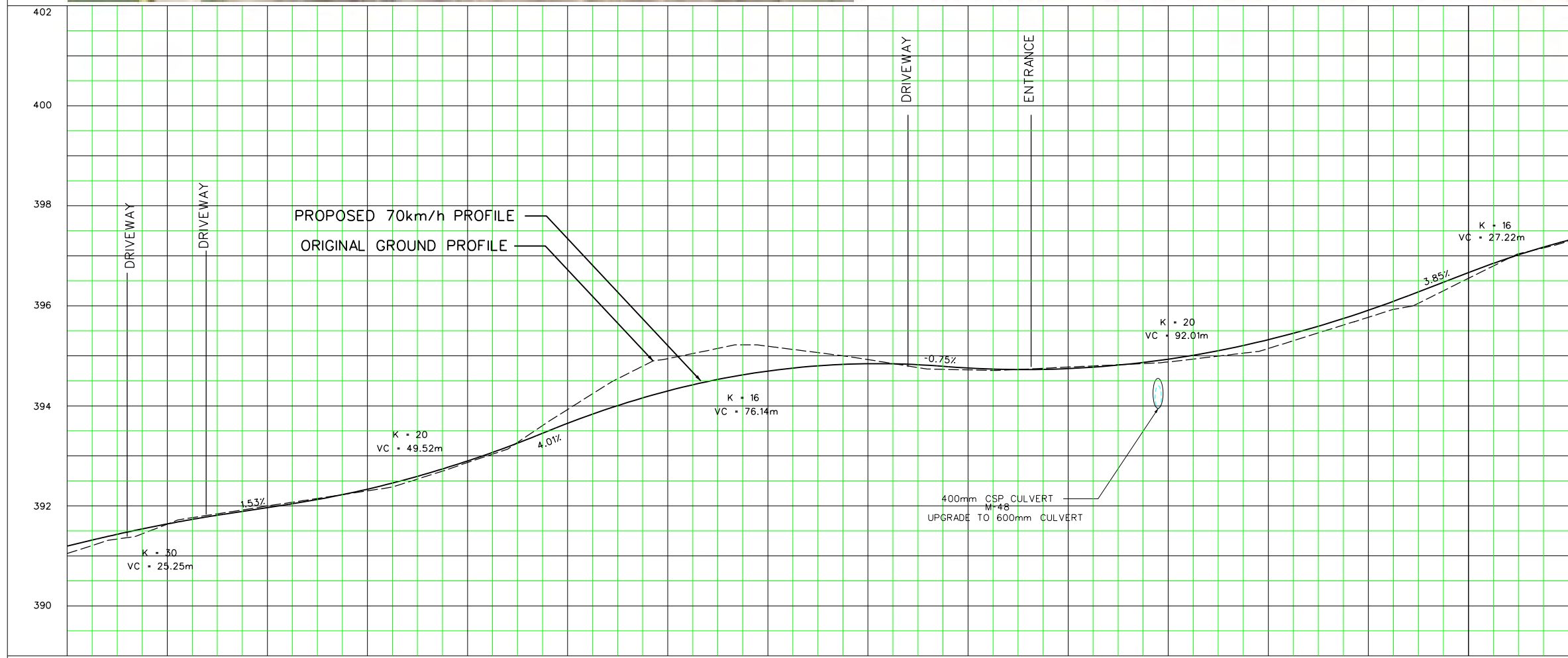
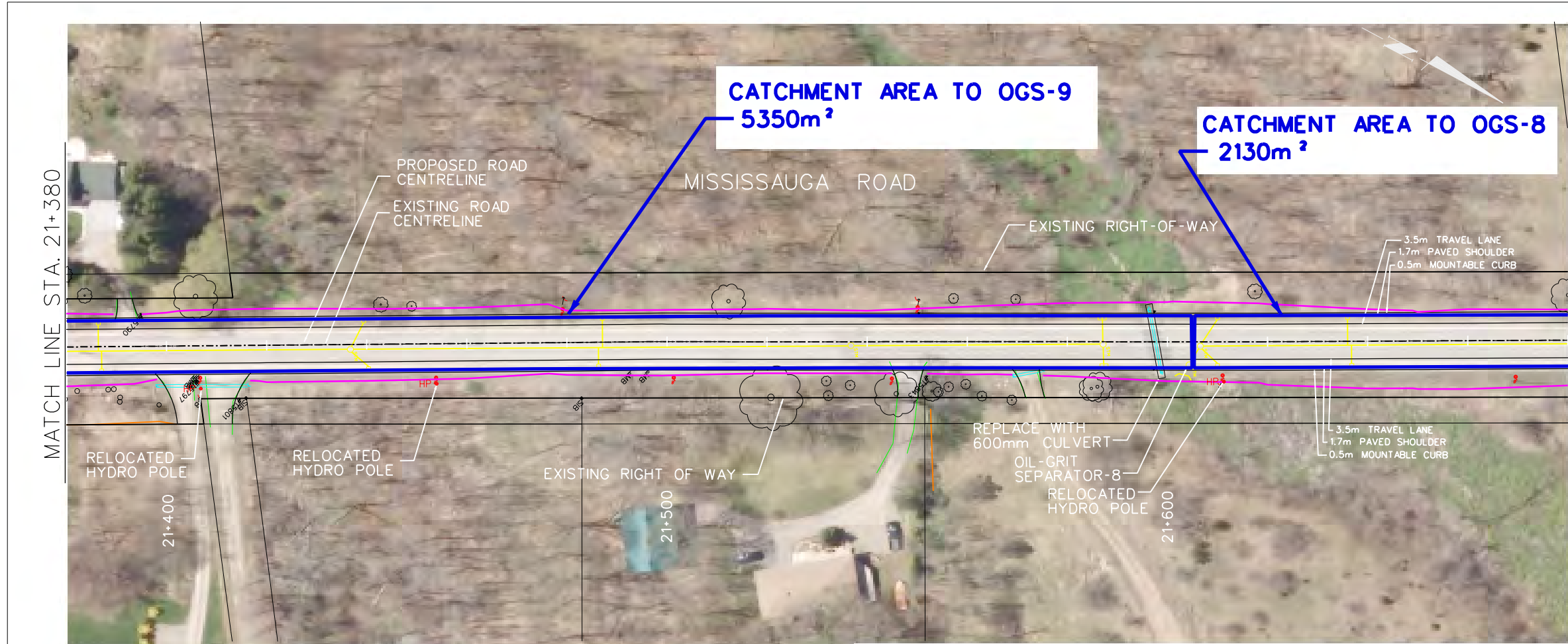


Region of Peel
Working for you

MISSISSAUGA ROAD/
OLD MAIN STREET
(FROM STA 21+380 to STA 21+680)

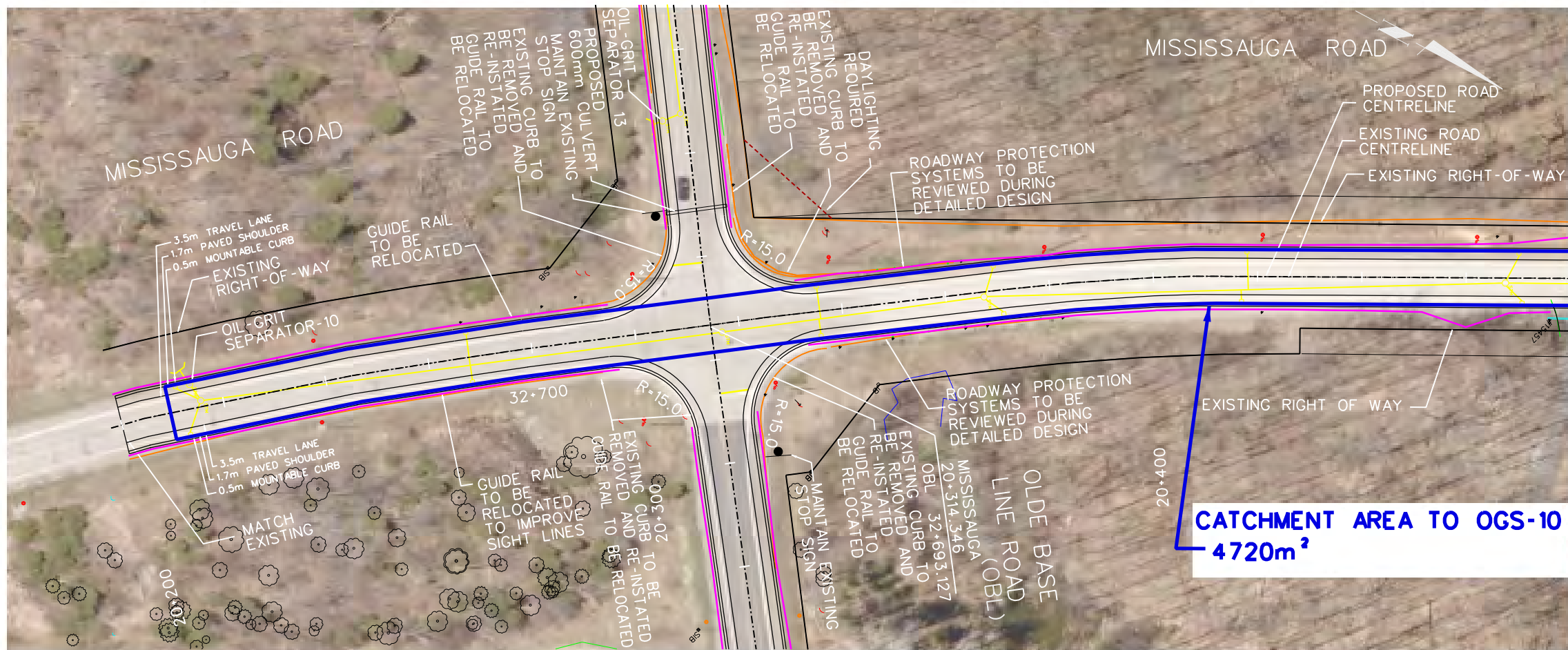
PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM. EX. ROAD ELEV.	CAD Area	Area x-x	Project No. XX-XXX
ROAD CHAINAGE	Checked by	Drawn by JM	Plan No.
	Date MAY, 2014	Sheet M4	- D

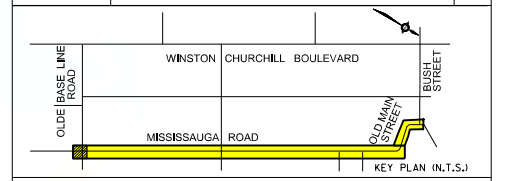


21+400	21+500	21+600
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Appendix J
Proposed OGS System Treatment Area
OGS 10 (Mississauga Rd.)



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

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- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

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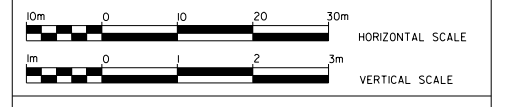
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
TOWN OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
BELL CANADA	HYDRO ONE TELECOM
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ROGERS CABLE
ONTARIO MINISTRY OF TRANSPORTATION	ALLSTREAM
ONTARIO CLEAN WATER AGENCY	PSN (PUBLIC SECTOR NETWORK)
HYDRO ONE NETWORKS	FUTUREWAY (FIBROBAND)
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

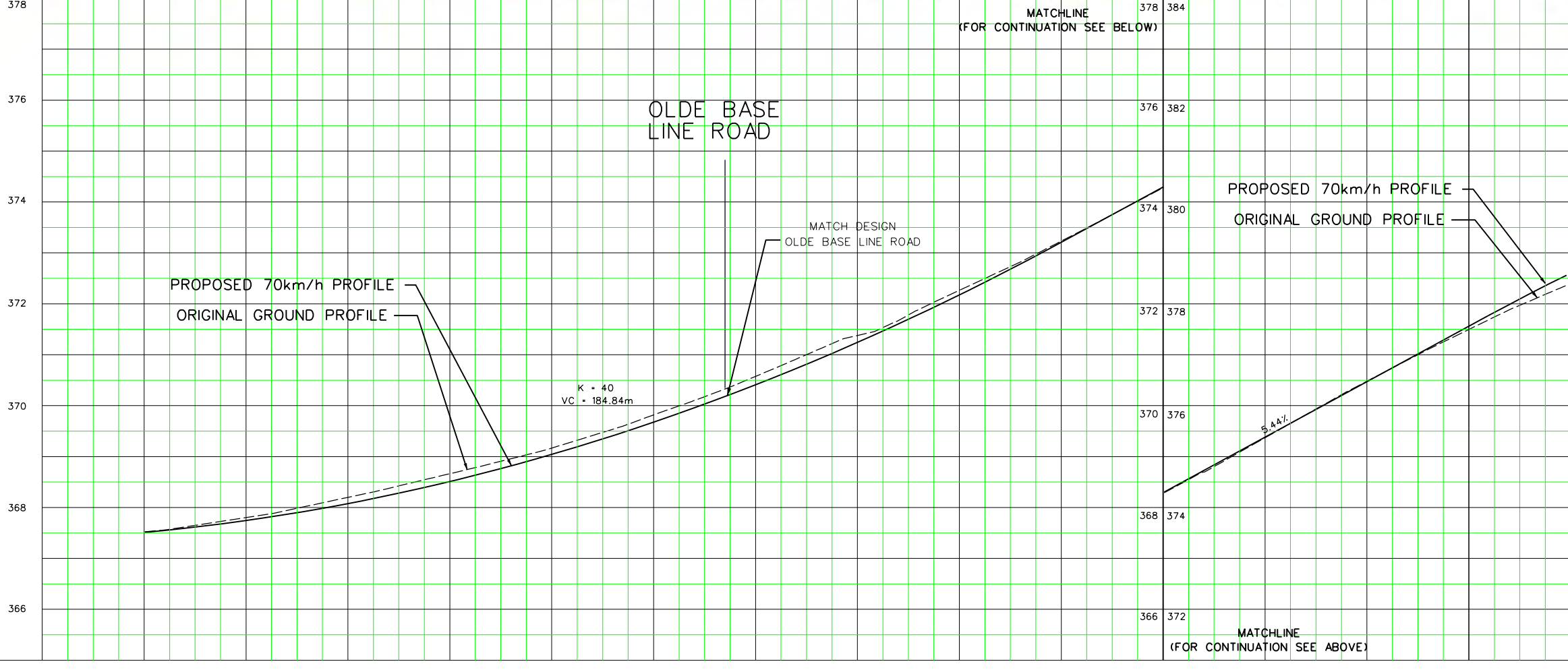


Region of Peel
Working for you

MISSISSAUGA ROAD/
OLD MAIN STREET
(FROM STA 20+200 TO STA 20+480)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM. EX. ROAD ELEV.	CAD Area	Area X-X	Project No. XX-XXX
ROAD CHAINAGE	Checked by	Drawn by JM	Plan No. -D
	Date MAY, 2014	Sheet MI	



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
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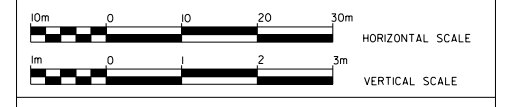
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

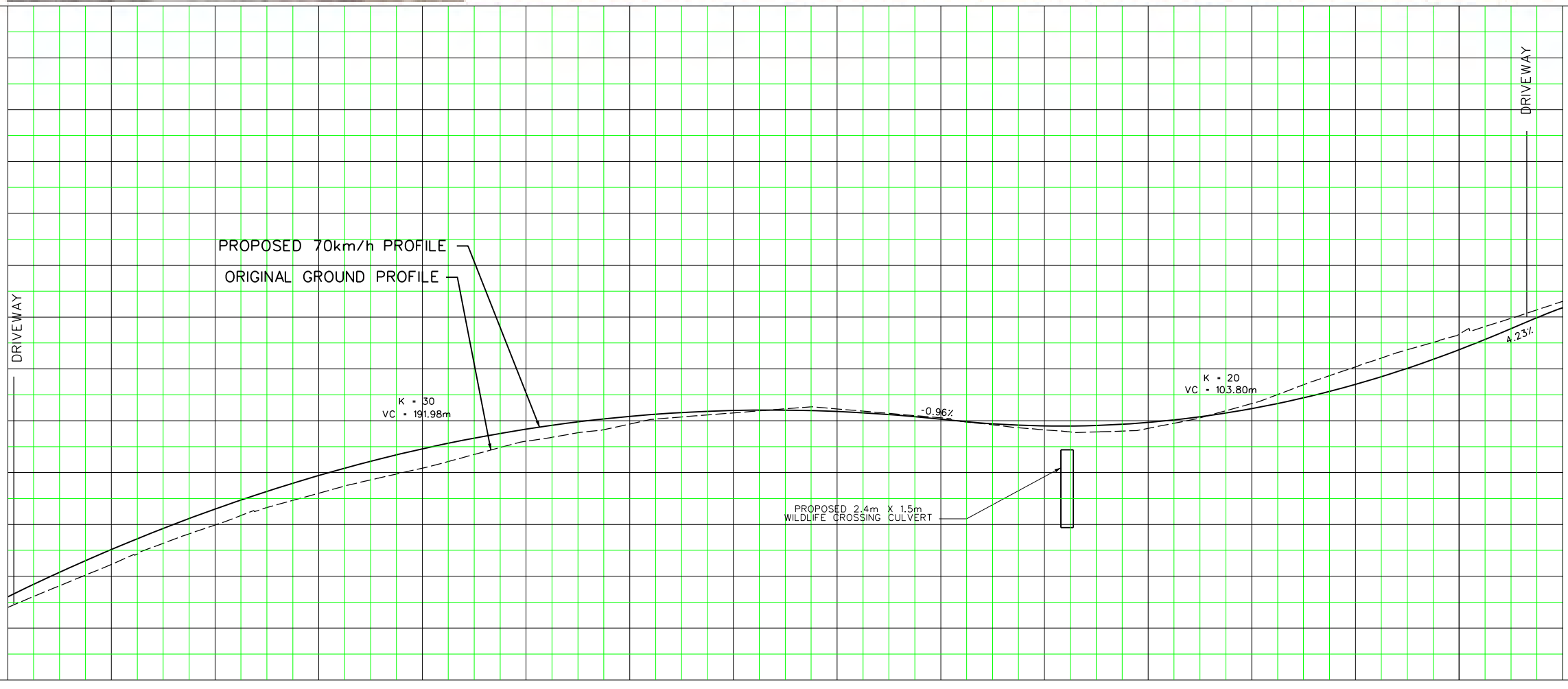
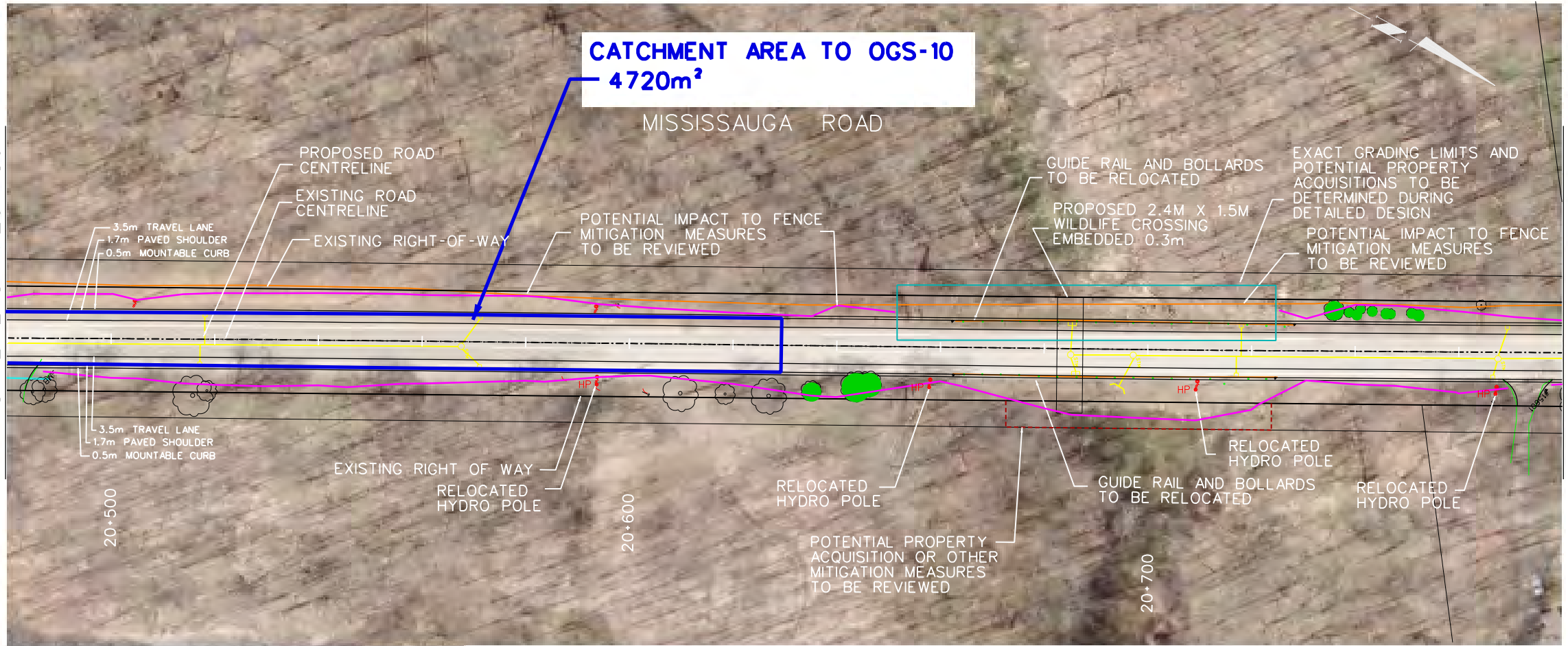
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS:	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



**MISSISSAUGA ROAD/
OLD MAIN STREET**
(FROM STA 20+480 to STA 20+780)

PROPOSED OGS SYSTEM TREATMENT AREAS		
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Sheet M2
Date MAY, 2014	Sheet M2	Plan No. -D



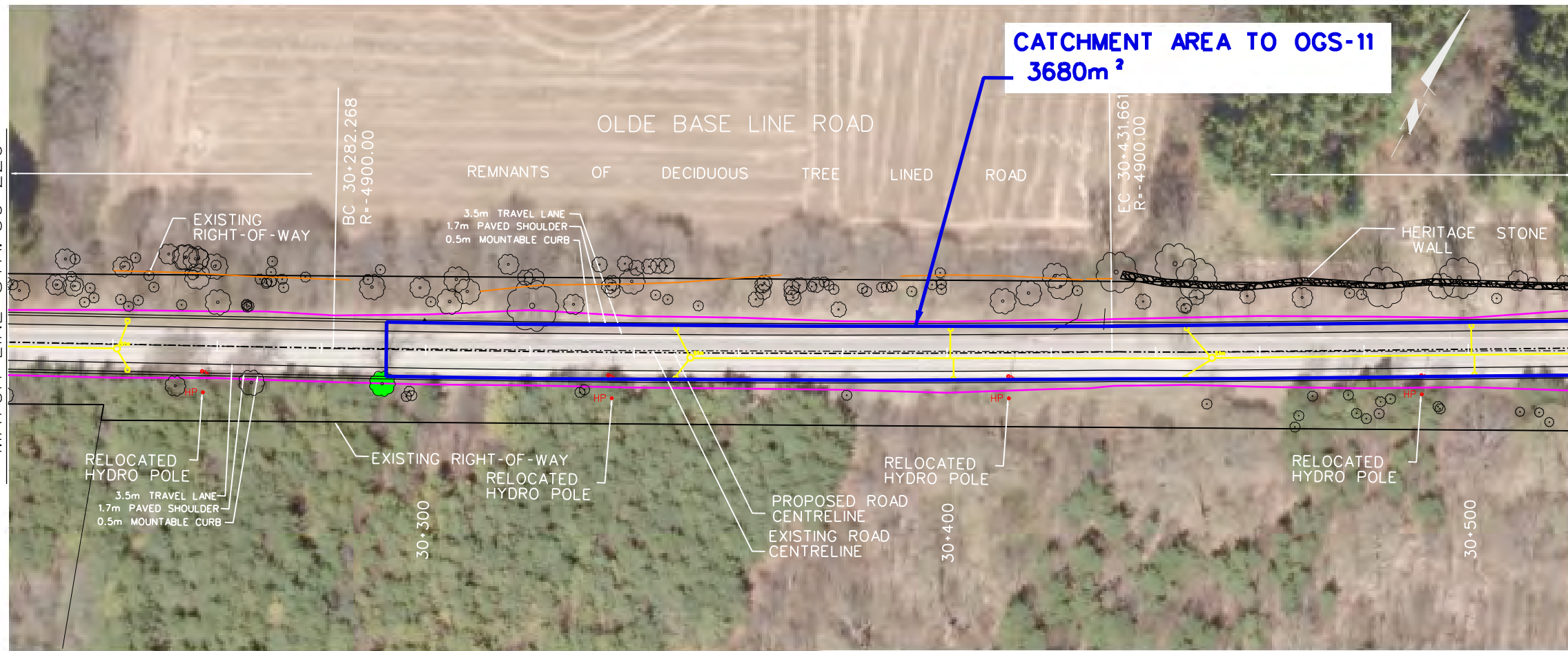
ROAD CHAINAGE	
20+500	20+700

BOT. EL. OF WM.
EX. ROAD ELEV.
ROAD CHAINAGE

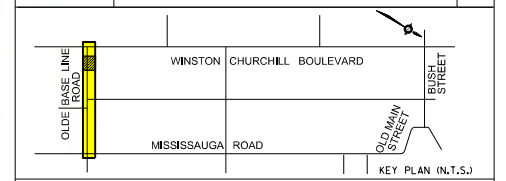
Appendix K
Proposed OGS System Treatment Area
OGS 11 (OBL-02)

MATCH LINE STA. 30+220

MATCH LINE STA. 30+520



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERS MAINS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- Denotes Building - Not Located
- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

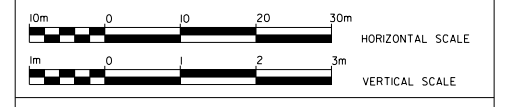
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

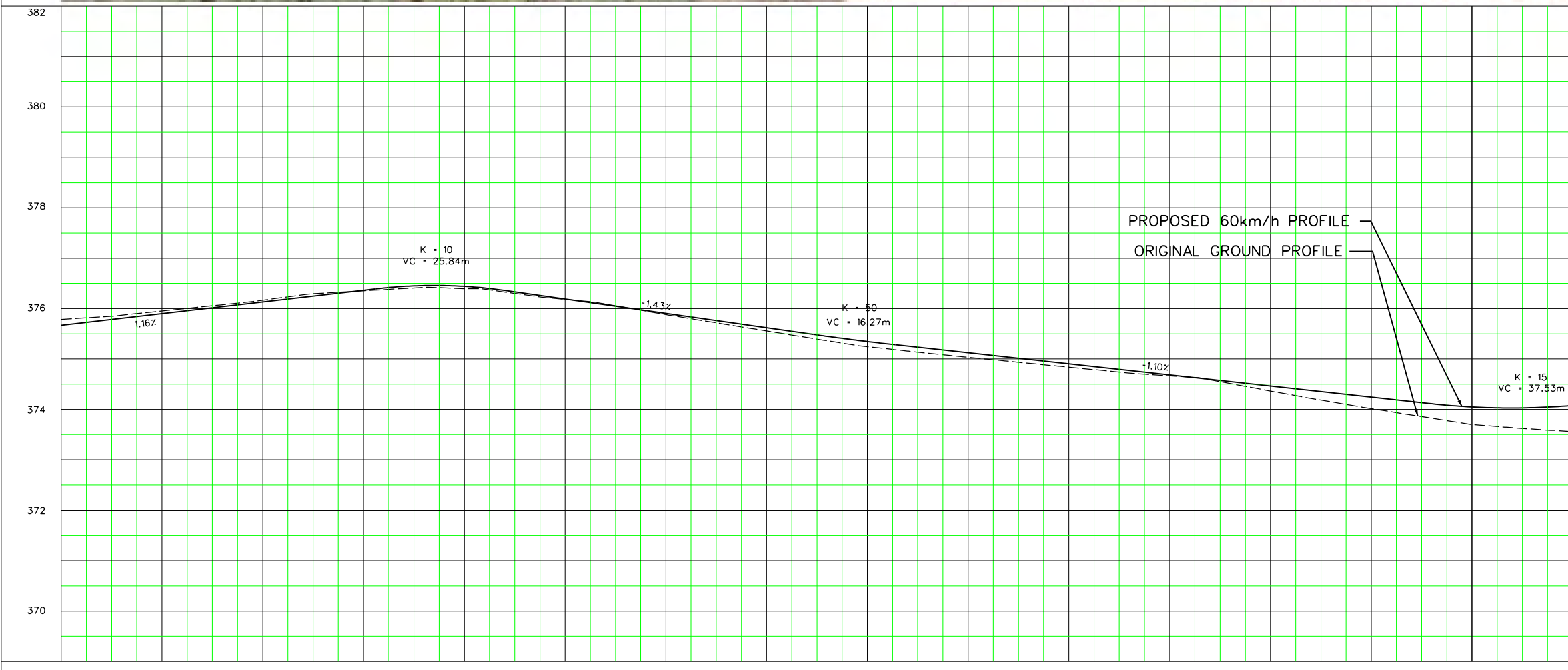


OLDE BASE LINE ROAD

(FROM STA 30+220 to STA 30+520)

PROPOSED OGS SYSTEM TREATMENT AREAS

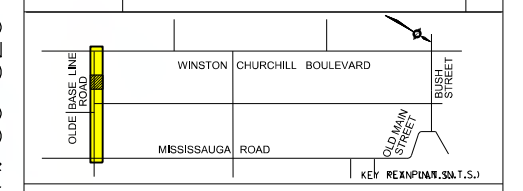
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	
Date MAY, 2014	Sheet OBL1	Plan No. -D



30+300	30+400	30+500	BOT. EL. OF WM.
			EX. ROAD ELEV.
			ROAD CHAINAGE

SERVICE DATA			
SERVICE	DATE	INIT.	DATE
SAN SEWERS			
STORM SEWERS			
WATERMANS			
TRANSIT			
PARKS & REC.			
ONT. CLEAN WATER			

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP • HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- ⊙ Denotes Building - Not Located
- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor Is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

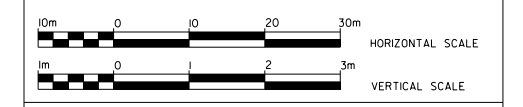
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

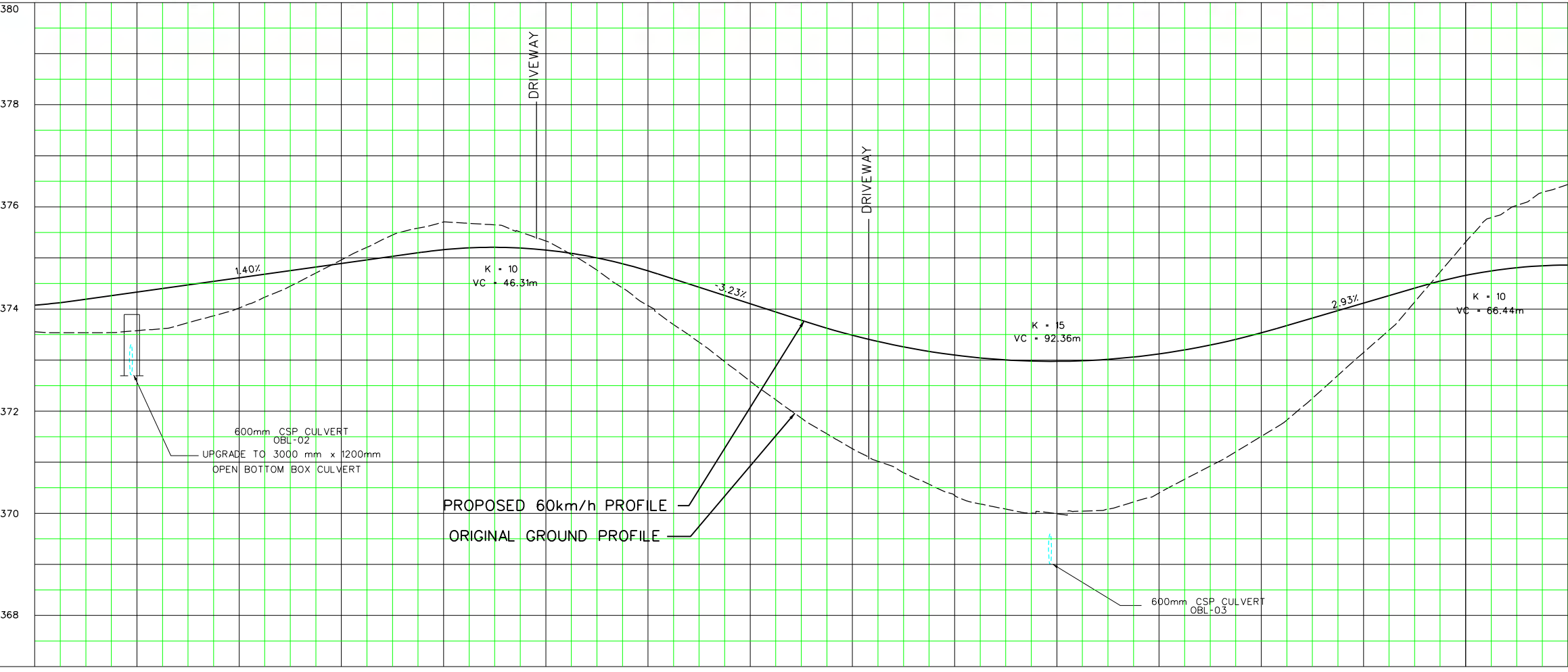
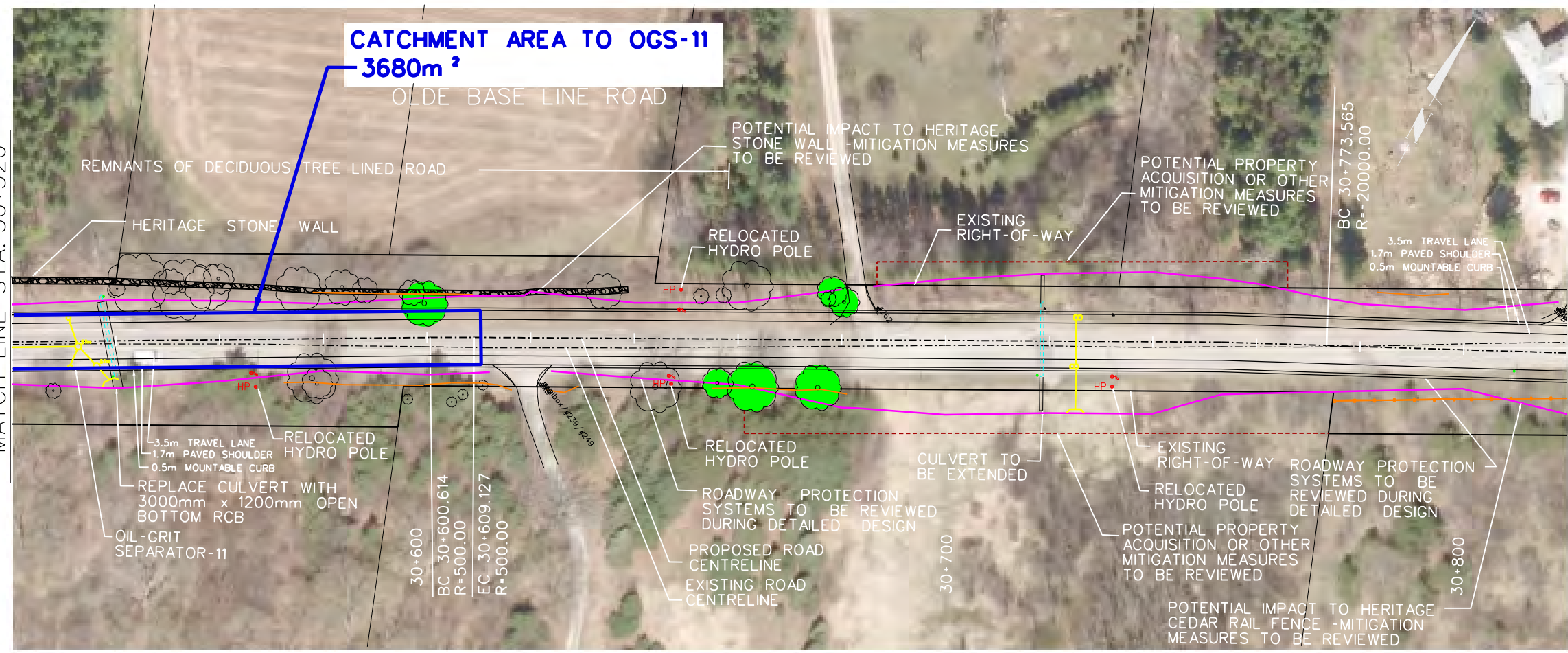
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FIBROBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



OLDE BASE LINE ROAD
(FROM STA 30+520 to STA 30+820)

PROPOSED OGS SYSTEM TREATMENT AREAS		
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet OBL2	Sheet No. -D



Appendix L
Proposed OGS System Treatment Area
OGS 12 (OBL-08)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
- CULTURALLY SIGNIFICANT FENCE
- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

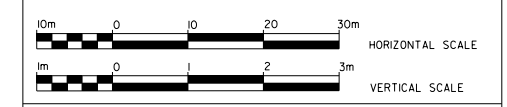
- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- Denotes Building - Not Located
- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.
The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Crkd. _____ Approved by _____

NOTICE TO CONTRACTOR
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

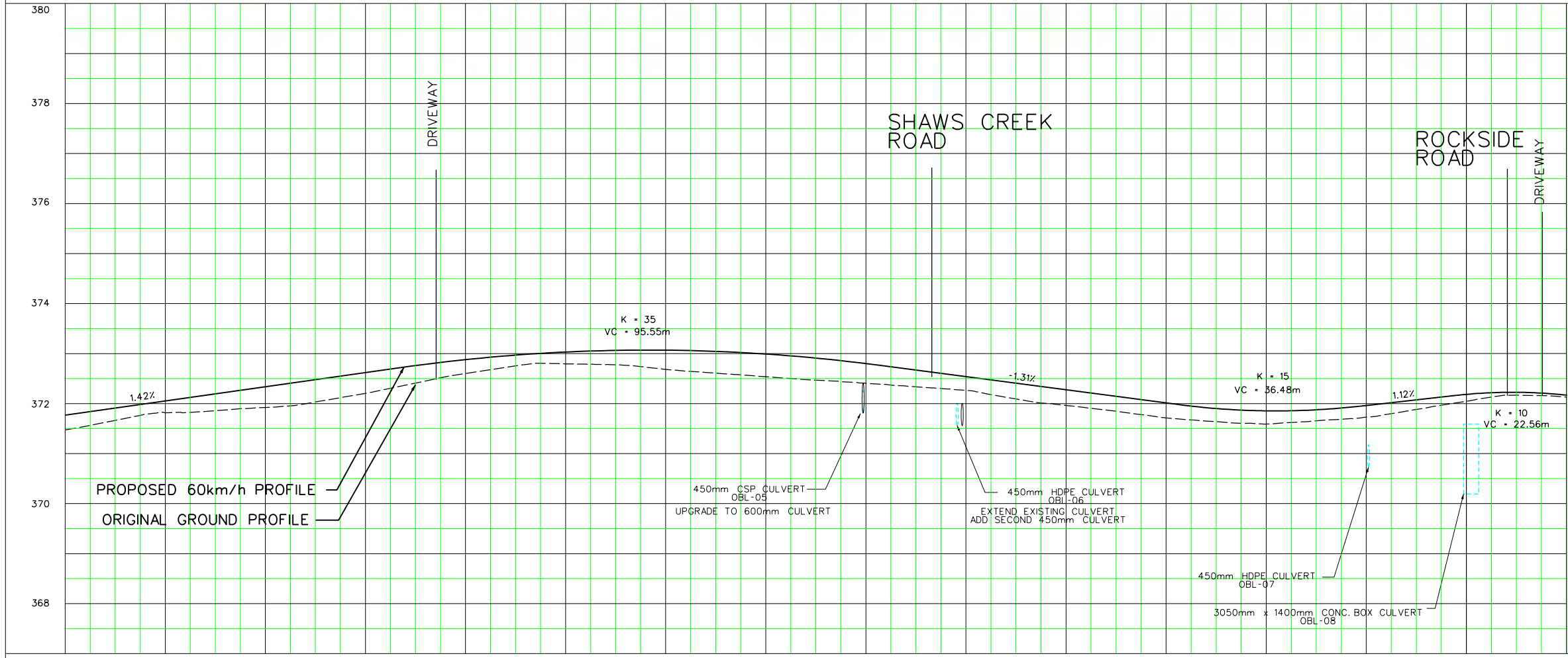
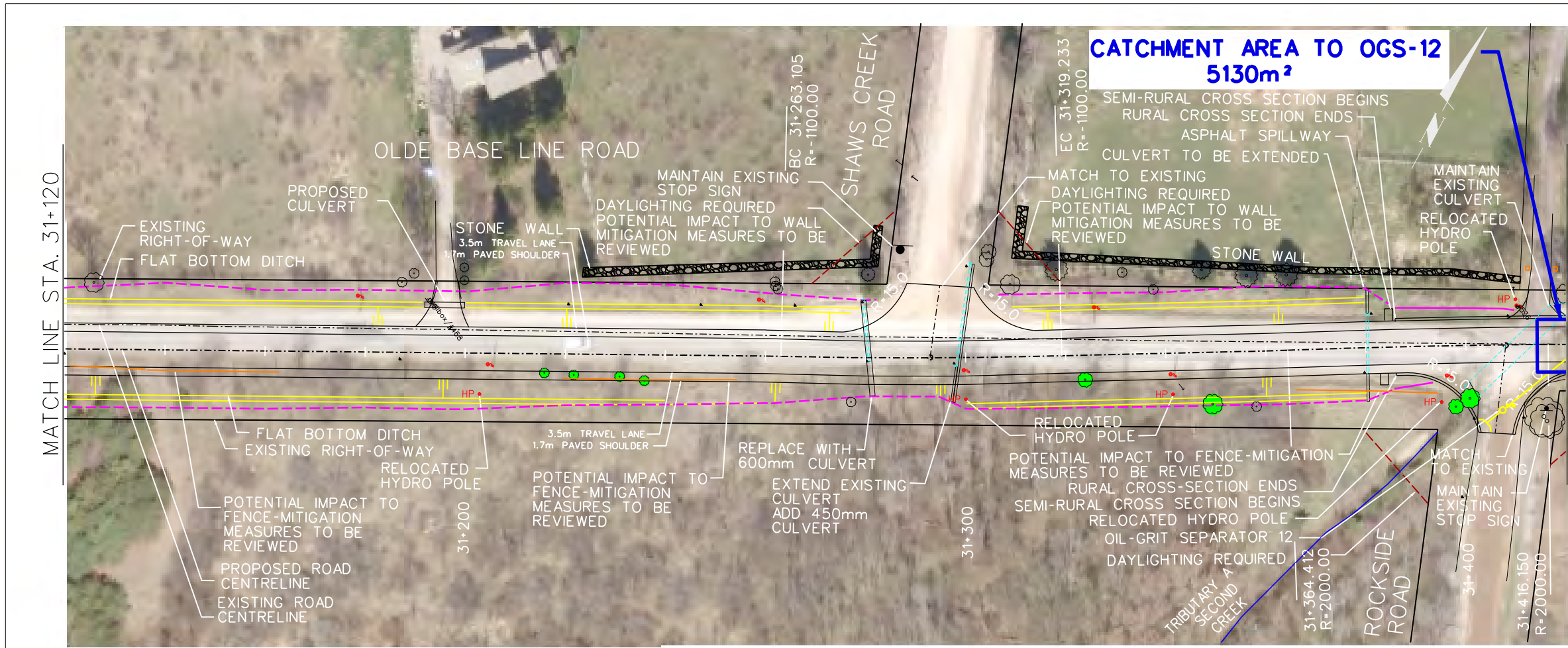
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



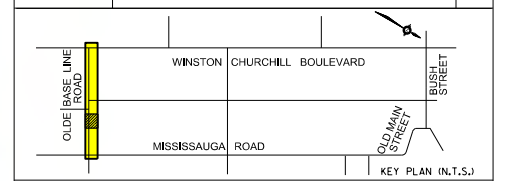
Region of Peel
Working for you

OLDE BASE LINE ROAD
(FROM STA 31+120 to STA 31+420)

CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet OBL3	

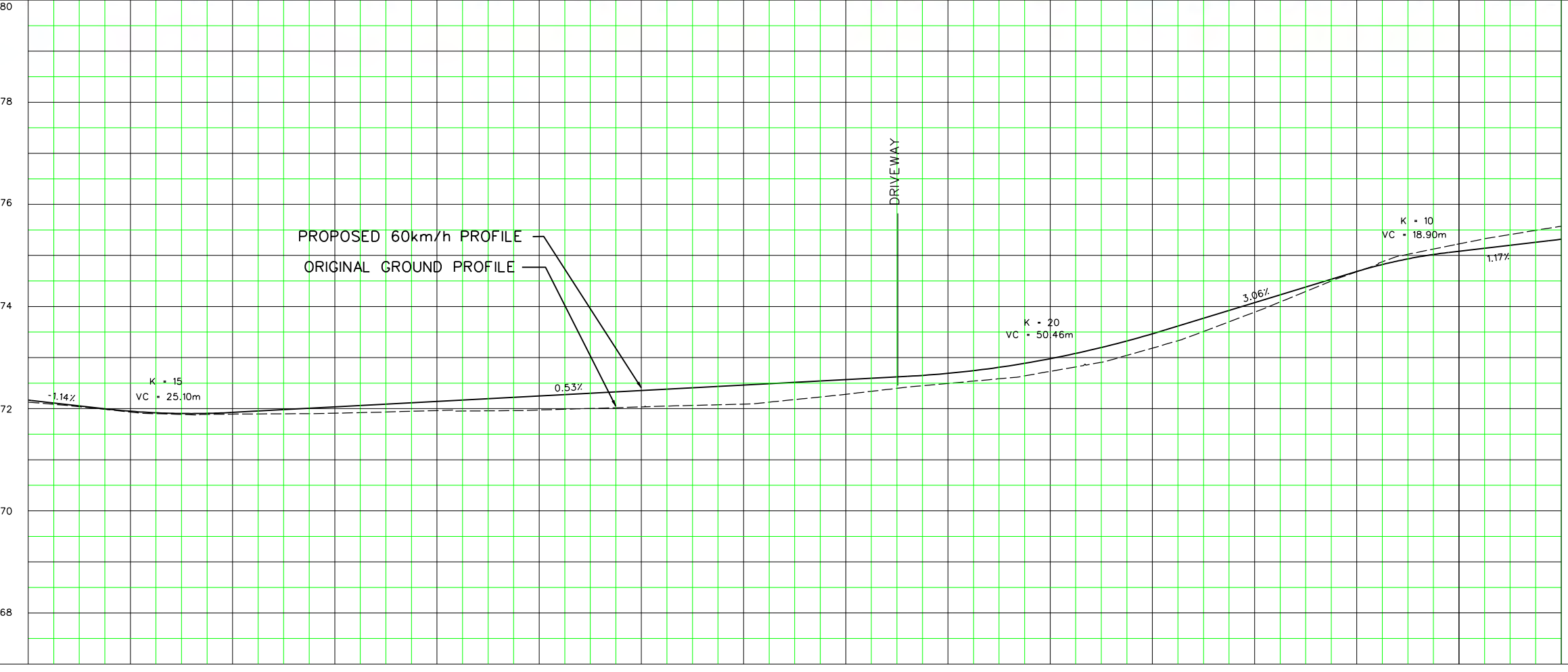
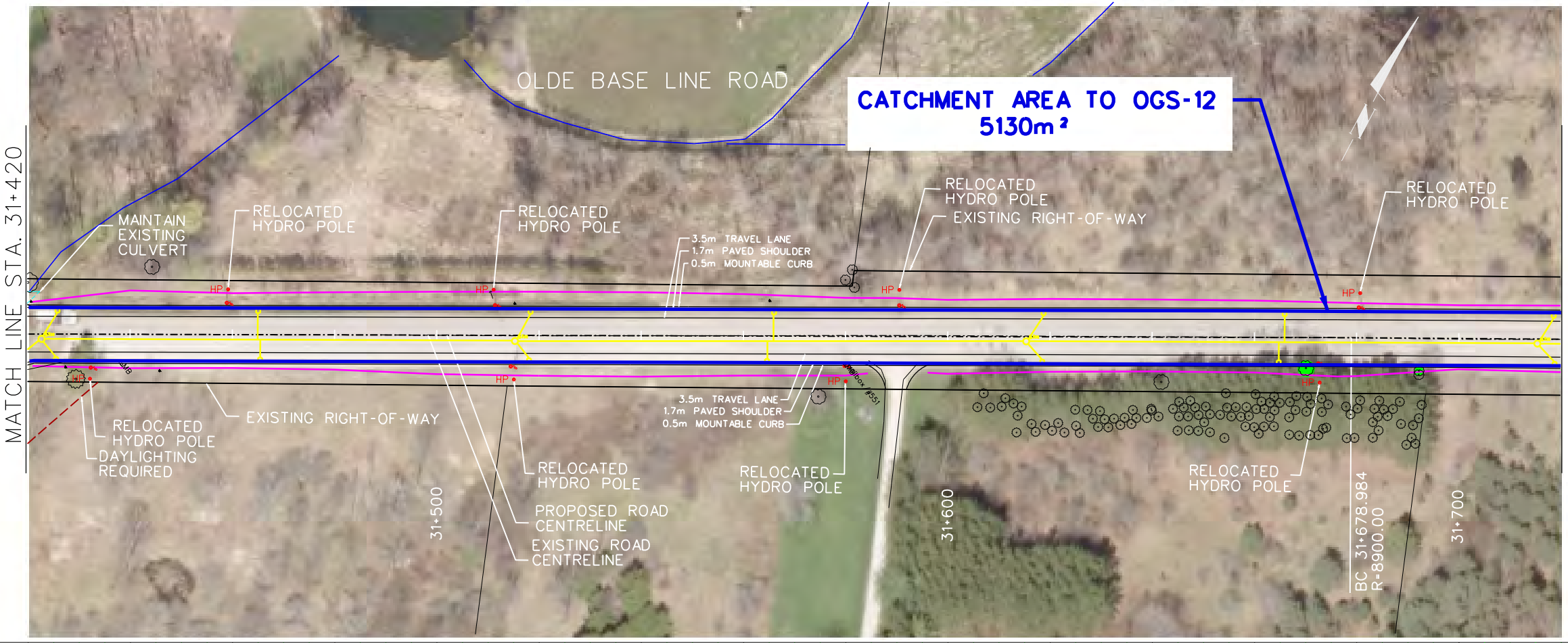


SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

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- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

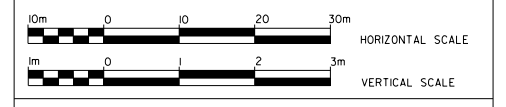
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

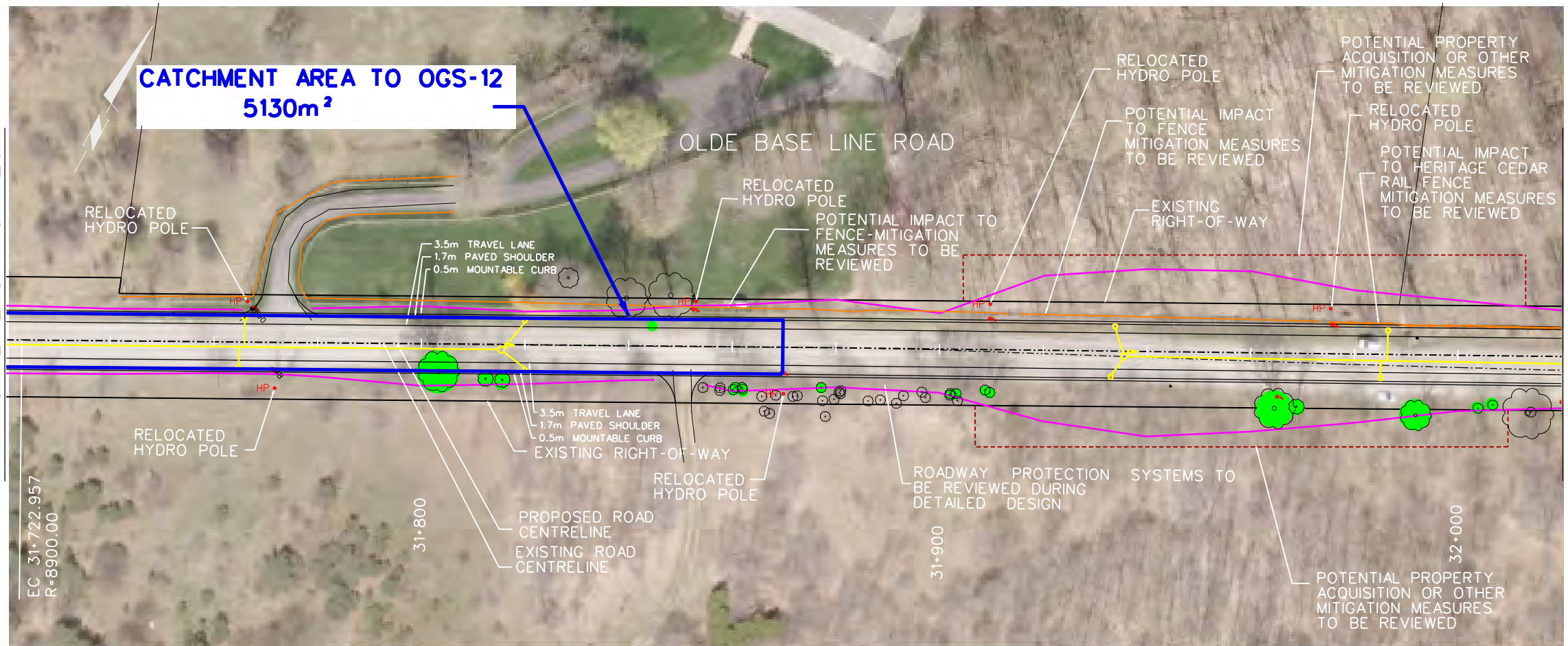


OLDE BASE LINE ROAD

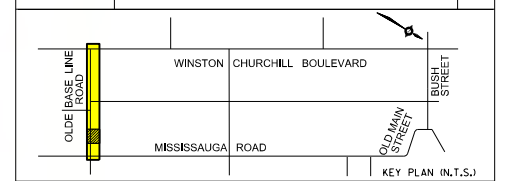
(FROM STA 31+420 TO STA 31+720)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
	Date MAY, 2014	Sheet OBL4	Plan No. -D



SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

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- Denotes Building - Not Located
- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

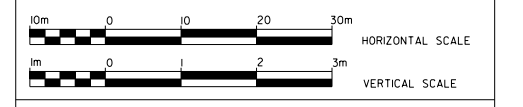
The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

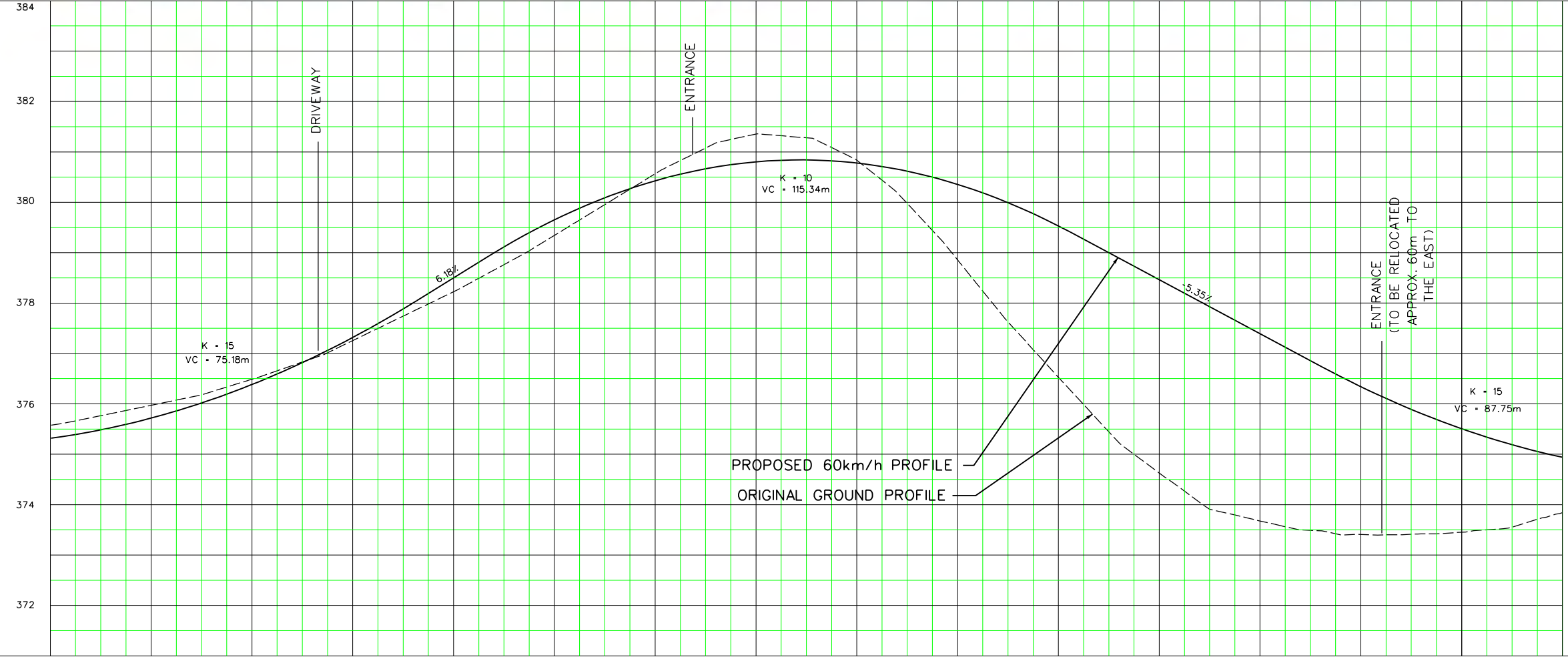
THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI/BROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



Region of Peel
Working for you

OLDE BASE LINE ROAD
(FROM STA 31+720 TO STA 32+020)

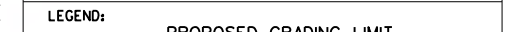
PROPOSED OGS SYSTEM TREATMENT AREAS		
CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	
Date MAY, 2014	Sheet OBL5	Plan No. -D



Appendix M
Proposed OGS System Treatment Area
OGS 13 (Old Base Line Road)

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HP HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN

General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
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- ⊞ Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (SAN)

B.M. No. Elev.

The Contractor Is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location Of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

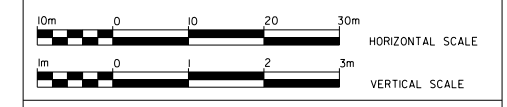
Designed by _____ Chkd. _____

Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FIBROBROADBAND)
HYDRO ONE NETWORKS	
ENERSOURCE HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	

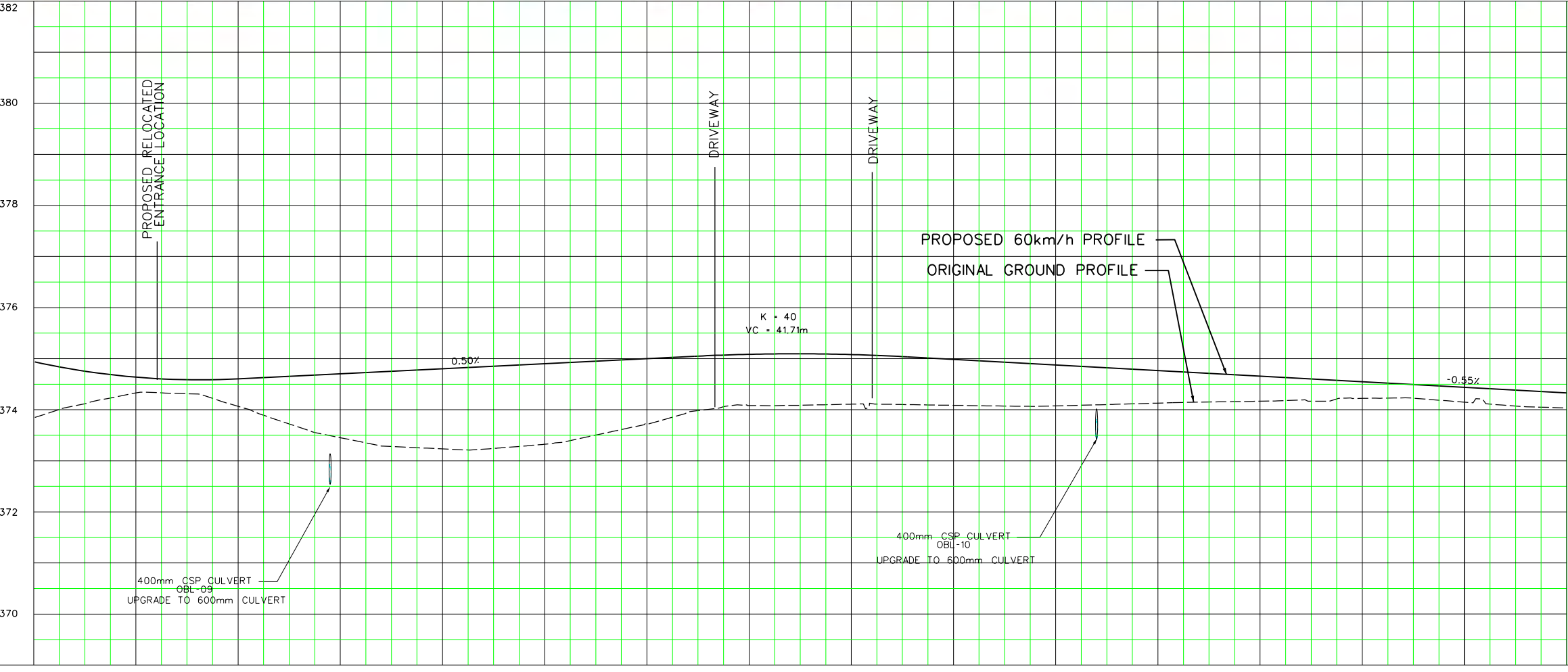
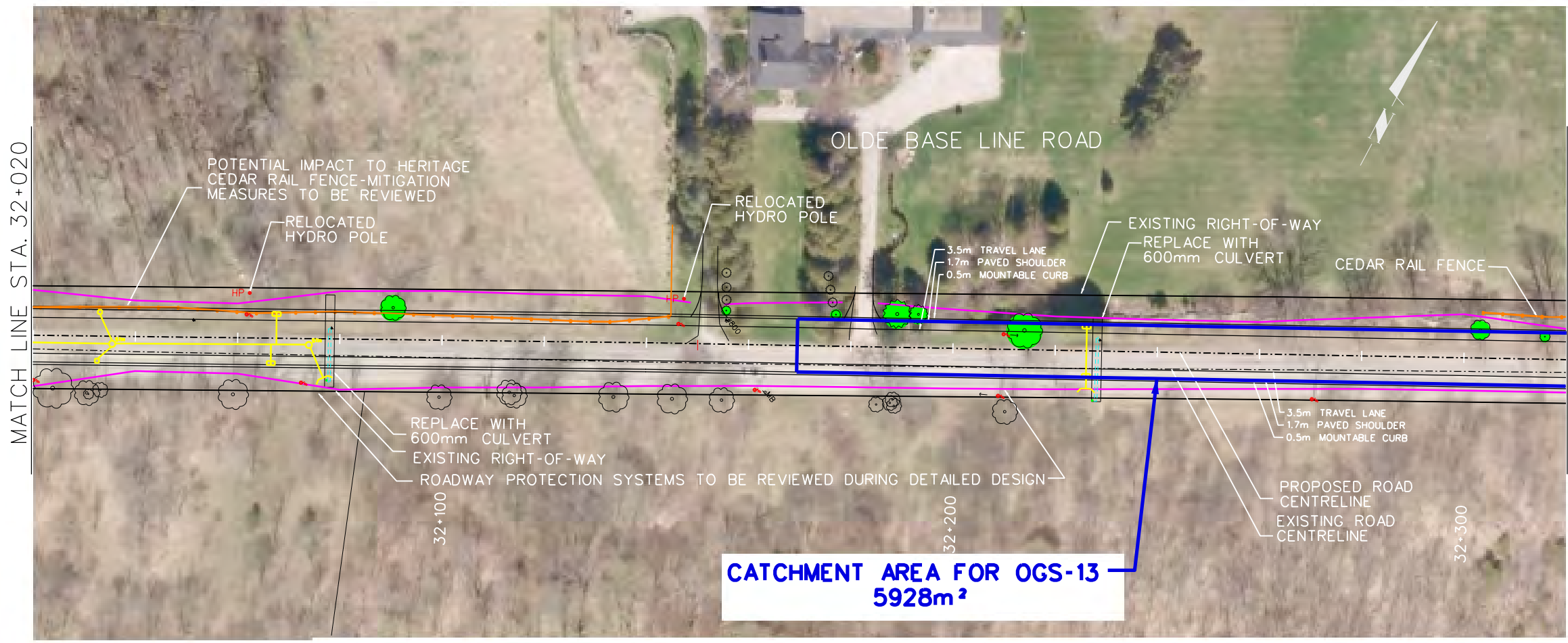


OLDE BASE LINE ROAD

(FROM STA 32+020 to STA 32+320)

PROPOSED OGS SYSTEM TREATMENT AREAS

CAD Area	Area X-X	Project No. XX-XXX
Checked by	Drawn by JM	Plan No.
Date MAY, 2014	Sheet OBL6	-D

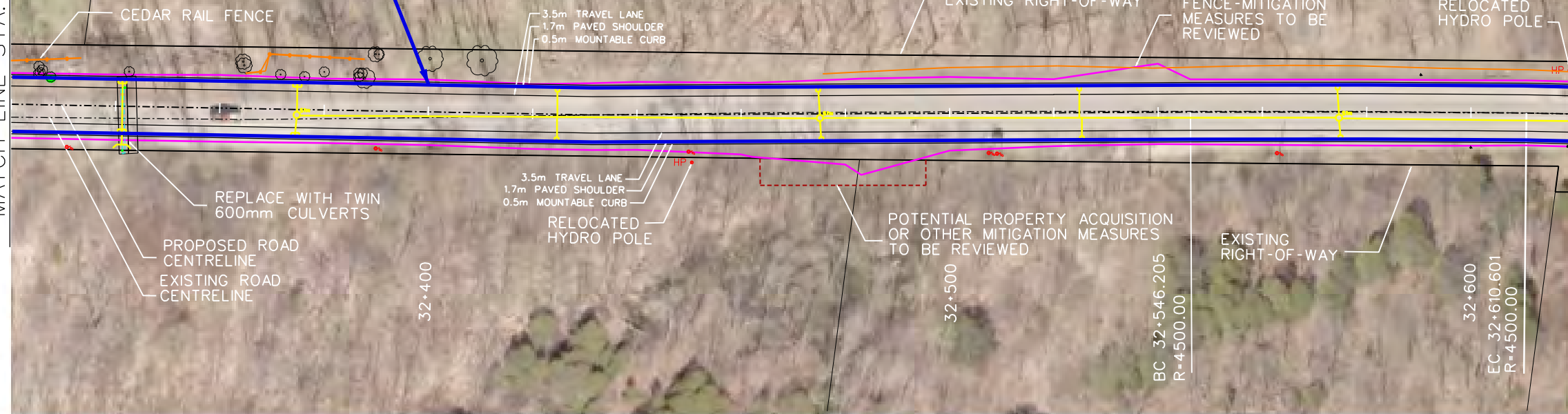


CATCHMENT AREA TO OGS-13
5928m²

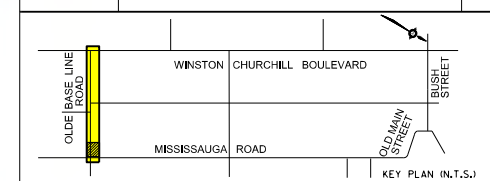
OLDE BASE LINE ROAD

MATCH LINE STA. 32+320

MATCH LINE STA. 32+620

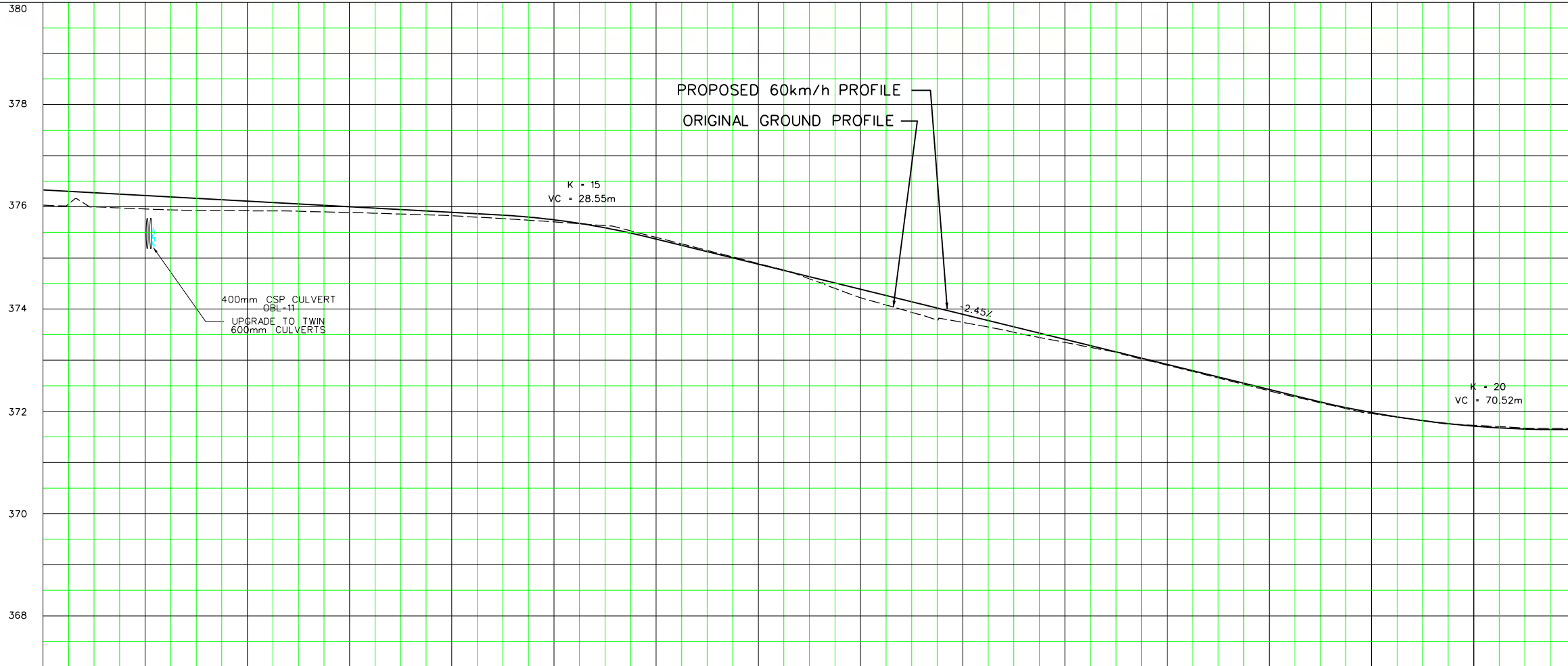


SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMAINS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CITY		
ONT. CLEAN WATER			COMMUNIC. CABLES		



- LEGEND:**
- PROPOSED GRADING LIMIT (RURAL CROSS SECTION)
 - PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
 - PROPOSED PROPERTY LINE
 - FENCE/GUIDE RAIL
 - CULTURALLY SIGNIFICANT FENCE
 - HERITAGE STONE WALL
 - PROPOSED CENTRE LINE
 - EXISTING CENTRE LINE
 - PROPOSED EDGE OF PAVEMENT
 - PROPOSED EDGE OF ASPHALT
 - EXISTING RIGHT OF WAY
 - EXISTING CULVERT
 - PROPOSED CULVERT
 - DITCH GRADING
 - PROPOSED STORM SEWER
 - PROPOSED CATCHBASIN
 - TRAFFIC SIGN
 - HYDRO POLE
 - VEGETATION REMOVALS

- NOTES**
- DRIVEWAYS TO BE REGRADED AS REQUIRED
 - HYDRO POLE RELOCATIONS ARE PRELIMINARY
 - REMOVAL OR REPLACEMENT OF DRIVEWAY CULVERTS IN SEMI-RURAL CROSS SECTIONS TO BE REVIEWED IN DETAILED DESIGN



General Notes

- All Driveways ASPHALT Unless Otherwise Noted.
- All Service Locations Are Approximate And Must Be Located Accurately In The Field
- Denotes Building - Not Located
- Denotes Building Located
- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

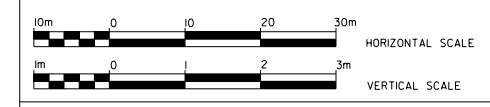
The Contractor is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location of Existing Utilities Approximate Only, To Be Verified In Field By Contractor.

Designed by _____ Chkd. _____ Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING:

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCI BROADBAND)
ENERSOURCE NETWORKS	
ENERSOURCE, HYDRO MISSISSAUGA	
HYDRO ONE BRAMPTON	



OLDE BASE LINE ROAD
(FROM STA 32+320 to STA 32+620)
PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM. EX. ROAD ELEV.	CAD Area	Area X-X	Project No. XX-XXX
32+400	Checked by	Drawn by JM	Plan No.
32+500	Date MAY, 2014	Sheet OBL7	-D
32+600	ROAD CHAINAGE		

SERVICE DATA					
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN SEWERS			GAS MAINS		
STORM SEWERS			BELL U/G CABLE		
WATERMANS			HYDRO U/G CABLE		
TRANSIT			HYDRO ONE		
PARKS & REC.			CTV		
ONT. CLEAN WATER			COMMUNIC. CABLES		

REVISIONS		
DATE	DETAILS	INIT.

LEGEND:

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- PROPOSED GRADING LIMIT (SEMI-RURAL CROSS SECTION)
- PROPOSED PROPERTY LINE
- FENCE/GUIDE RAIL
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- HERITAGE STONE WALL
- PROPOSED CENTRE LINE
- EXISTING CENTRE LINE
- PROPOSED EDGE OF PAVEMENT
- PROPOSED EDGE OF ASPHALT
- EXISTING RIGHT OF WAY
- EXISTING CULVERT
- PROPOSED CULVERT
- DITCH GRADING
- PROPOSED STORM SEWER
- PROPOSED CATCHBASIN
- TRAFFIC SIGN
- HYDRO POLE
- VEGETATION REMOVALS

NOTES

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- Type 'B' Bedding Unless Otherwise Noted (S&N)

B.M. No. Elev.

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Designed by _____ Ckd. _____ Approved by _____

NOTICE TO CONTRACTOR

48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL	CABLE TELEVISION/FIBROPTIC PROVIDERS:
CITY OF MISSISSAUGA WORKS DEPT.	BELL CANADA
CITY OF BRAMPTON WORKS DEPT.	ENERSOURCE TELECOM
TOWN OF CALEDON WORKS DEPT.	HYDRO ONE TELECOM
BELL CANADA	ROGERS CABLE
ENBRIDGE INCORPORATED-GAS DISTRIBUTION	ALLSTREAM
ONTARIO MINISTRY OF TRANSPORTATION	PSN (PUBLIC SECTOR NETWORK)
ONTARIO CLEAN WATER AGENCY	FUTUREWAY (FCIBROADBAND)

HYDRO ONE NETWORKS
ENERSOURCE, HYDRO MISSISSAUGA
HYDRO ONE BRAMPTON

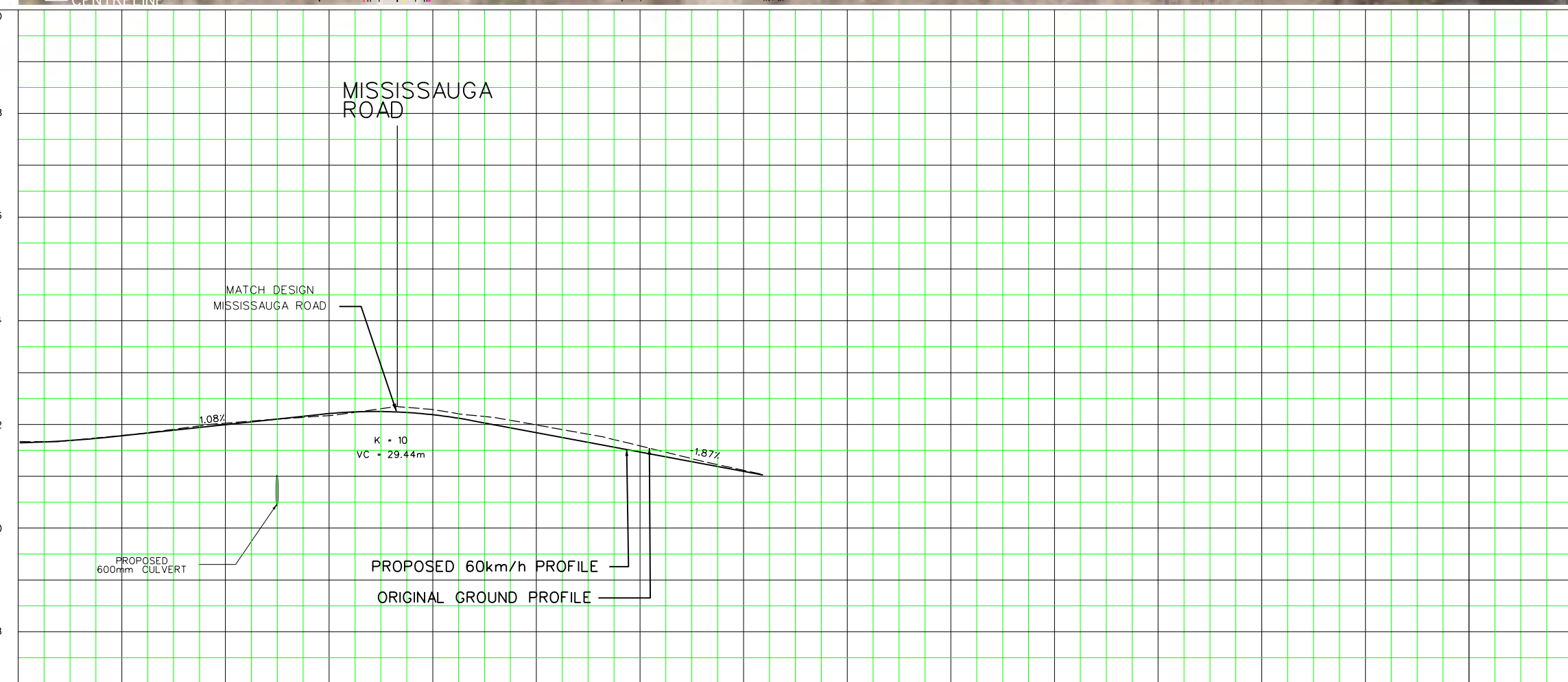
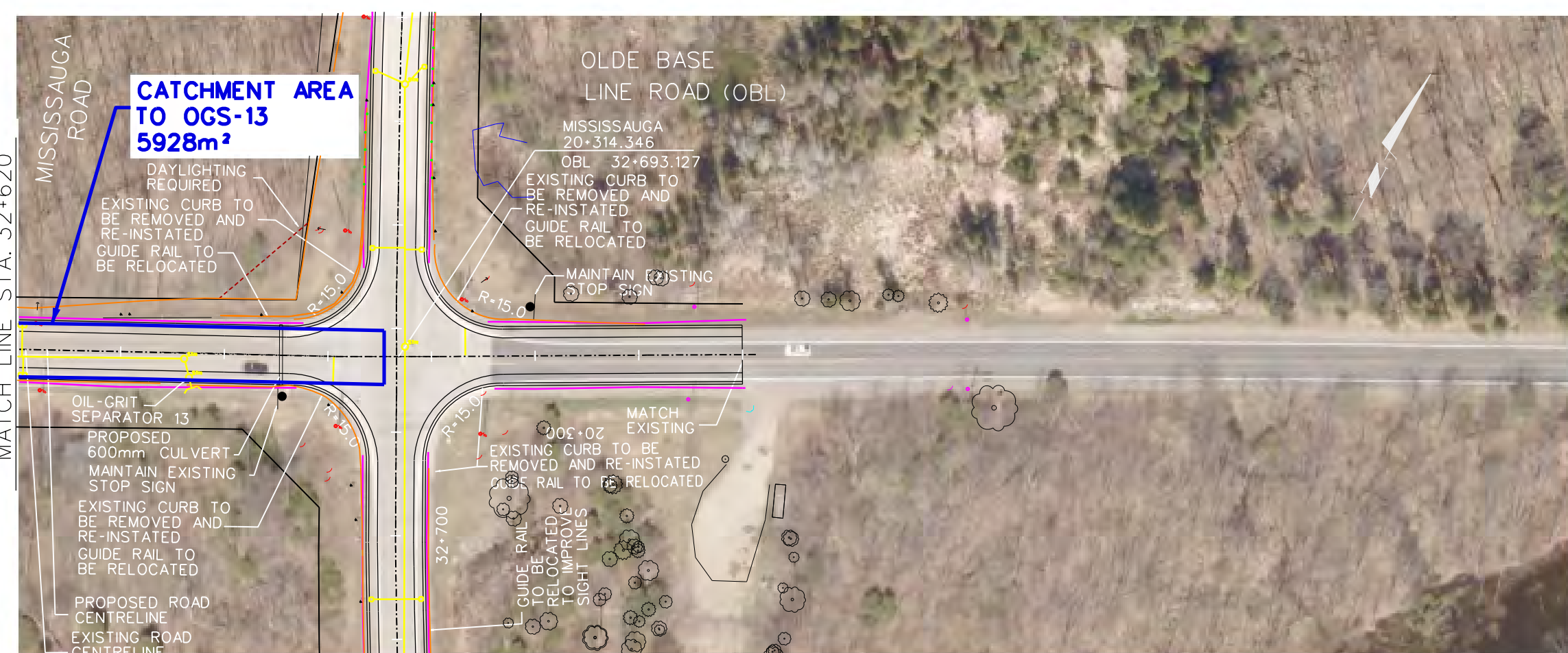
10m 0 10 20 30m HORIZONTAL SCALE
1m 0 1 2 3m VERTICAL SCALE

Region of Peel
Working for you

OLDE BASE LINE ROAD
(FROM STA 32+620 TO STA 32+760)

PROPOSED OGS SYSTEM TREATMENT AREAS

BOT. EL. OF WM.	CAD Area	Area X-X	Project No. XX-XXX
EX. ROAD ELEV.	Checked by	Drawn by JM	
	Date MAY, 2014	Sheet OBL8	Plan No. -D





HDR